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1984 DIRECT STRIKE LIGHTNING DATA

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National Aeronautics and Space Administration

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^{*}Part 2 and Part 3 published under separate cover.

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1984 DIRECT STRIKE LIGHTNING DATA

Mitchel E. Thomas and Harold K. Carney Langley Research Center Hampton, Virginia 23665

SUMMARY

This report presents the wideband waveforms recorded during the 1984 Direct-Strike Lightning Tests of the NASA Langley Research Center lightning-instrumented F-106B aircraft. The tests were conducted within about 150 nautical miles of the NASA Langley Research Center, Hampton, Virginia, where the aircraft was based. The entire transient recorder data obtained for 247 strikes and 11 nearby flashes in the 1984 campaign are presented in this report.

SYMBOLS

```
magnetic flux density, tesla
          electric flux density, coulomb per square meter
 D
          current, ampere
 I
A/m^2
          ampere per square meter
m
          meter
MHz
          megahertz
T/s
          tesla per second
Α
          ampere
         ampere per second
A/s
V
         volt
SUBSCRIPTS:
f
         forward fuselage
1
         longitudinal
n
         nose
t
         tail
         wing
W
wl
         wing-left
wr
         wing-right
```

In the text and on the computer plots of the waveforms, the rate of change of a quantity is indicated by a dot over the symbol-e.g., $\boldsymbol{\beta}_1$

В

INTRODUCTION

This report presents the wideband direct-strike lightning data obtained from the digital transient recorders during the 1984 Lightning Flight Tests of the NASA Langley Research Center lightning-instrumented F-106B aircraft.

There were 247 strikes to the aircraft during this campaign; there were 10 strikes in each of the 1980 and 1981 tests which were reported in references 1 and 2, and 156 strikes in 1982 which were reported in reference 3, and 214 strikes in 1983 which were reported in reference 4. The instrumentation system, transient recorders, external sensors, a summary overview of the previous tests and internal sensors and cables are described in references 5, 6, 7, 8, and 9, respectively.

DATA SYSTEMS

Data from seven external, wide-band, electromagnetic field sensors, three current sensors, and eight voltage and current sensors on internal aircraft cables was recorded with a twelve-channel, digital transient recorder configured to accomodate various combinations of these sensors. The external sensors (reference 7) and internal sensors (reference 9) demonstrate frequency response from near zero to 100MHz. Transmission lines connecting sensors to the recorder are 50-ohm coaxial cables, all properly terminated. Solid shield coaxial cable was used for long (15-20 feet) transmission lines in the aircraft, with some short lengths (less than 3 feet) of more flexible doublebraid shielded cable used in close proximity to the sensors. The transmission lines, including coaxial cables, connectors, and power splitters, were tested for frequency response and the results are given in reference 9. The twelve transient recorder channels are configured in four units of three channels each. The available trigger options are: to trigger each unit of three channels from a separate data source, or to trigger any combination up to all channels from a single source, or to trigger all channels from any one of four seperate sources. These options are available by using a special "fan-out" device (see figure 1). The transient recorder stores 65536 data samples for each channel with 8-bit resolution and selectable sample rates from 200MHz to 1.5625MHz (sample interval from 5 nanoseconds to 640 nanoseconds). The sample interval selected for each measurement, and trigger source for each channel is shown in table 1. Dynamic range for each measurement was established by using selected attenuators inserted in the transmission lines from sensors to the transient recorder. Post-season calibration of the attenuators showed a maximum uncertainty between +2.3dB and -2.6dB in the attenuation factor used to process the data.

1984 LIGHTNING DATA

The 1984 tests resulted in 247 direct strikes to the aircraft and 11 nearby flashes from storm penetration flights at flight levels generally above 20,000 feet for the first half of the season, and generally below 20,000 feet for the remainder of the season. Table 2 summarizes, by flight number, the 1984 data records acquired with the twelve-channel transient recorder. The entries under the various sensor headings are the run numbers of each 65536 sample record acquired with the transient recorder system for a lightning strike or nearby flash. (A run consists of all the trasient recorder data associated with a trigger from one lightning event.) Typically, a single dynamic sensor response was captured in memory for each channel of the transient recorder for a lightning strike or nearby flash and plots of these dynamic waveforms are presented with an expanded time scale in this report. Labeling on each plot indicates flight number, run number, trigger time, and a strike or nearby-flash code- e.g., S-001 or N-001, for each recorded event which can be used to correlate this data with other waveforms for the same event. A zero on the horizontal axis of the data plots indicates the trigger time of the transient recorder as it was triggered by the lightning event.

The minus values, on the horizontal axis, indicate pre-trigger time, while the positive values indicate post-trigger time. The correlation to other supporting data is through time of occurrence (trigger time) which is shown on the plot. The sign conventions established for the measurements shown in figure 2 indicates positive quantities in the direction of the arrows; the relation between the sign conventions of the variables D, B, and I and their derivatives are shown in the measurement polarity time history also in figure 2.

The external sensor locations on the aircraft are shown in figure 2, and the following labels identify the waveform plots for each sensor: I_n is the current measurement and $\dot{\mathbf{I}}$ is the rate-of-change of current measurement in the pitot boom at location 1, $\dot{D}_{\rm f}$ is the rate-of-change of electric flux density measurement at location 2, $\dot{\textbf{B}}_{l}$ is the rate-of-change of magnetic flux density measurement at location 6, \dot{B}_{w1} is the rate-of-change of magnetic flux density measurement at location 8, $\dot{D}_{\omega 1}$ is the rate-of-change of electric flux density measurement at location 9, $\dot{B}_{w\,r}$ is the rate-of-change of magnetic flux density measurement at location 10, $\dot{D}_{w\,r}$ is the rate-of-change of electric flux density measurement at location 11, \dot{D}_{t} is the rate-of-change of electric flux density measurement at location 12, $I_{\rm t}$ is the current measurement between the vertical fin cap and aircraft structure at location 13. Voltage and current measurements on internal wires and cables are labeled and located in the aircraft as follows: V_{ω} (or TP100) is a voltage measurement on an insulated, 18-gauge wire located in the leading edge of the left wing (see figure 3), $V_{\rm f\,a}$ is a voltage measurement on a shielded, 18-gauge wire in the forward fuselage (see figure 4), $V_{\rm fb}$ (or TP101) is a voltage measurement on an insulated, 18gauge wire in the forward fuselage (see figure 4), $V_{\rm fc}$ (or TP102) is a voltage measurement on the center conductor of a coaxial cable in the forward fuselage (see figure 4), TP114 is a current measurement on the power cable for the

vertical fin position light (see figure 5), TP116 is a current measurement on a position light power cable in mid-fuselage (see figure 6), TP123 is a current measurement on the power cable to an aircraft radio, and TP125 is a current measurement on the shield of a coaxial antenna cable to the same radio (see figure 7). The voltages are measured at 50-ohm terminations at one end of the wires and cables, and the other end (shields also) are connected to aircraft structure. The currents are measured on functional aircraft cables.

Channel assignments for the twelve-channel transient recorder were changed six times during the season to acquire data from 18 sensors described above, and each configuration is shown in table 1. An operational problem with an integrator/amplifier signal conditioning component caused all data acquired on one channel of the transient recorder to be unusable. Consequently, data from only eleven transient recorder channels are presented in this report. Measurement ranges, recorder trigger thresholds, and recorder sampling intervals for each configuration are also shown in table 1. On flights 84-013 through 84-039, all transient recorder channels were triggered simultaneously by stimuli to the $\dot{D}_{\mathbf{f}}$ sensor only. On flights 84-040 through 84-048, all channels were triggered by the first response above the trigger threshold of either $\dot{D}_{\rm f}$ or $\dot{D}_{\rm t}$, and on fights 84-049 through 84-052, all channels were triggered by the first response above the trigger threshold of either $\dot{D}_{\!f}$, $\dot{D}_{\!t}$, or $\dot{D}_{w\,r}$. The sample intervals shown in table 1 indicate that the 200MHz sample rate (5 nanosecond interval) was employed for the internal measurements to acquire data on high frequency resonances which were anticipated on internal conductors. External sensor data was sampled at 100MHz (10 nanosecond sample interval), which was appropriate for the fundamental resonant frequency associated with the longitudinal dimension of the aircraft structure (6-8 MHz) and several higher harmonic frequencies. A sample rate of 25MHz (40 nanosecond sample interval) was utilized for two magnetic field, and

subsequently, two current measurements to achieve a longer memory storage time (65536 samples and 40 nanosecond sample interval results in 2.621440 milliseconds memory length) to investigate multiple current impulses during a lightning strike to the aircraft.

Two battery powered peak-level recorders were used on the aircraft in 1984 to continuously monitor and record the maximum amplitude achieved by the \dot{D}_f and \dot{I} measurements for each flight through 84-048, and \dot{D}_f and I_t measurements for the remaining flights (the results are shown in table 3). The maximum current recorded from the I_t sensor was 54,000 A and occurred on flight 84-049, and the maximum rate of change of current recorded from the \dot{I} sensor was 19.38E+10 A/s and occurred on flight 84-036, and the largest peak level recorded for \dot{D}_f was 75 A/m² on flight 84-048, although there were some "overscales" (>97 A/m²) indicated for \dot{D}_f throughout the season.

CONCLUSION

The waveforms recorded in 1984 are a significant addition to the data set of simultaneously recorded currents and electromagnetic fields which have been acquired to study and define the aircraft/lightning interaction. The data presented in this paper is the first large data set of time correlated electromagnetic measurements from multiple points on the surface of the aircraft with 10 nanosecond time resolution. The 1984 data also includes voltage and current measurements on internal aircraft wires and cables. Data was acquired from lightning strikes to the aircraft between the altitudes of 15,000 and 39,000 feet. The bandwidth of the data system makes it possible to analyze electromagnetic data acquired on the surface of the aircraft at the aircraft fundamental resonant frequency and several higher harmonics.

Accuracy of this data is limited by a maximum uncertainty between +2.3dB and -2.6dB in the value of attenuation used to establish transient recorder channel sensitivity.

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TABLE 1. 1984 LIGHTNING MEASUREMENT RANGES

FLIGHT			SAMPLE	TRIGGER THRESHOLD
NUMBER 84-013 to -018	SENSOR B _{w 1}	FULL SCALE +930 T/s	INTERVAL _	triggered by D _f
04-013 60 010	B _{wr}	+930 T/s	10 ns	triggered by $\dot{\mathtt{D}}_{\mathtt{f}}$
	Ď _t	+10 A/m ²	10 ns	triggered by D _f
	i i	+2.4E+11 A/s	10 ns	triggered by $\mathfrak{D}_{\mathbf{f}}$
	₿₁	- +1800 T/s	10 ns	triggered by $\mathfrak{D}_{\mathbf{f}}$
	Ď _{w r}	+19 A/m ²	10 ns	triggered by $\dot{\mathtt{D}}_{\mathtt{f}}$
	Ď _{w 1}	- +19 A/m ²	10 ns	triggered by $\dot{\mathtt{D}}_{\mathbf{f}}$
	Ď _f	+12 A/m ²	10 ns	$\pm 3.7 \text{ A/m}^2$
	-	+51 V	10 ns	triggered by D _f
	In	+9100 A	10 ns	triggered by $\dot{\mathtt{D}}_{\!\mathbf{f}}$
	 I _t	+9100 A	10 ns	triggered by $\dot{\mathtt{D}}_{\mathtt{r}}$
	•	_		
84-019 to -027	₿ _{w 1}	+930 T/s	40 ns	triggered by D _f
	₿ _{w r}	+930 T/s	40 ns	triggered by D _f
	Ďŧ	$\pm 2.5 \text{ A/m}^2$	10 ns	triggered by D _f
	t	+2.4E+11 A/s	10 ns	triggered by D _f
	В́ı	<u>+</u> 1800 T/s	10 ns	triggered by D _r
	Ď	<u>+</u> 19 A/m ²	10 ns	triggered by D _f
	Ď _{w 1}	±19 A/m ²	10 ns	triggered by D _f
	Ď _f	+12 A/m ²	10 ns	±3.7 A/m²
	$V_{f,a}$	<u>+</u> 51 V	10 ns	triggered by D _f
	I _n	<u>+</u> 9100 A	10 ns	triggered by D _f
	I _t	<u>+</u> 9100 A	10 ns	triggered by D _f
84-028 to -034	In	+16200 A	40 ns	triggered by D _f
	I _t	<u>+</u> 16200 A	40 ns	triggered by D _f
	Ď _t	$\pm 2.5 \text{ A/m}^2$	10 ns	triggered by D _f
	İ	<u>+</u> 2.4E+11 A/s	10 ns	triggered by $D_{\mathbf{f}}$
	$\dot{\mathtt{B}}_{1}$	<u>+</u> 1800 T/s	10 ns	triggered by D _f
	Ď _{w r}	<u>+</u> 19 A/m²	10 ns	triggered by D _f
	D _{w 1}	+19 A/m ²	10 ns	triggered by D _f
	Ď _f	+12 A/m²	10 ns	±3.7 A/m²
	V, TP100) <u>+</u> 51 V	10 ns	triggered by D _f
	V _{fb} TP10		10 ns	triggered by D _f
	V _{fc} TP102		10 ns	triggered by D _f

TABLE 1 Continued

FLIGHT NUMBER	SENSOR	FULL SCALE	SAMPLE	TID I CCEP THIRD CIVOL D
84-035 to -039	$\frac{JLINSOR}{I_n}$	+16200 A	INTERVAL 40 ns	TRIGGER THRESHOLD triggered by D.
	It	+16200 A	40 ns	triggered by D.
	Ď _t	$\pm 2.5 \text{ A/m}^2$	10 ns	triggered by D _f
	İ	+2.4E+11 A/s	10 ns	triggered by D _f
	$\dot{\mathtt{B}}_{\mathtt{l}}$	<u>+</u> 1800 T/s	10 ns	triggered by $\dot{D}_{\!f}$
	Ď _{ω r}	<u>+</u> 19 A/m²	10 ns	triggered by $\dot{\mathbf{D}}_{\mathbf{f}}$
	Ď _{w 1}	<u>+</u> 19 A/m²	10 ns	triggered b y Ď _f
	Ď _f	$\pm 12 \text{ A/m}^2$	10 ns	±3.7 A/m²
	V _w TP100	±51 V	5 ns	triggered by Ď _f
	V _{fb} TP101	<u>+</u> 51 V	5 ns	triggered b y Ď _f
	TP123	<u>+</u> 14 V	5 ns	triggered by $\dot{D}_{\mathbf{f}}$
84-040 to -048	I _n	+16200 A	40 ns	triggered by Ď₄ or Ď₊
	I _t	+16200 A	40 ns	triggered by D. or D.
	Ď _t	- +2.8 A/m ²	10 ns	+0.8 A/m²
	İ	+2.4E+11 A/S	10 ns	triggered by D, or D,
	₿ ₁	+1800 T/s	10 ns	triggered by D, or D.
	Ď _{w r}	+19 A/m²	10 ns	triggered by D, or D,
	Ď _{w 1}	+19 A/m ²	10 ns	triggered by D, or D,
	$\dot{\mathtt{D}}_{\mathbf{f}}$		10 ns	+3.7 A/m²
	V _w TP100	<u>+</u> 26 V	5 ns	triggered by D _f or D _t
	V _{fb} TP101	<u>+</u> 26 V	5 ns	triggered by \dot{D}_{f} or \dot{D}_{t}
	TP123	+2.6 V	5 ns	triggered by $D_{\mathbf{f}}$ or $D_{\mathbf{t}}$
84-049 to -050	In	+16200 A	40 ns	triggered by $\dot{D}_{\mathbf{f}}$ or $\dot{D}_{\mathbf{t}}$ or $\dot{D}_{\mathbf{wr}}$
		+22800 A		triggered by \dot{D}_{r} or \dot{D}_{t} or \dot{D}_{wr}
		- +2.8 A/m ²	10 ns	+0.8 A/m ²
	_	+2.4E+11 A/s		triggered by D _f or D _h or D _{ur}
	$\dot{\mathtt{B}}_{1}$	+1800 T/s	10 ns	triggered by \dot{D}_{r} or \dot{D}_{t} or \dot{D}_{ur}
	Ď _{w r}	+21 A/m ²	10 ns	+6.2 A/m²
		<u>+</u> 15 A/m²	10 ns	triggered by D, or D, or D,
	$\dot{D}_{\mathbf{f}}$	<u>+</u> 12 A/m²	10 ns	+3.7 A/m ²
	V, TP100	<u>+</u> 26 V	5 ns	triggered by D _f or D _t or D _{wr}
	V _{fb} TP101	<u>+</u> 26 V	5 n s	triggered by \dot{D}_{f} or \dot{D}_{t} or \dot{D}_{wr}
	TP123	±2.6 V	5 n s	triggered by \dot{D}_{r} or \dot{D}_{t} or \dot{D}_{wr}

TABLE 1 Concluded

FLIGHT NUMBER	SENSOR	FULL SCALE	SAMPLE INTERVAL	TRIGGER THRESHOLD
84-051 to -052	I	+16200 A	40 ns	triggered by D, or D, or D,
	I,	+22800 A	40 ns	triggered by Ď _r or Ď _t or Ď _{ur}
	Ďŧ	+2.8 A/m ²	10 ns	+0.8 A/m²
	t	+2.4E+11 A/s	10 ns	triggered by D _f or D _t or D _{wr}
	Β̈́ι	- +1800 T/s	10 ns	triggered by \dot{D}_{f} or \dot{D}_{t} or \dot{D}_{wr}
	Ď,	+21 A/m ²	10 ns	+6.2 A/m ²
	Ď _{w 1}	+15 A/m ²	10 ns	triggered by D _f or D _t or D _{wr}
	Ď _e	+12 A/m²	10 ns	$\pm 3.7 \text{ A/m}^2$
	TP114	+0.26 V	* ns	triggered by D _f or D _t or D _{wr}
	TP116	- +0.26 V	* ns	triggered by \hat{D}_{f} or \hat{D}_{t} or \hat{D}_{wr}
	TP125	+0.26 V	* ns	triggered by $D_{_{\mathbf{f}}}$ or $D_{_{\mathbf{t}}}$ or $D_{_{\mathbf{v},\mathbf{r}}}$

 $[\]star$ 5 ns for flight 84-051 and 10 ns for flight 84-052

TABLE 2. 1984 DATA SUMMARY FOR FLIGHTS 84-014 through 84-052

	PAGE NUMB	22-37	38-73	74-82	83-148	149-225	226-258	259-280	281-348	349-509		510-542	543-591	592-612	613-634	999-589	829-299
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MBERS	M.	} !	 		Dwr 1-6	1,3-8	1-3	1-2	1,3-7	1-15		1-3	D _{Wr}	1-2	1-2	1-3	!
RUN NUMBERS B, D		1-2	1-5	-	₿ <u>1</u>	1,3-8	1-3	1-2	1,3-7	1-15	!	1-3	в ₁	1-2	1-2	1-3	1-4
•+	-	1-2	1-5	-	1-1-6	1,3-8	1-3	1-2	1,3-7	1-15	!	1-3	1-5	1-2	1-2	1-3	1-4
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TABLE 2 Concluded

RUN NUMBERS

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101	1-5	1-6	1-10 12-20		1-6	1-4	1-3	101	101	1-5	101	i i i	116	1,2
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DATE	7/16	1/24	7/25	7/27	8/8	6/8	8/9	(SENS(8/12	(SENSC 8/13	8/14	(SENSO 8/23	8/30	(SENS)	10/18

TABLE 3. 1984 DATA SUMMARY-PEAK LEVELS

	FLIGHT	NUMBER OF	NUMBER OF	PEA		
DATE	NUMBER	STRIKES	NEAR-BY	Ď _f	İ	I _t
E /27	84-014	2	0	*	*	
	84-015	6	2	37 A/m^2	.38E+10 A/s	
5/28	84-017	2	õ	*	*	
6/5	84/019	10	Ŏ	*	*	
6/6	84-020	7		**	7.79E+10 A/s	
	84-021	, 3	1 1 0 3 1	0	0	
	84-023	3 3 7	Ō	40 A/m^2	.19E+10 A/s	
	84-024	7	3	37 A/m ²	3.04E+10 A/s	
6/13	84-025	19	ī	39 A/m ²	1.71E+10 A/s	
	84-026		Ō	40 A/m ²	4.37E+10 A/s	
	84-027	5 6 3 2 5	1	28 A/m ²	4.75E+10 A/s	
	84-028	6	0	40 A/m^2	1.52E+10 A/s	
	84-029	3	0	31 A/m^2	.19E+10 A/s	
	84-031	2	0	26 A/m^2	0	
	84-032	5	0	28 A/m^2	1.14E+10 A/s	
	84-033	14	0 1	*	*	
	84-035	7	0	30 A/m^2	.57E+10 A/s	
	84-036	9	0	44 A/m ²	19.38E+10 A/s	
	84-037	72	0	**	5.32E+10 A/s	
7/27	84-038	2	0	23 A/m^2	3.99E+10 A/s	
	84-043	6	0	**	11.02E+10 A/s	
	84-044	6	0	17 A/m^2	16.15E+10 A/s	
	84-045	3	0	28 A/m^2	7.79E+10 A/s	
	84-046	2	0	7 A/m^2	8.74E+10 A/s	
	84-047	3 2 5 5	0	28 A/m^2		
8/14	84-048		1	75 A/m²	12.73E+10 A/s	
8/23	84-049	1	0		9.69E+10 A/s	54KA
	84-050	27	0		17.48E+10 A/s	44KA
	84-051	1	0		8.17E+10 A/s	*
10/18	84-052	2	0		8.36E+10 A/s	*

^{*} Peak Detector inoperative ** Off-scale reading

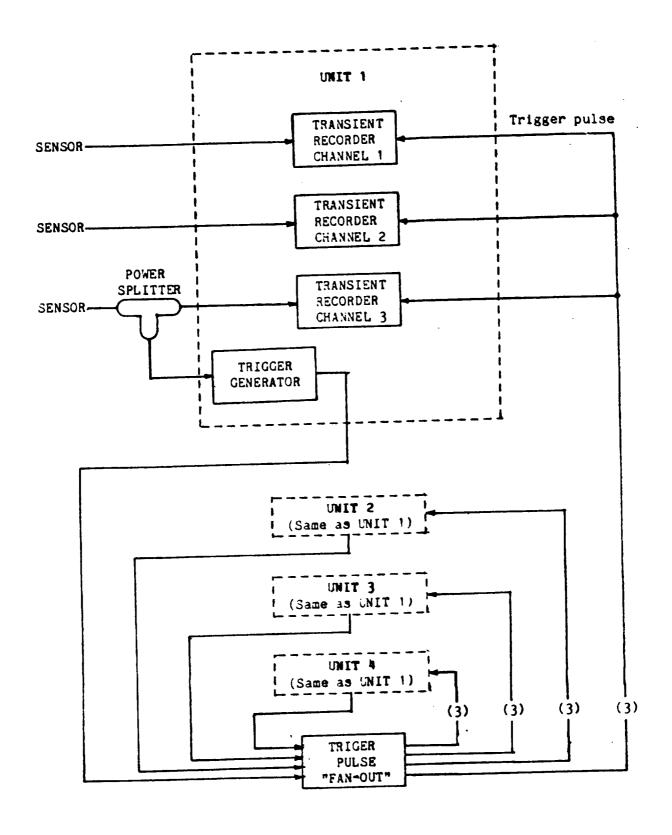


FIGURE 1. Transient Recorder Trigger Configuration

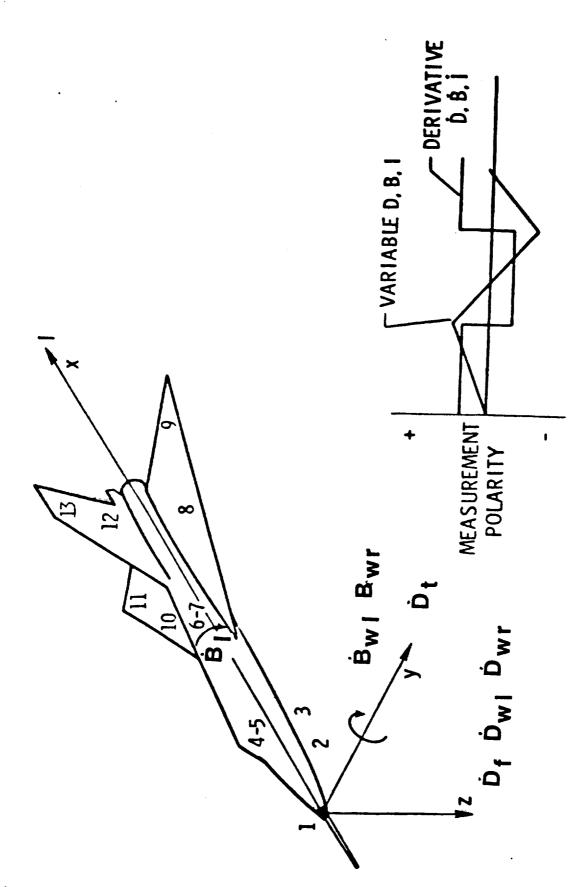


Figure 2. - Electromagnetic sign conventions and sensor locations.

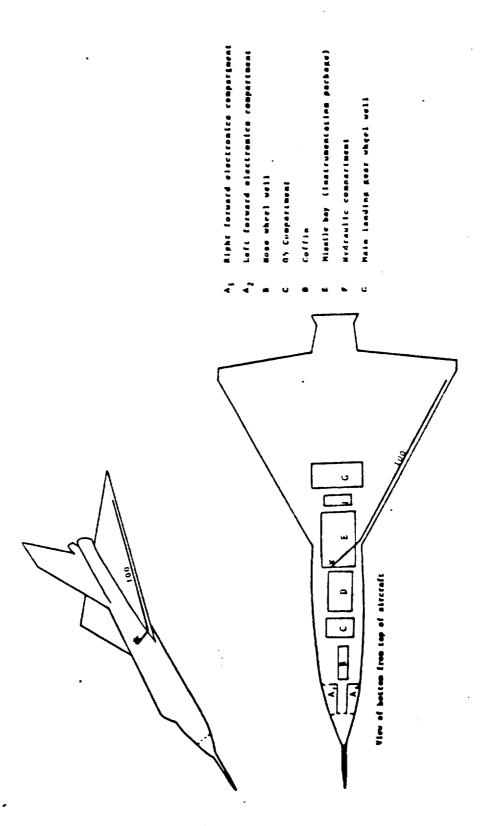
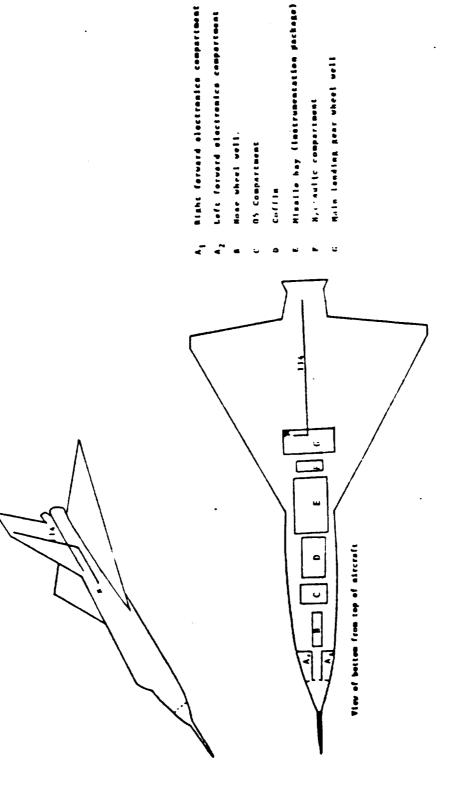
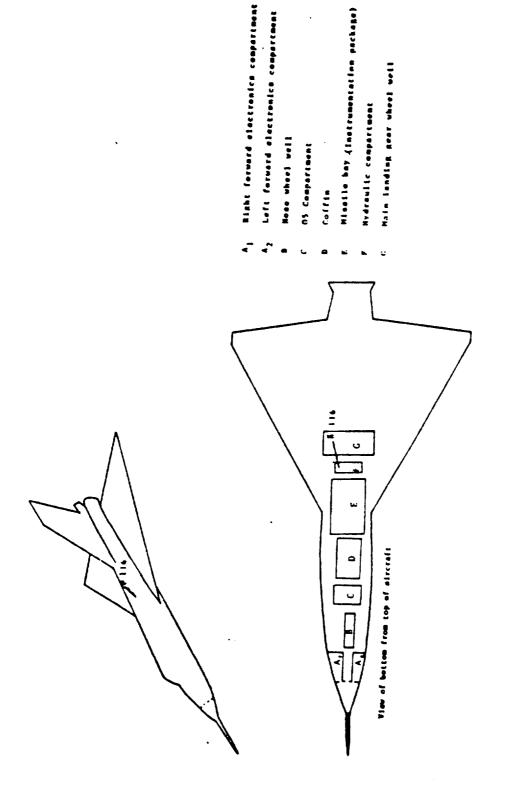


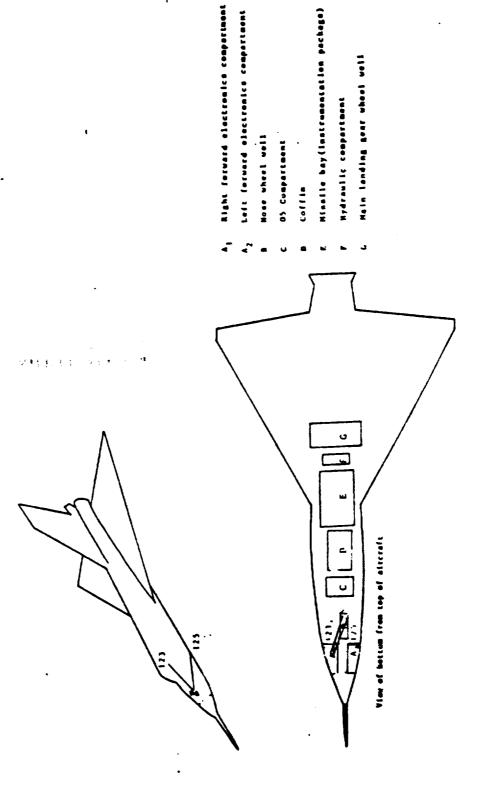
Figure 4. TP 101, 102, and $V_{\mathbf{fa}}$

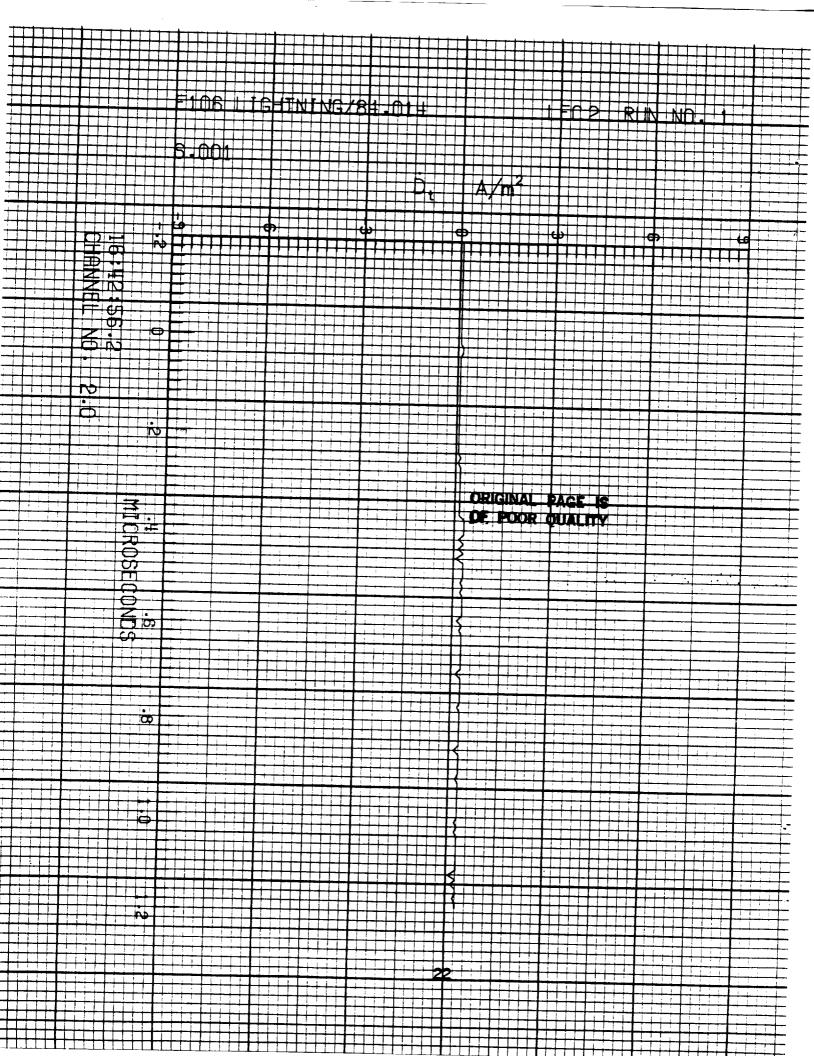
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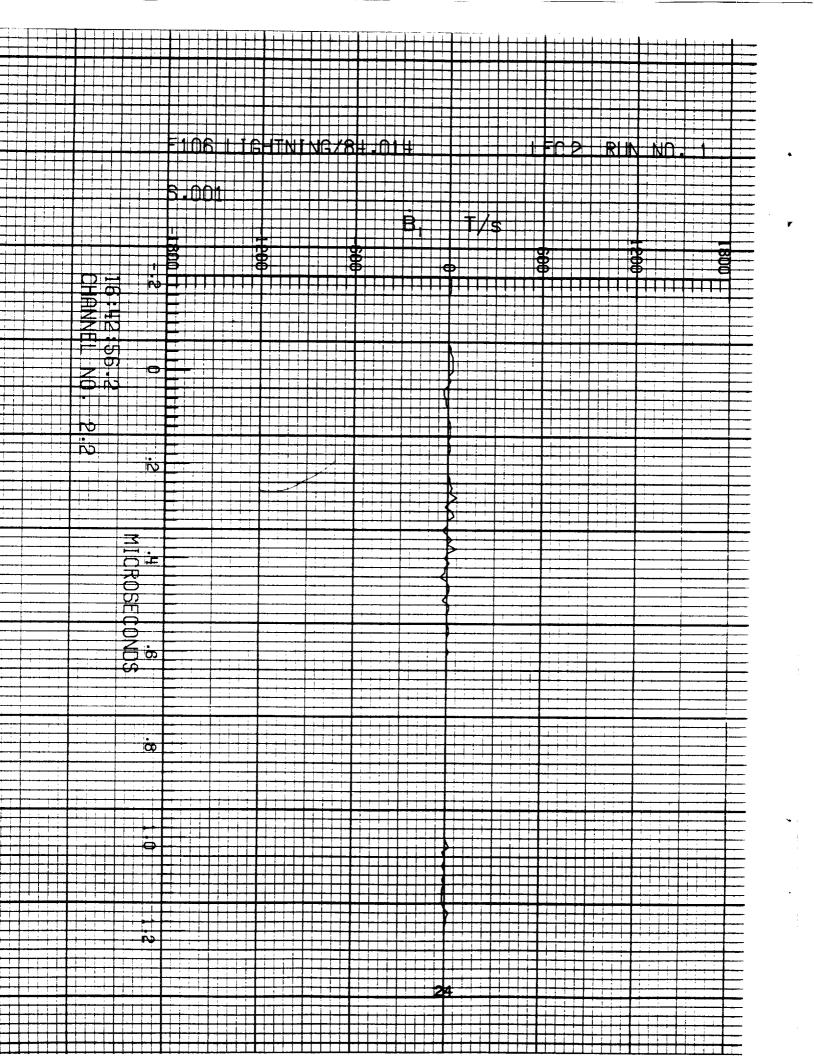


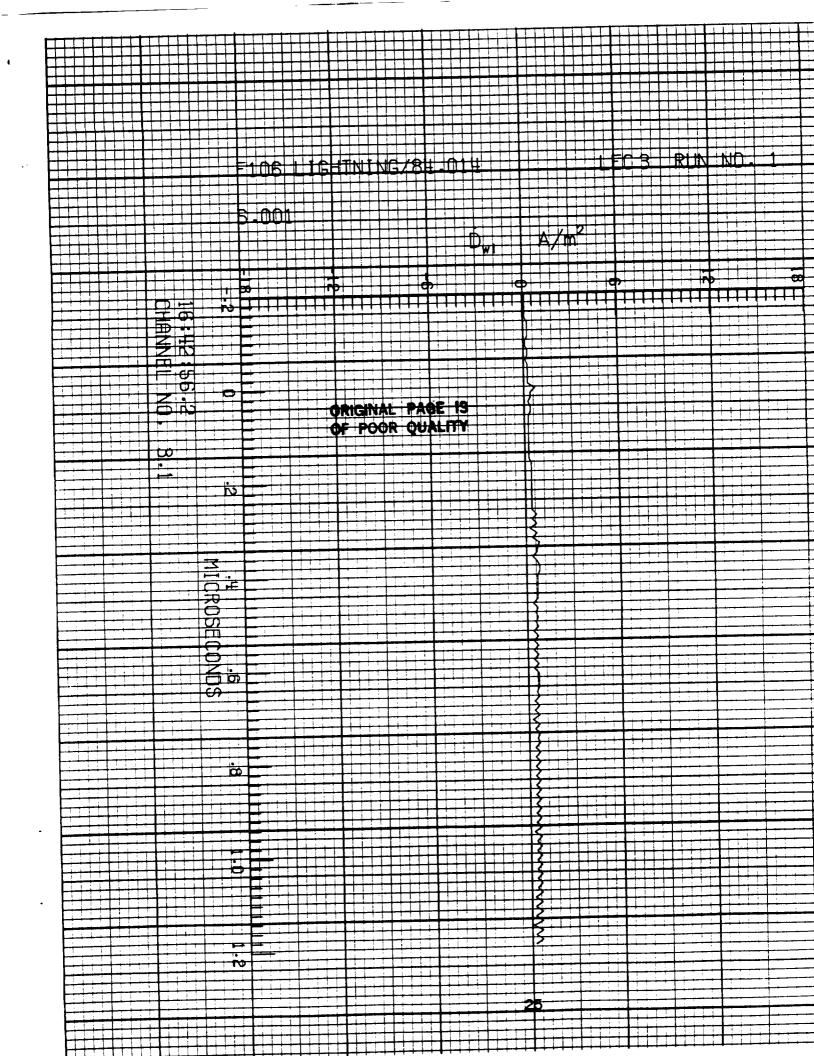
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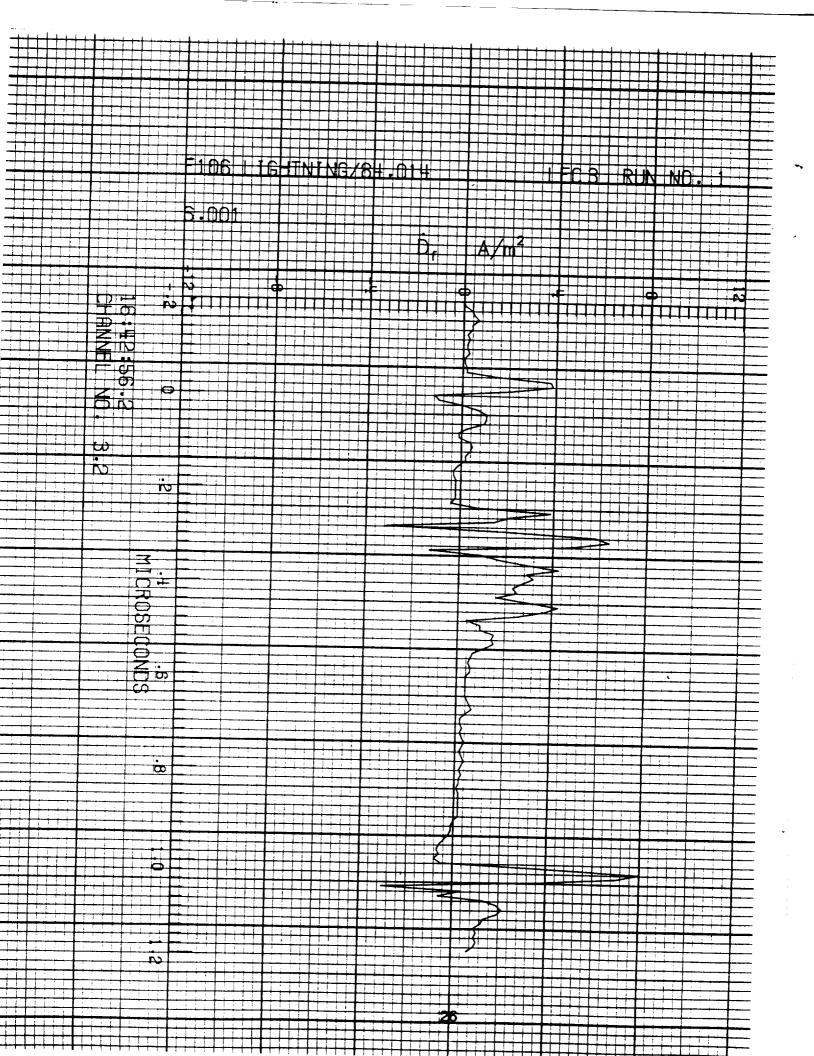


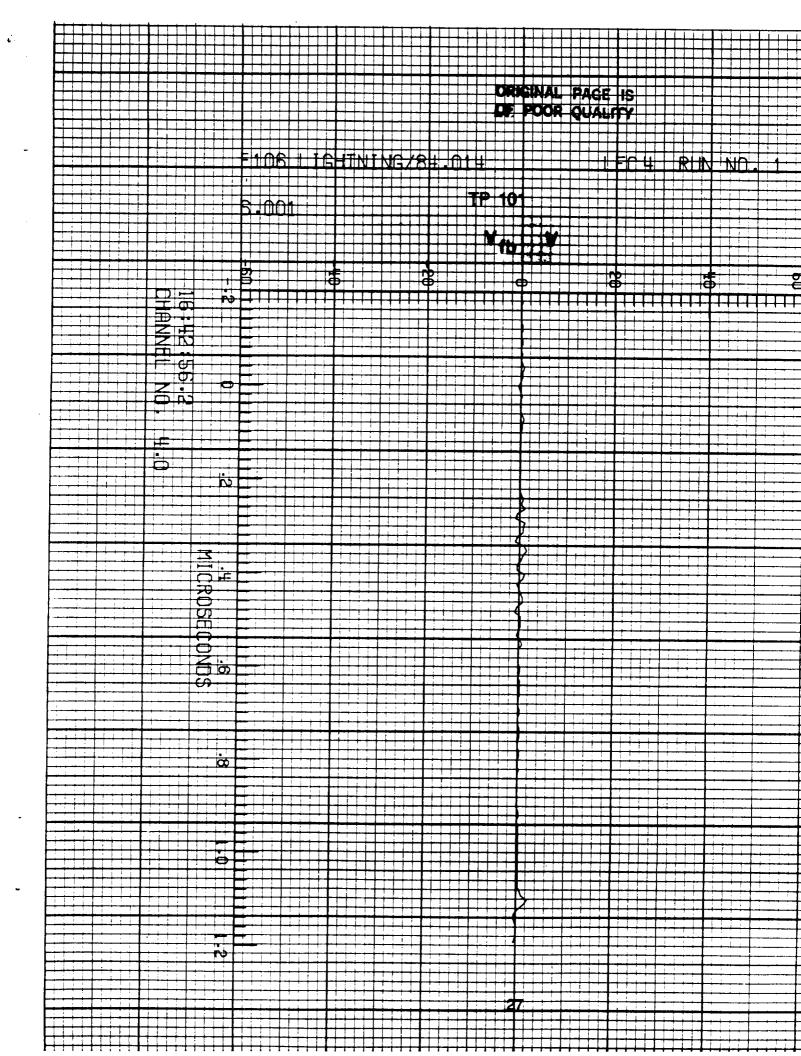


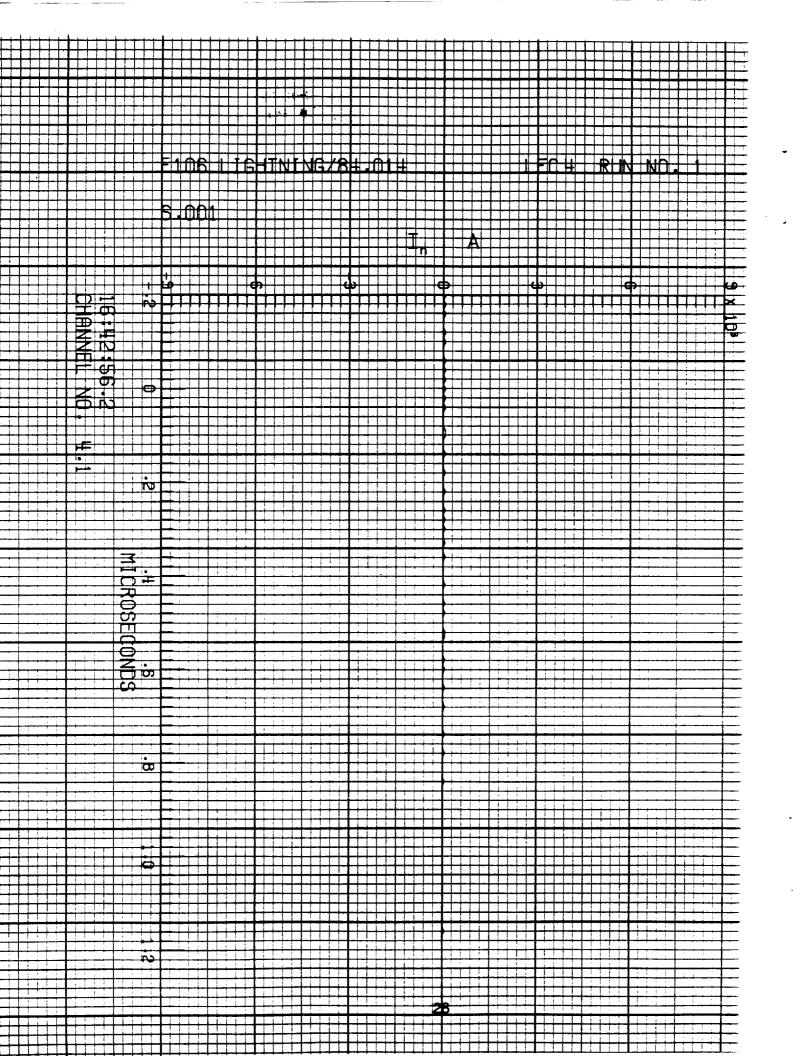
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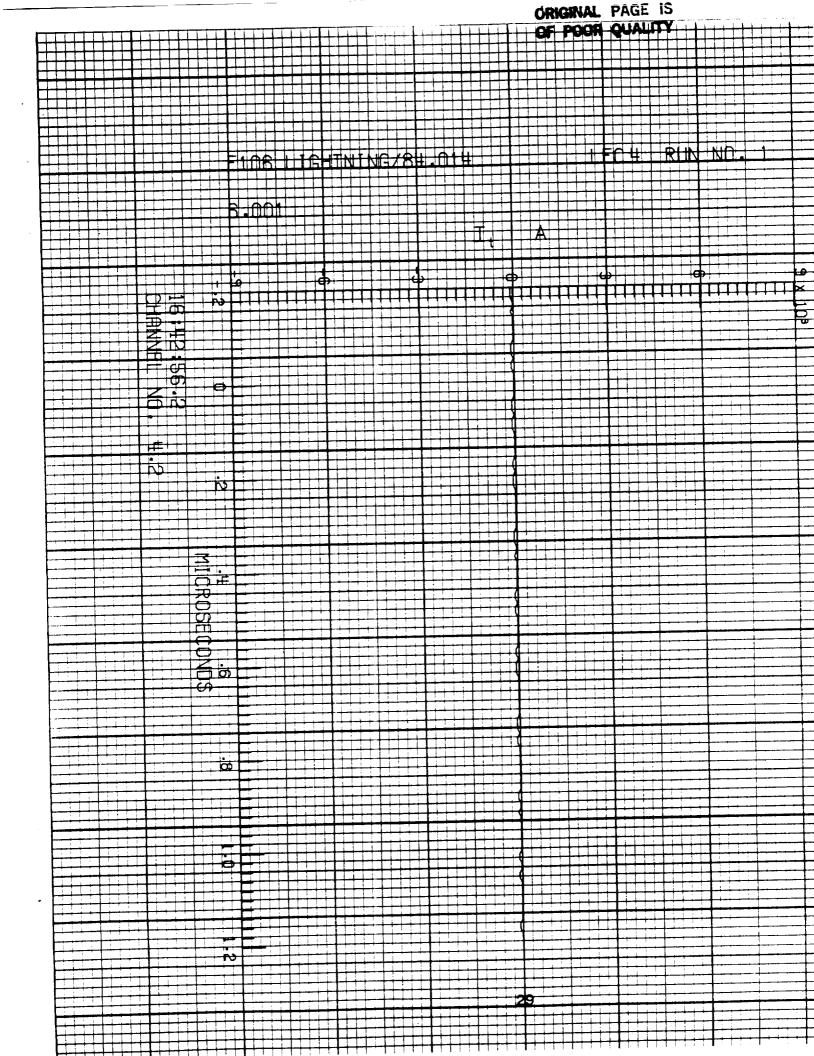


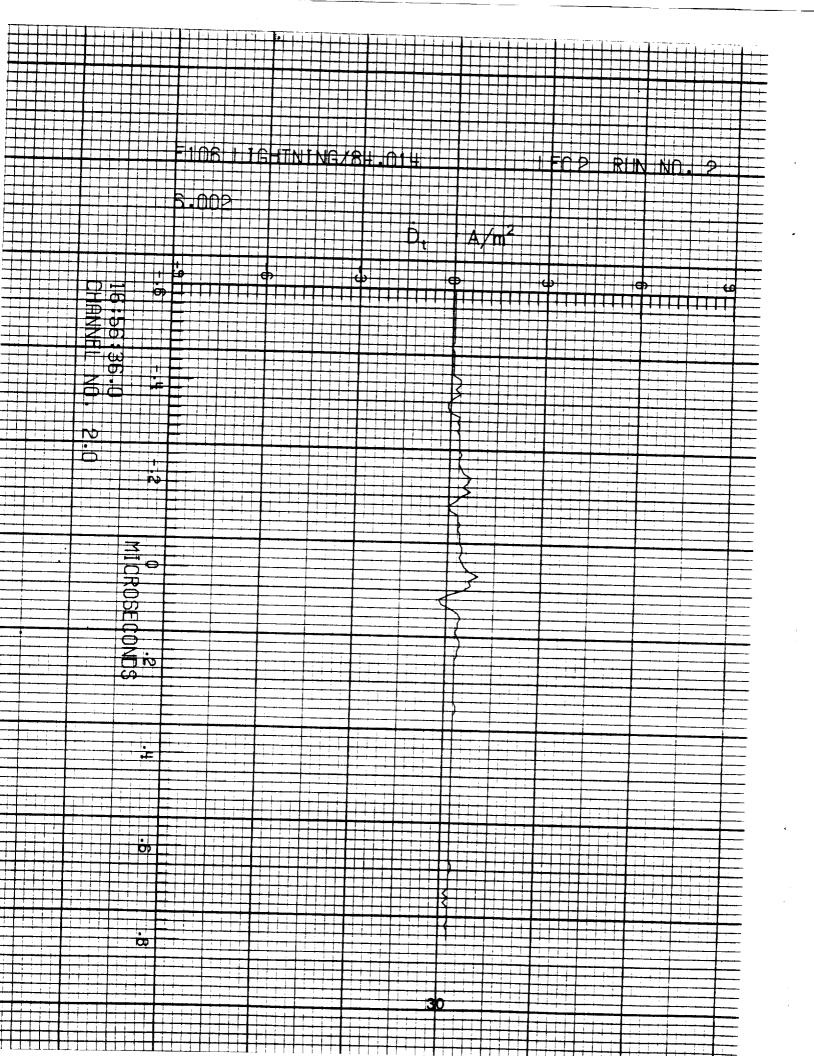


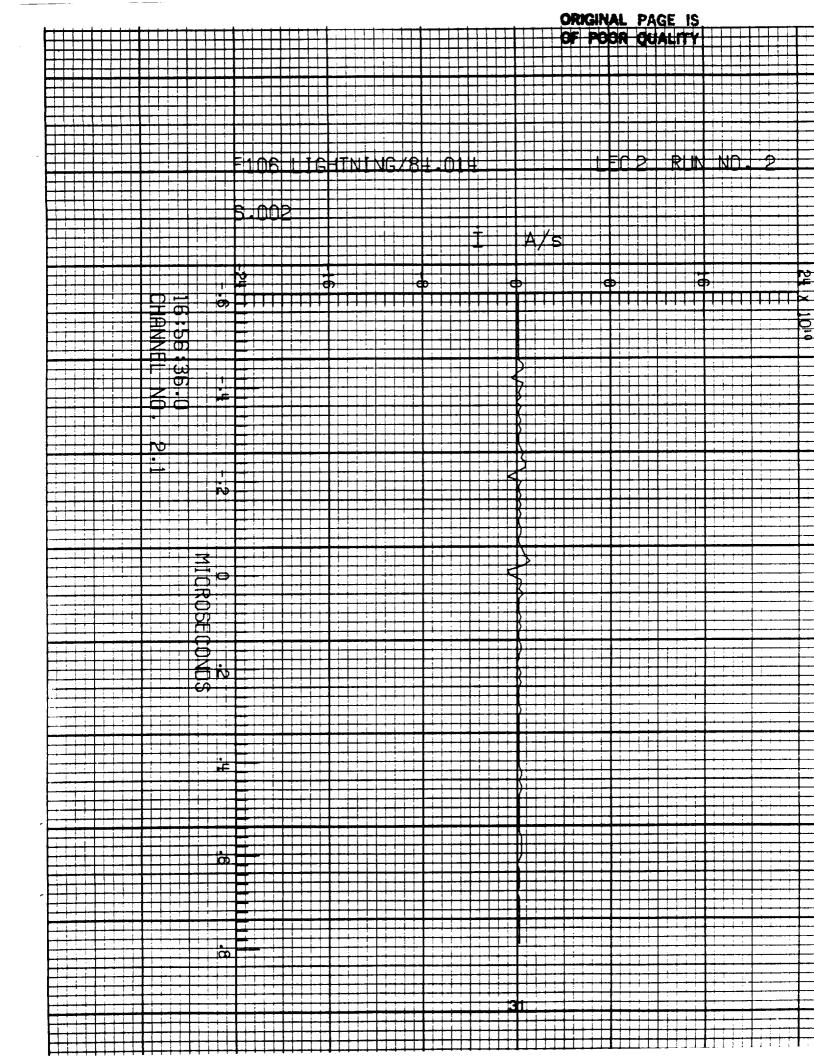


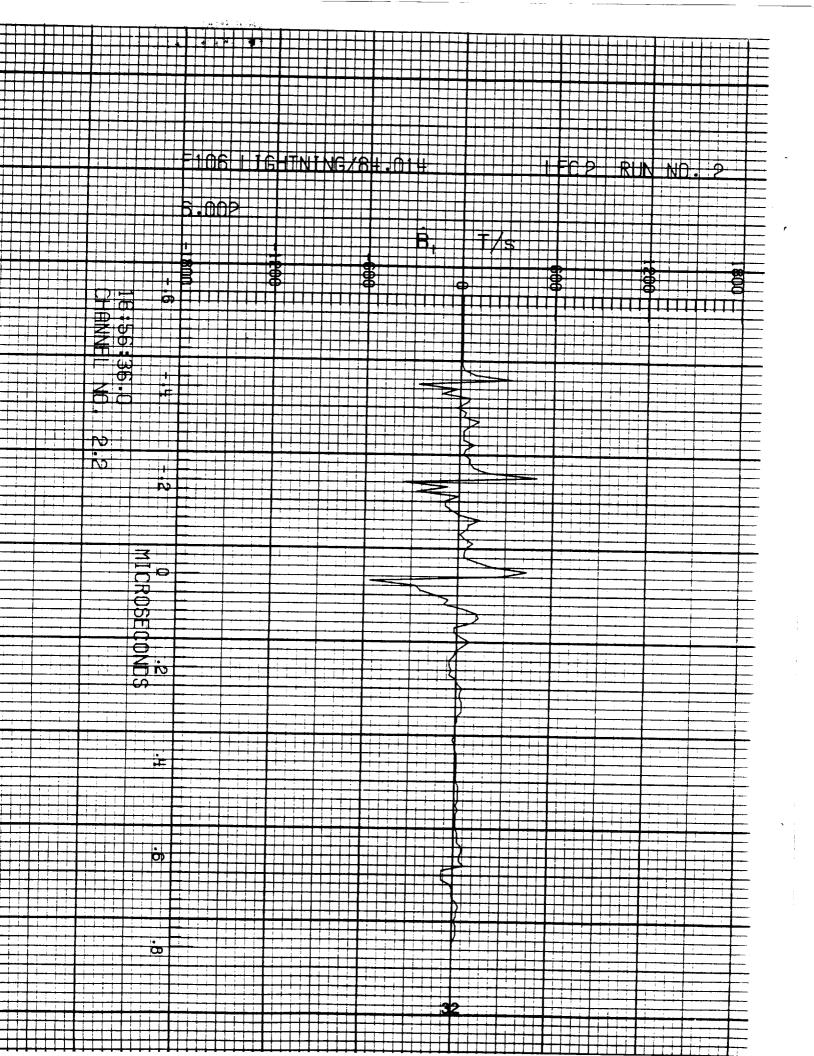


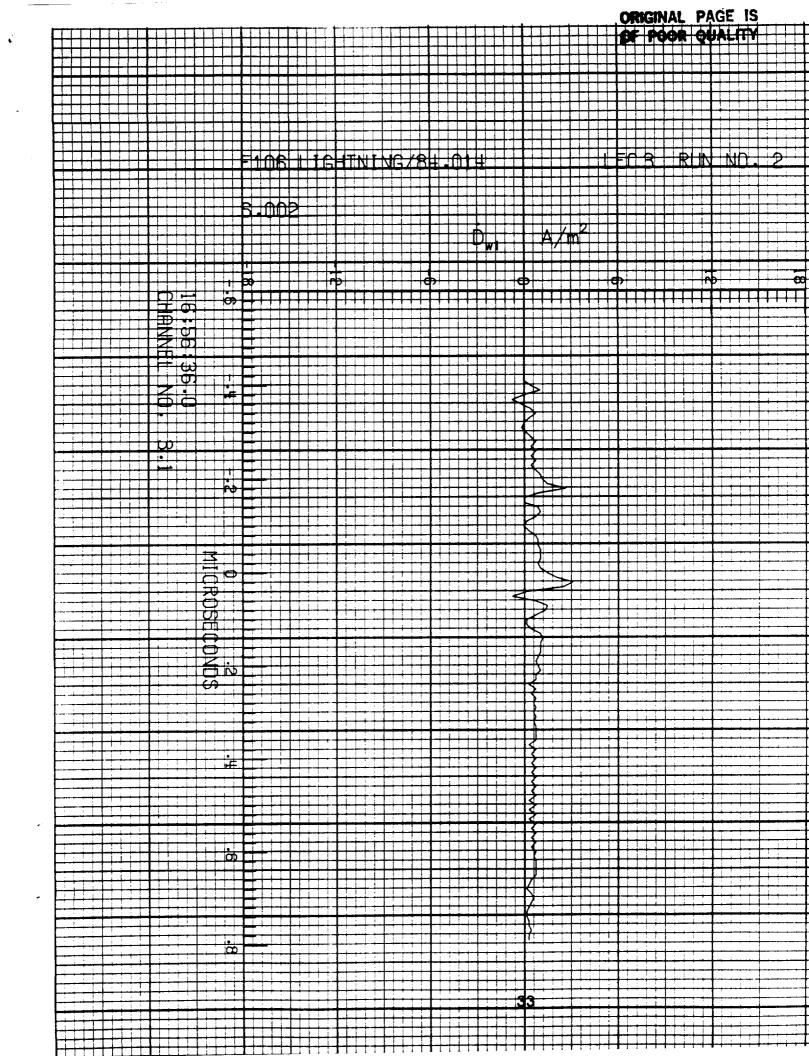


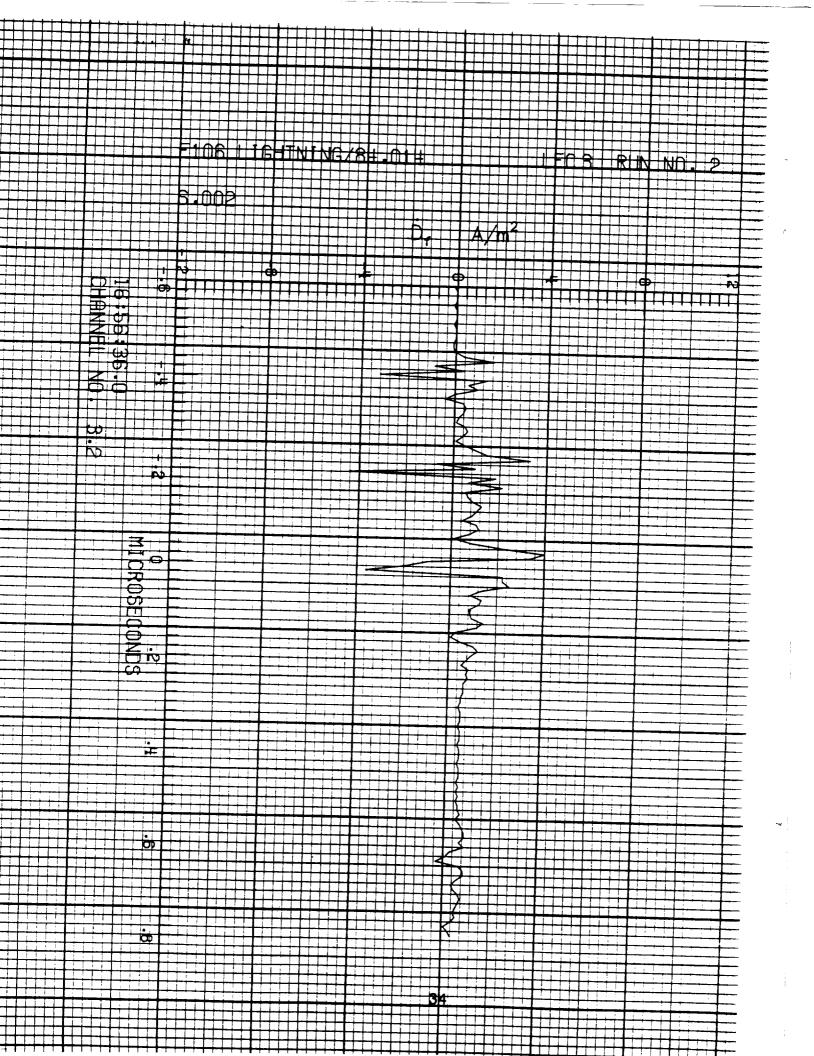


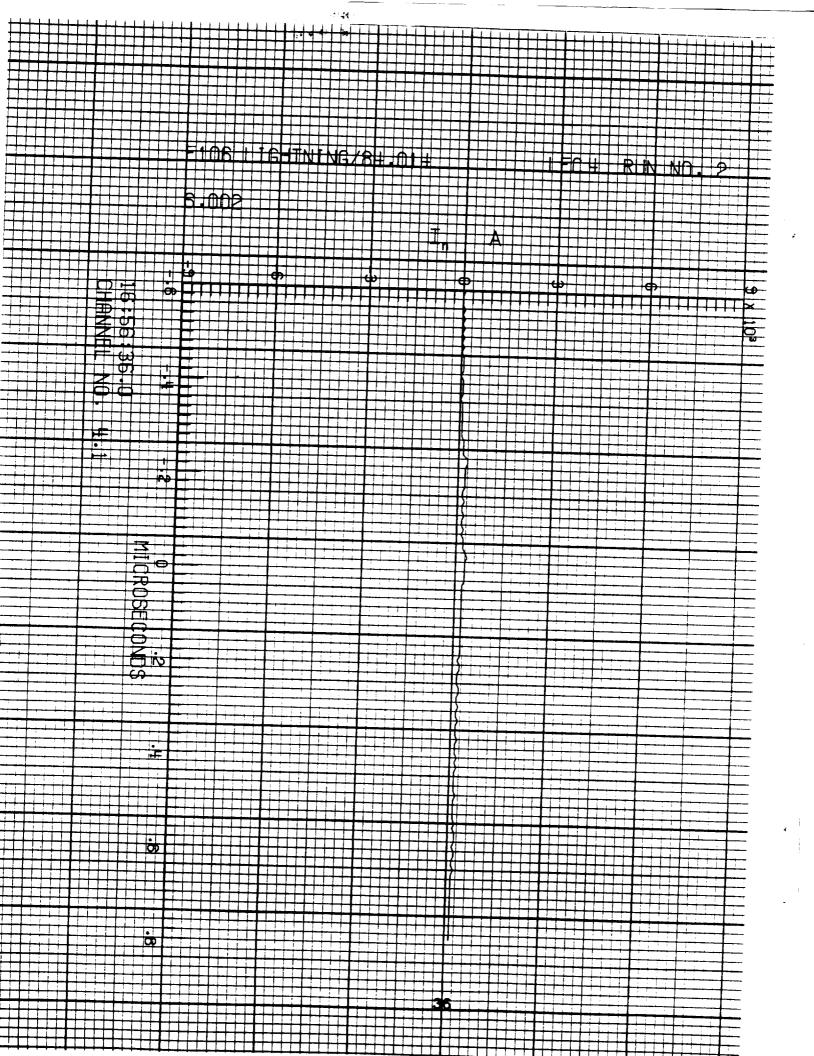


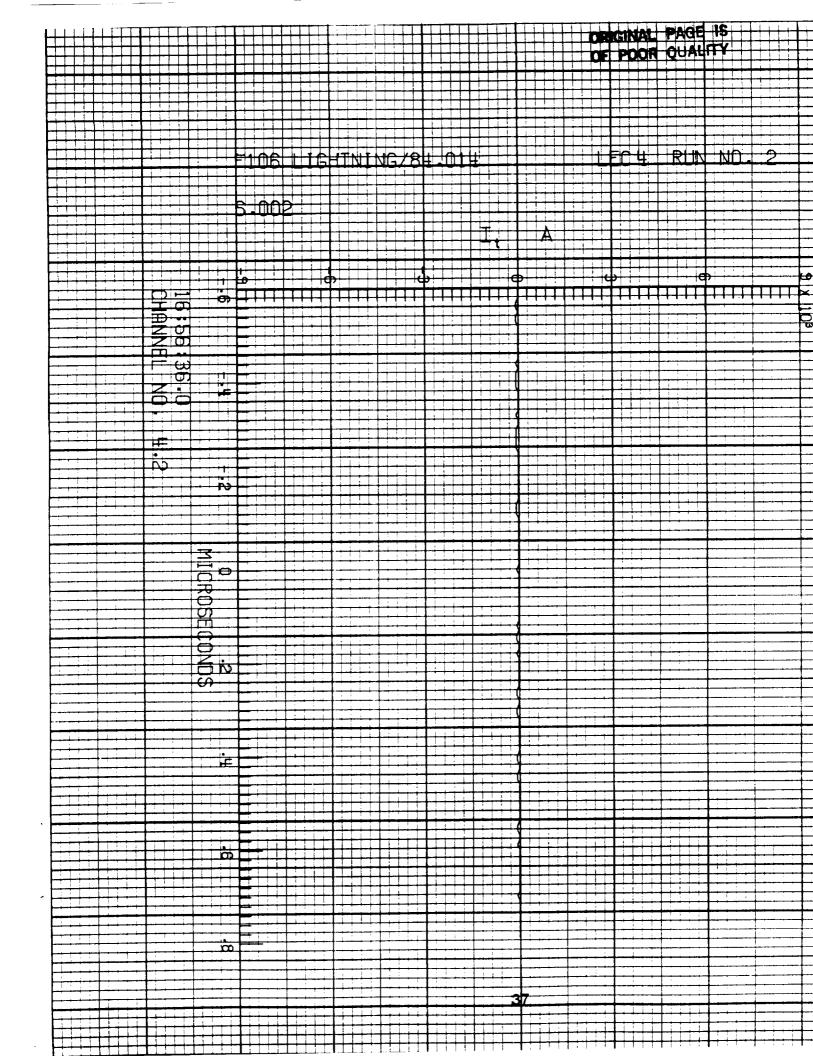


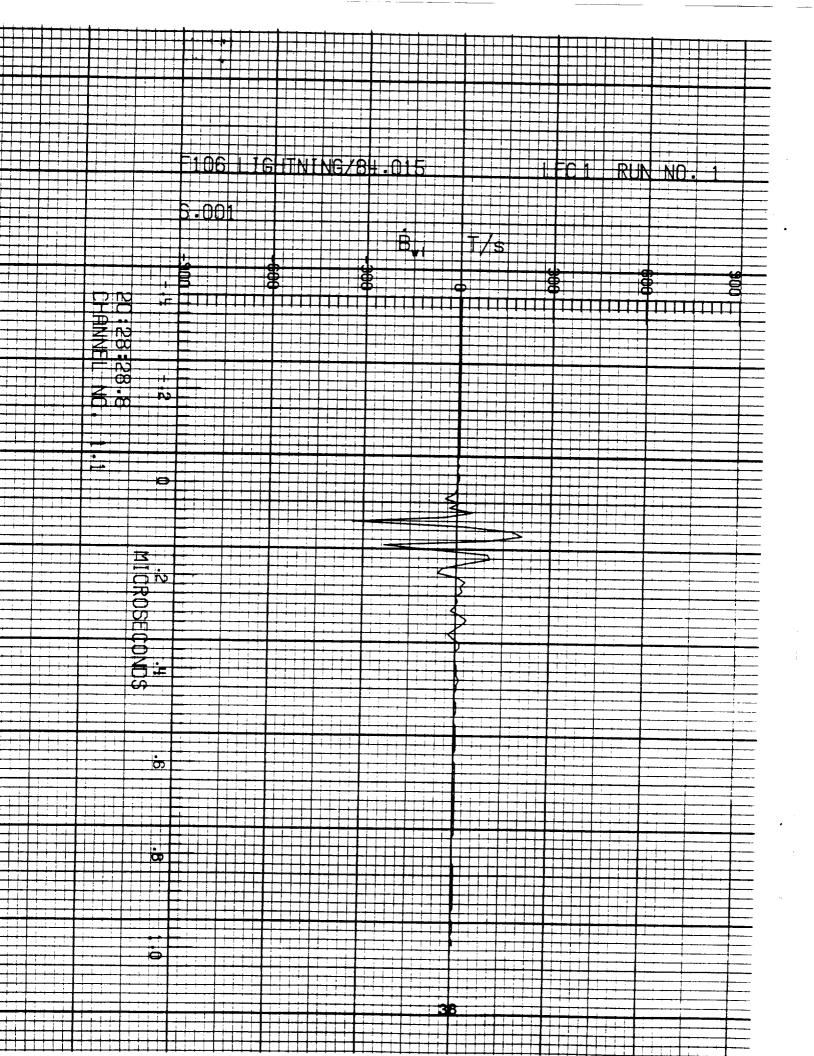


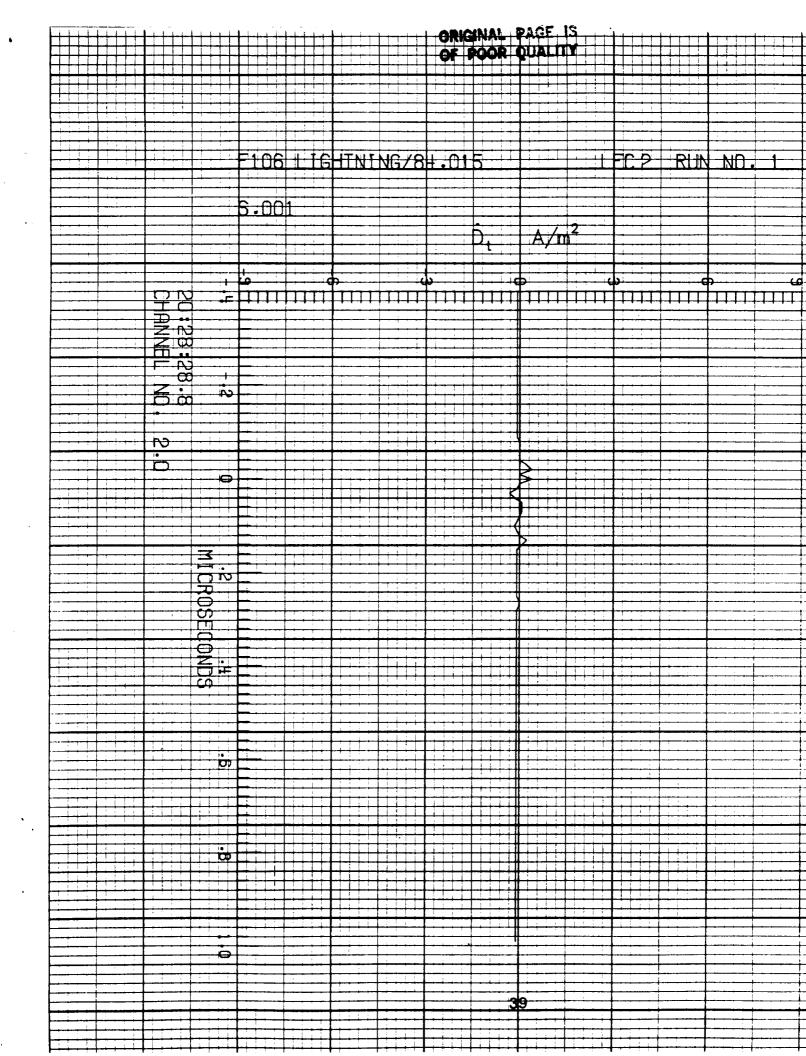


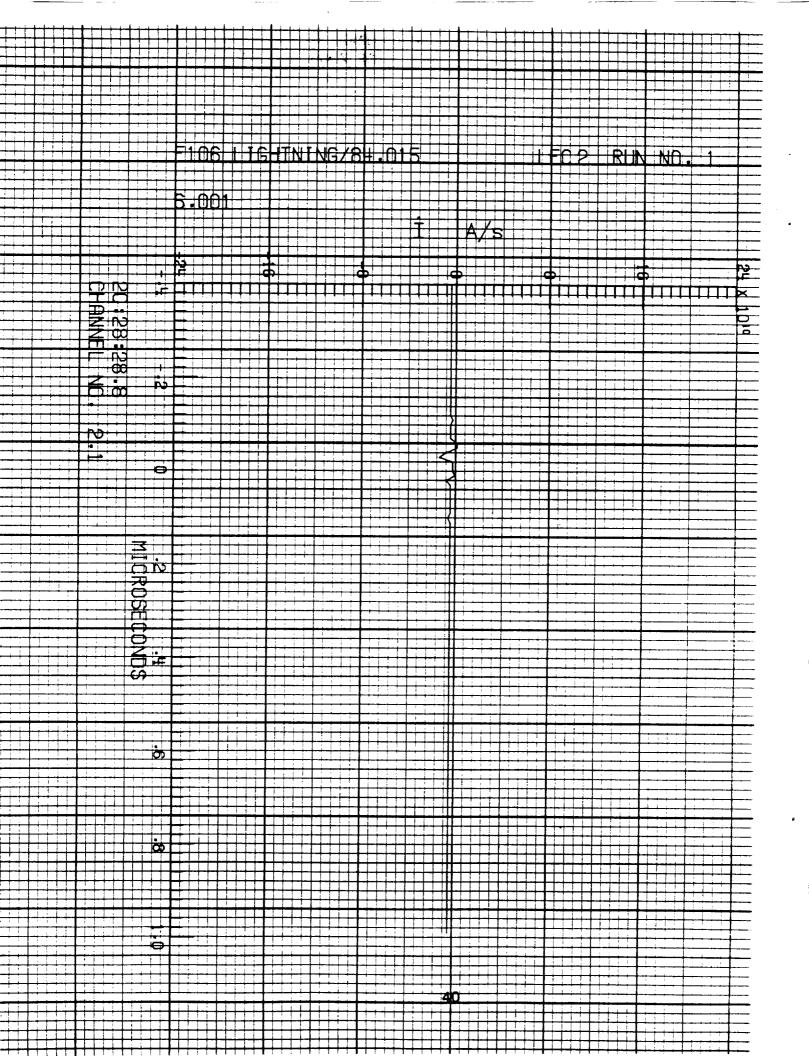


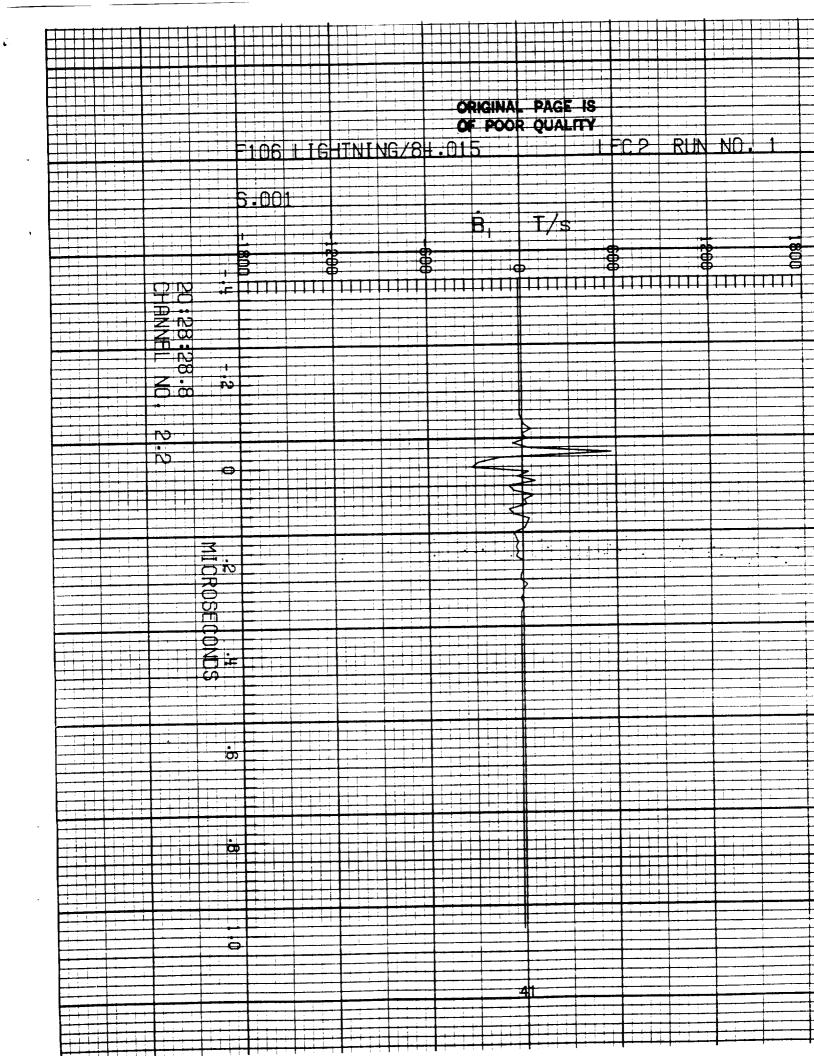


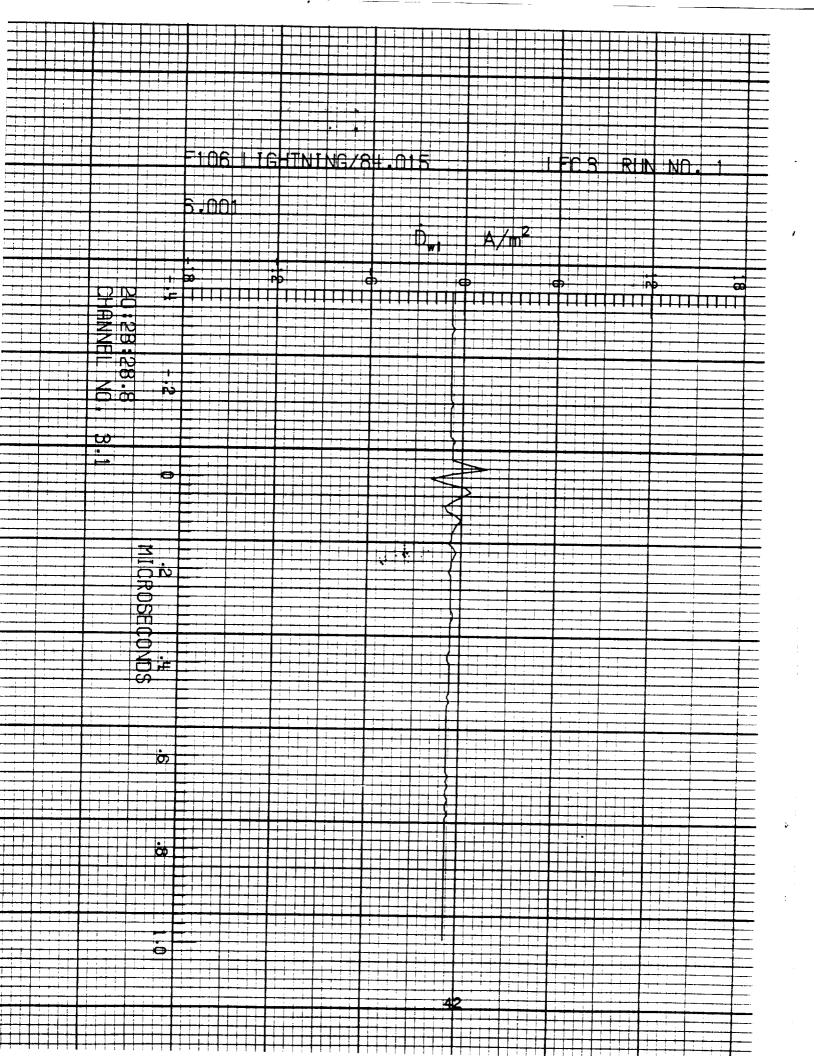


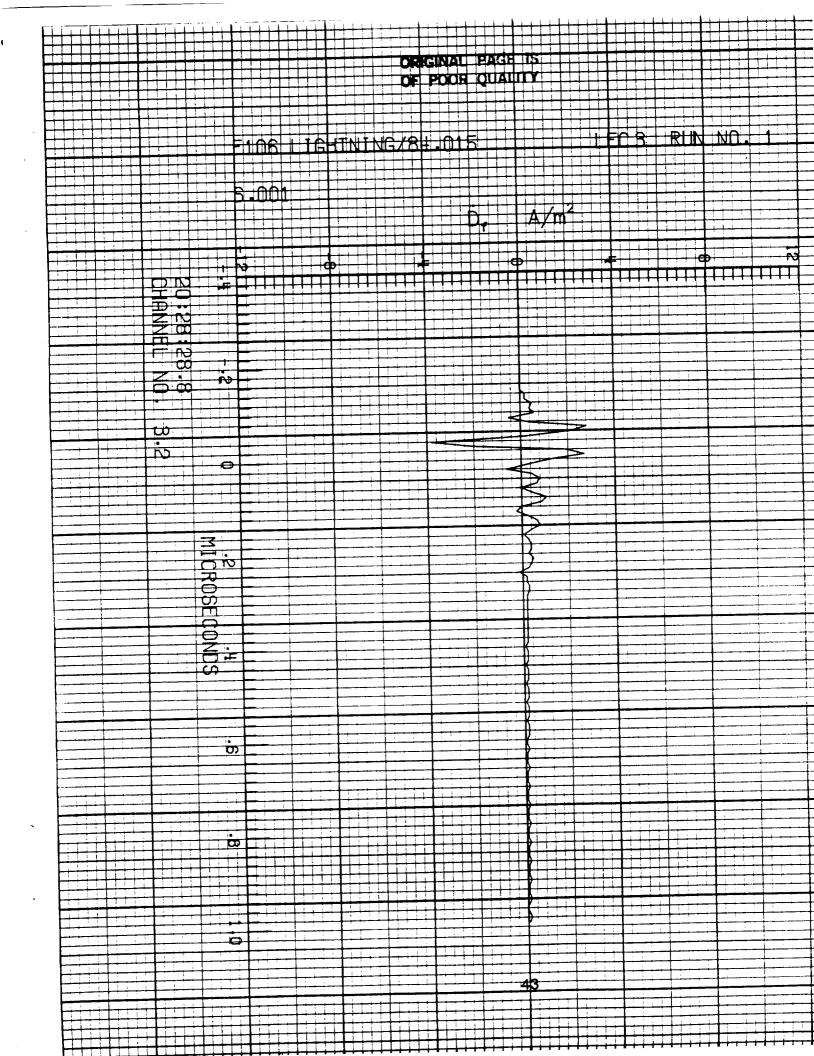


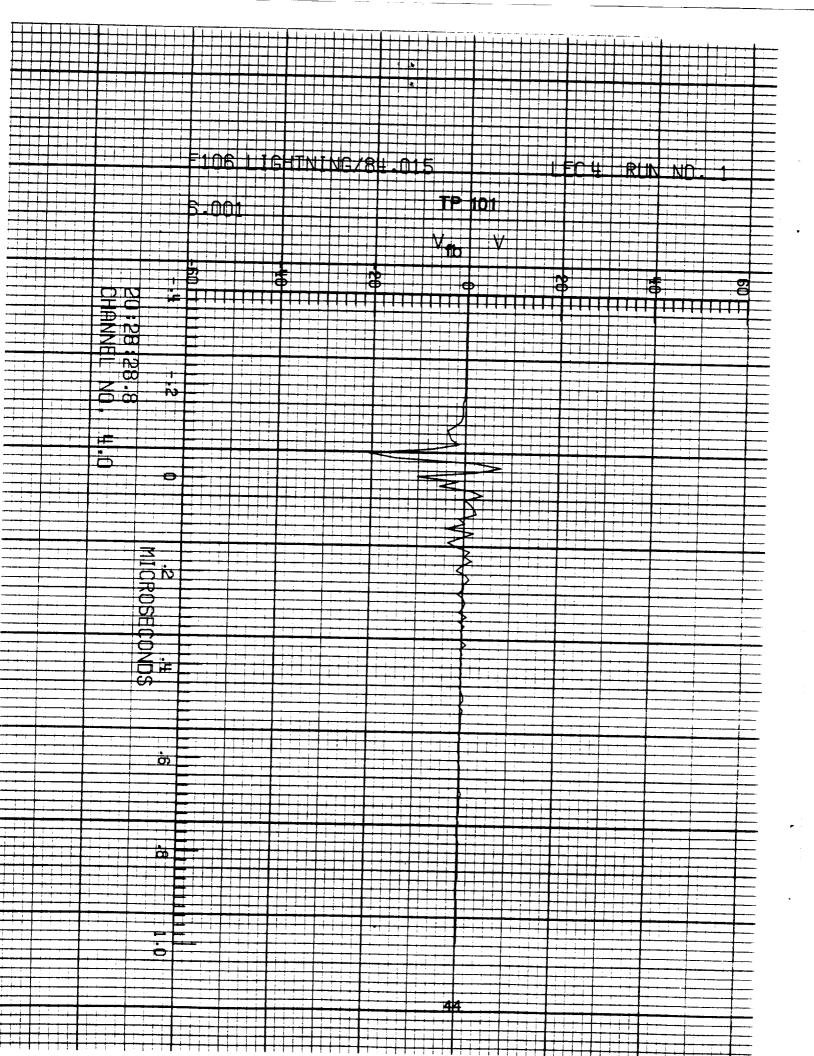


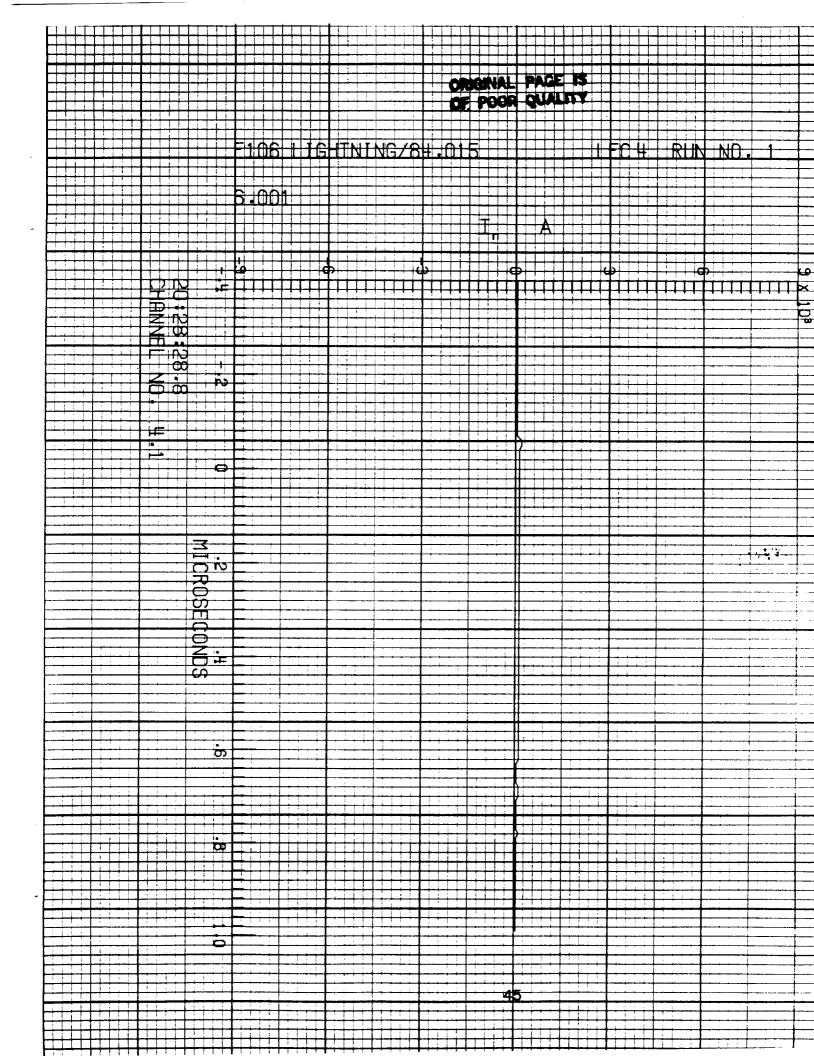


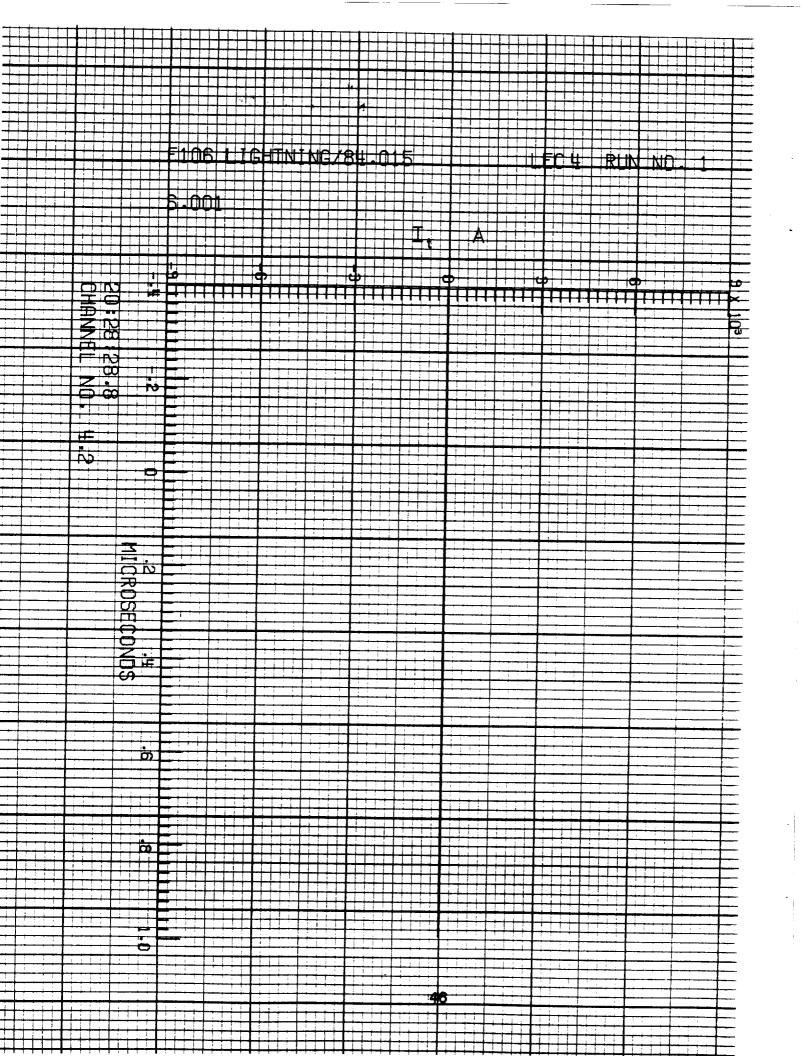


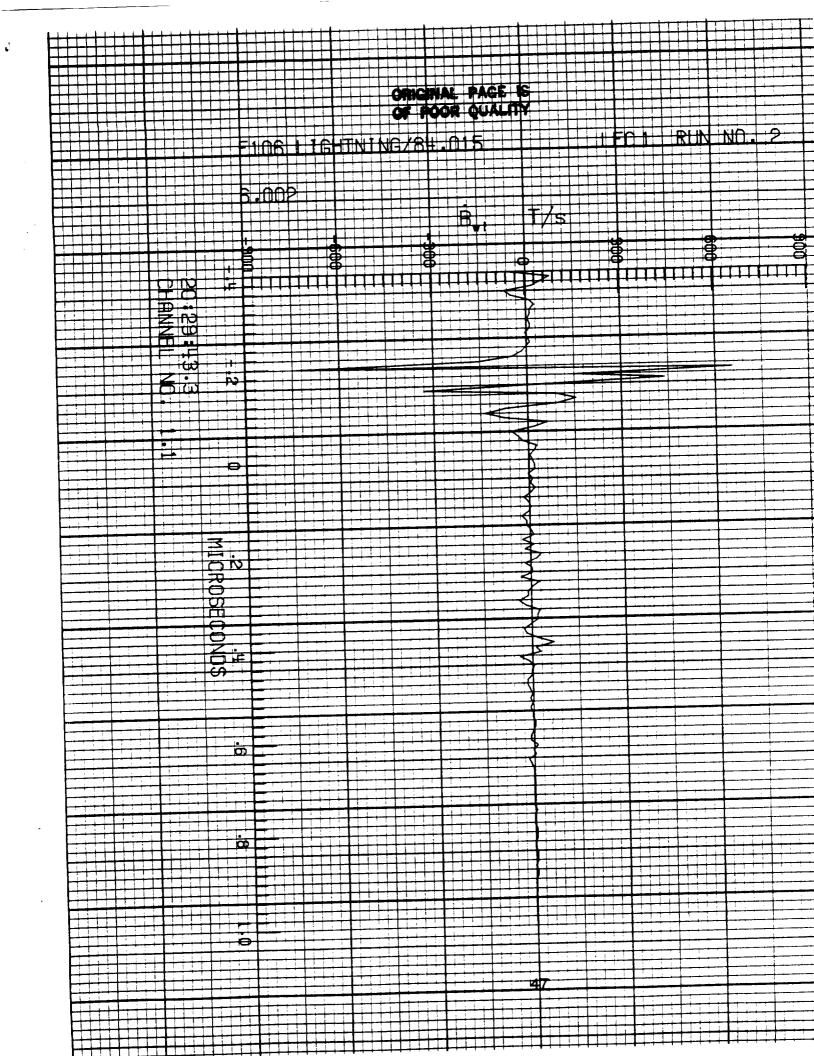


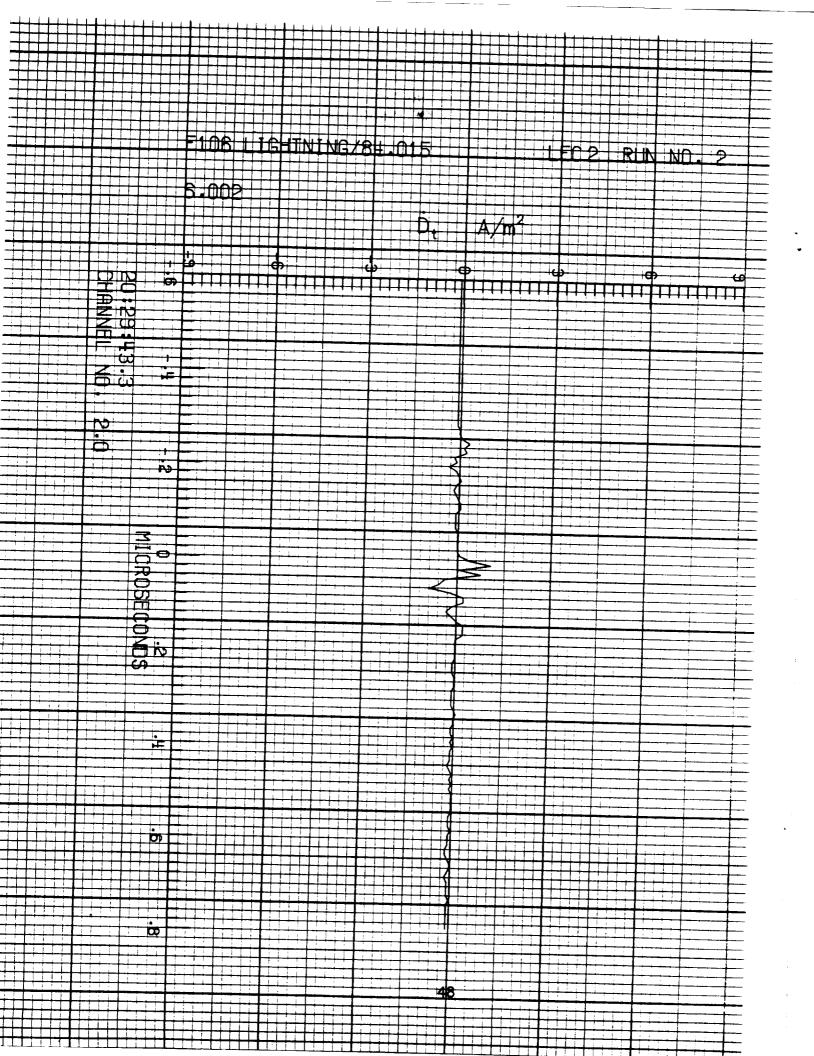


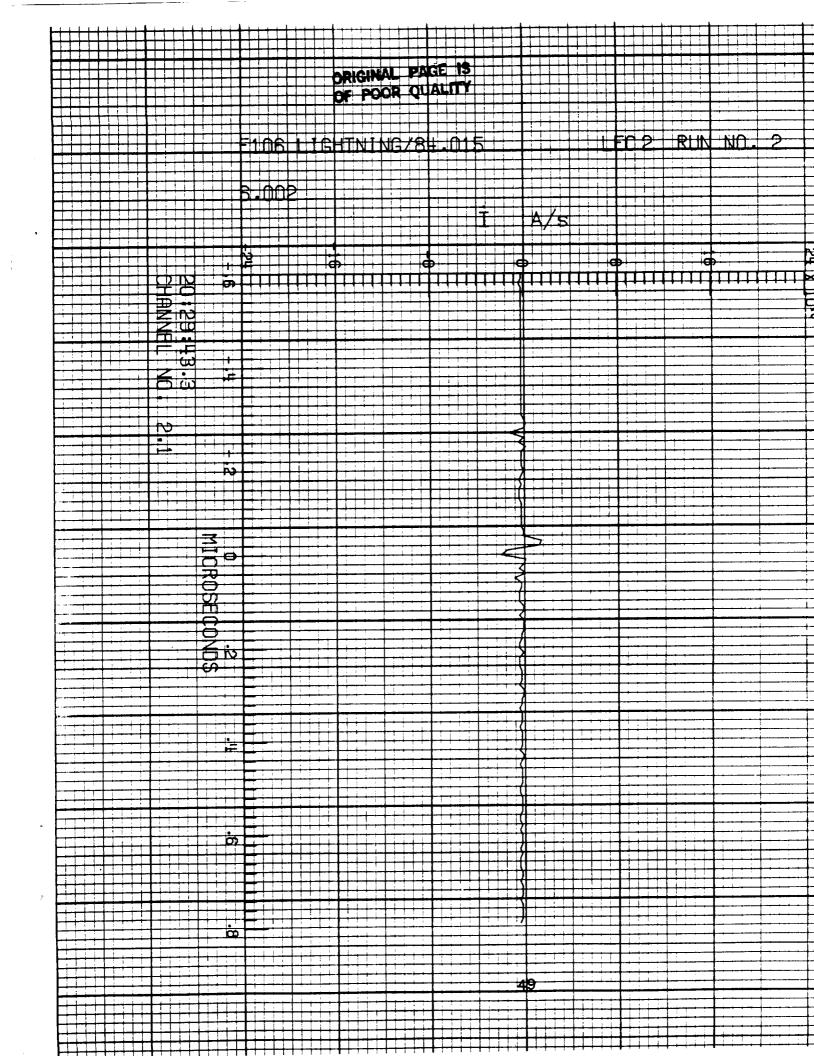


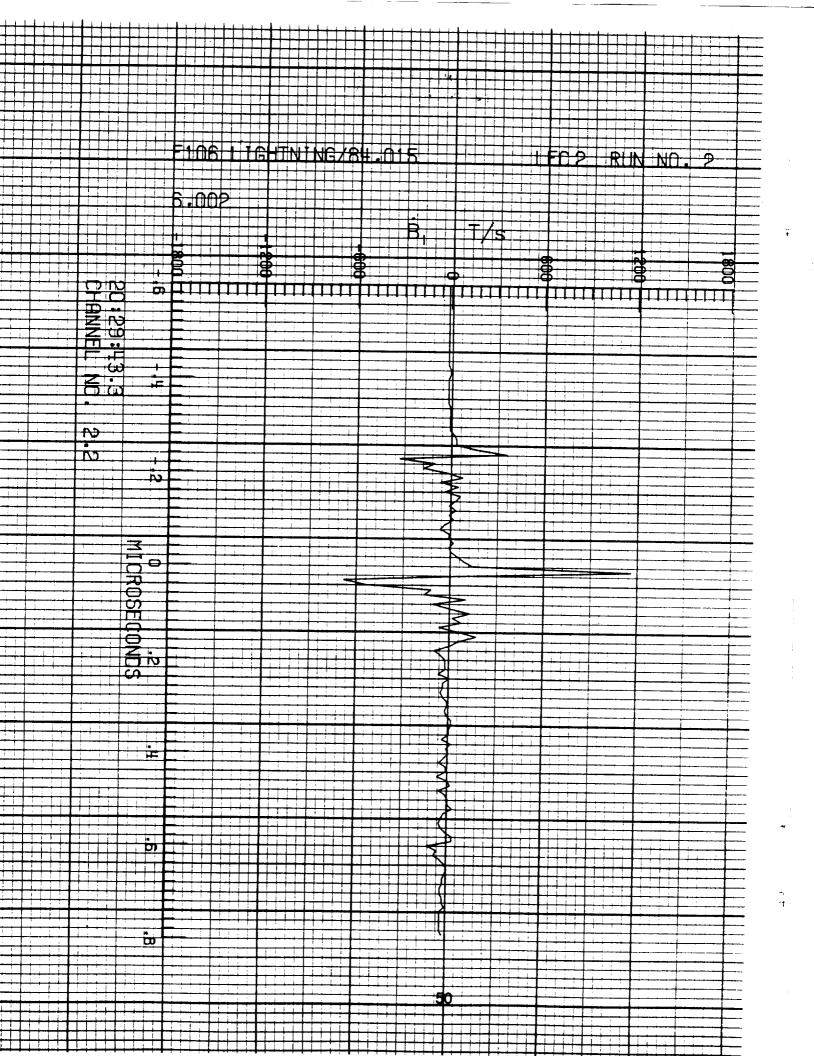


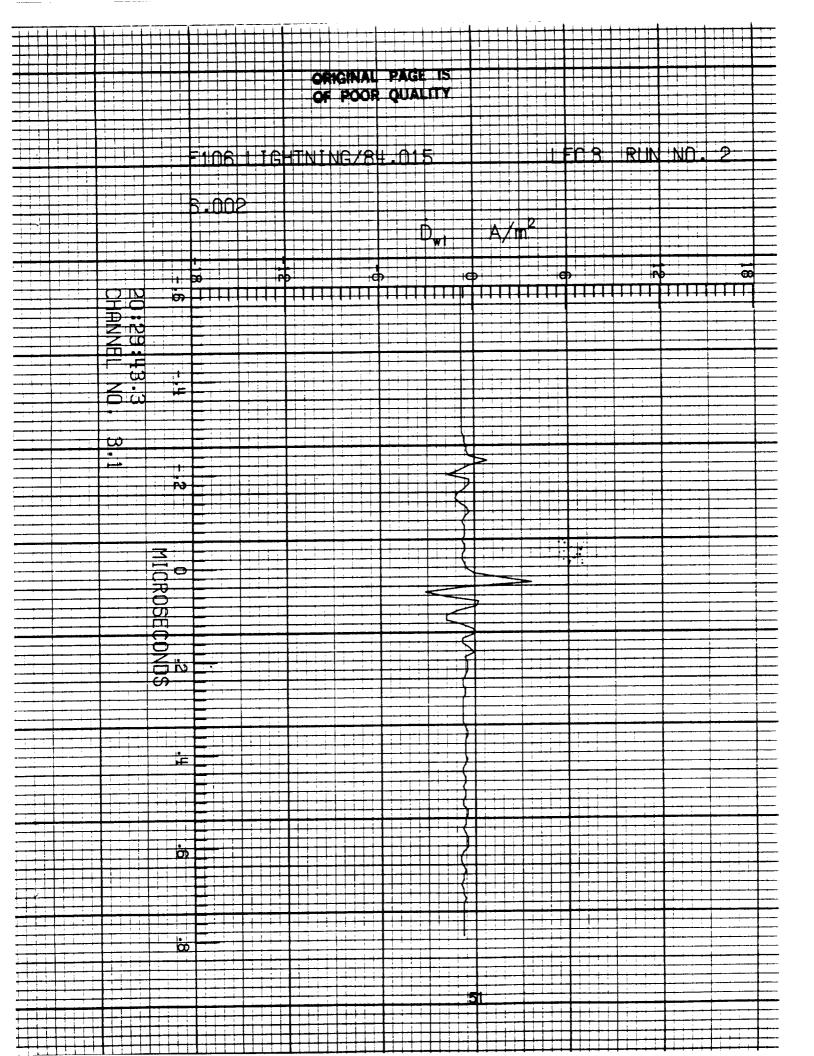


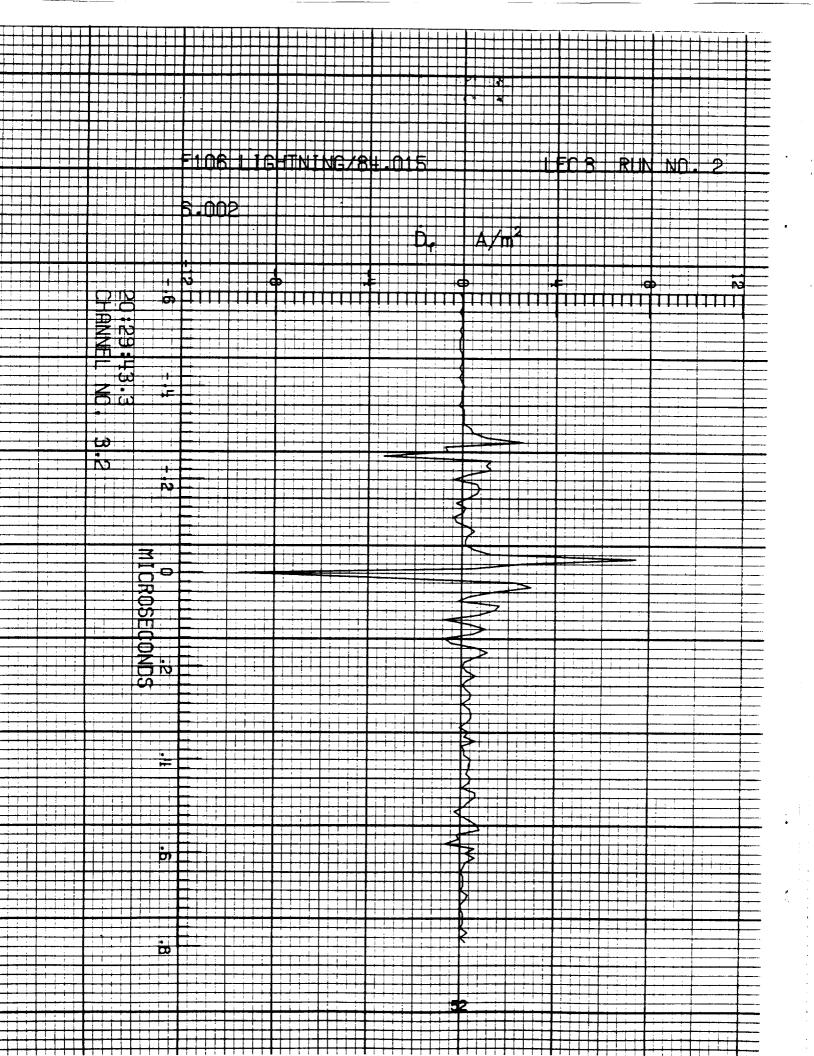


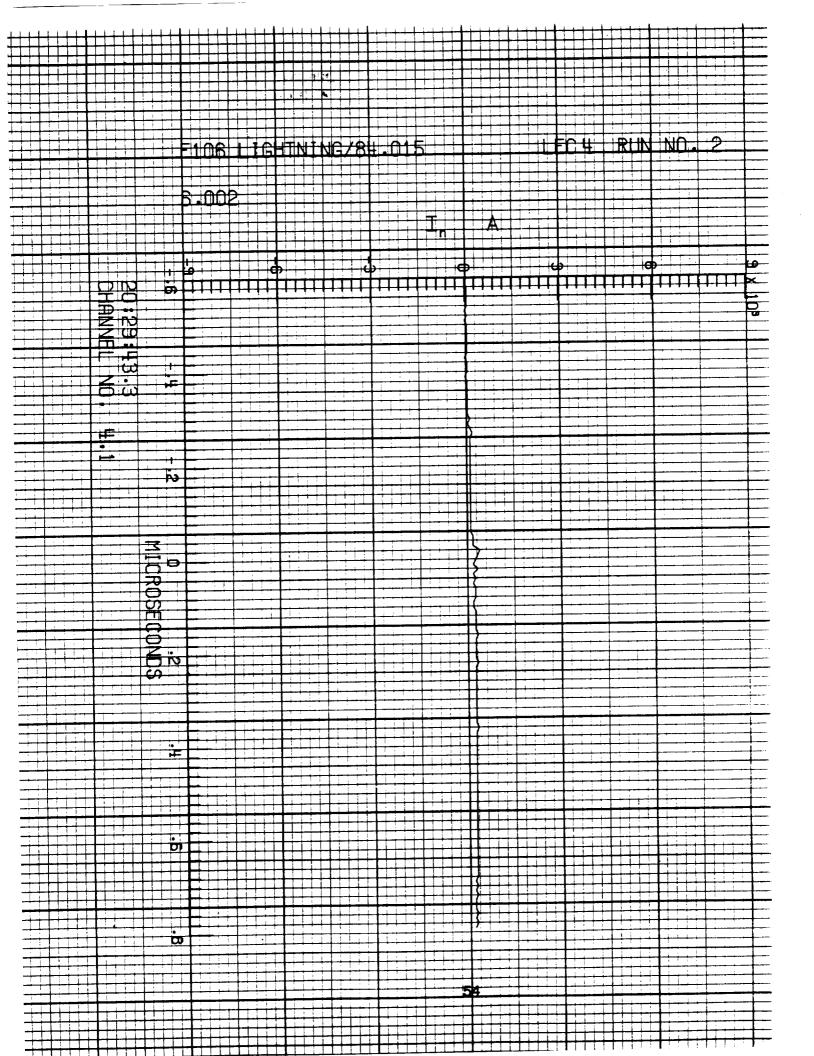


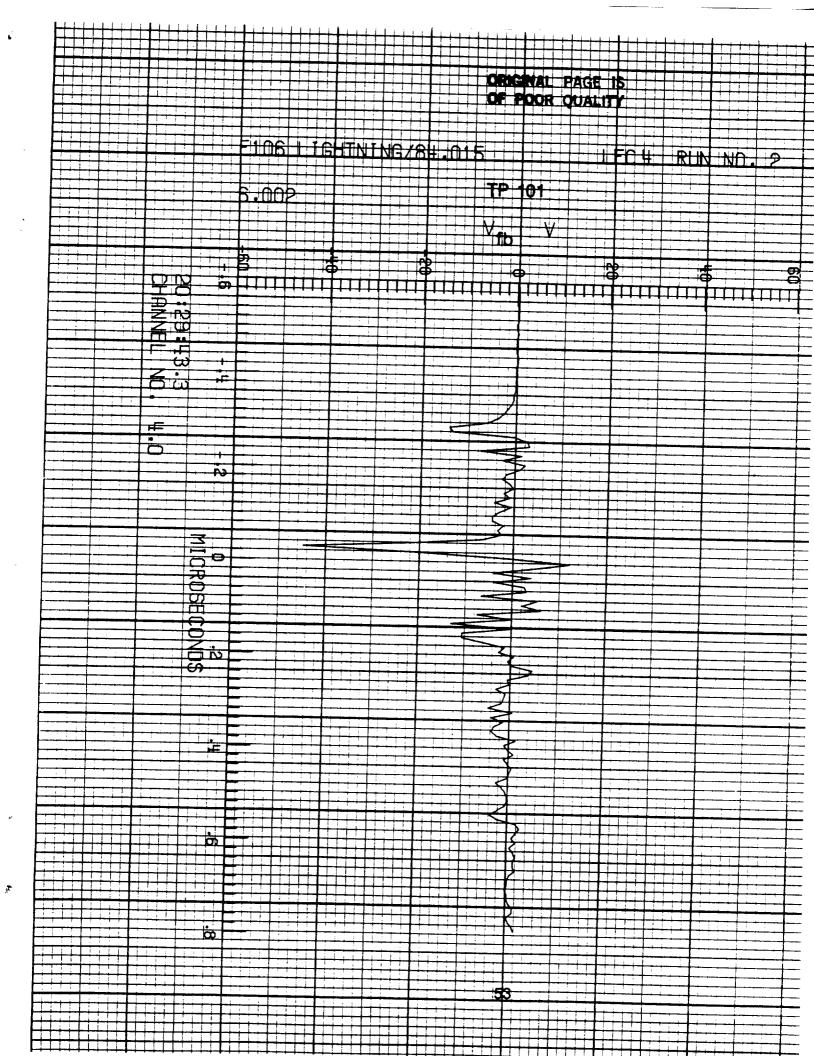


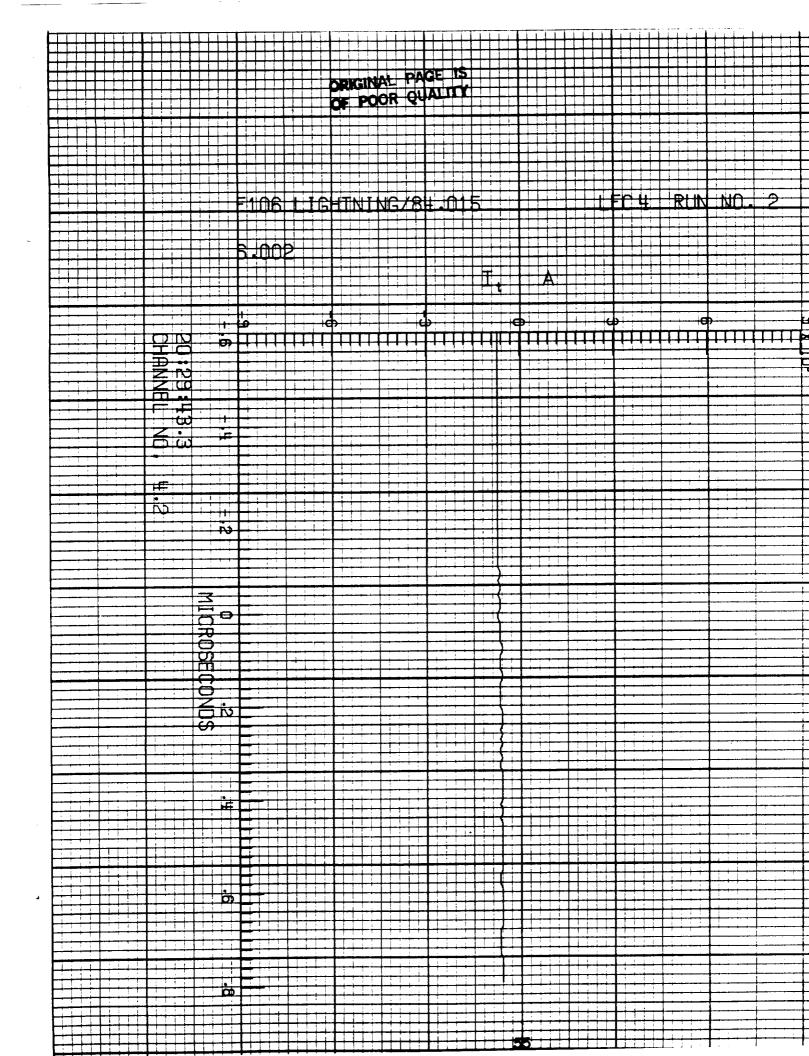


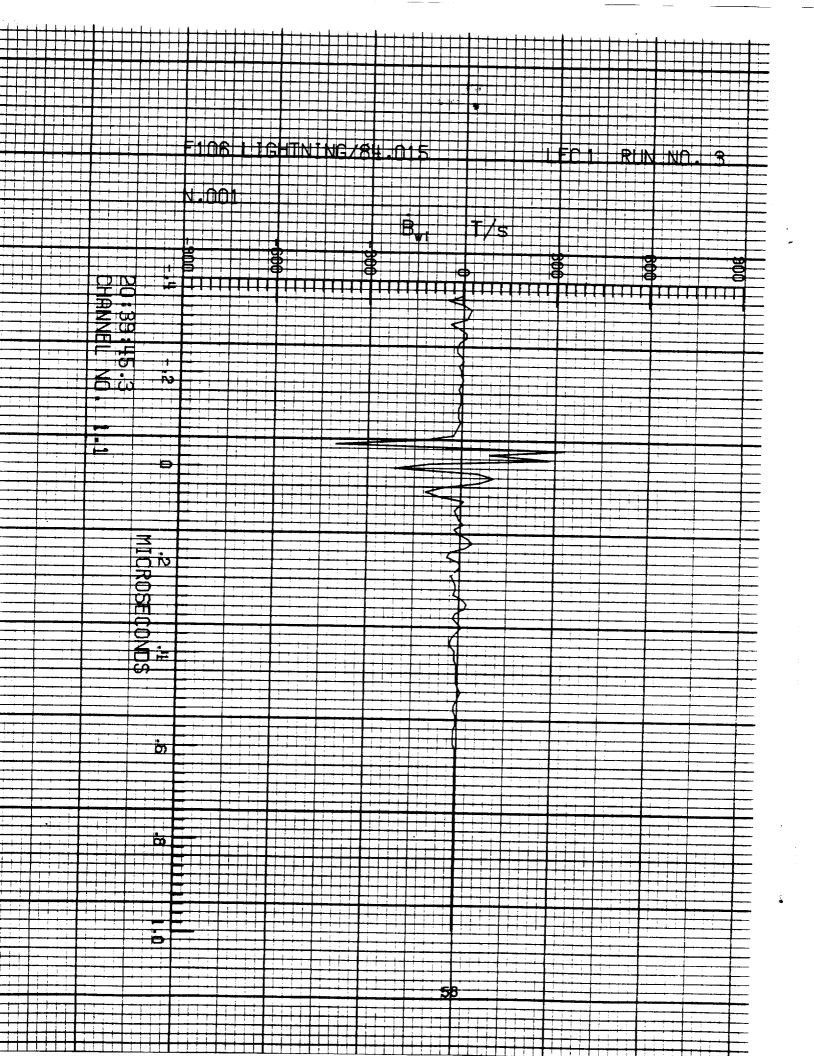


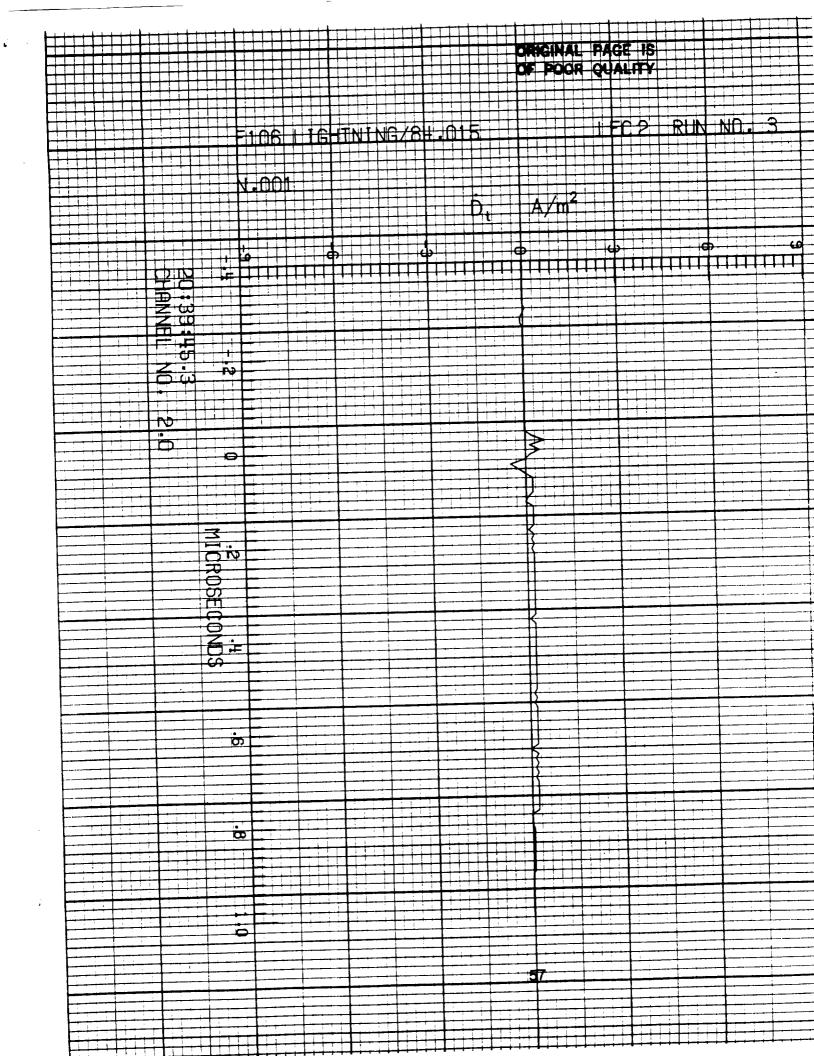


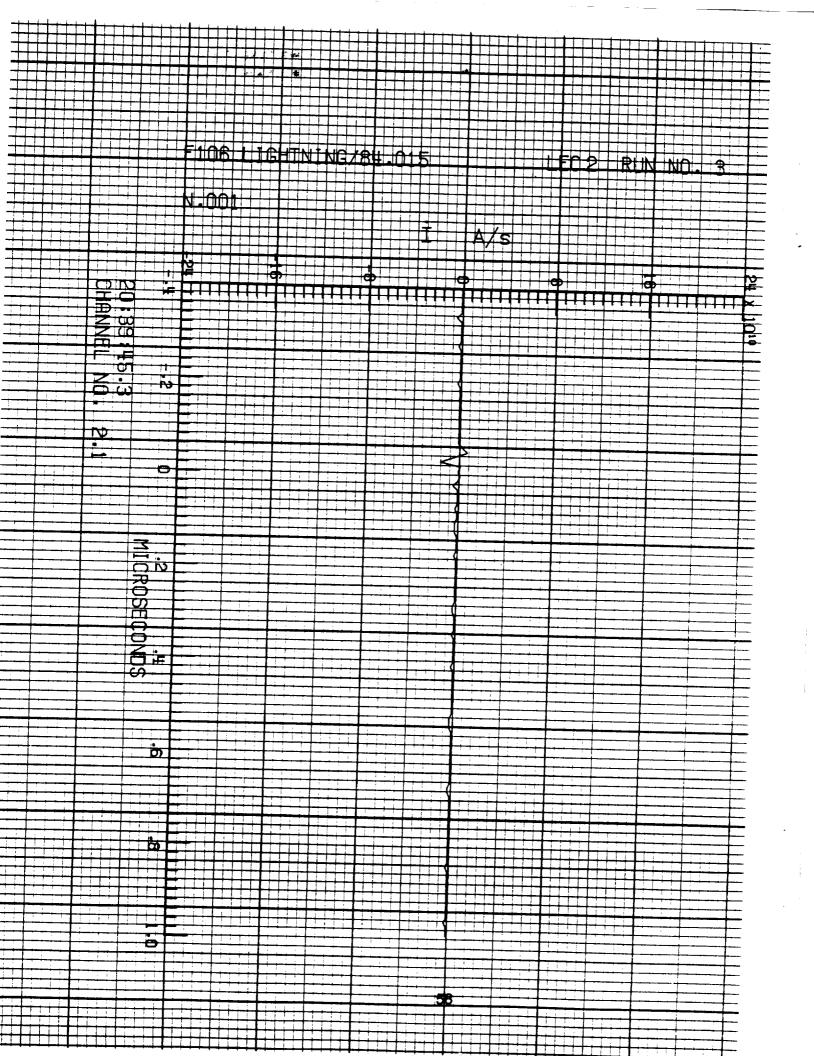


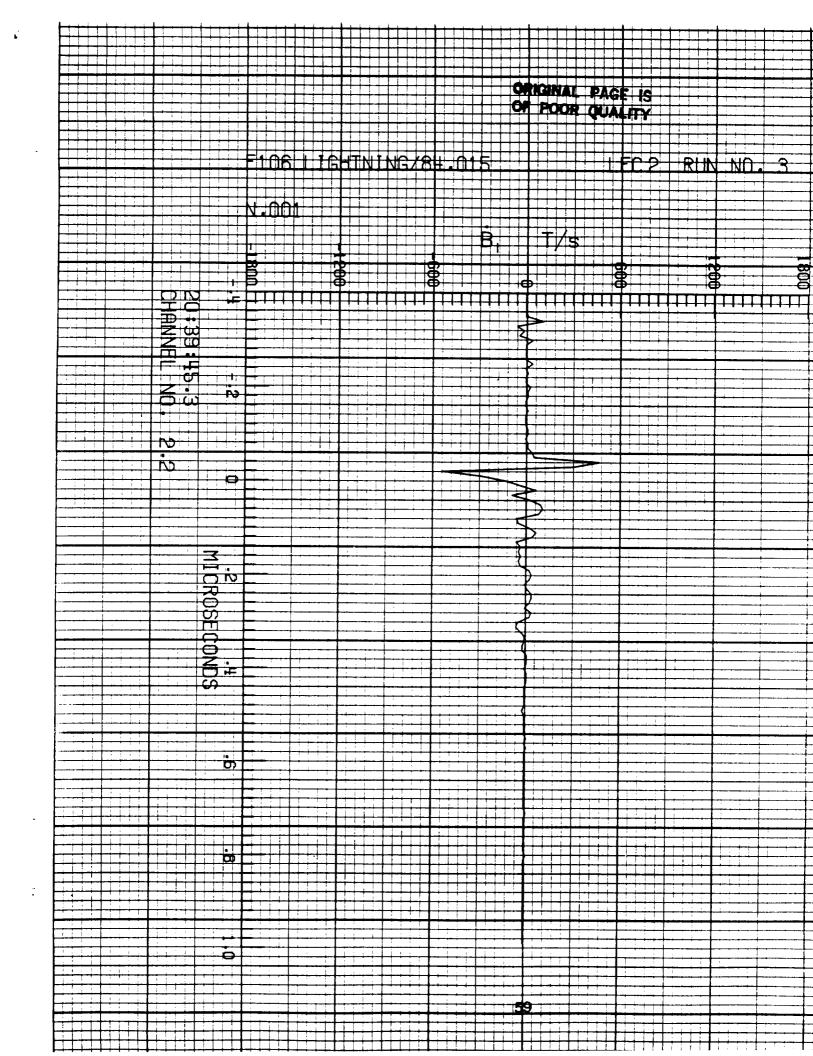


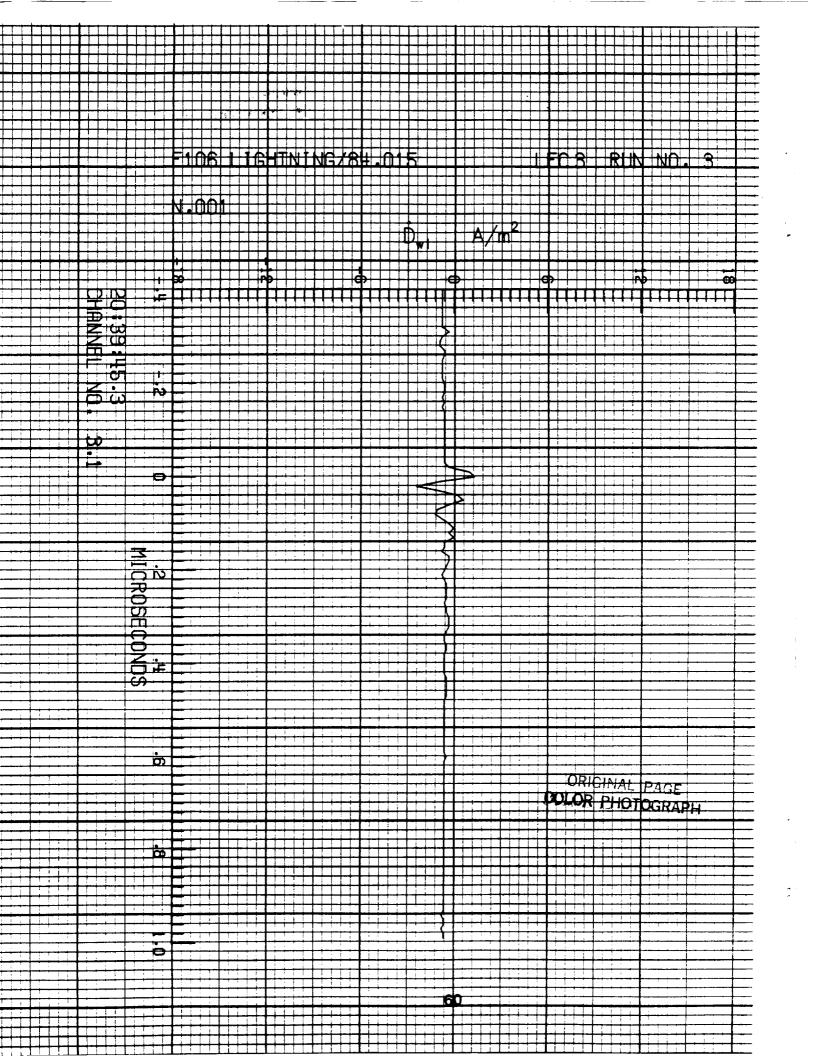


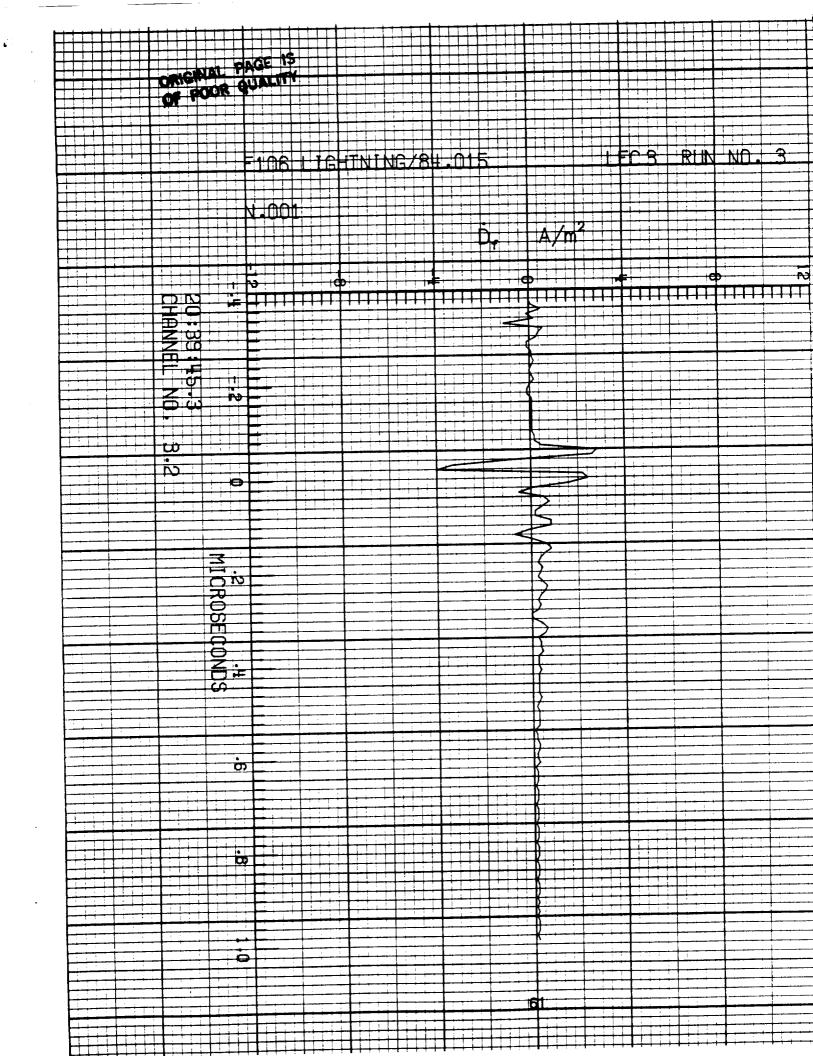


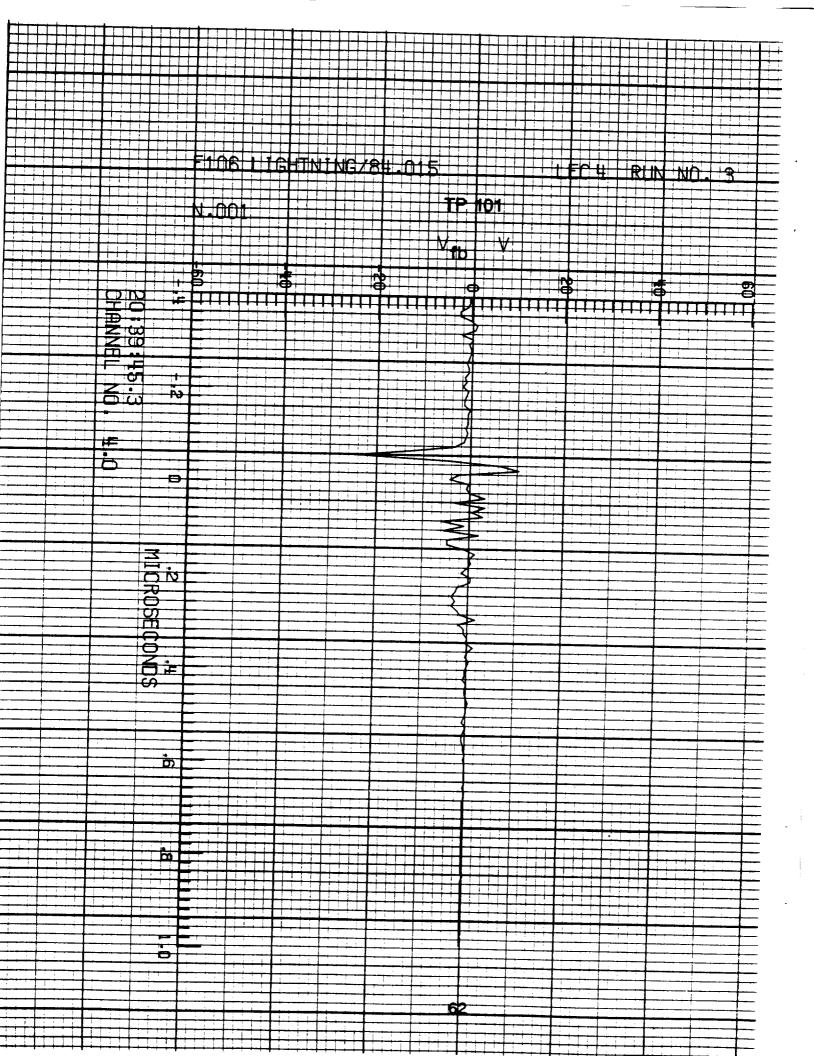


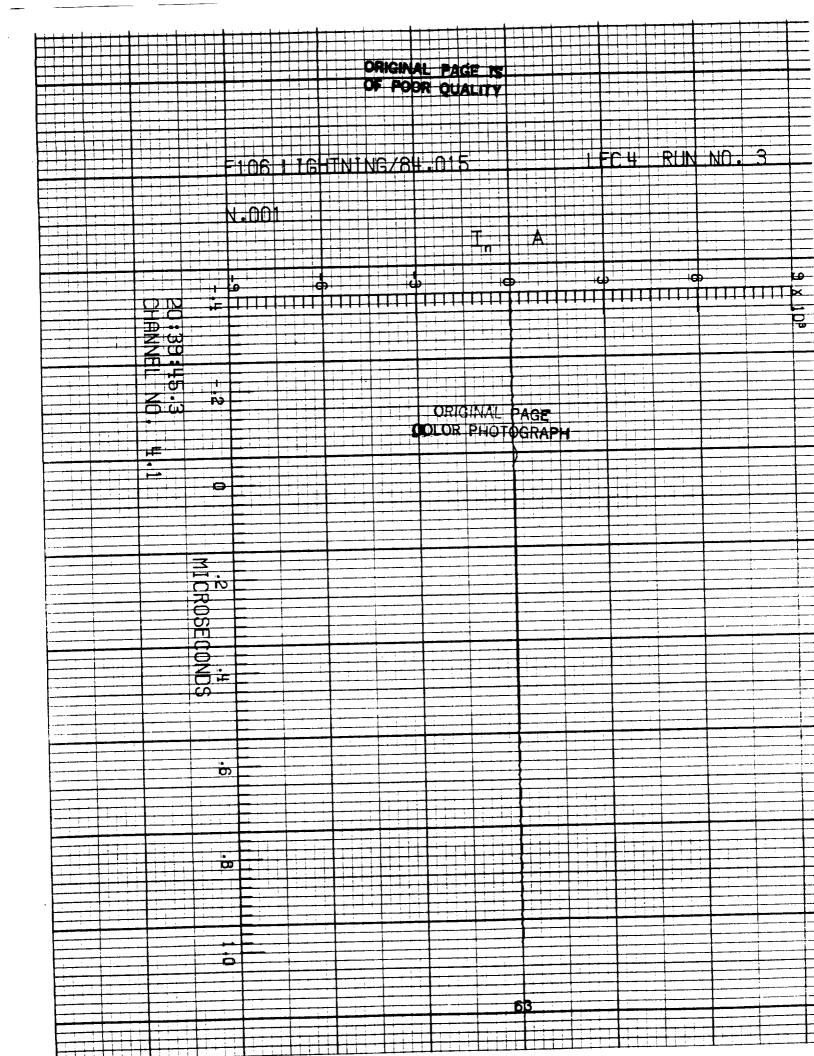


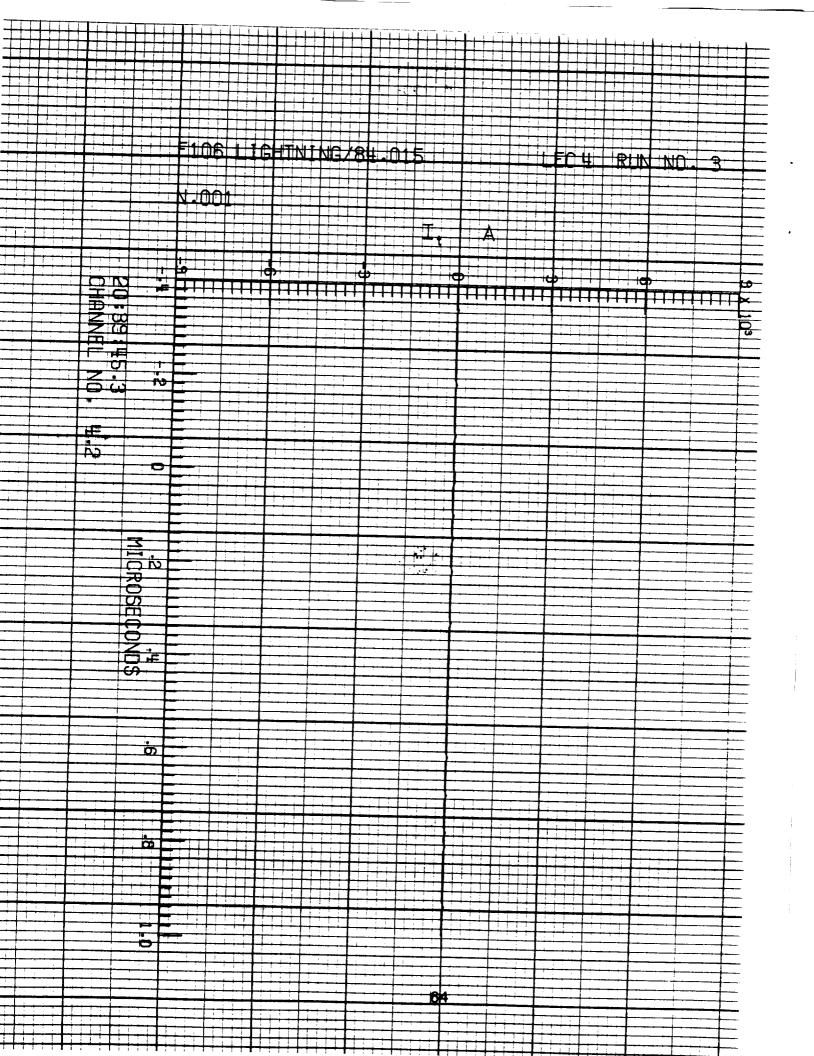


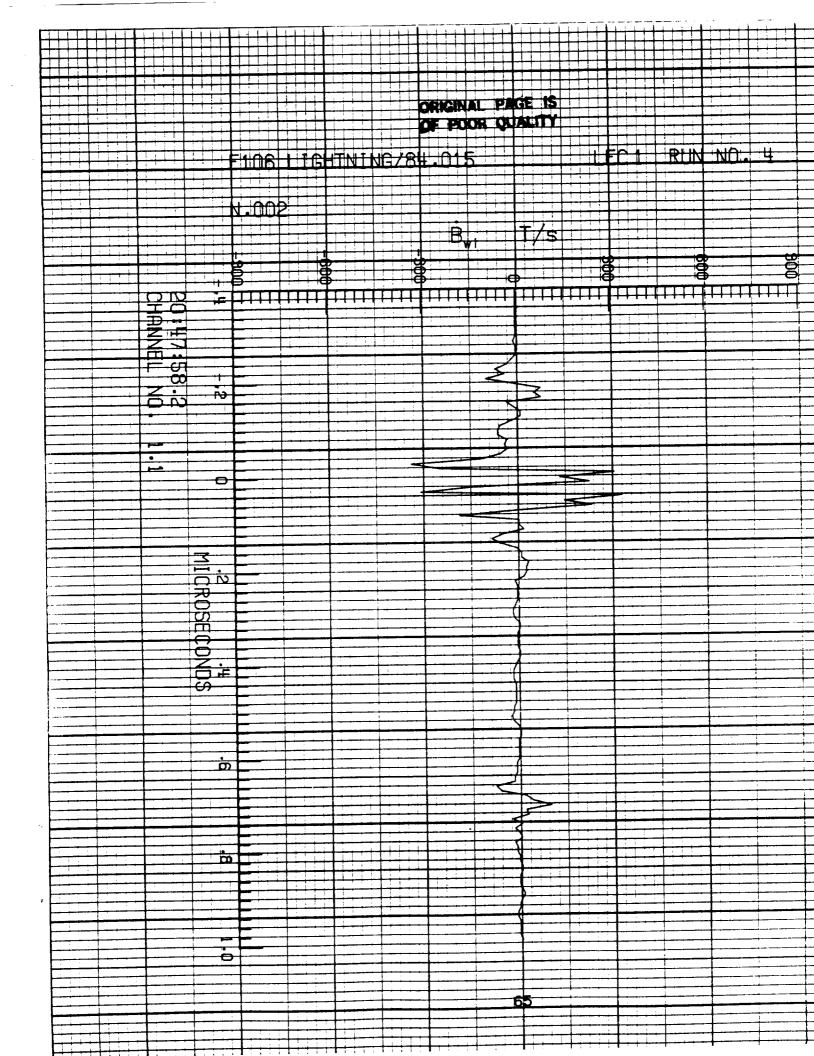


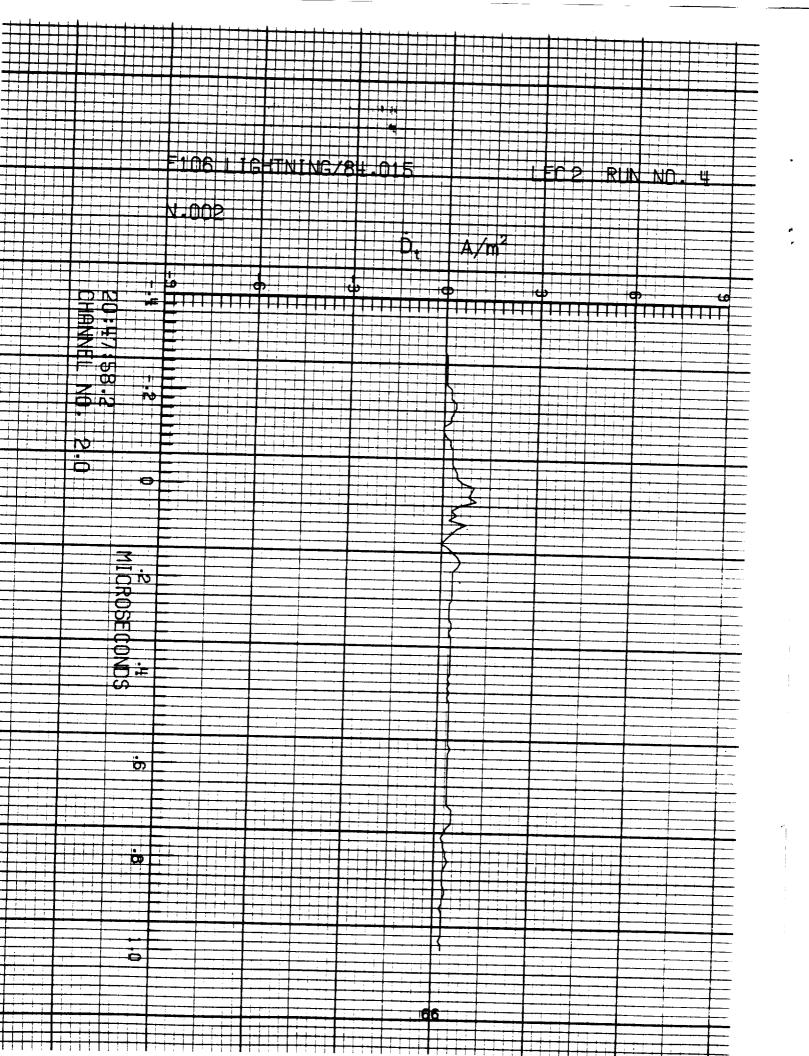


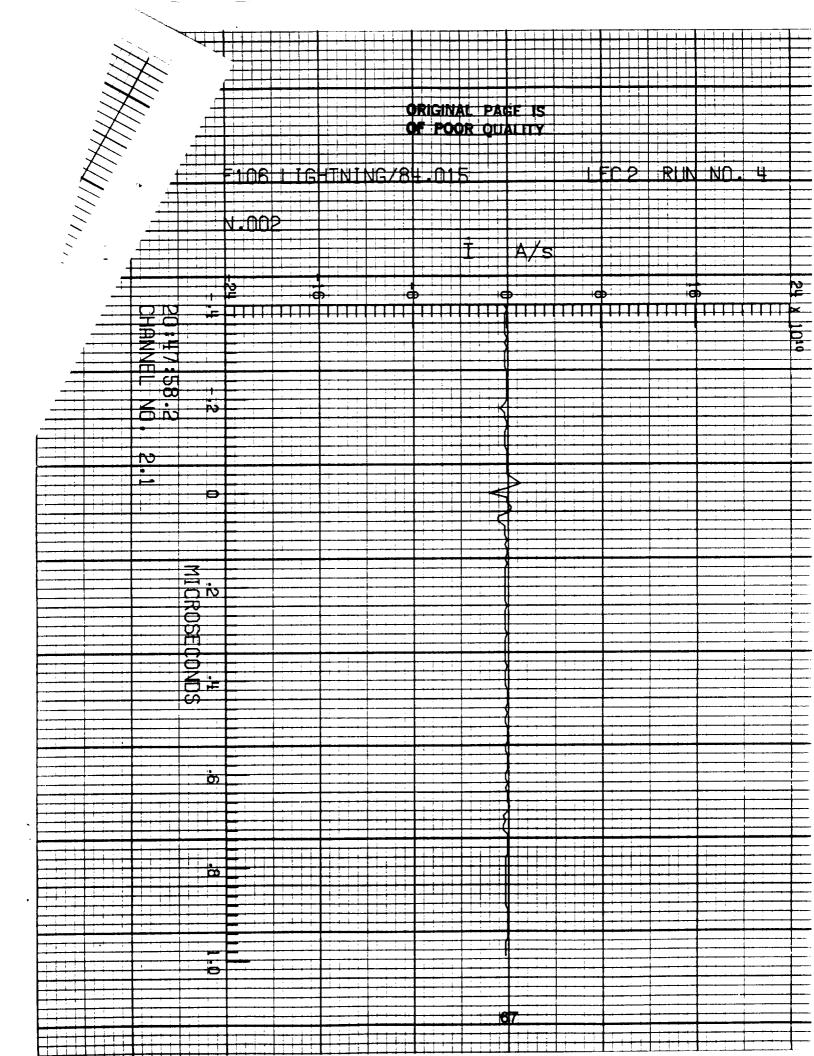


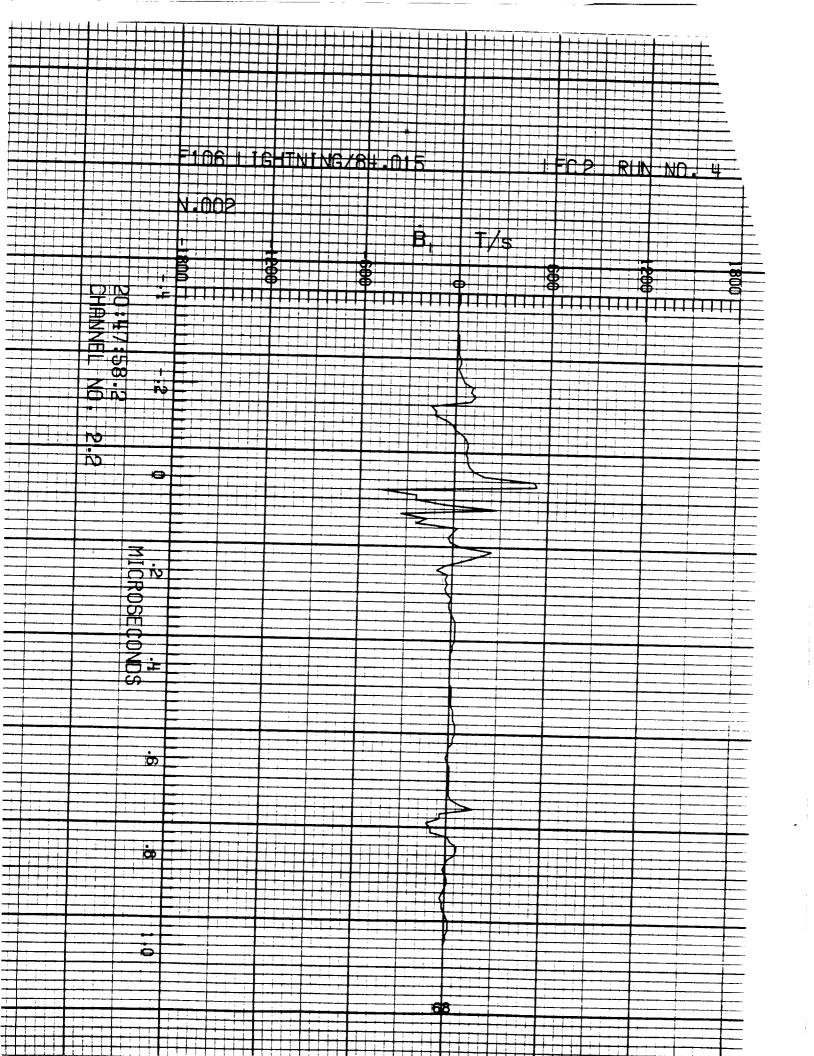


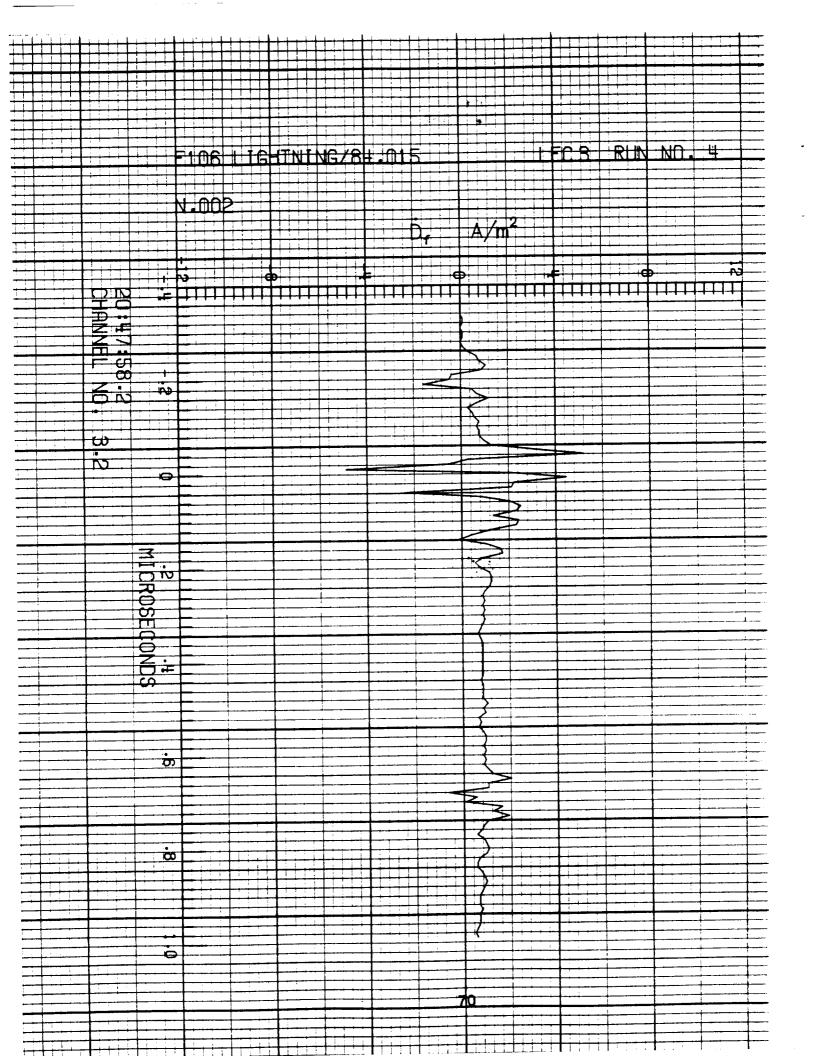


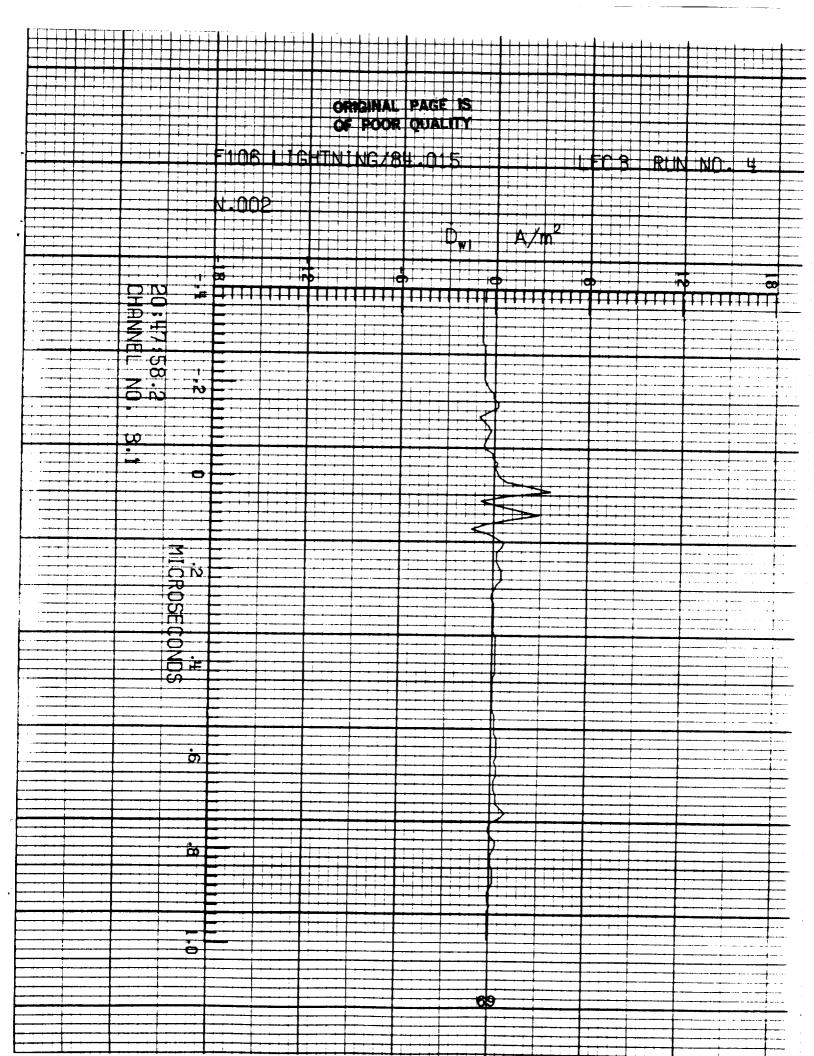


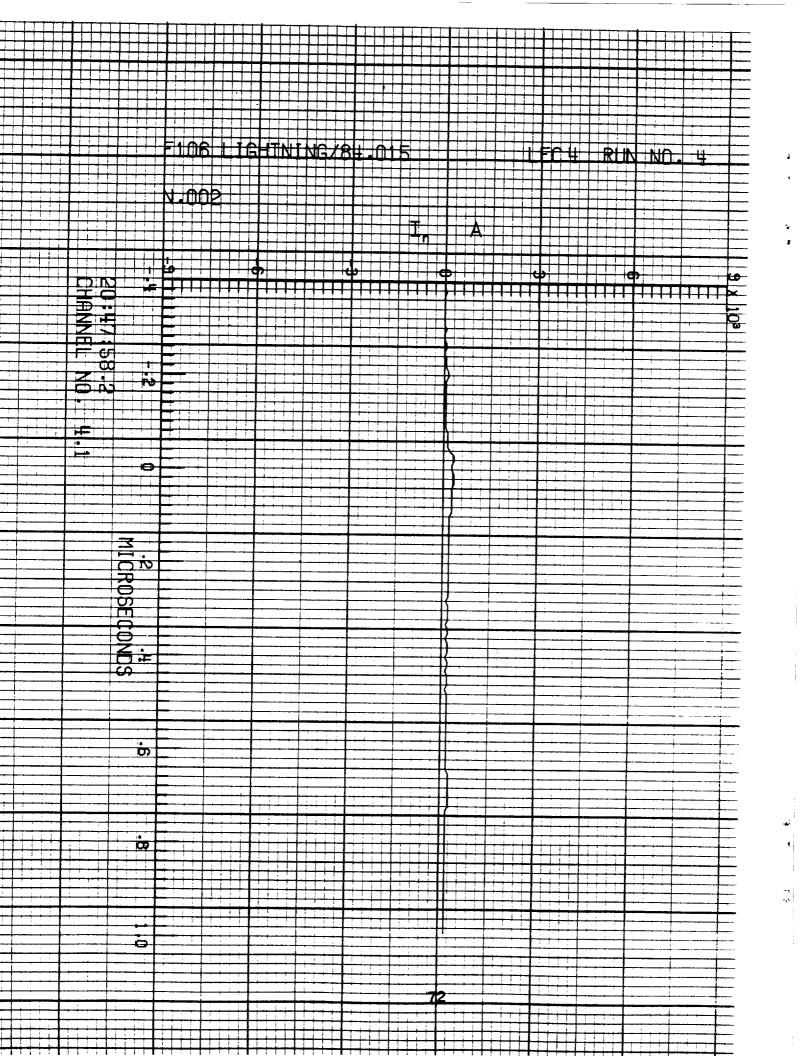


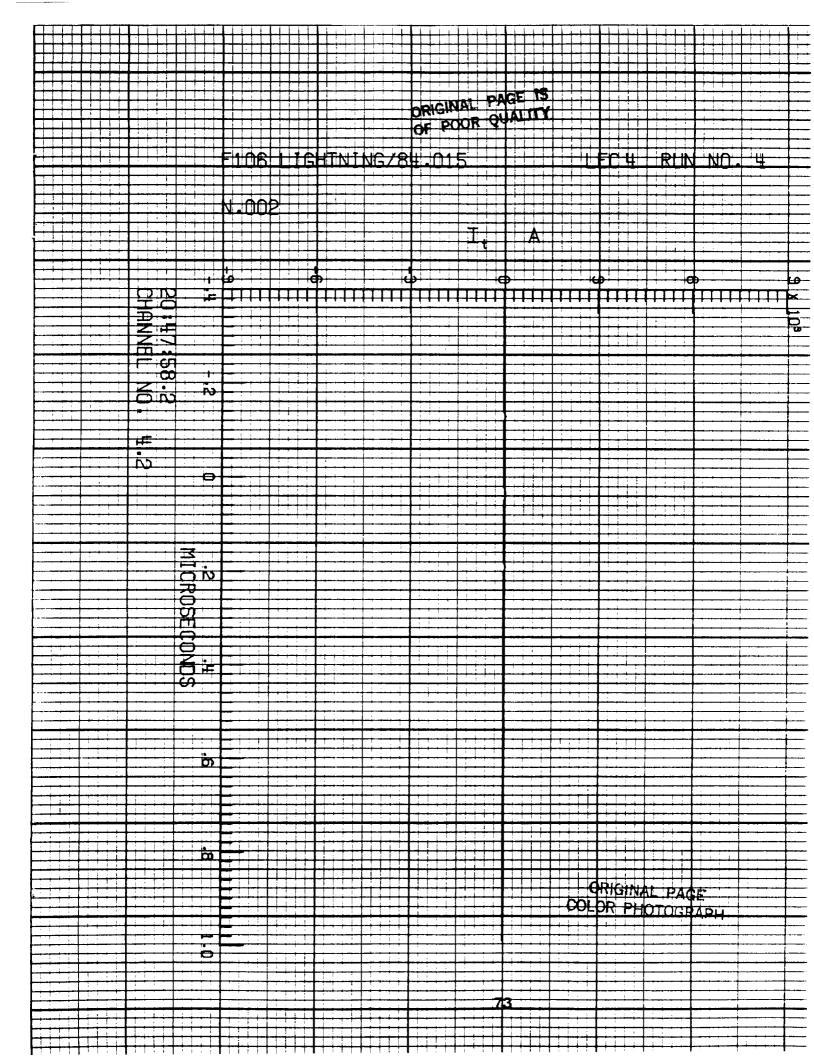


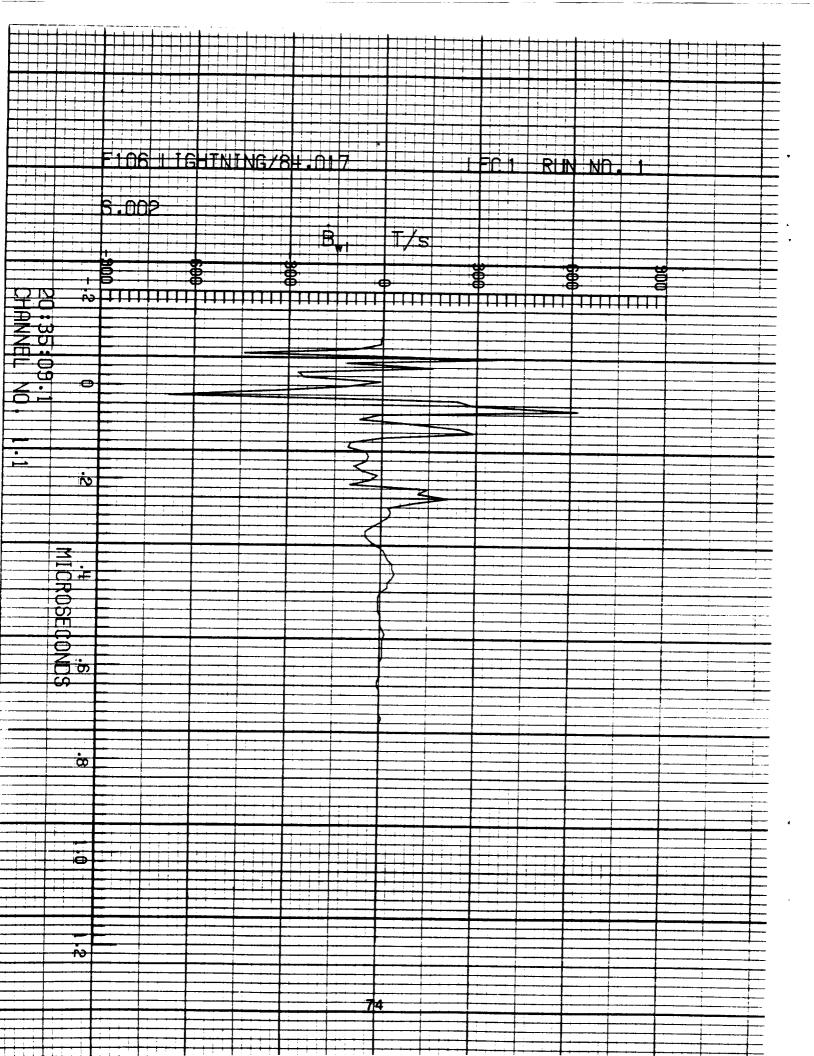


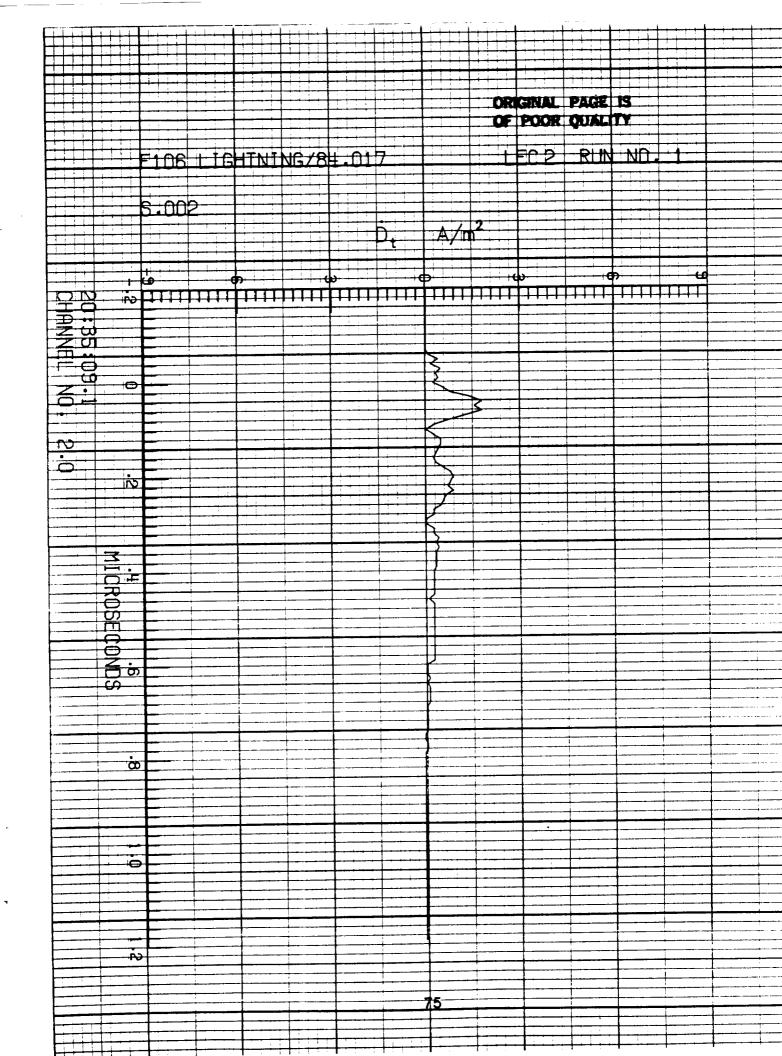


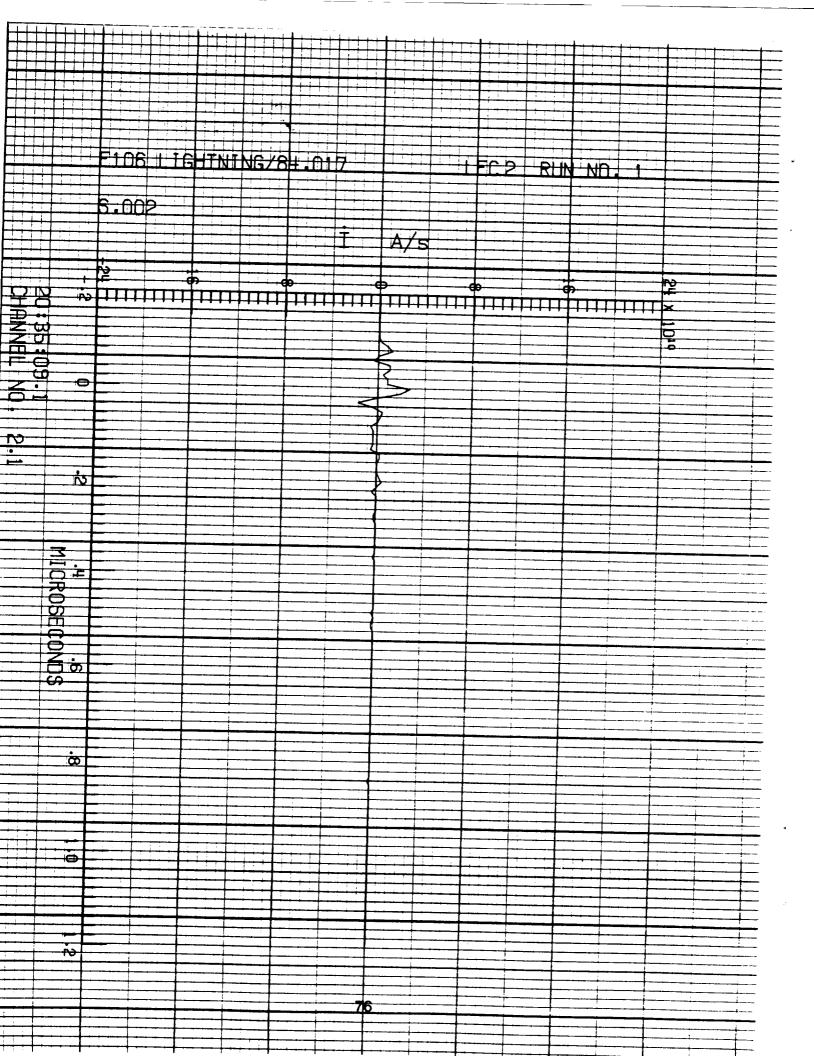


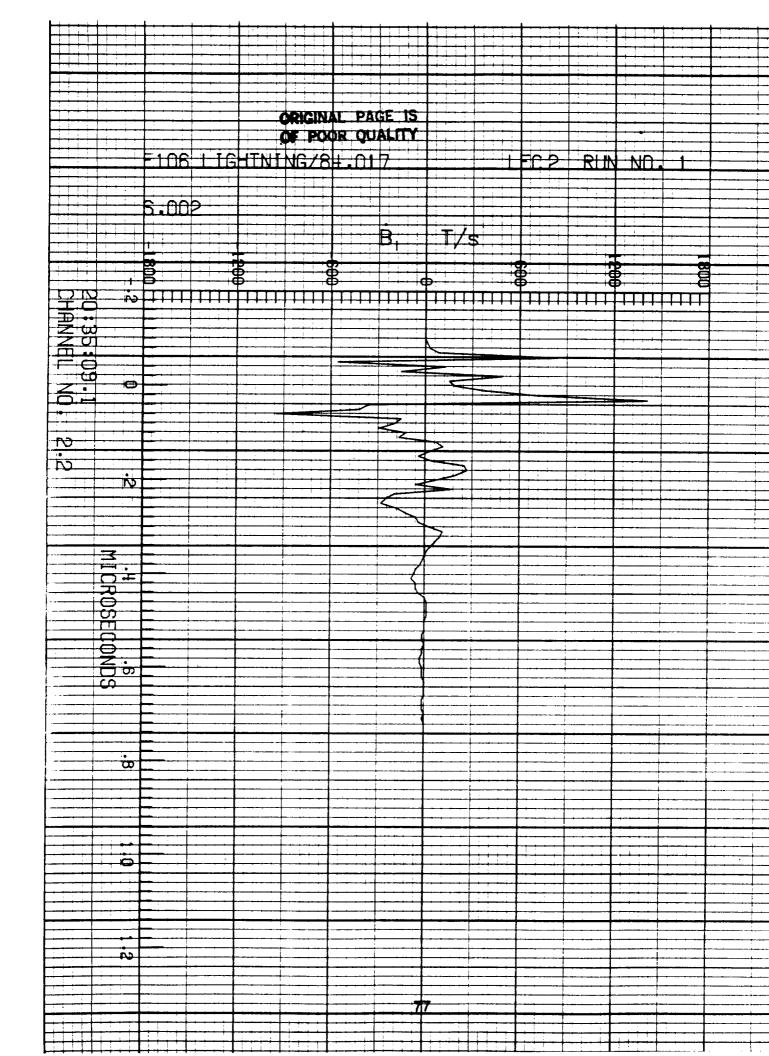


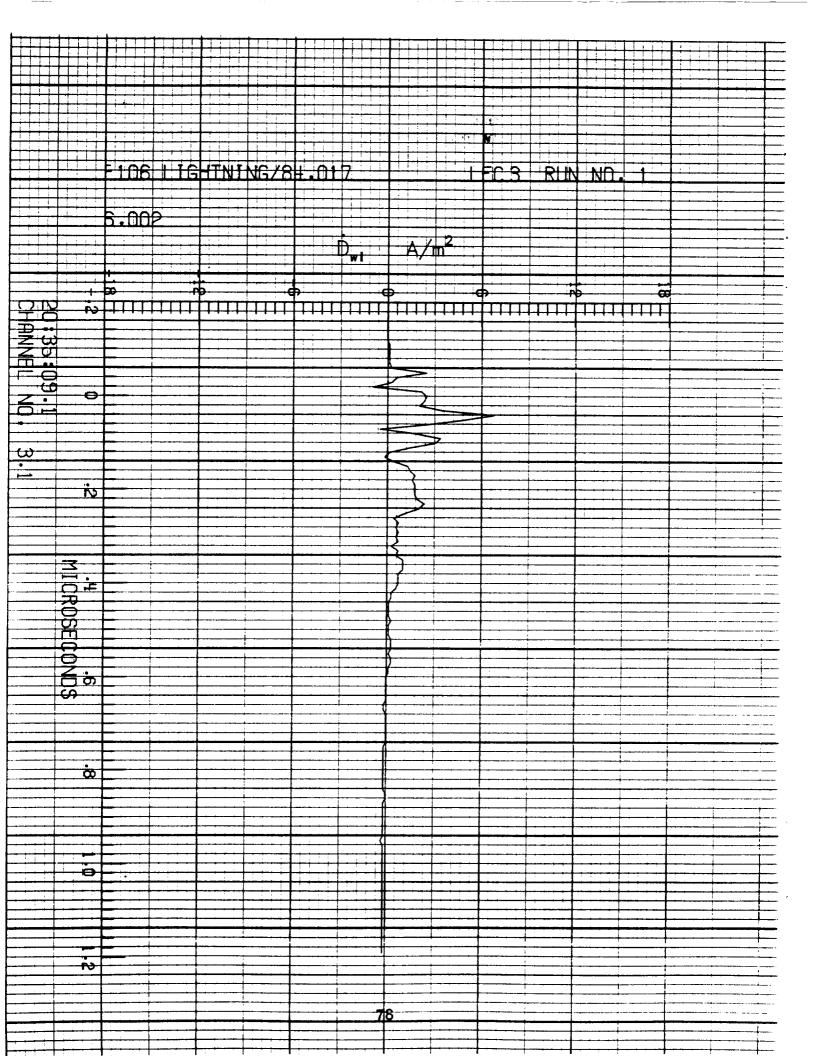


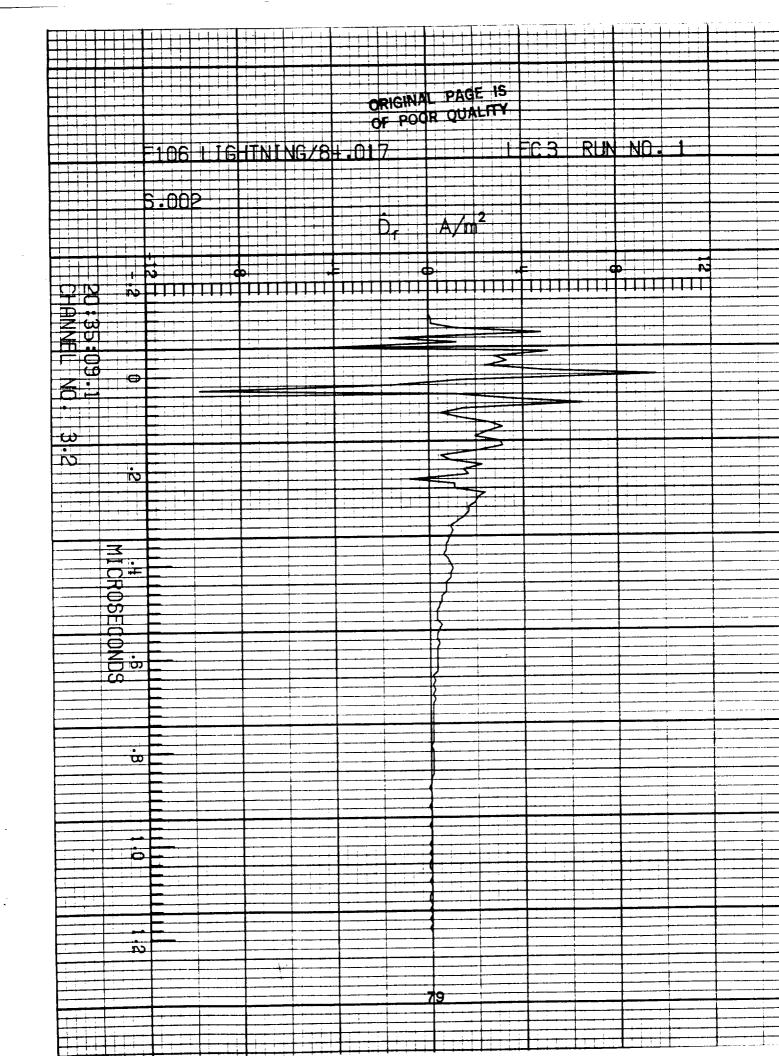


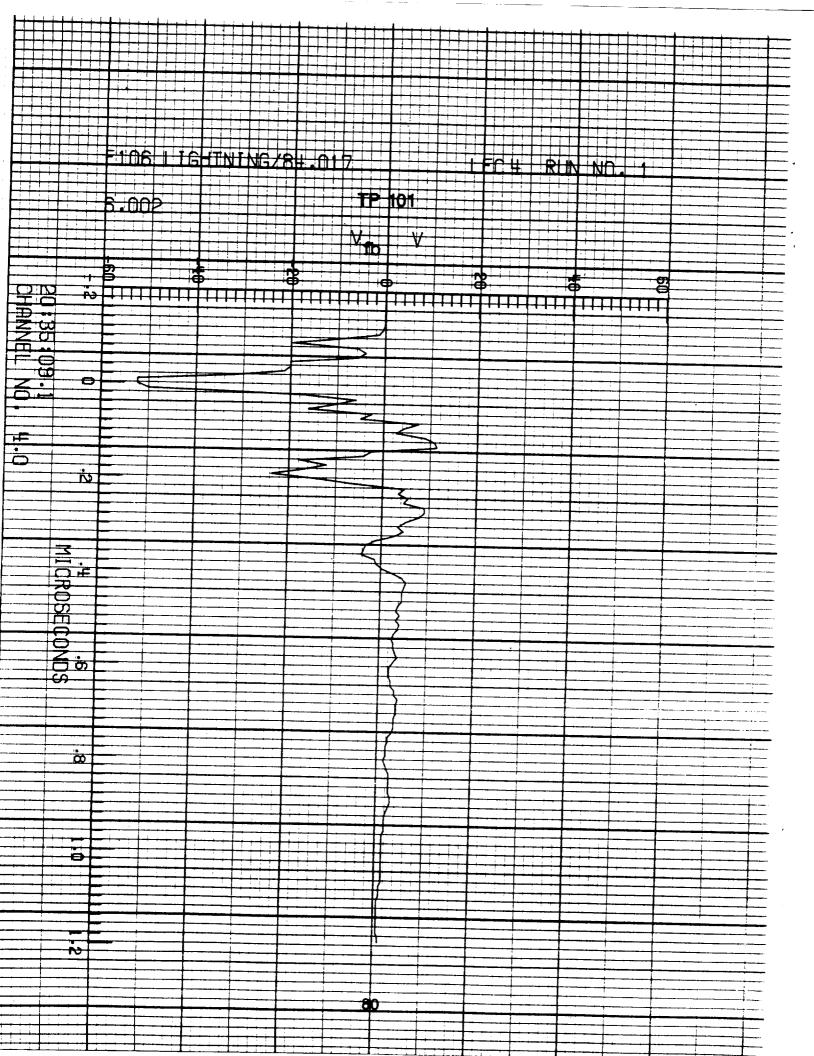


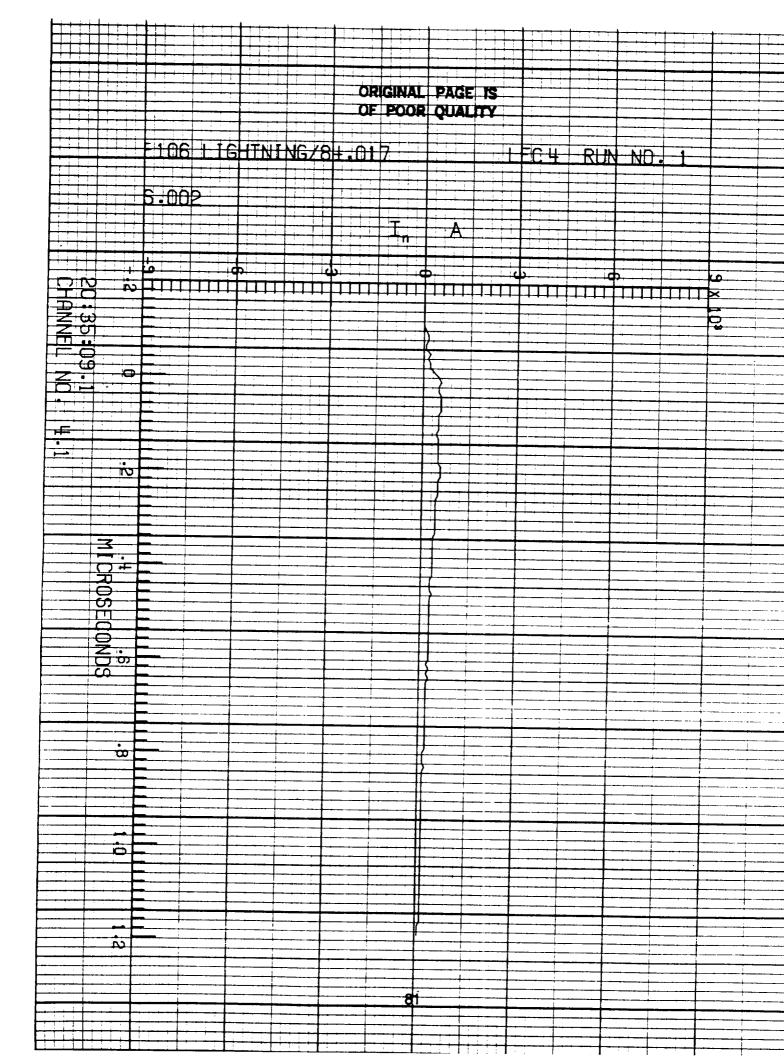


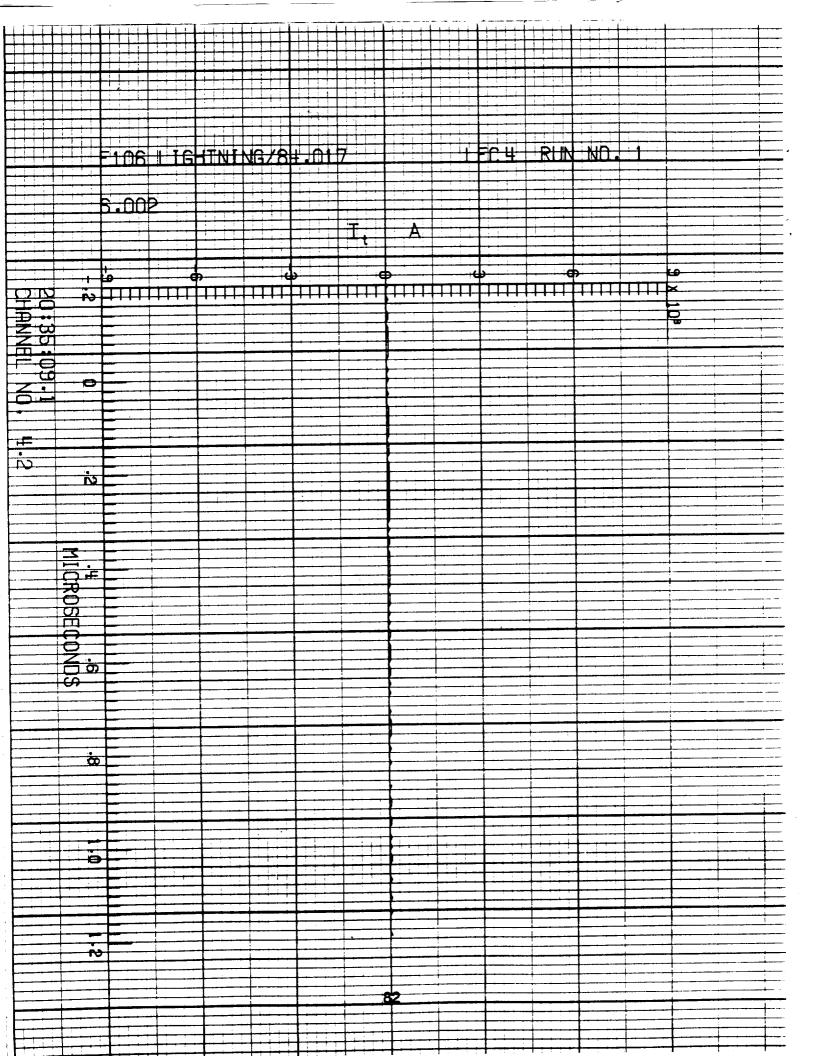


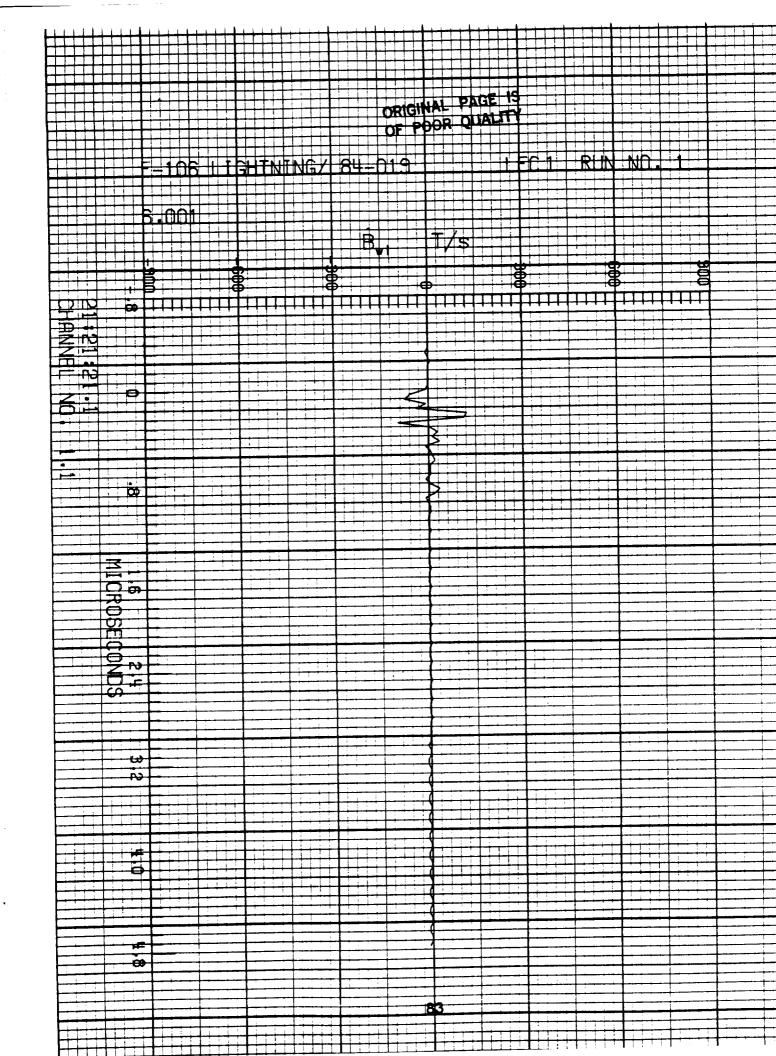


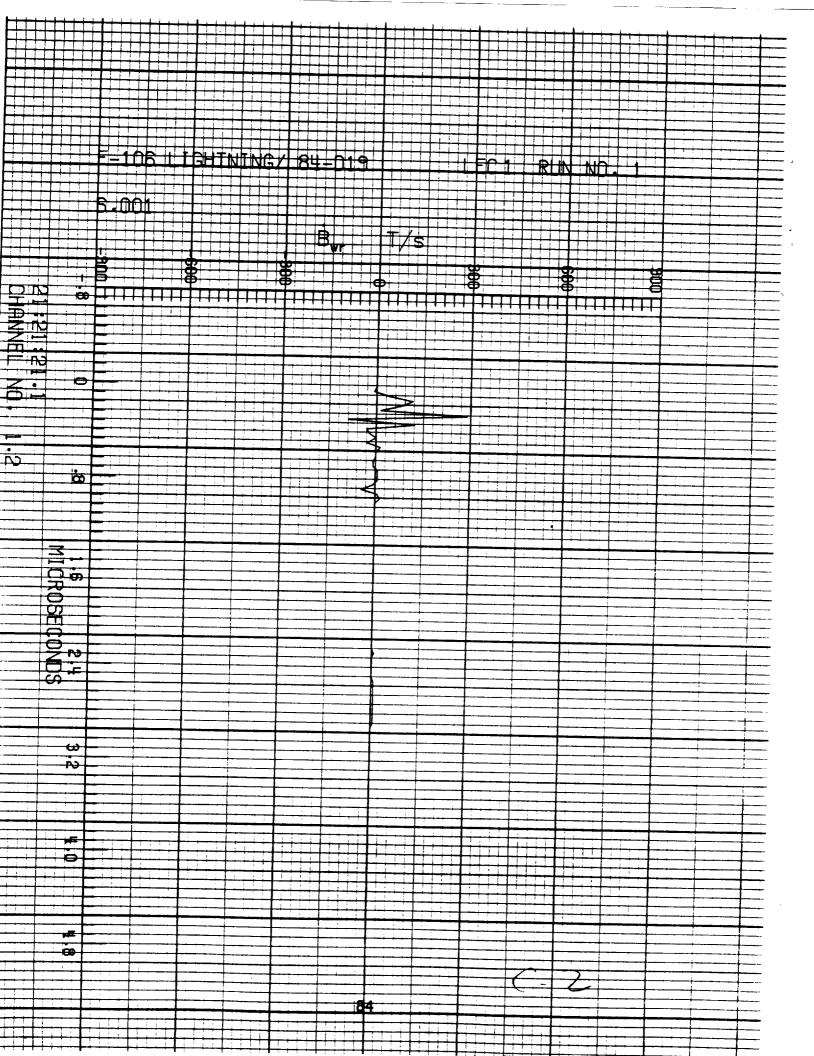


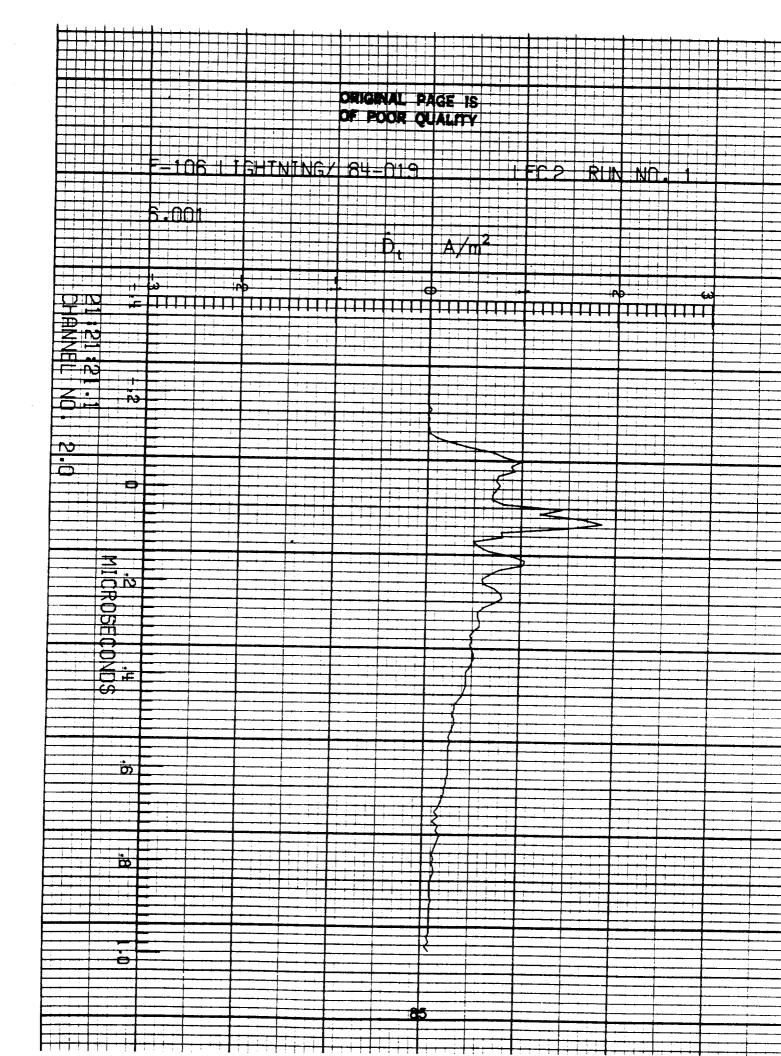


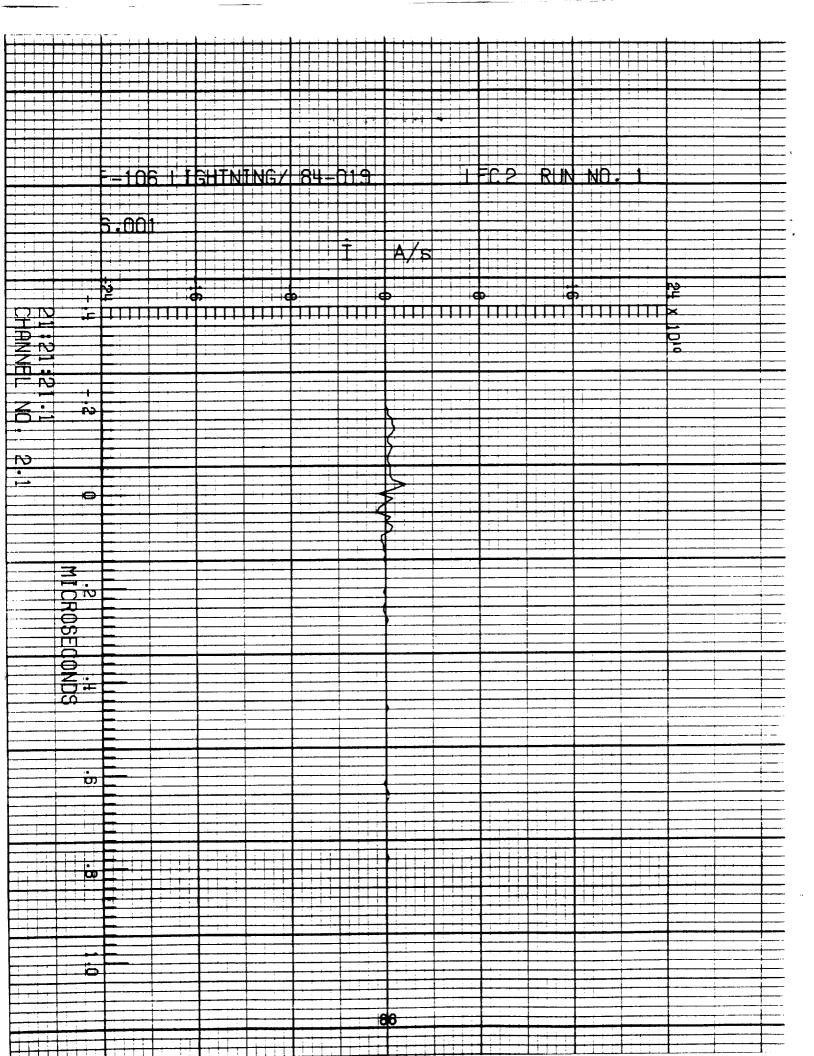


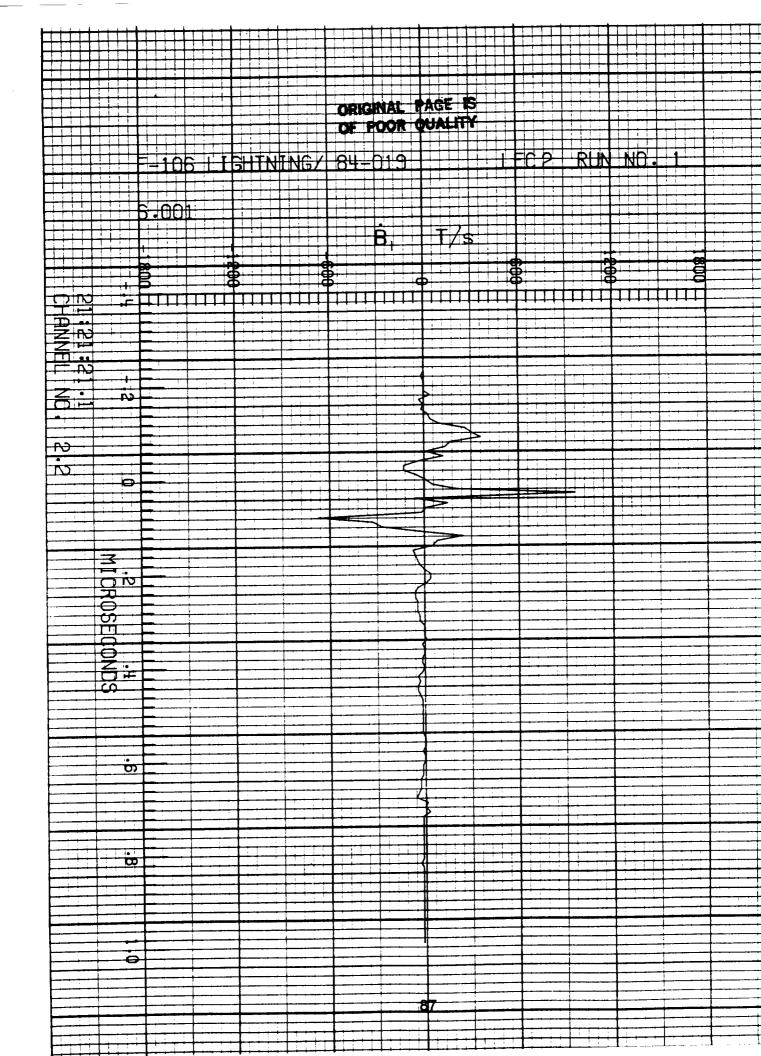


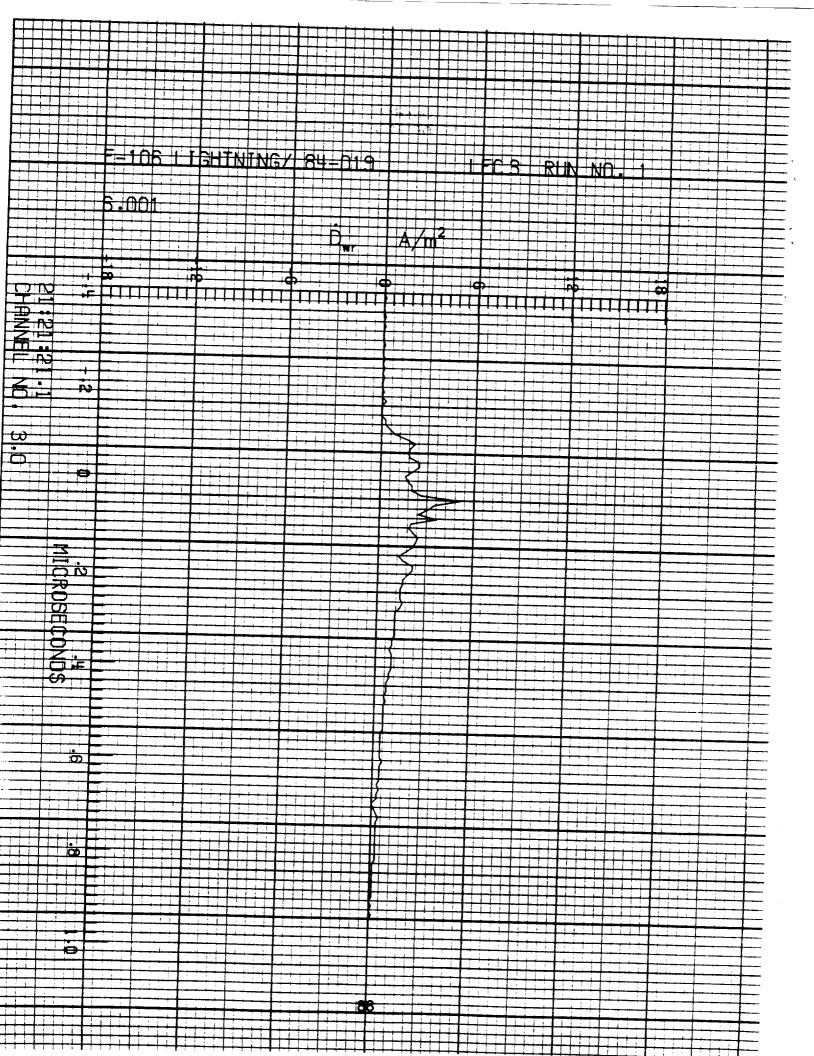


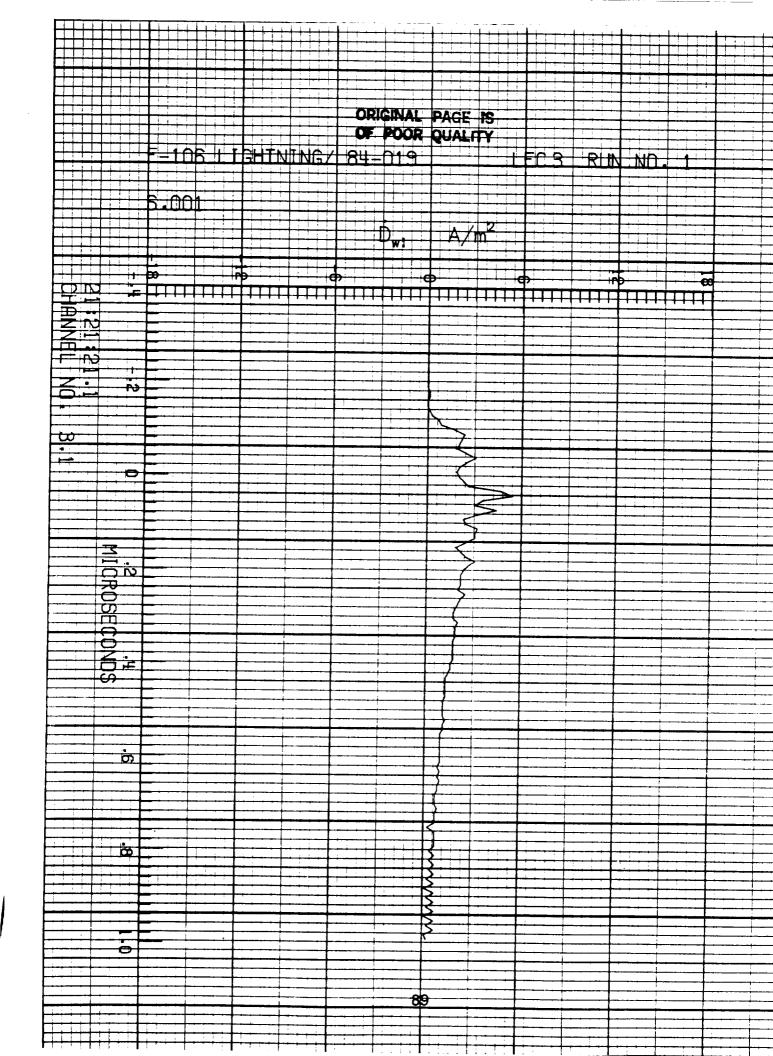


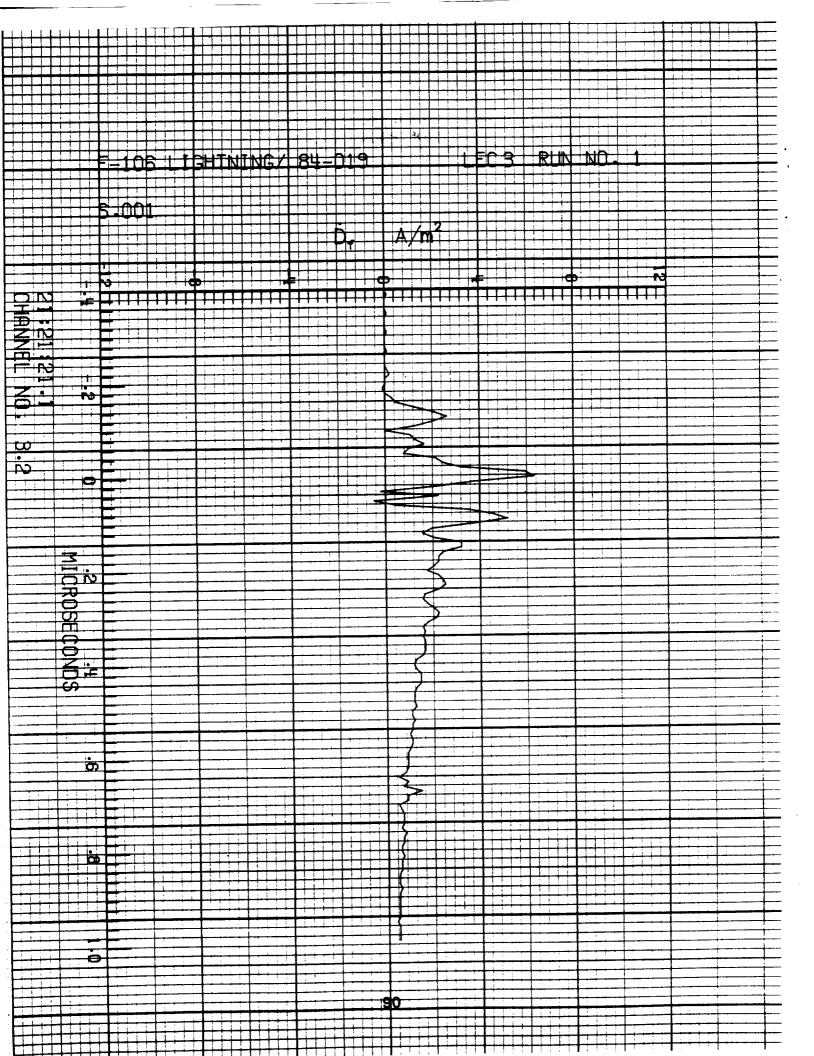


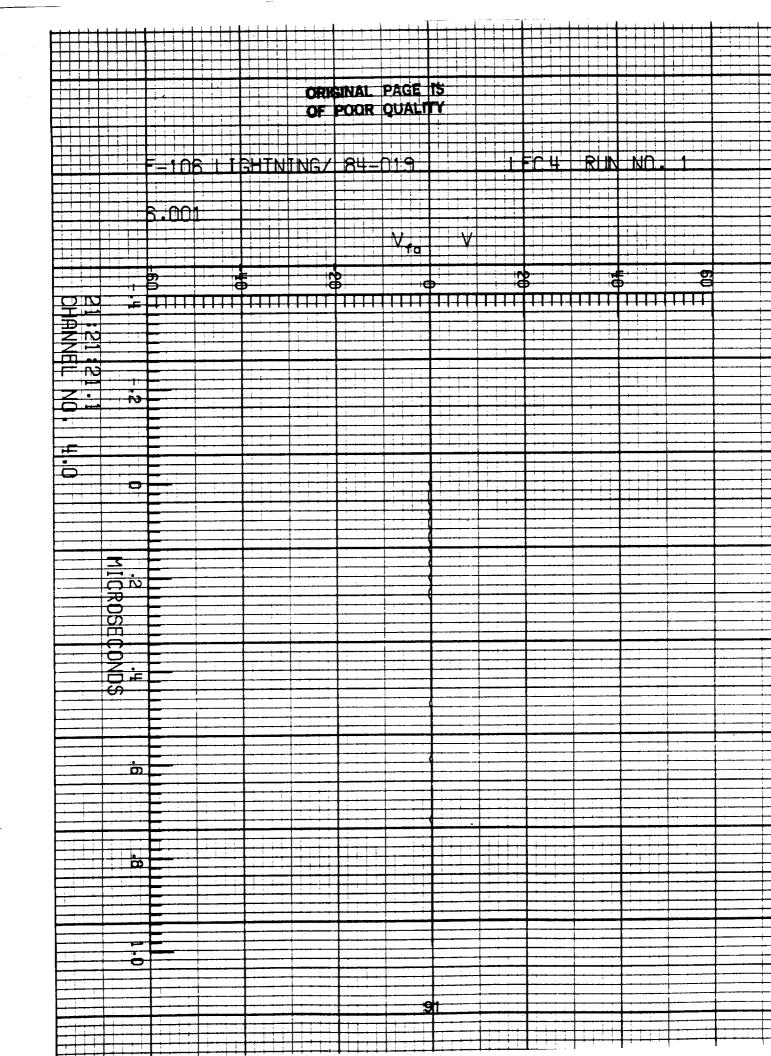


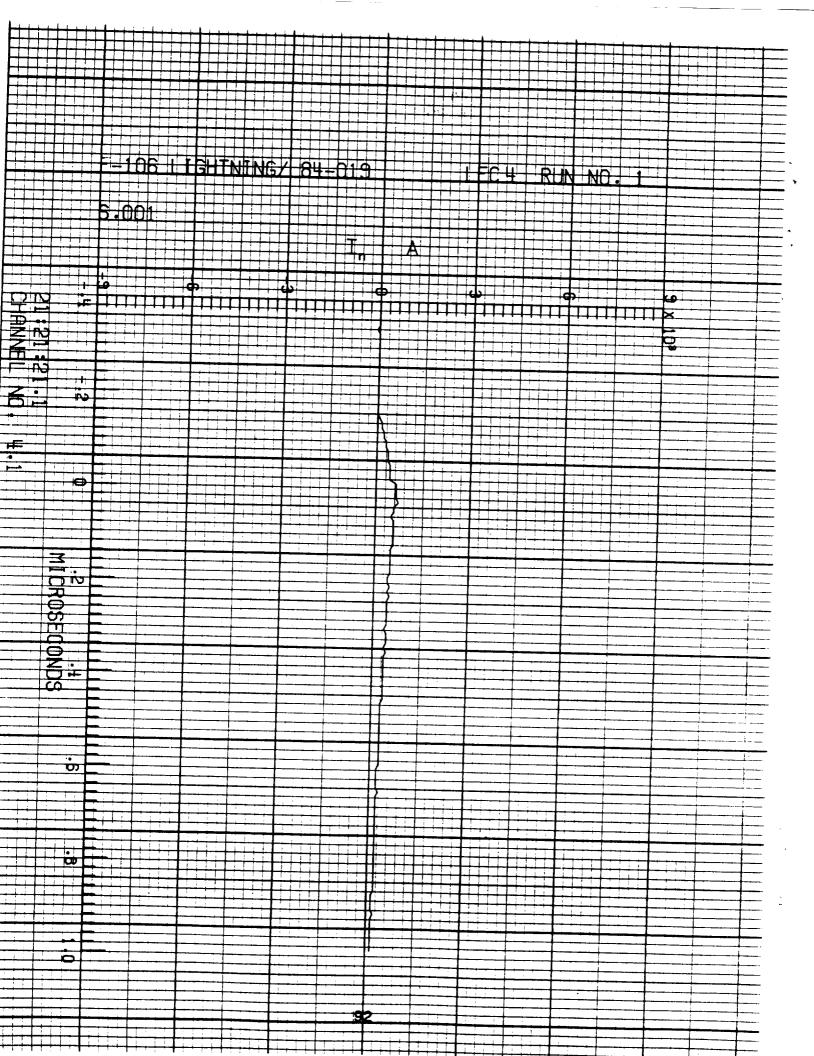


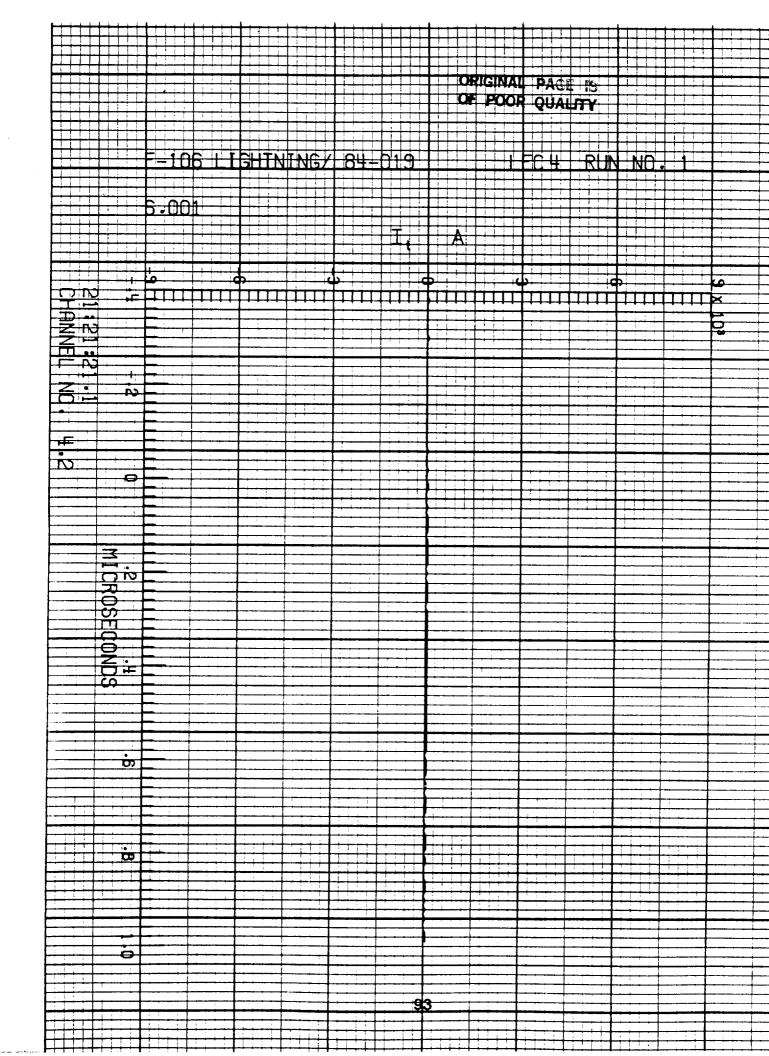


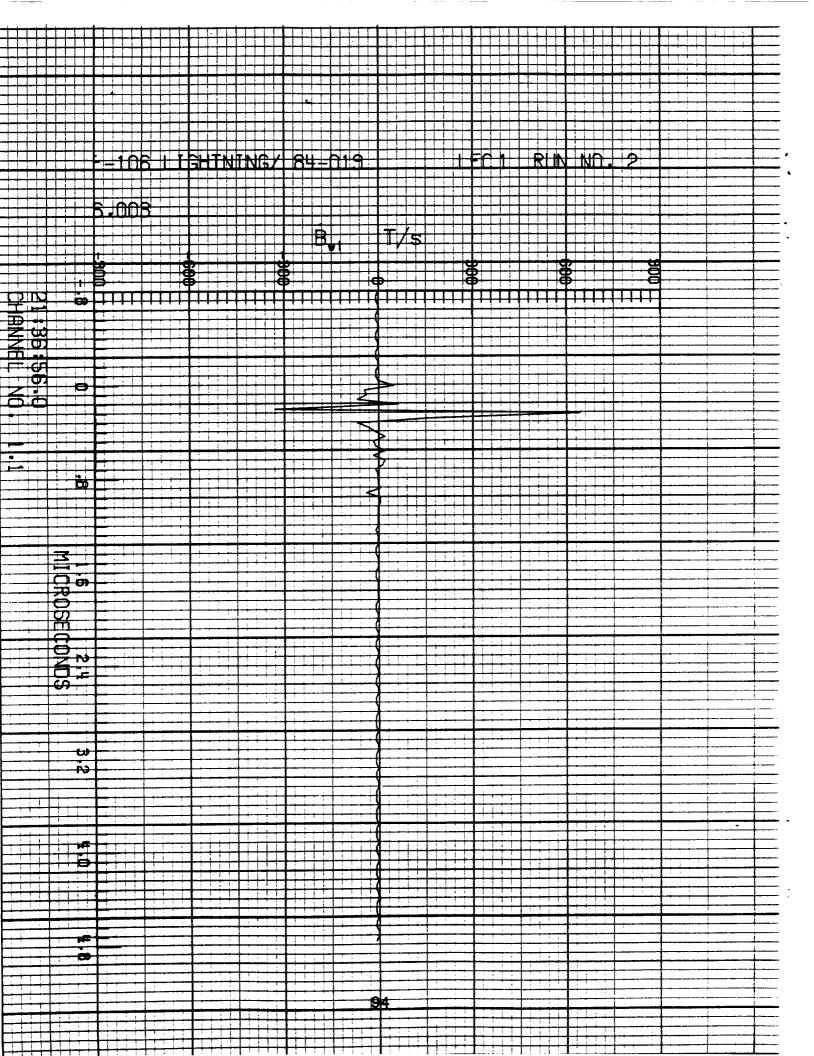


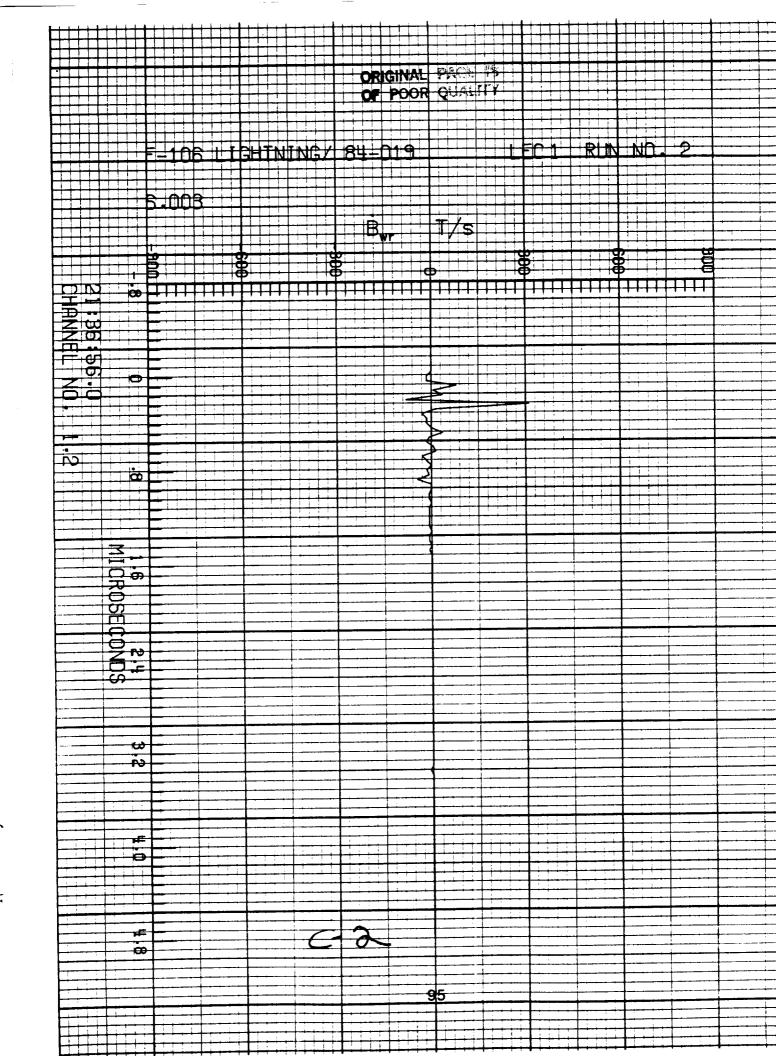


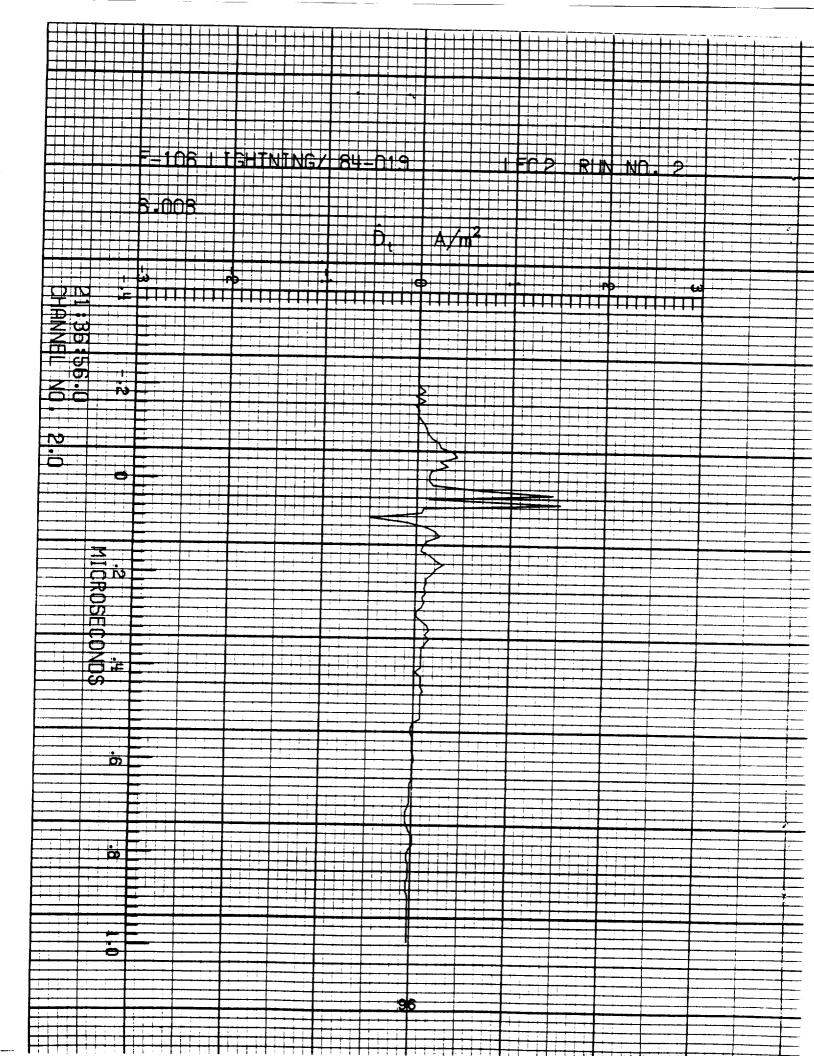


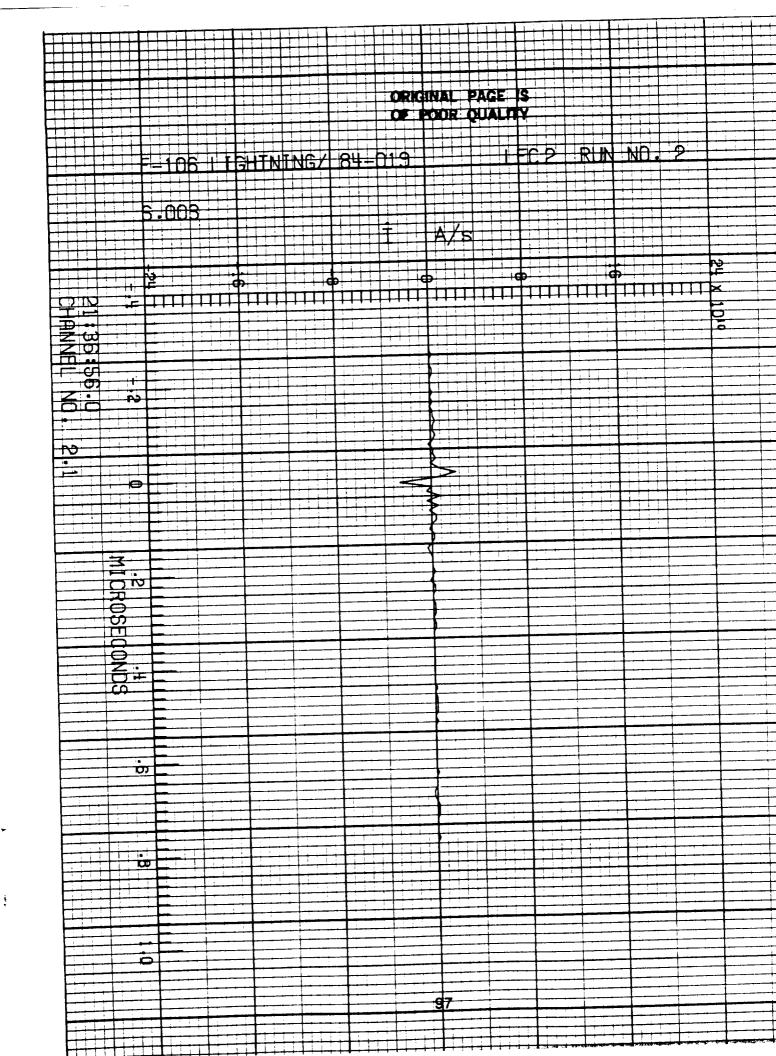


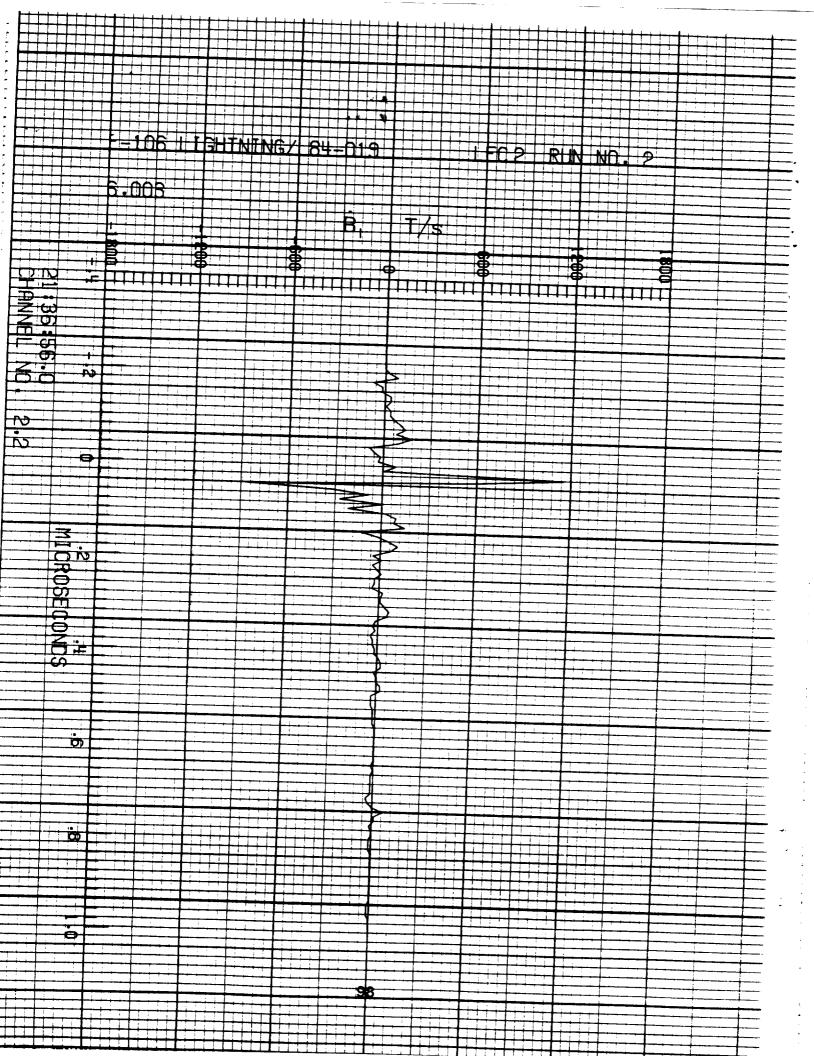


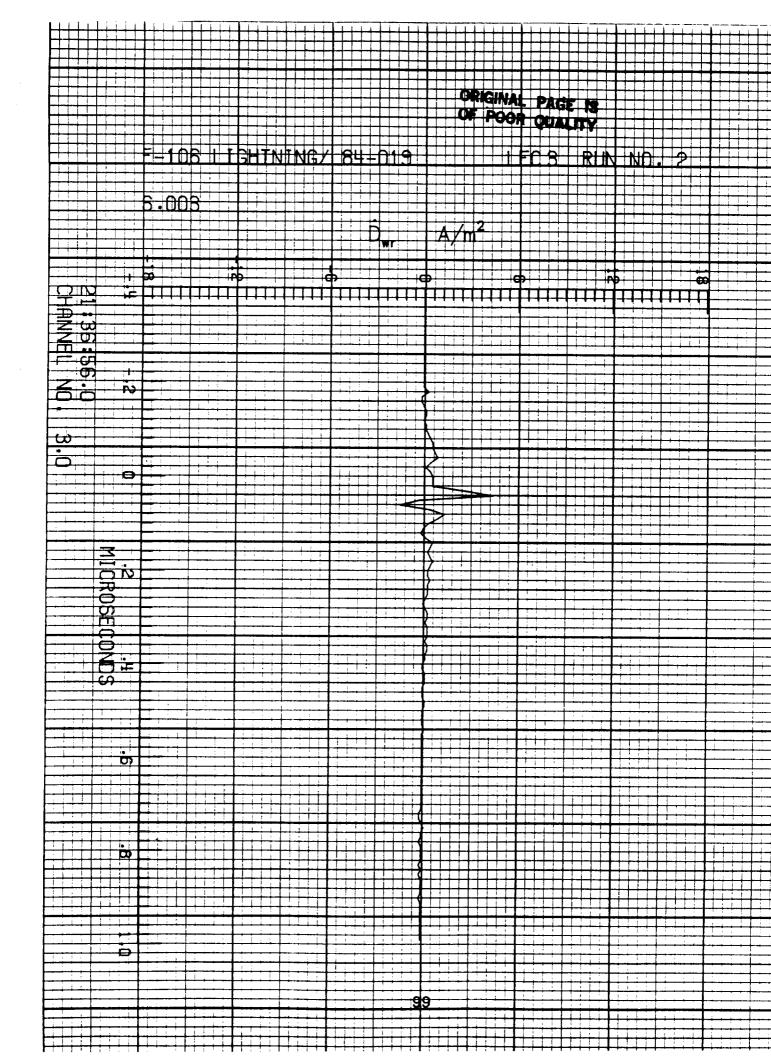


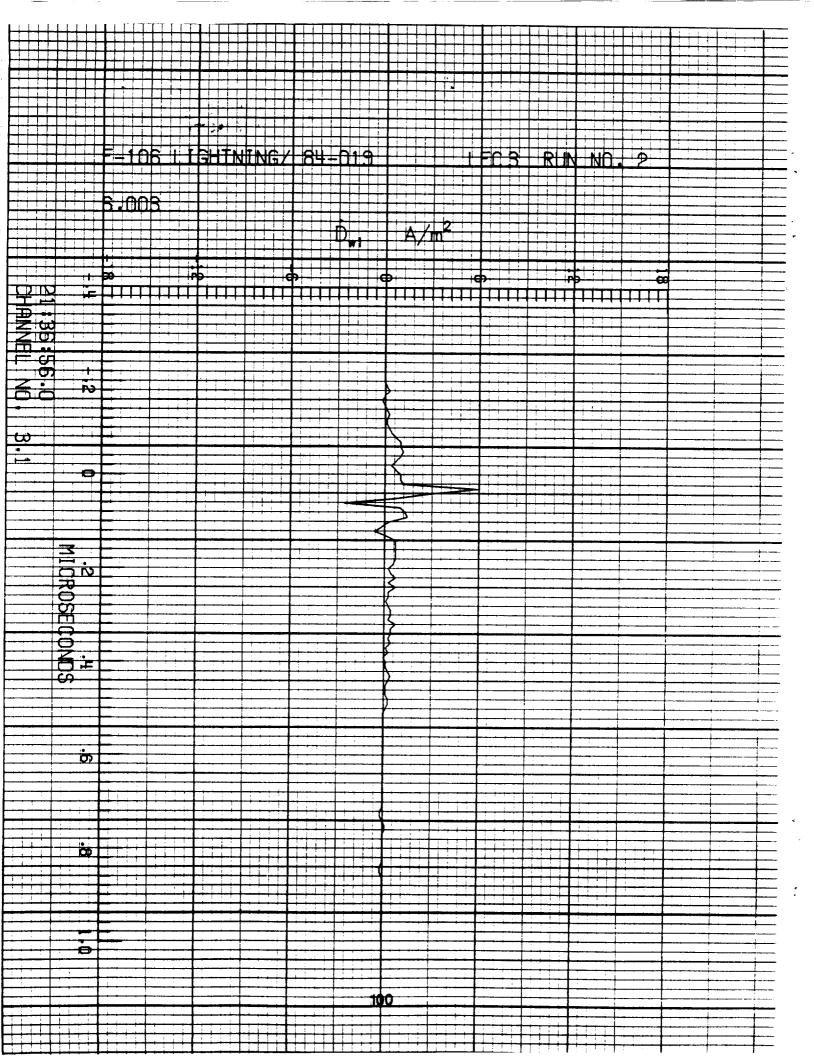


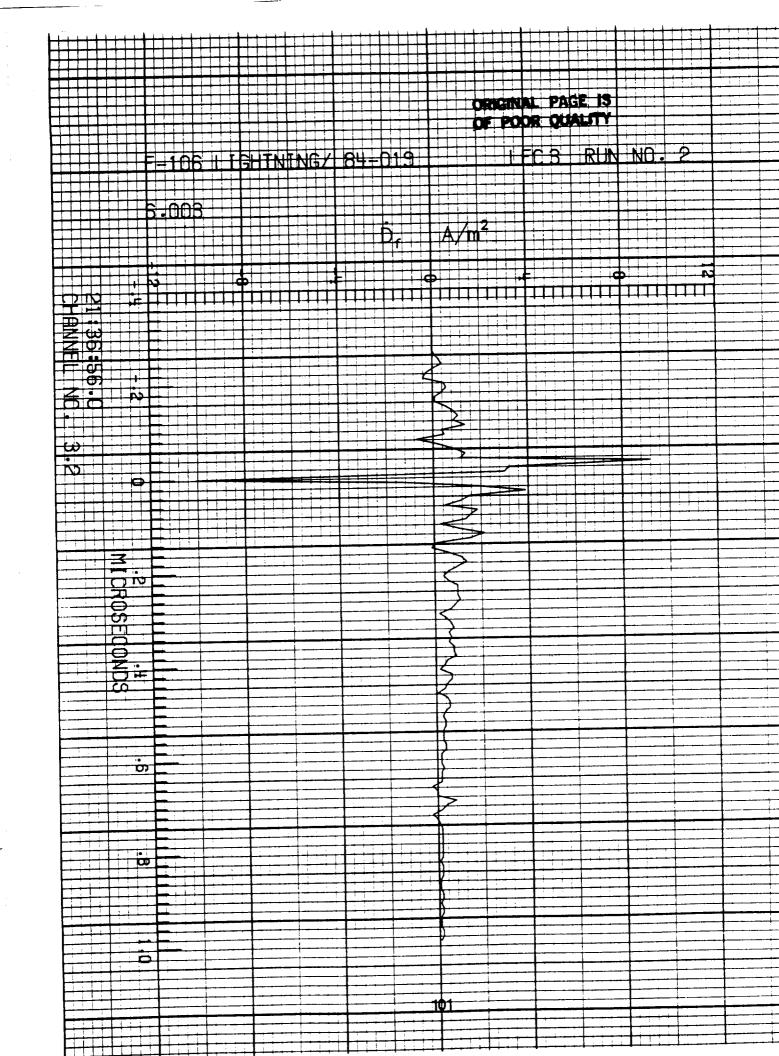


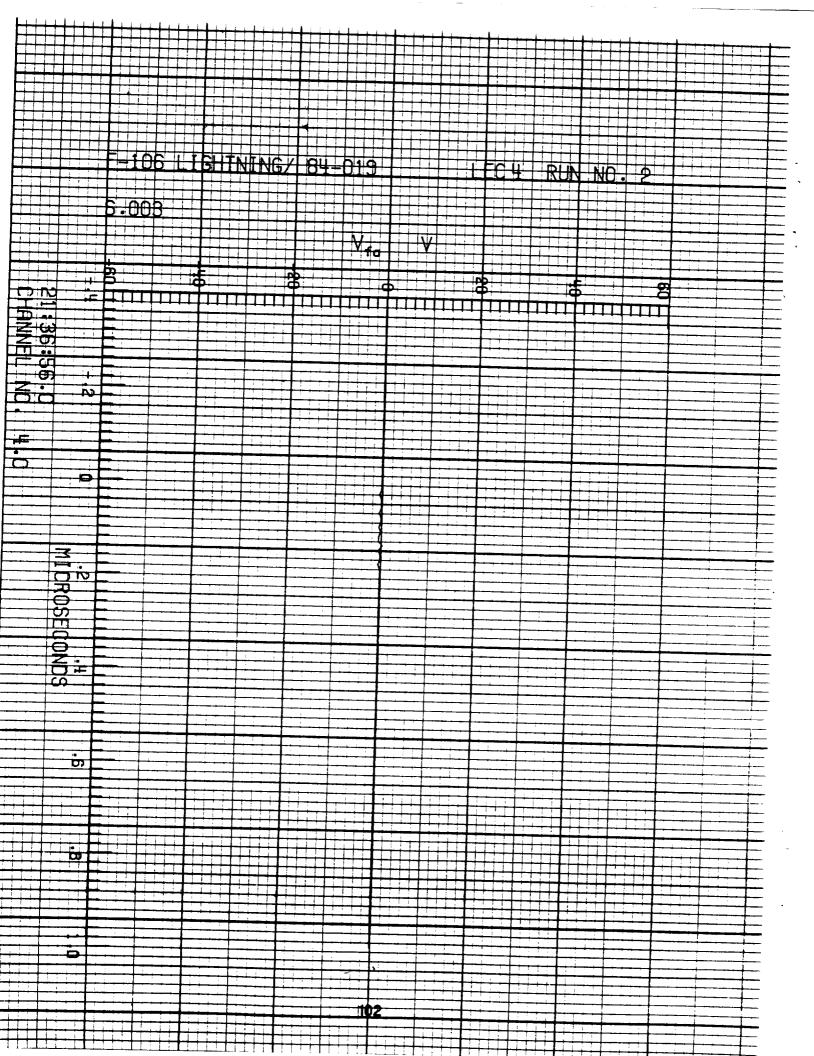


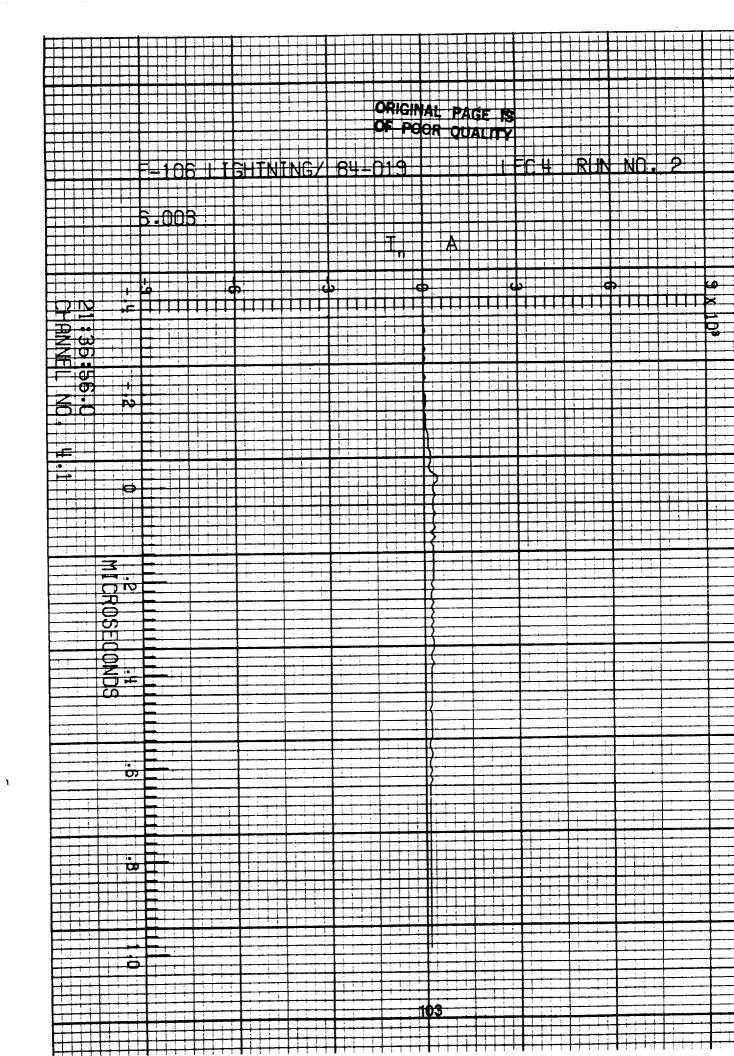


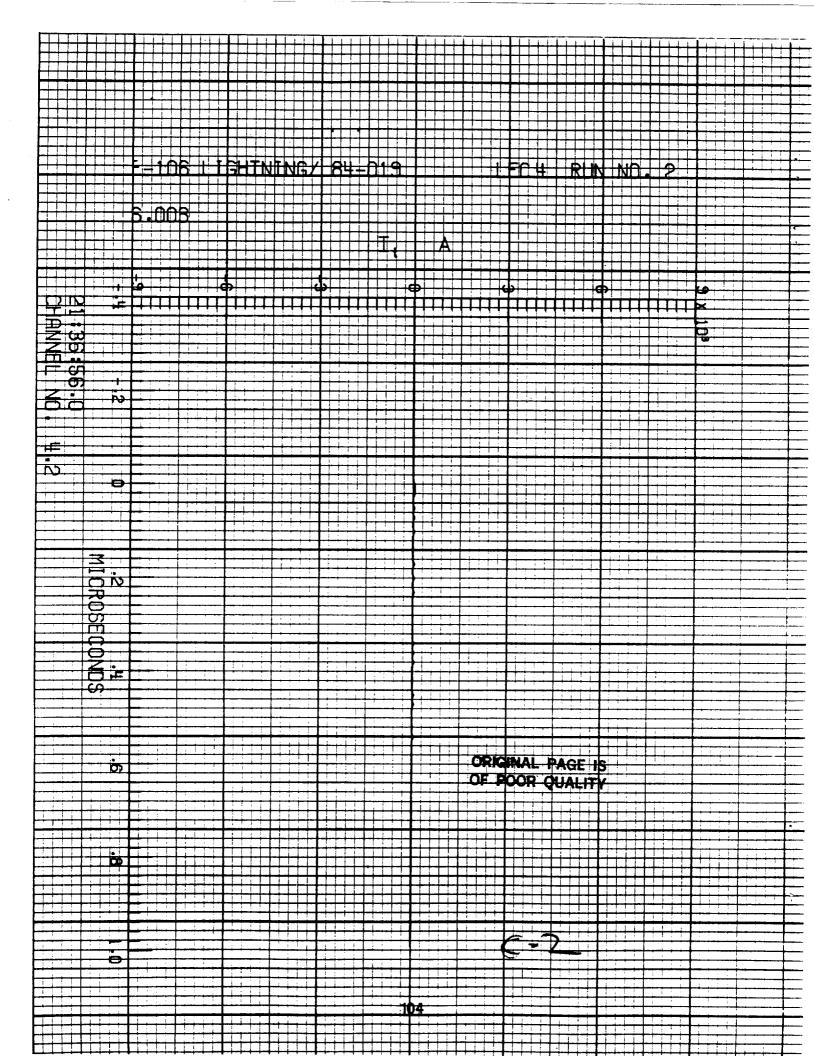


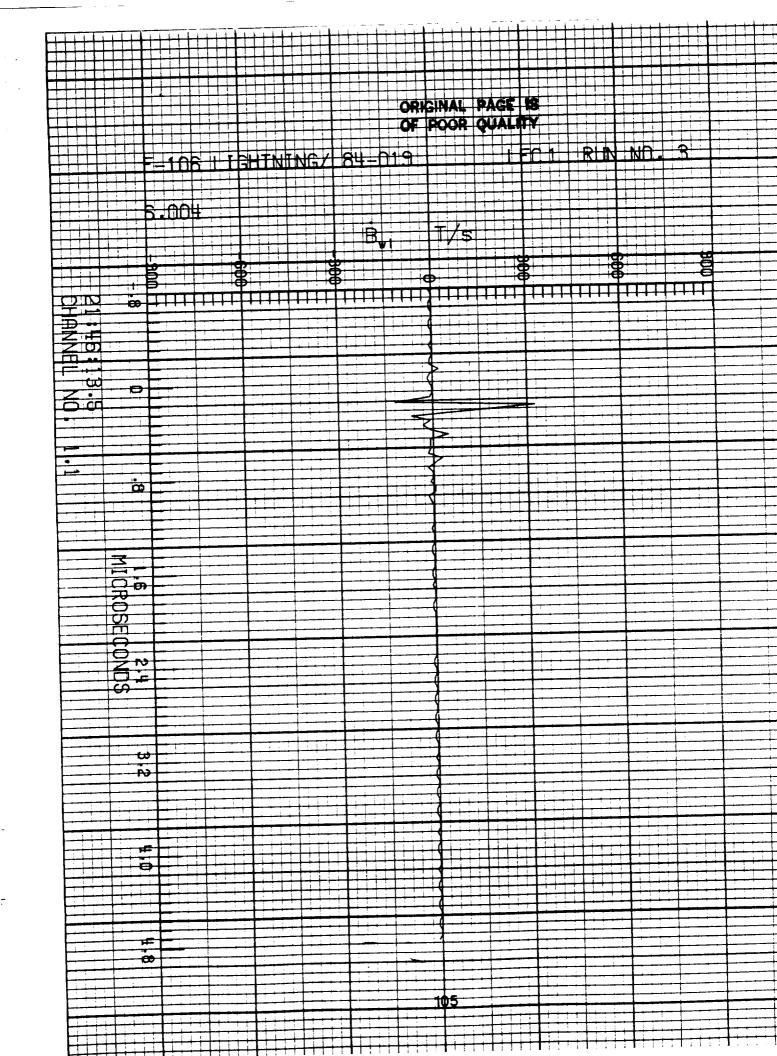


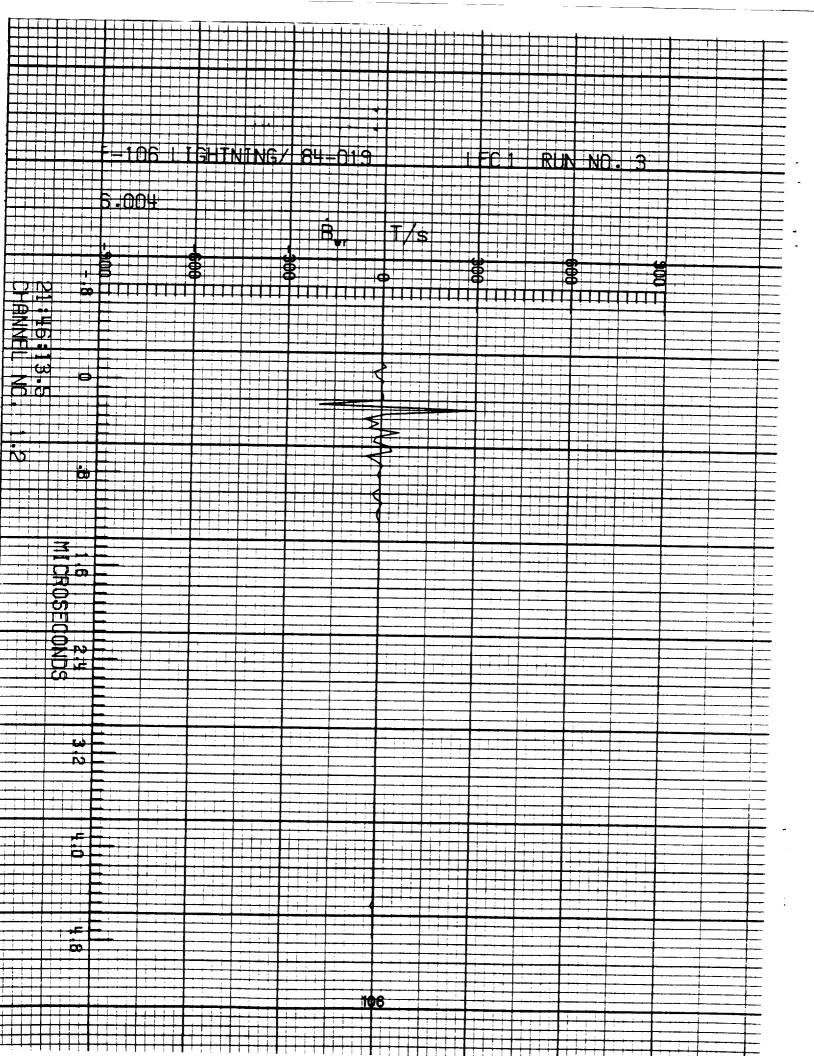


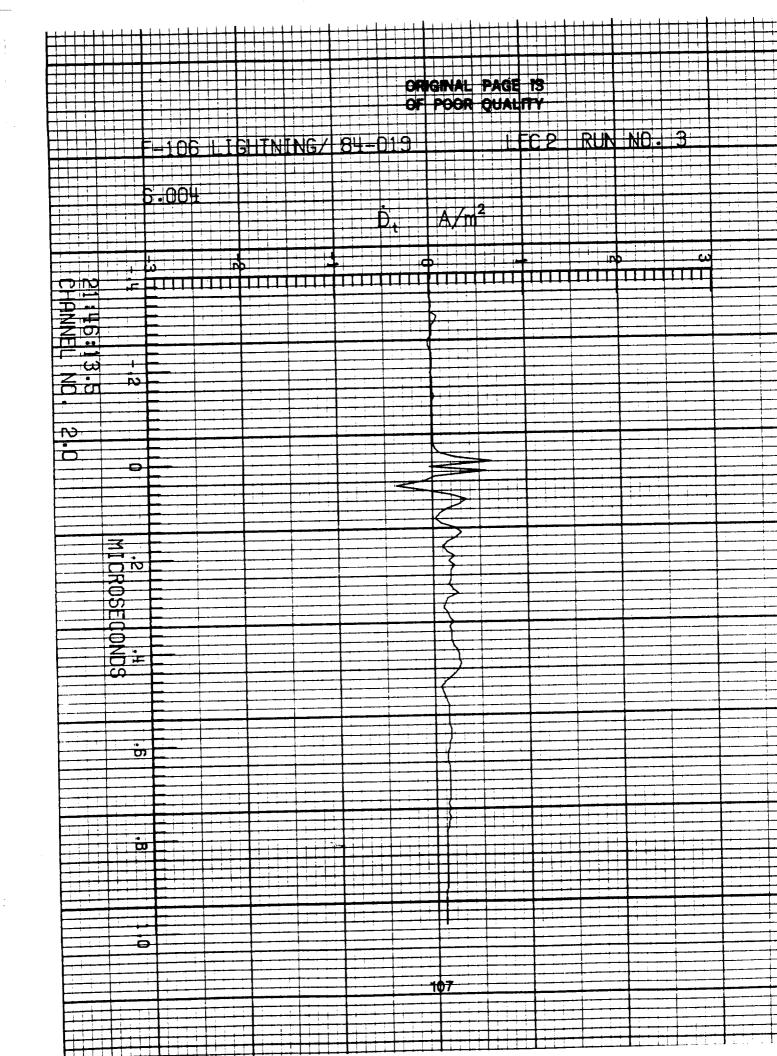


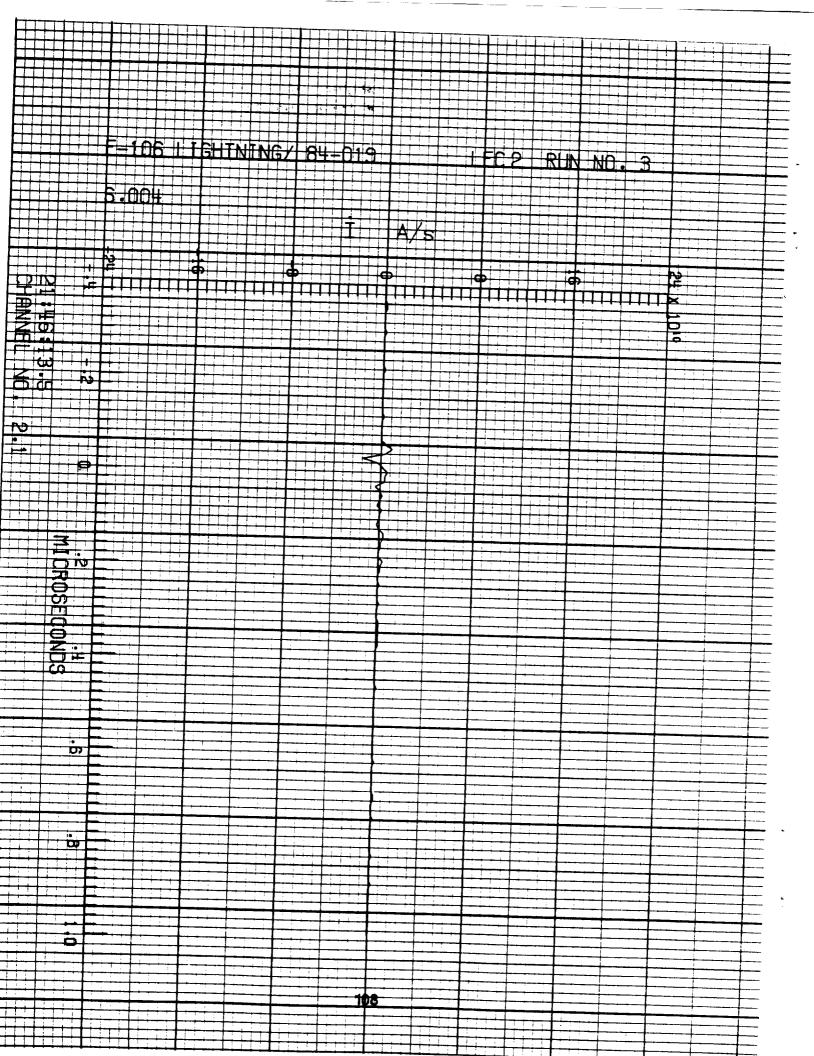


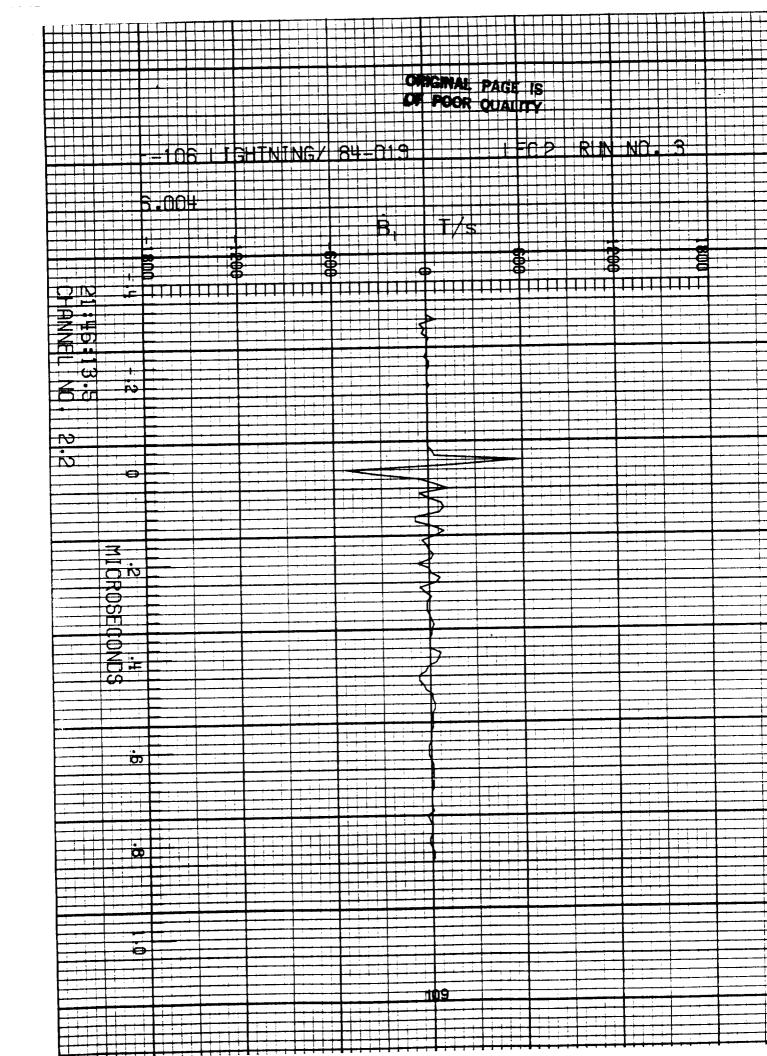


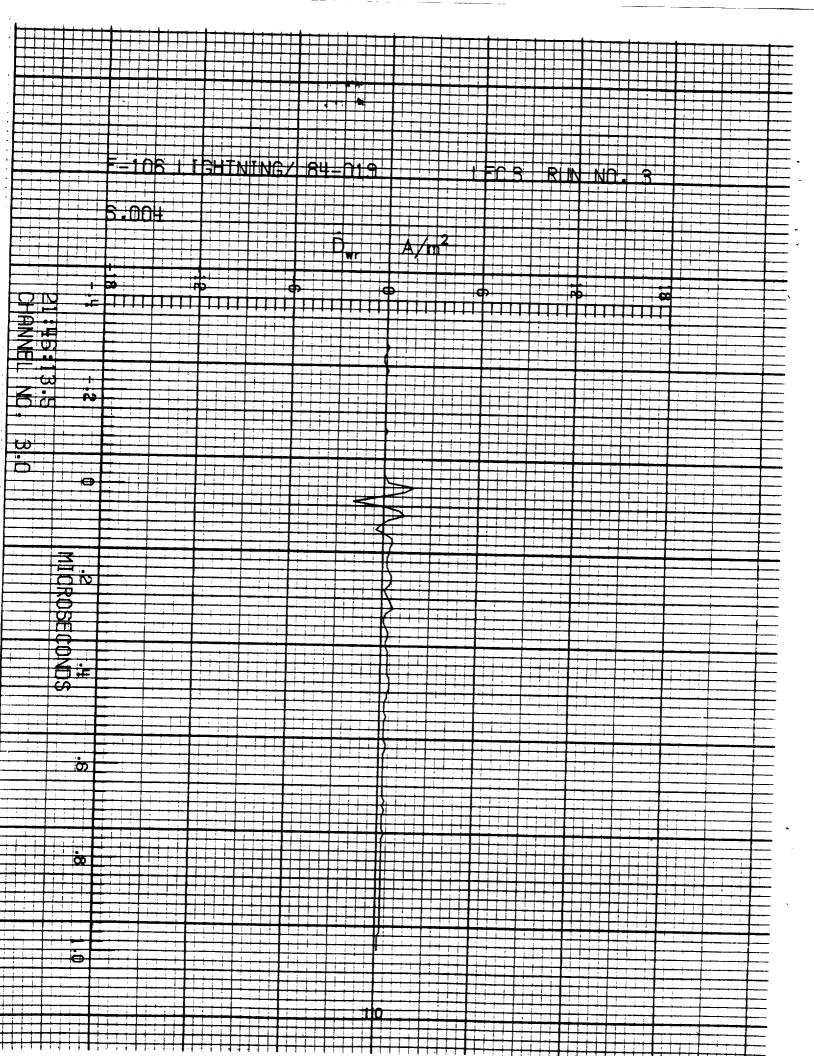


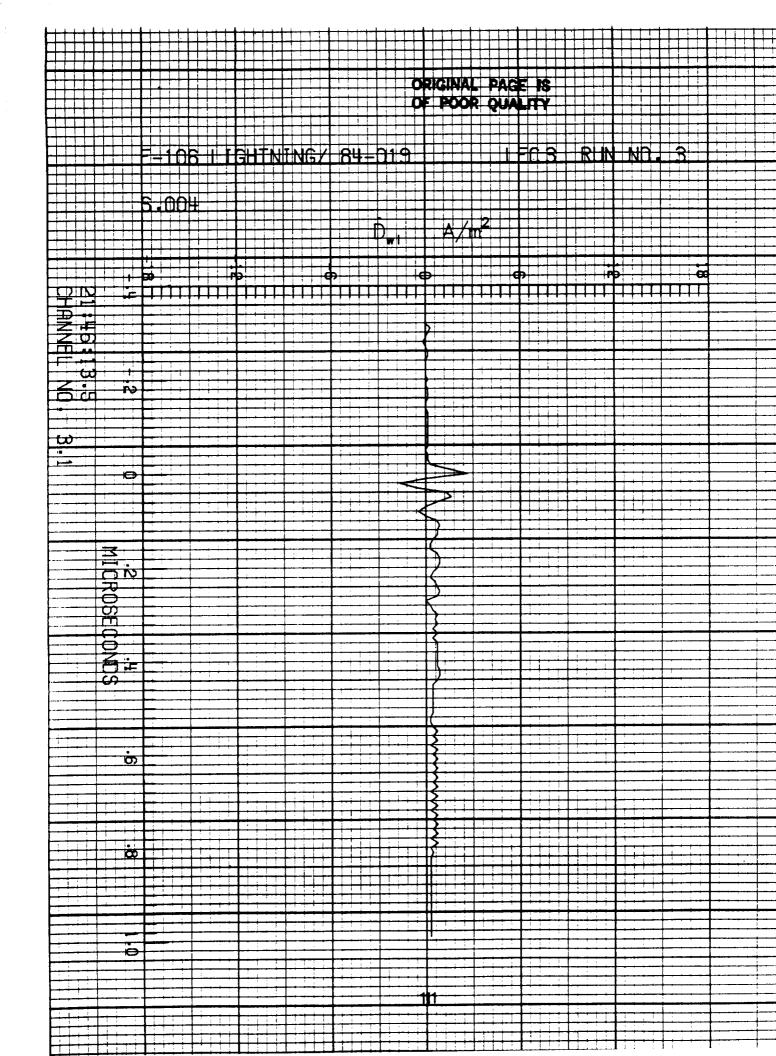


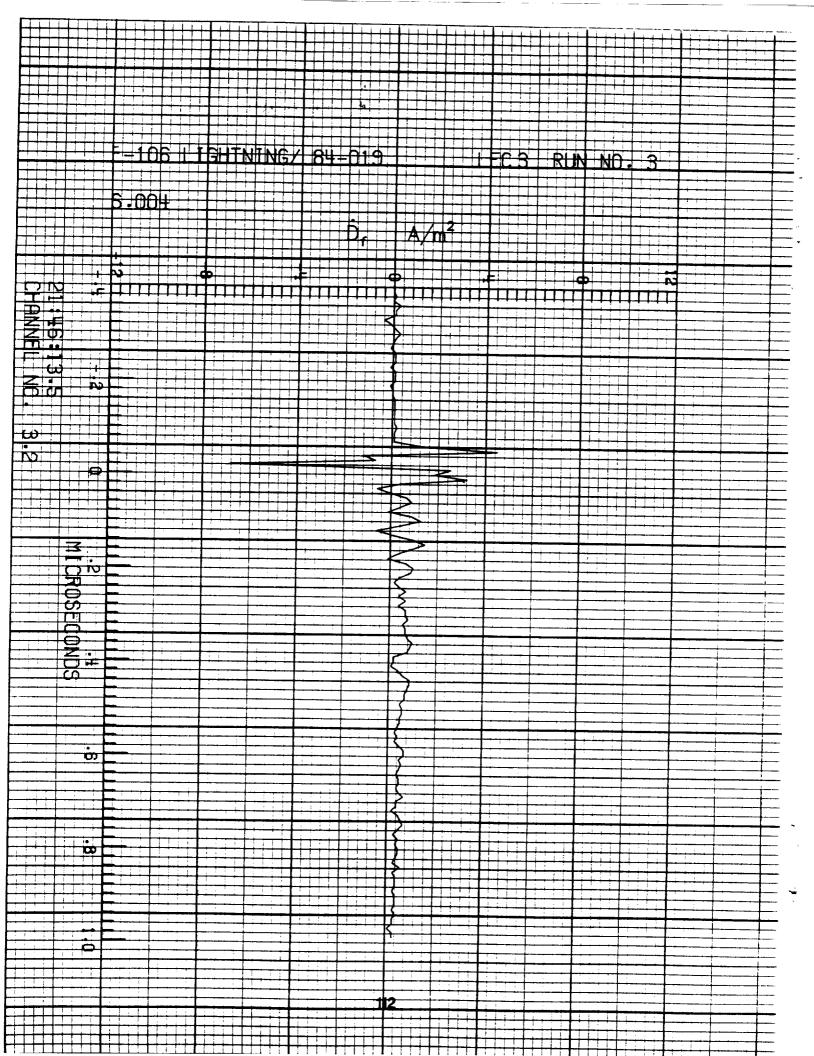


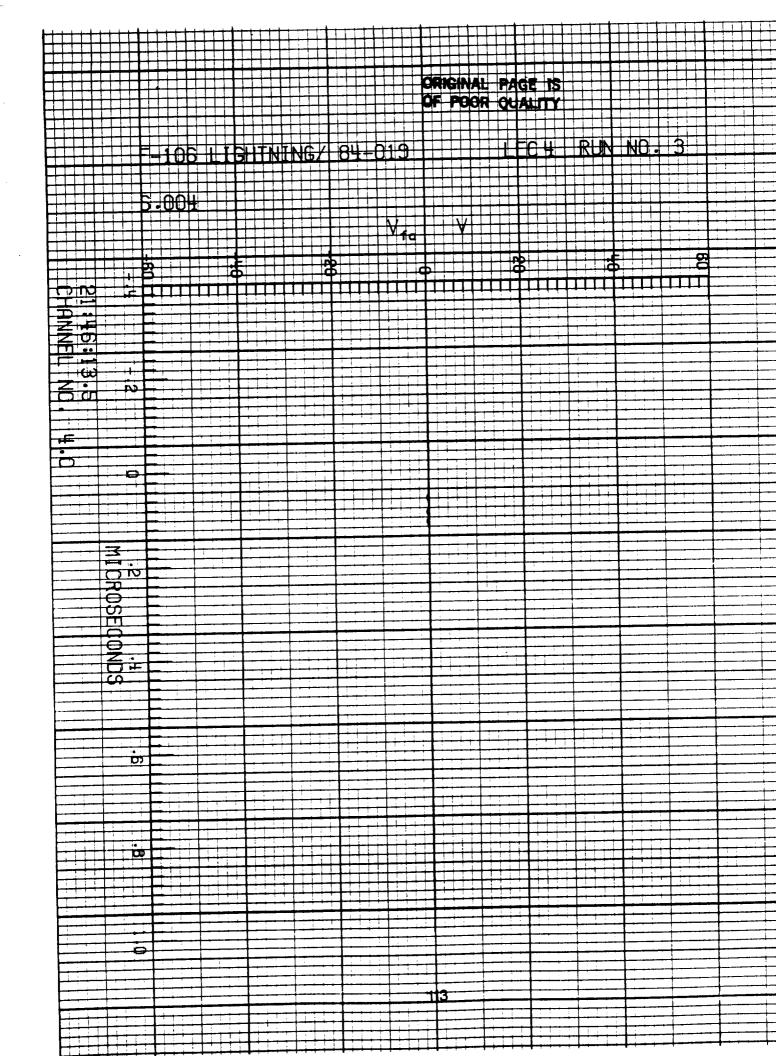


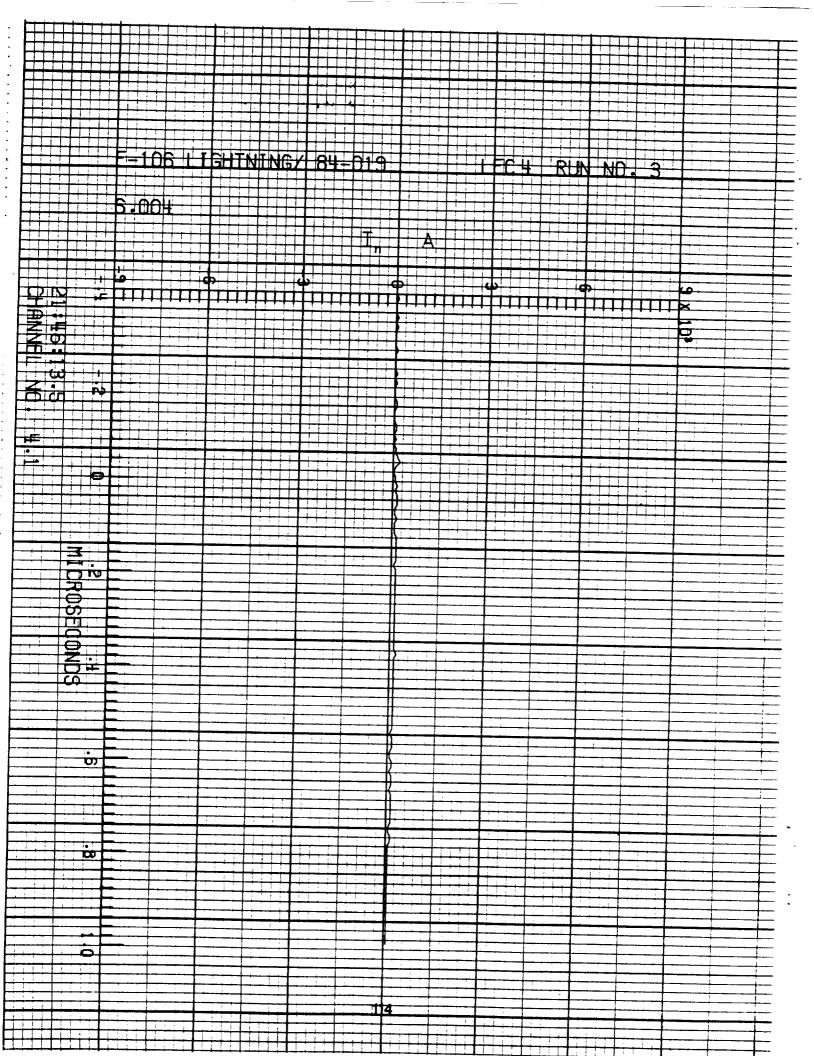


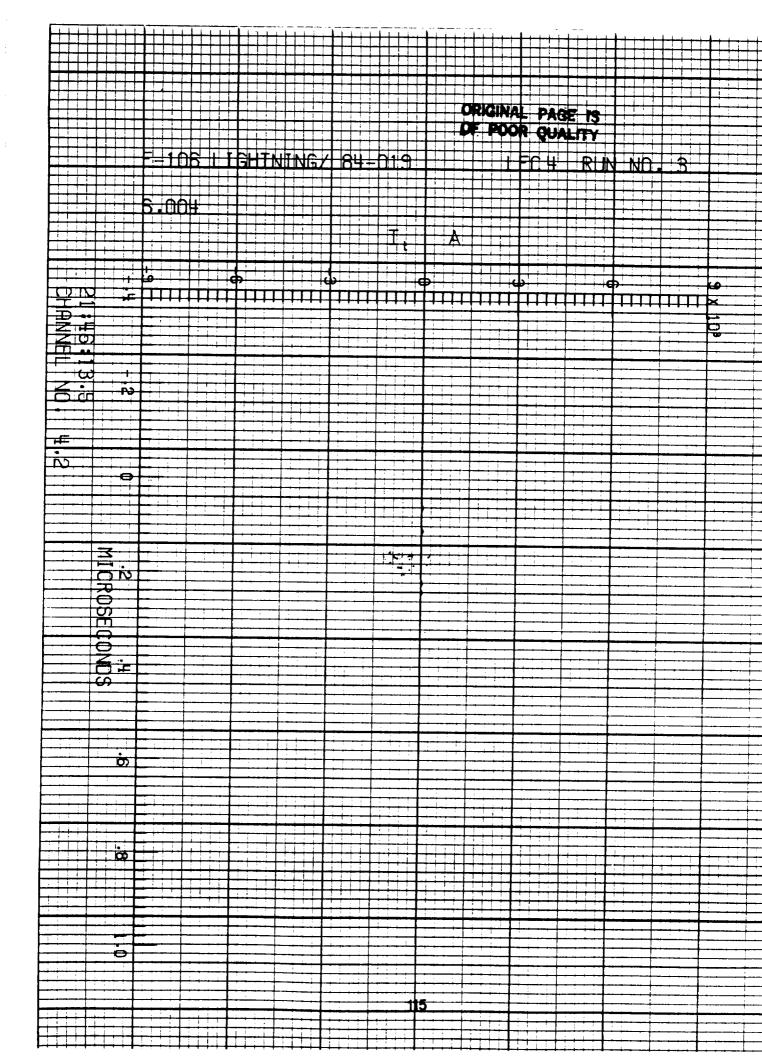


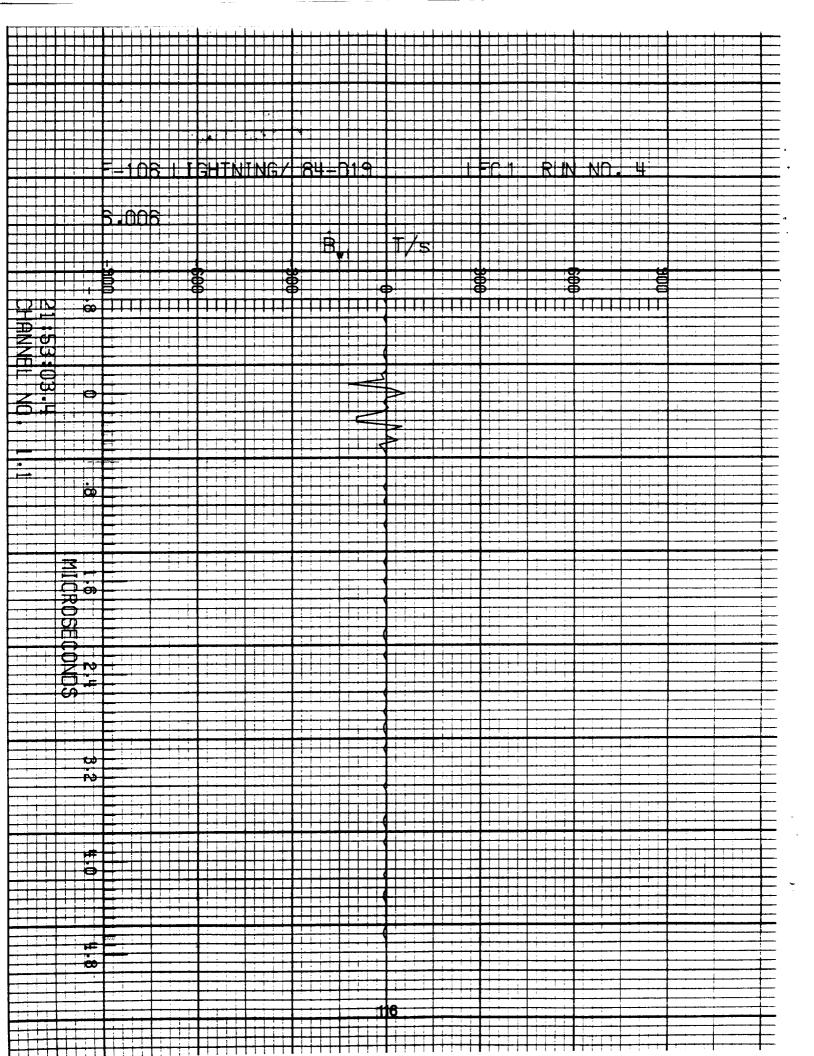


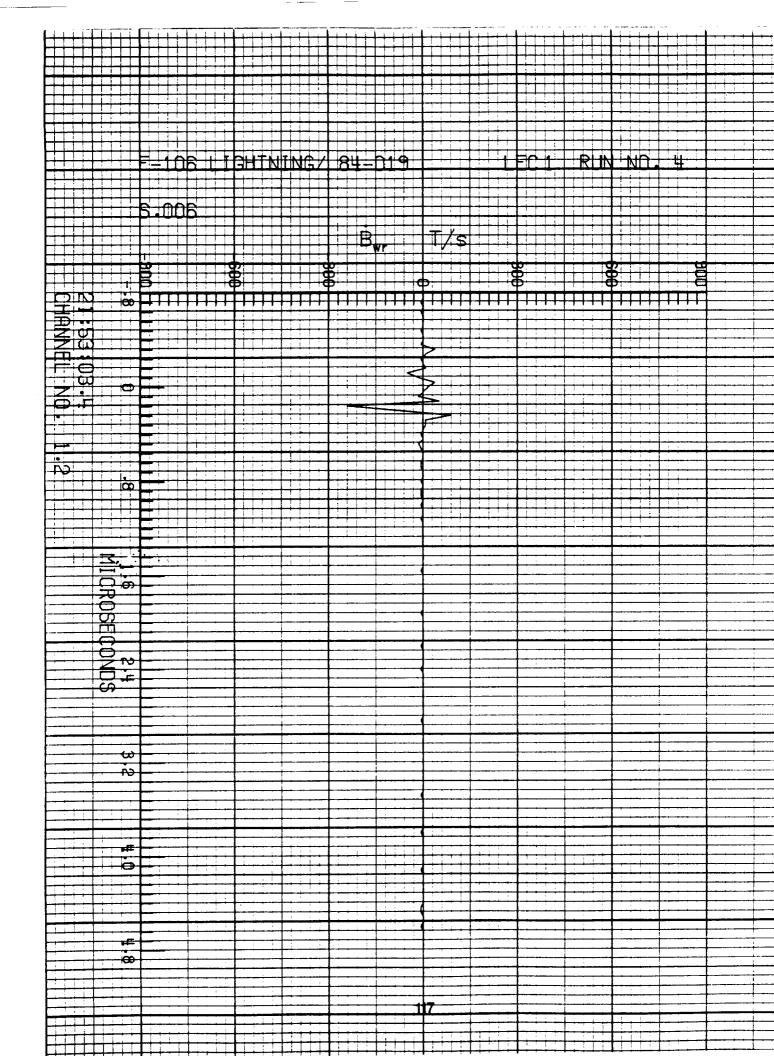


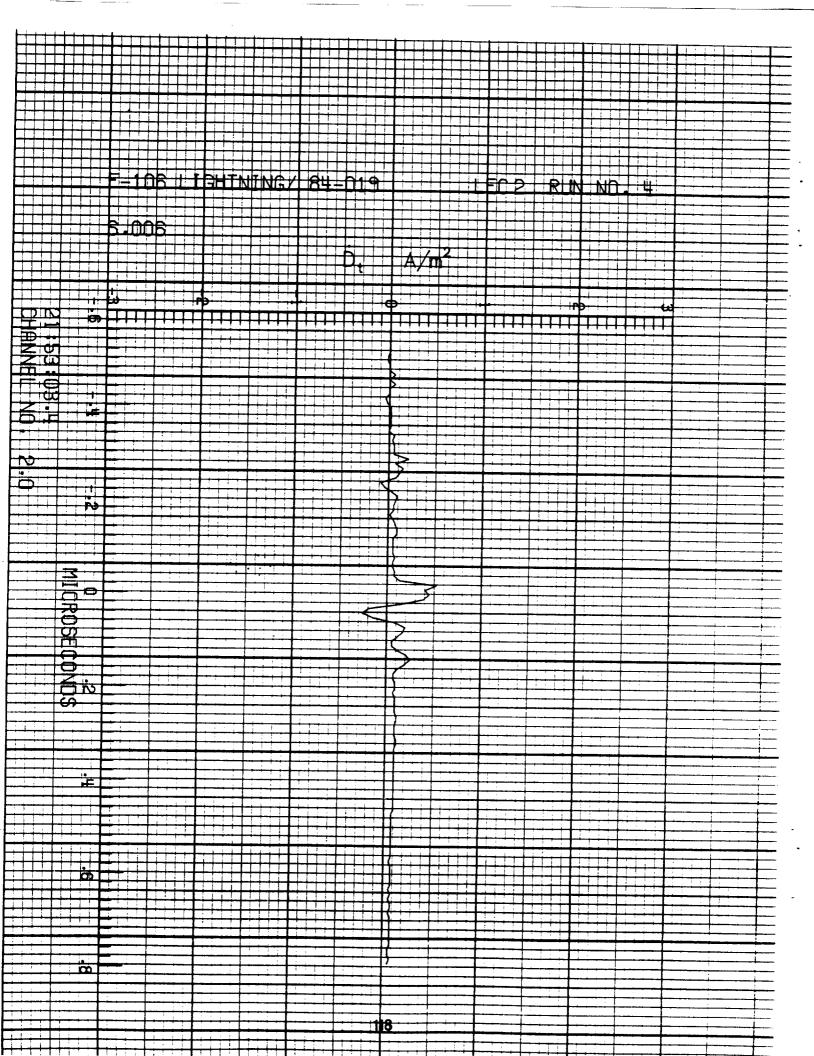


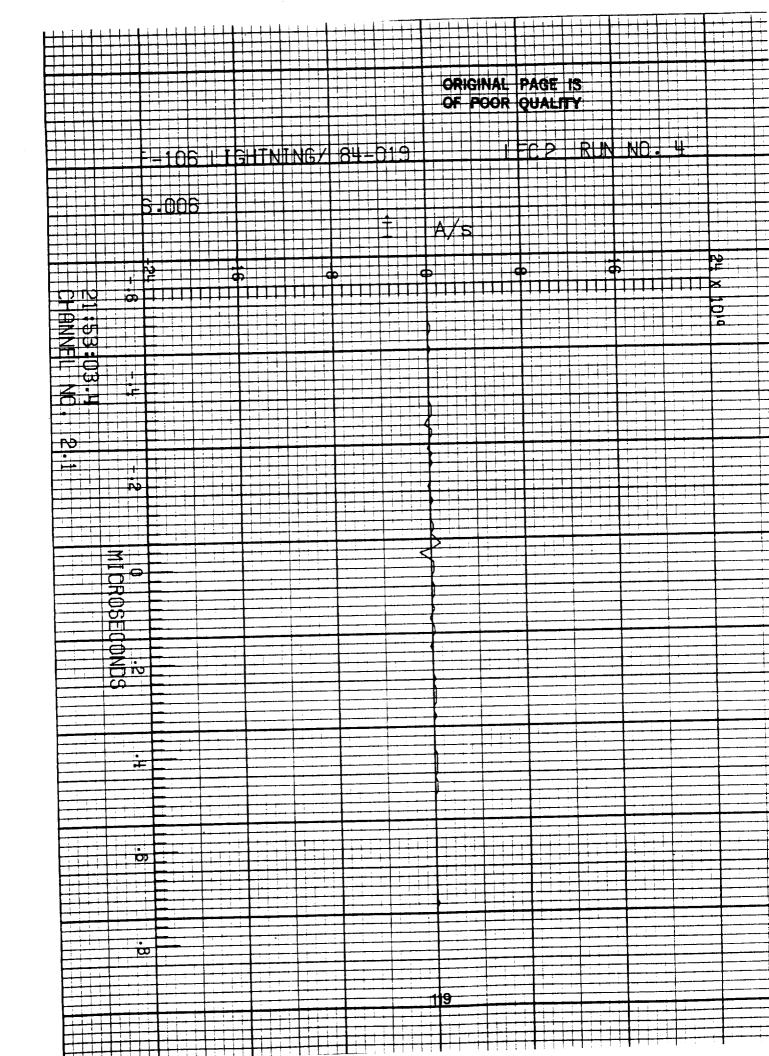


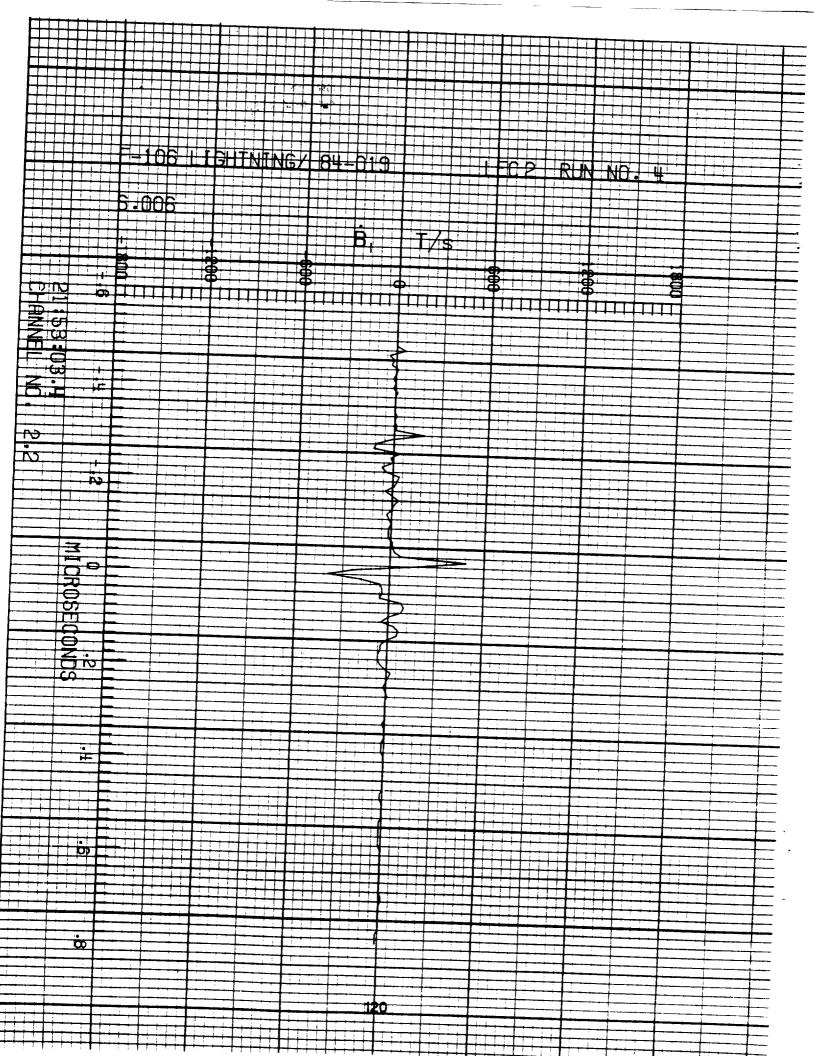


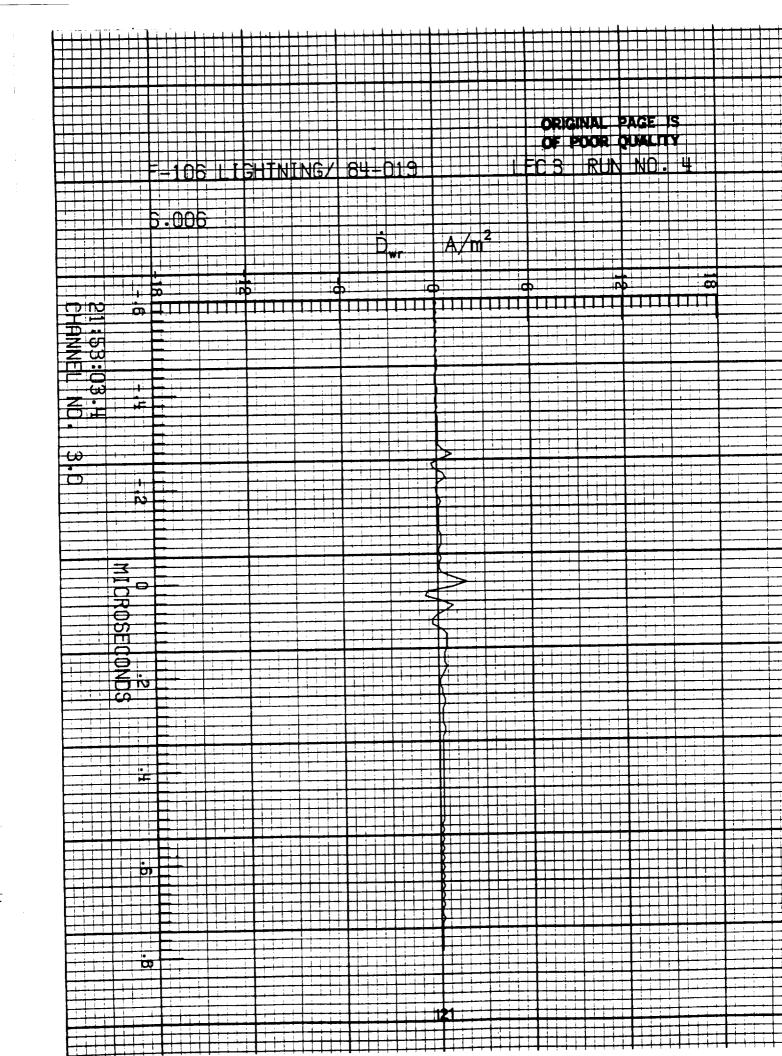


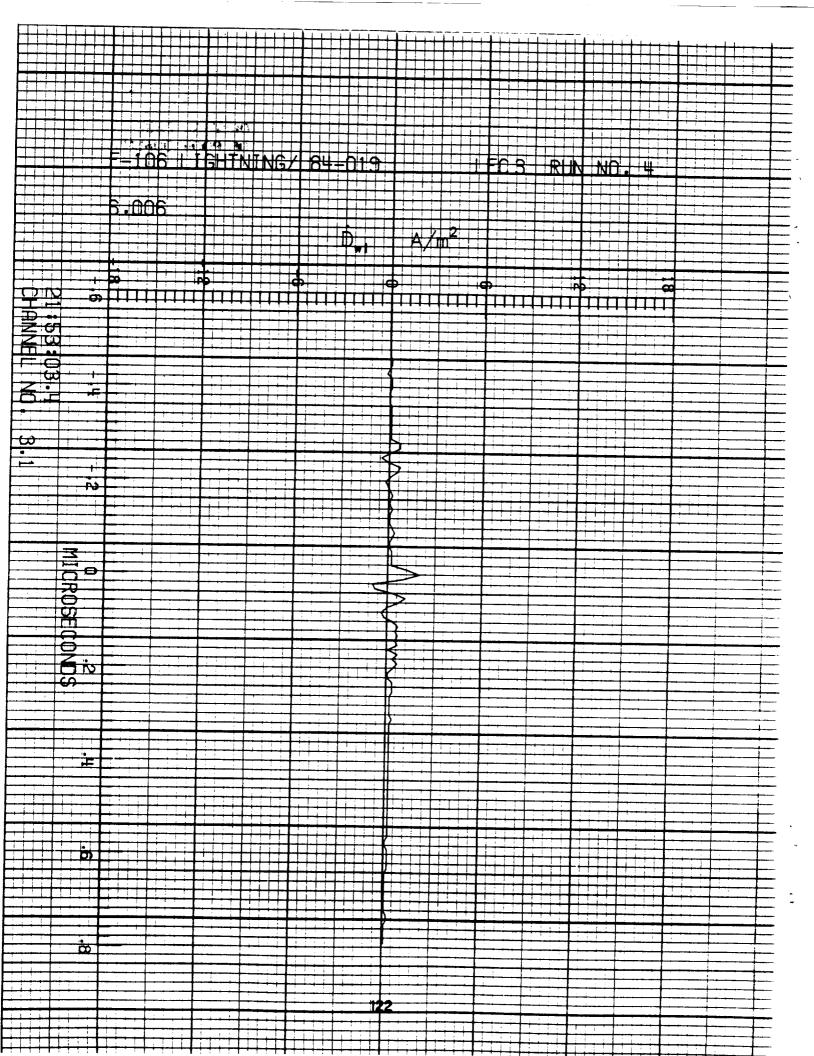


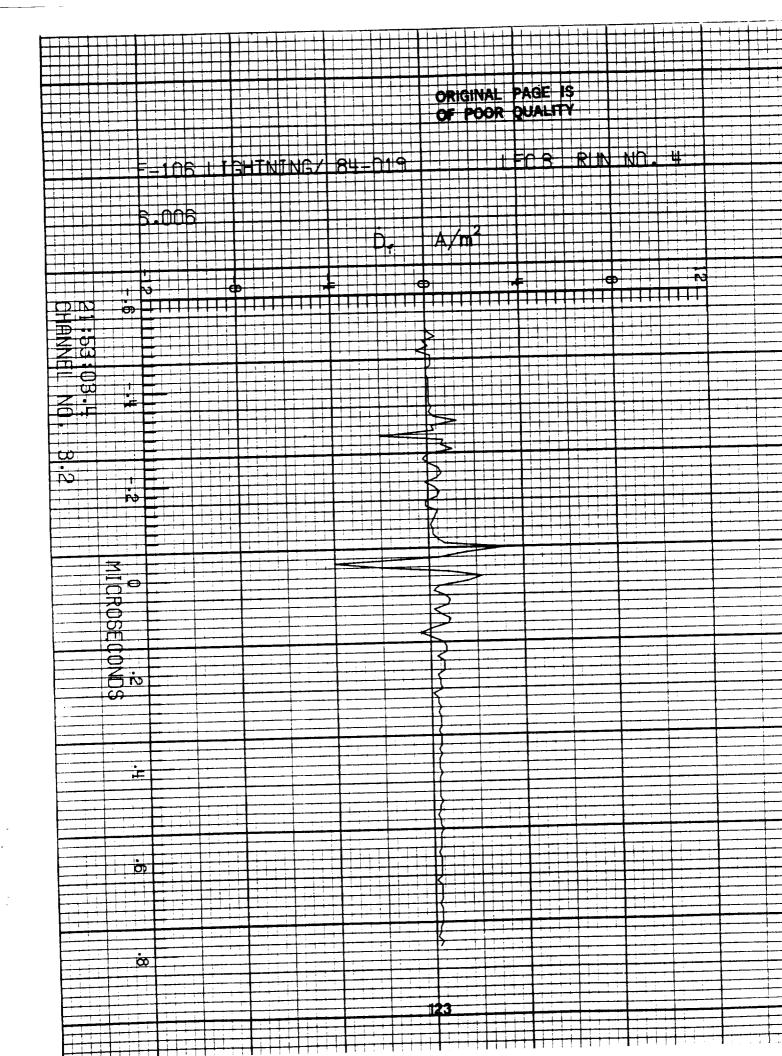


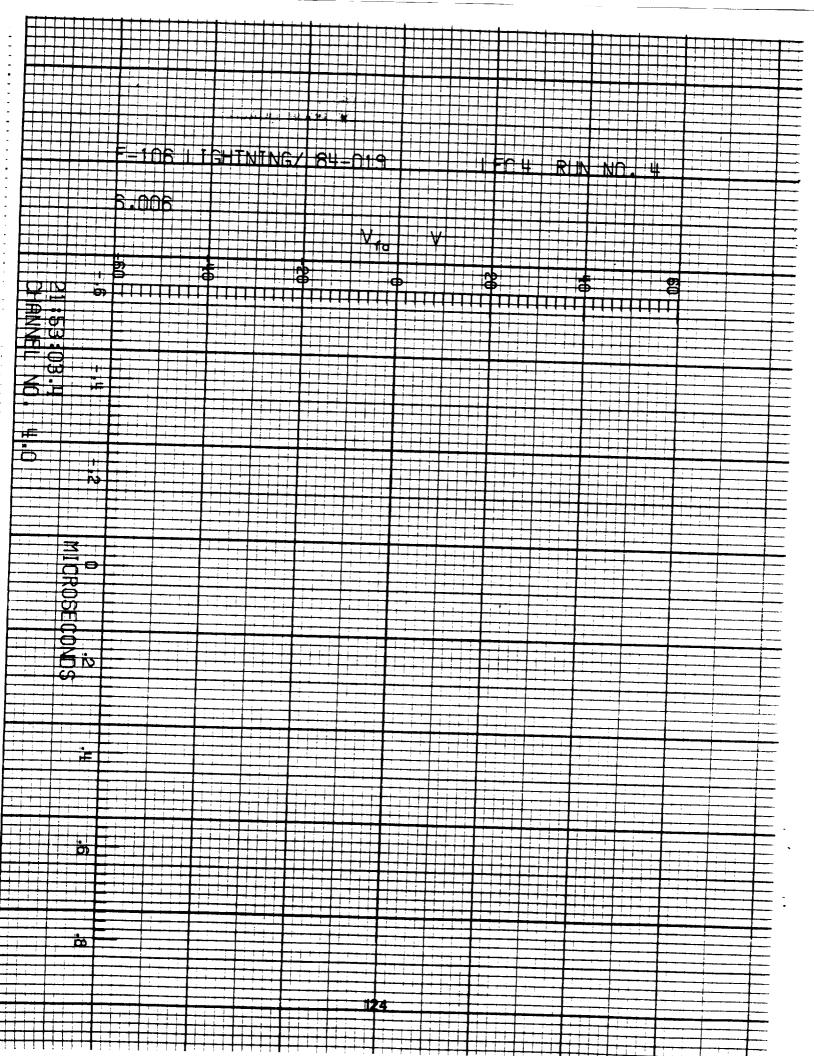




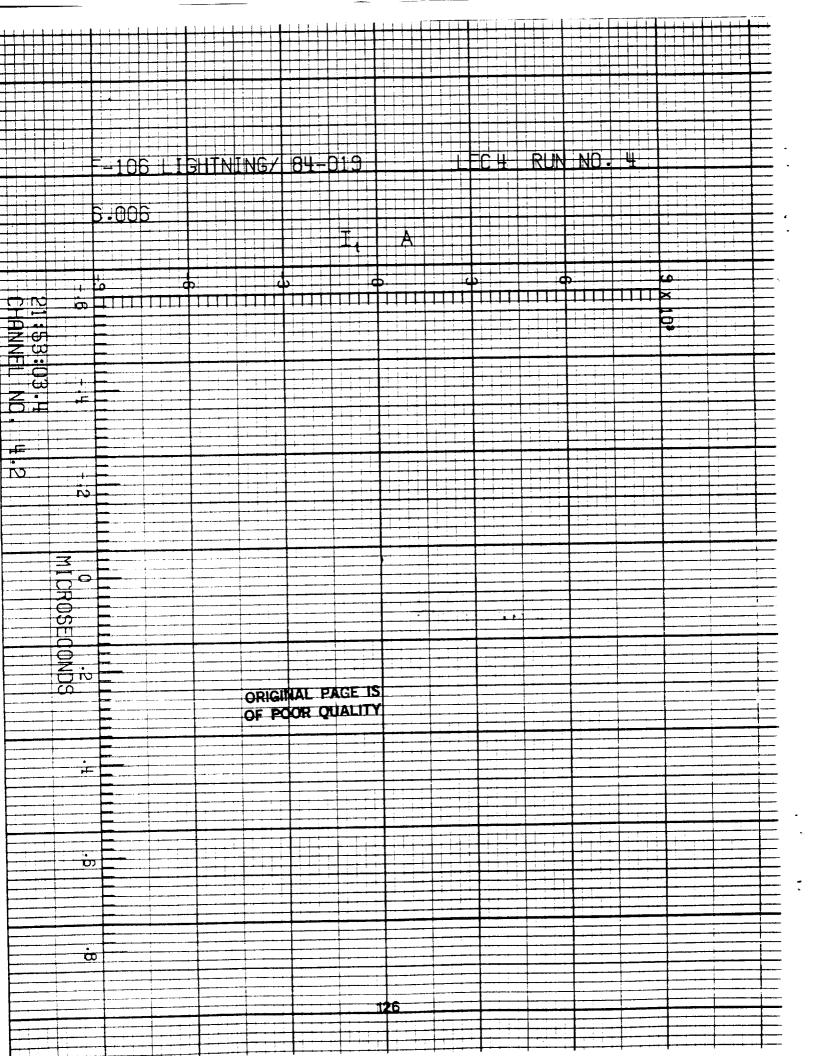


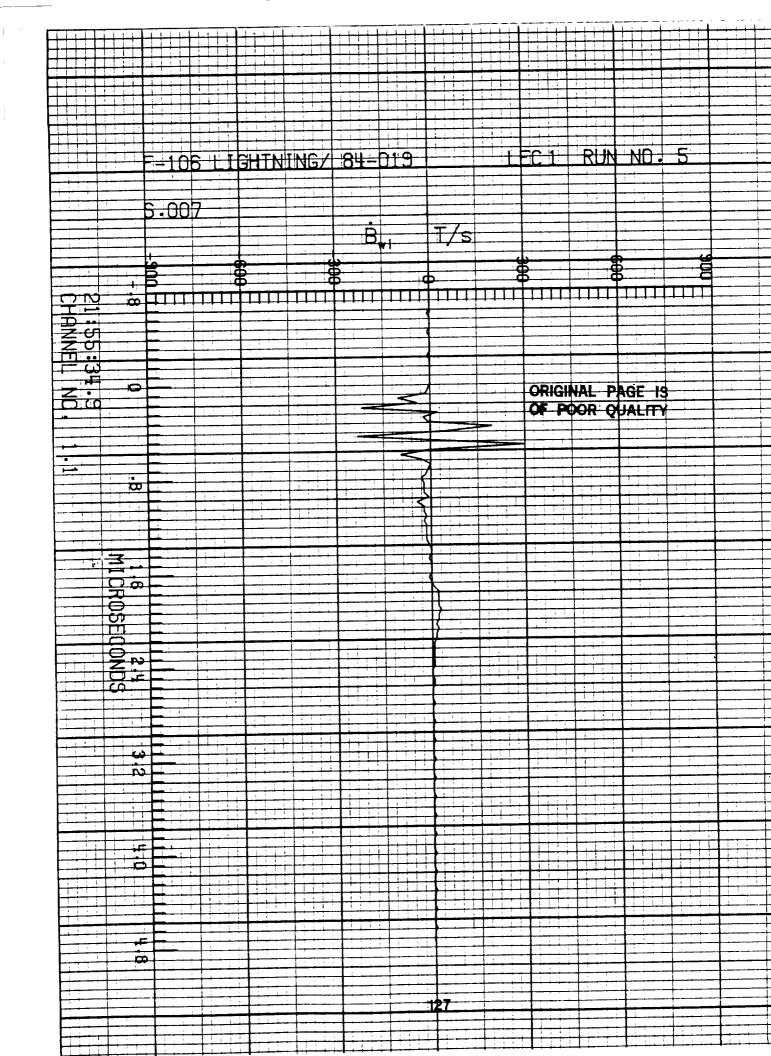


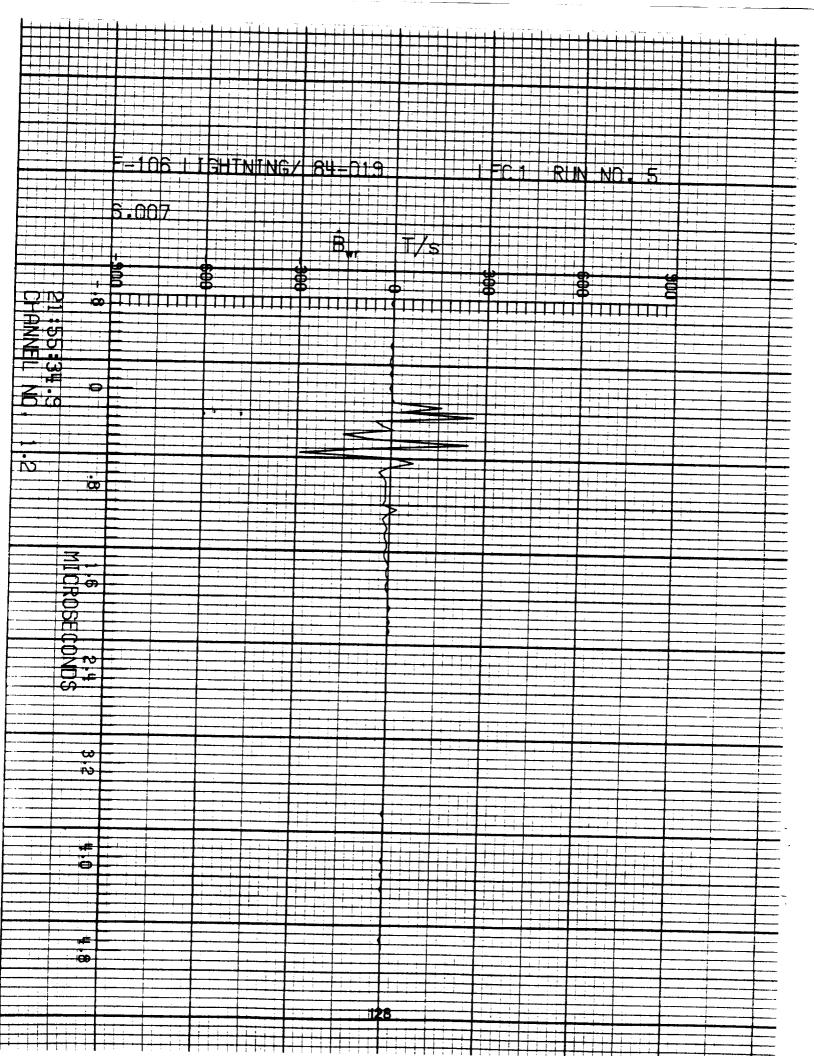


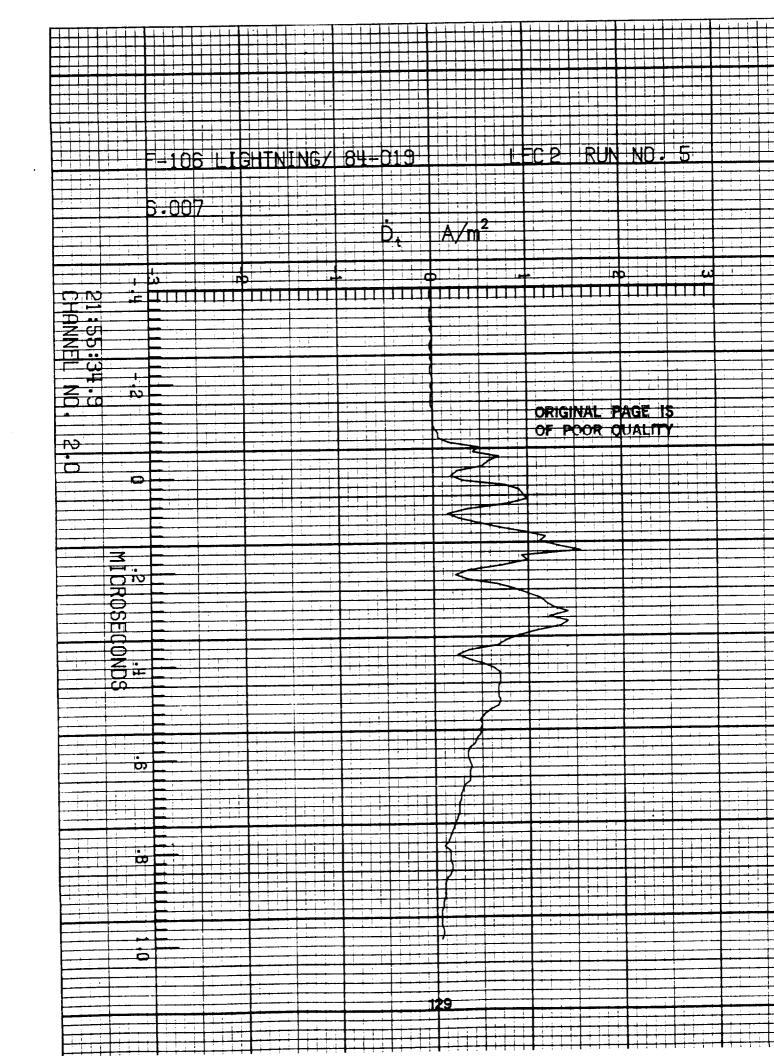


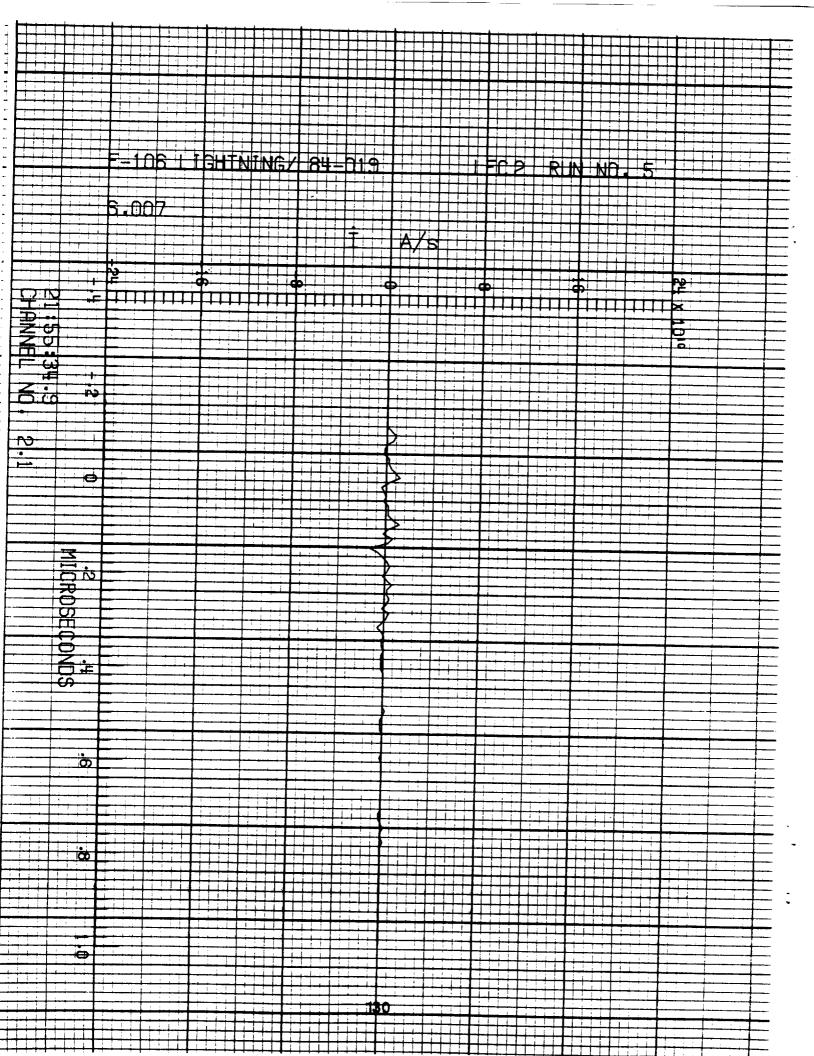
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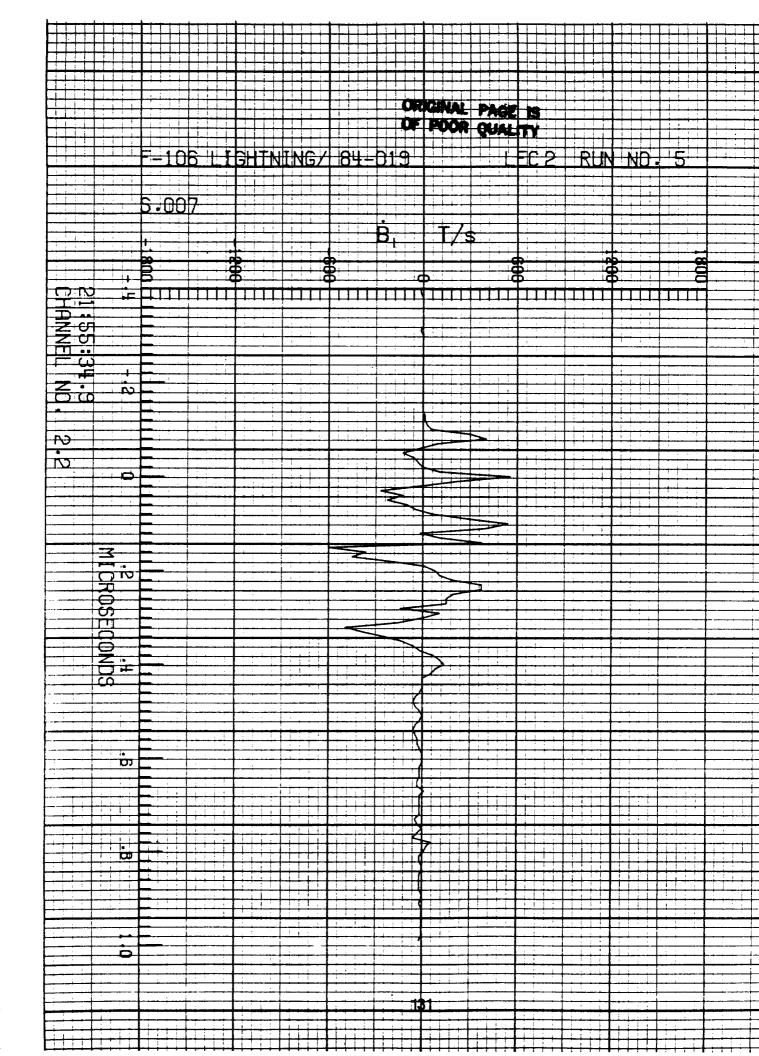


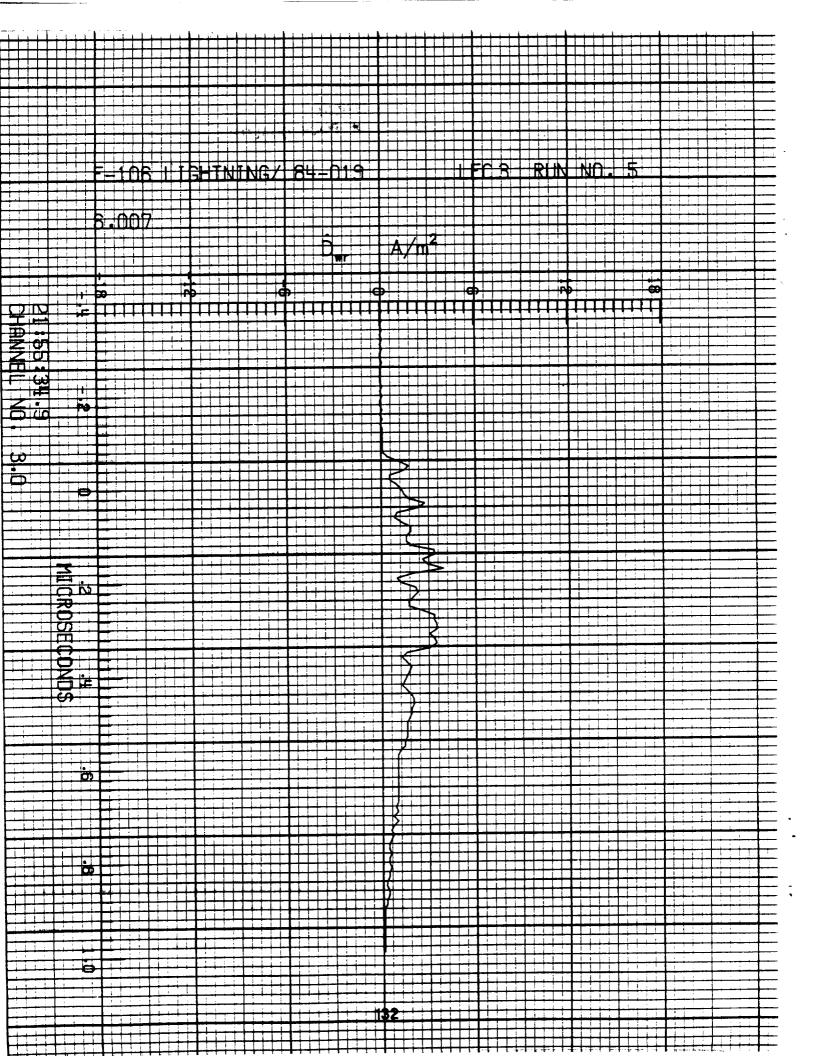


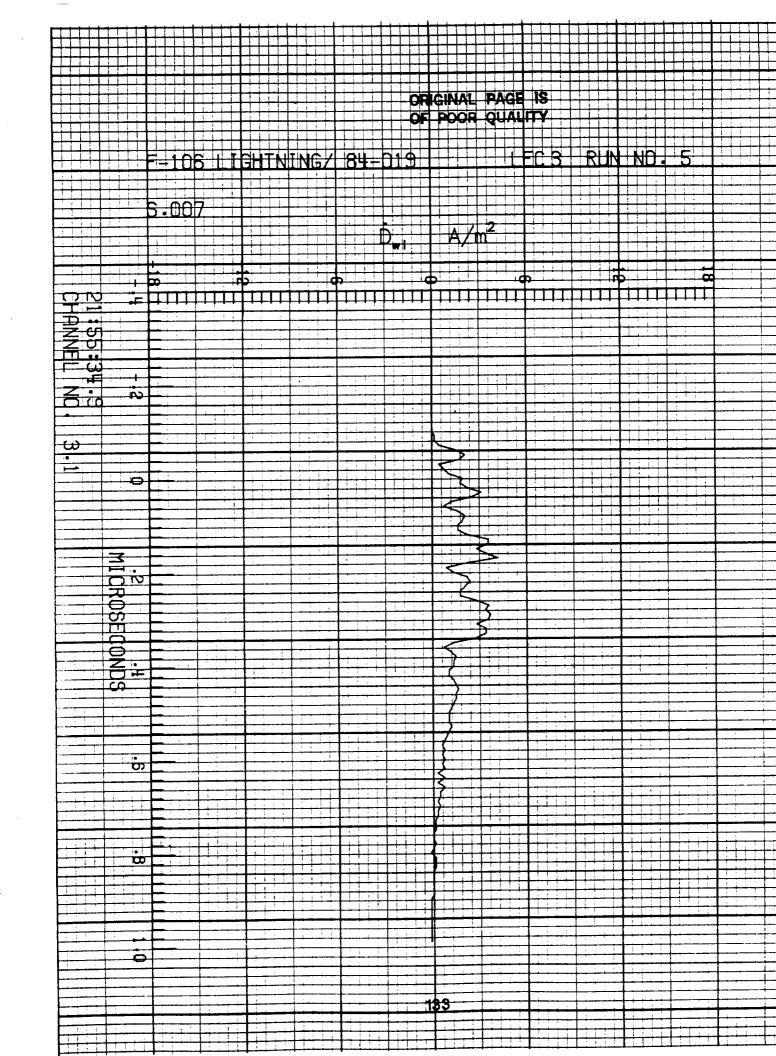


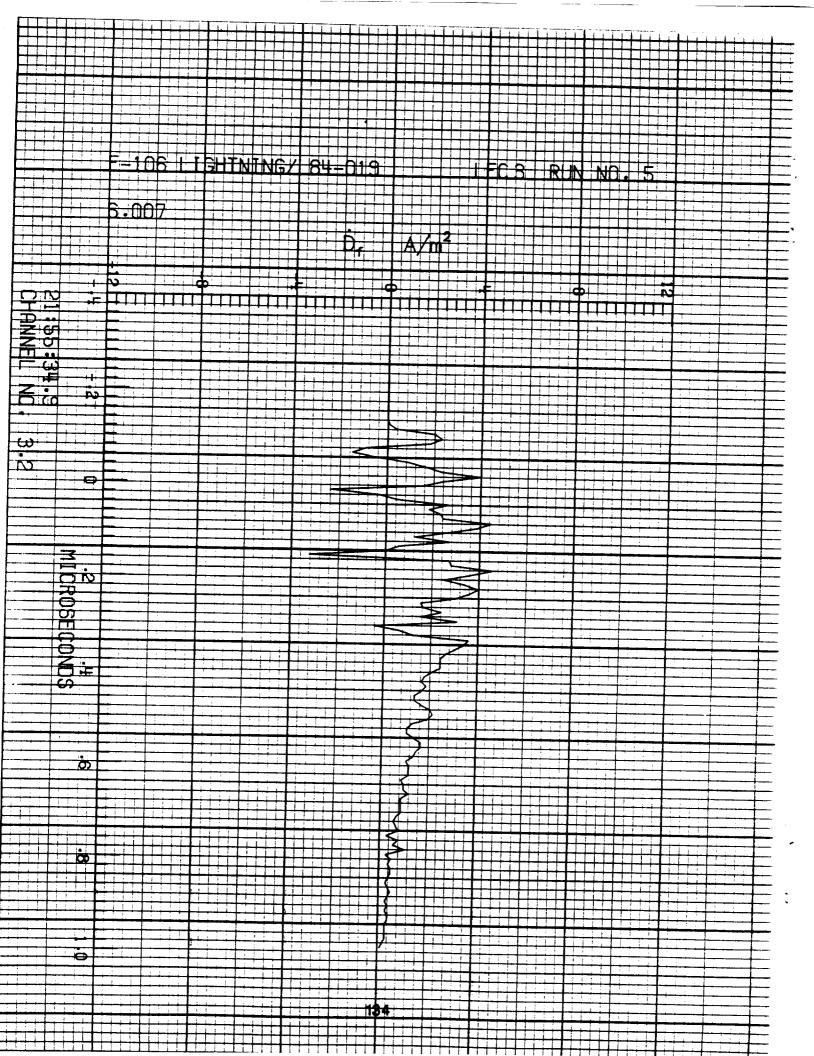


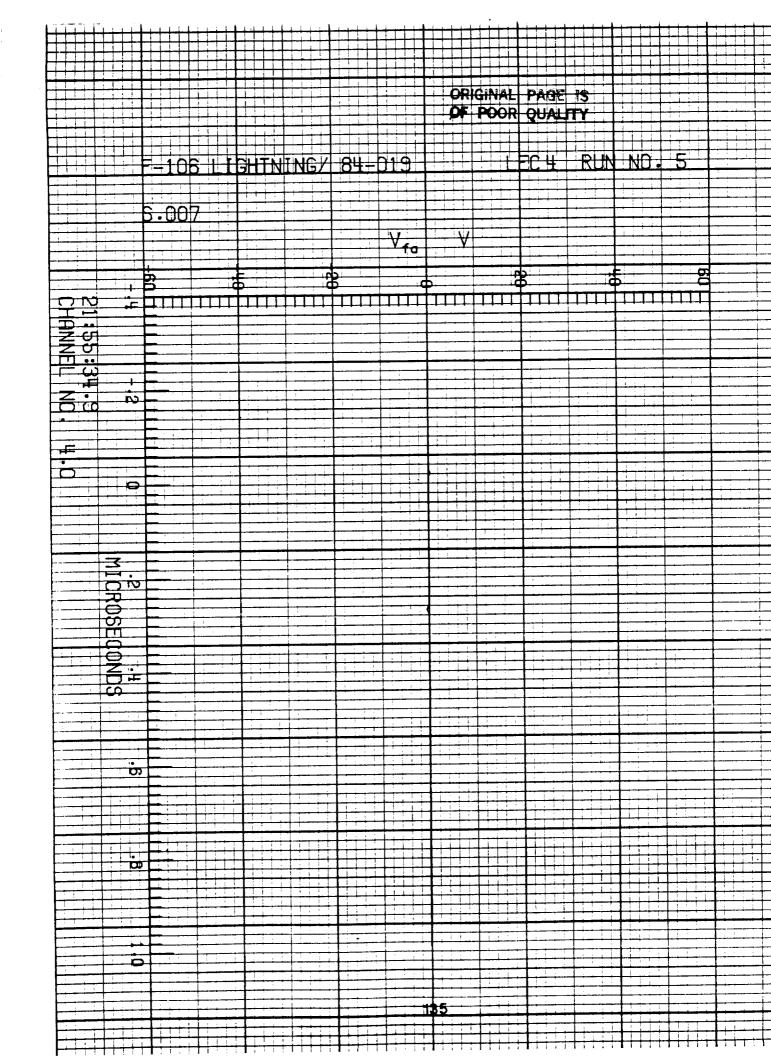


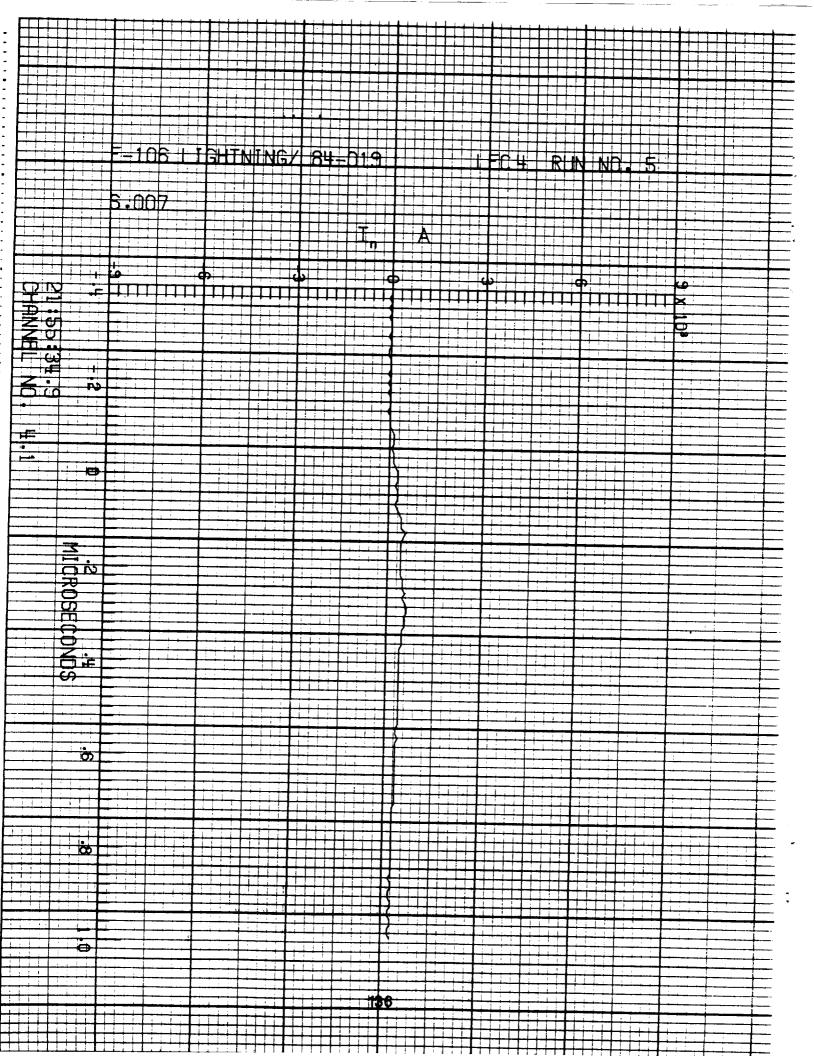


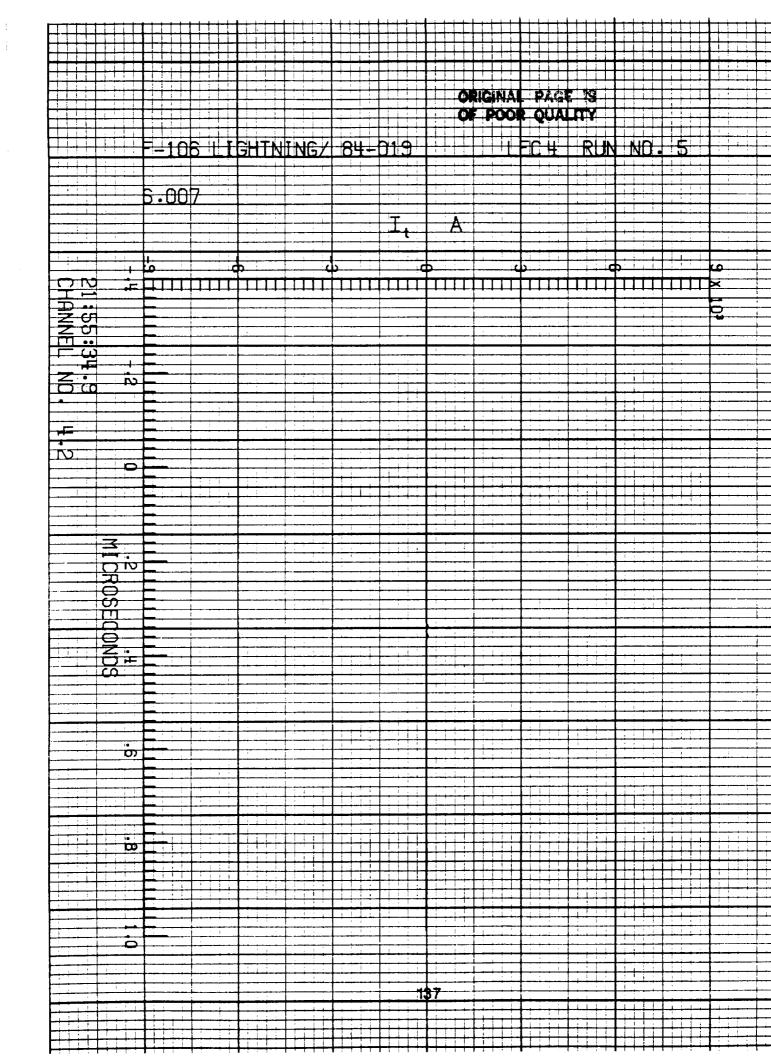


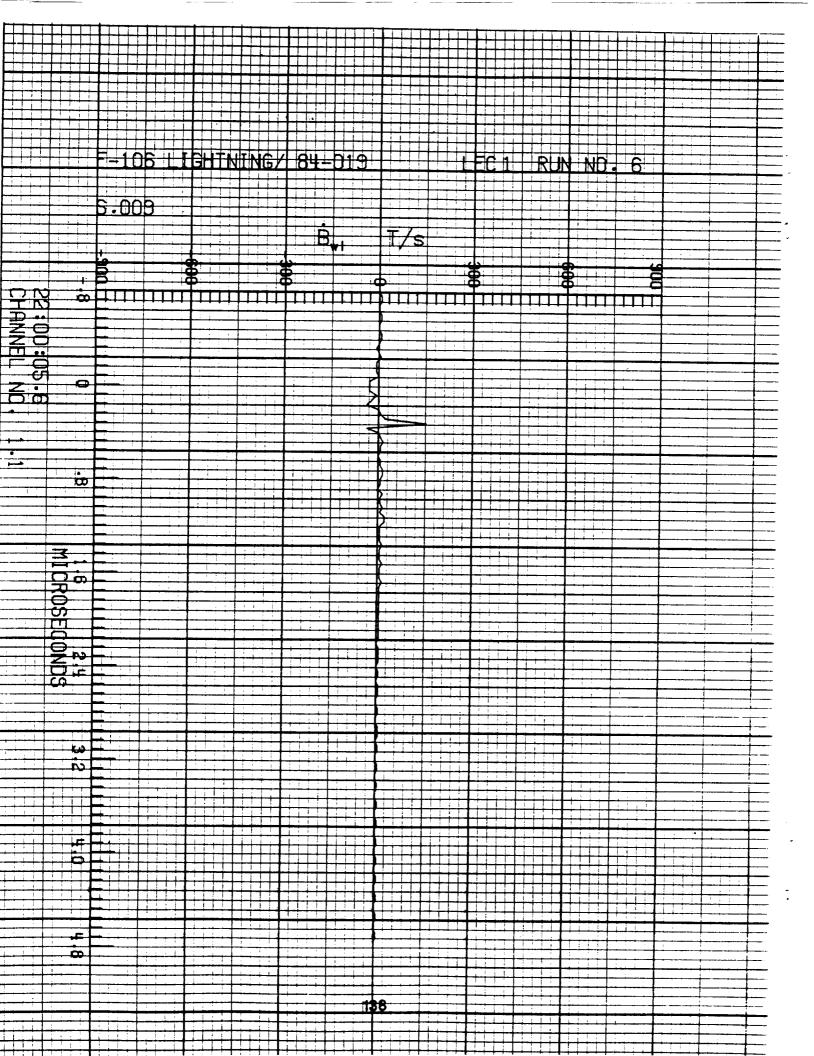


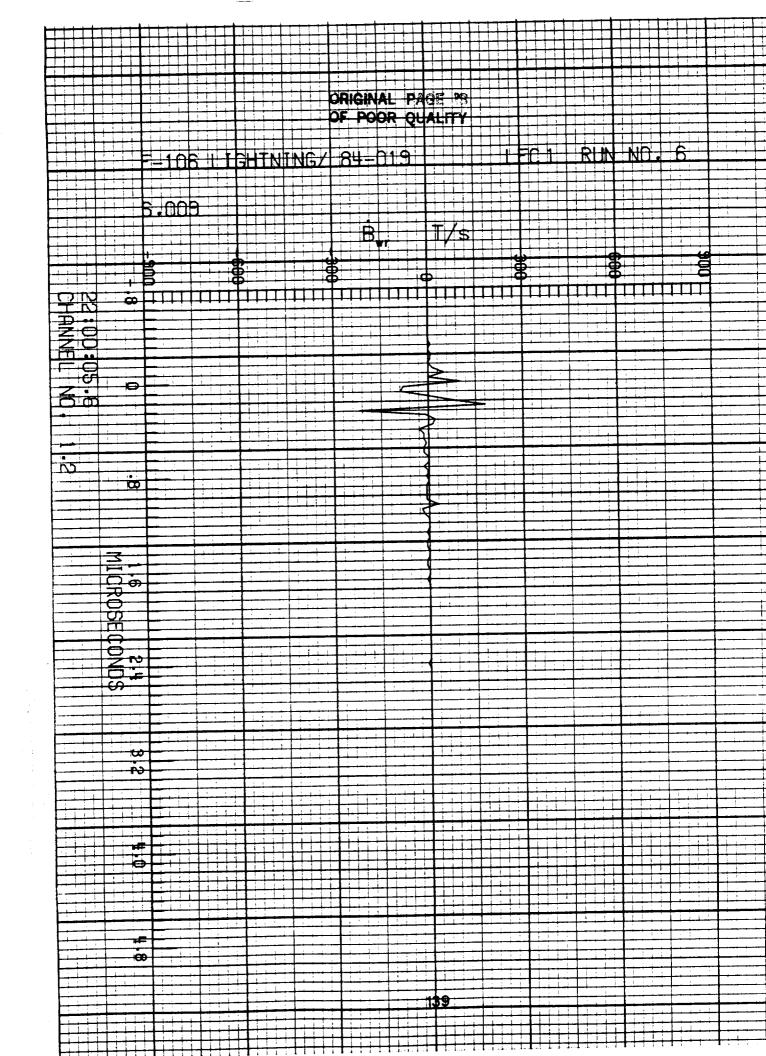


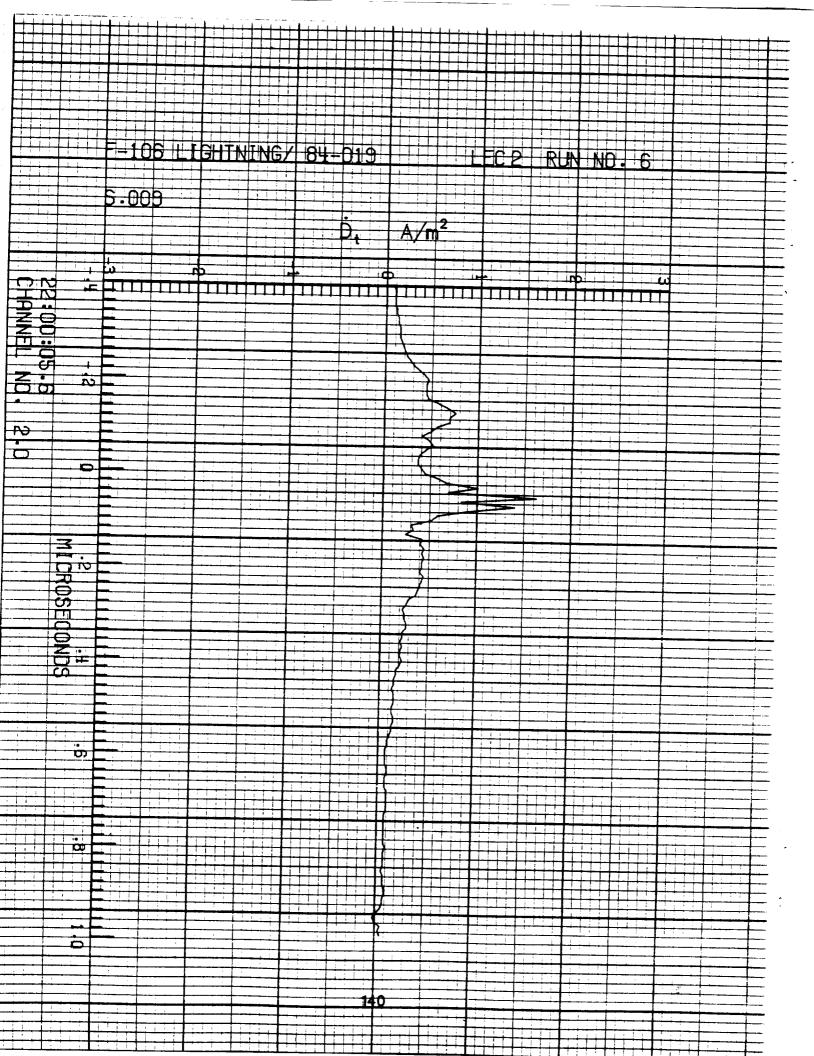


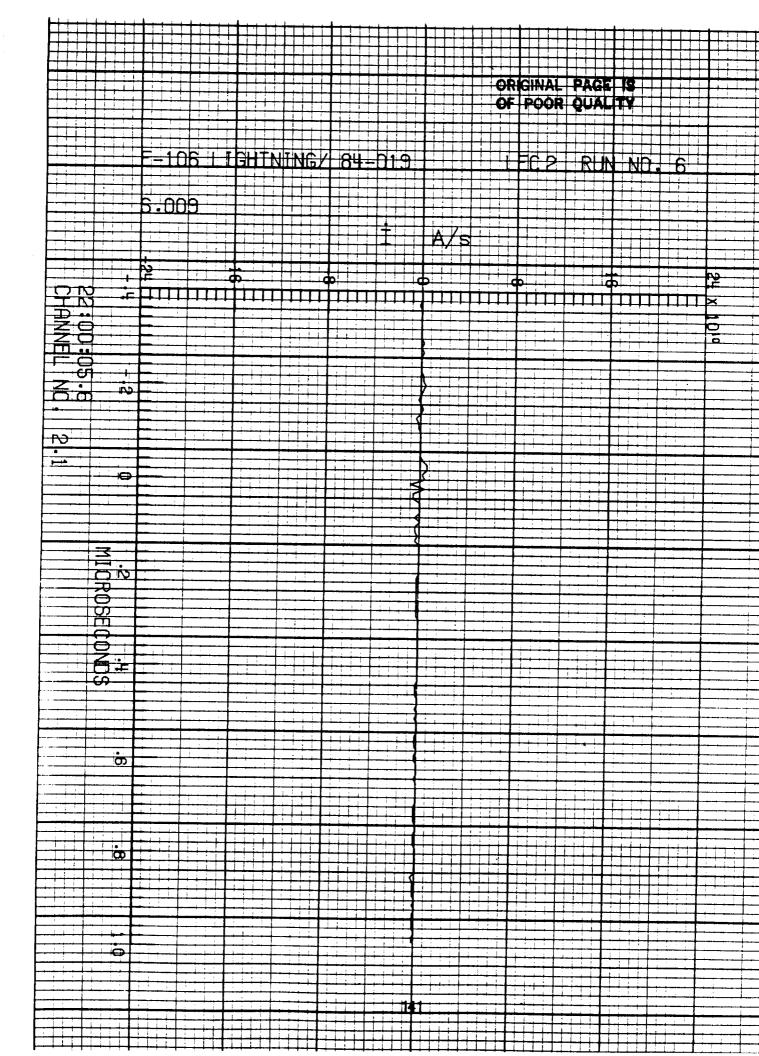


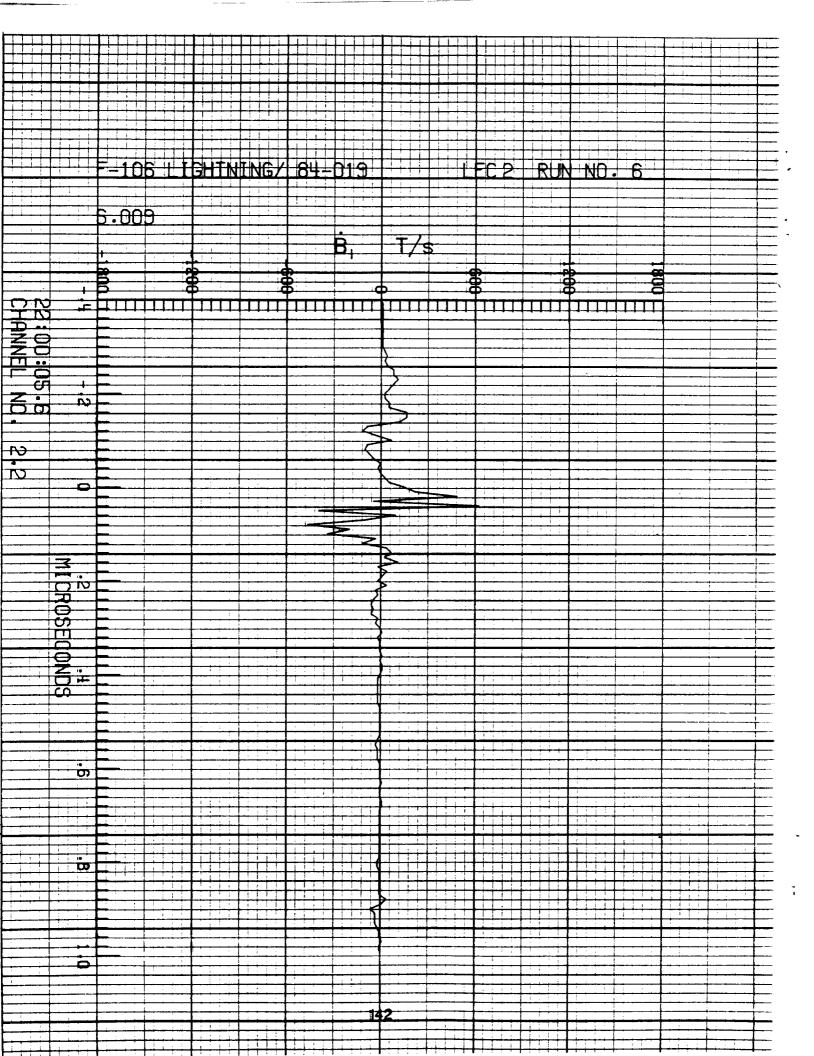


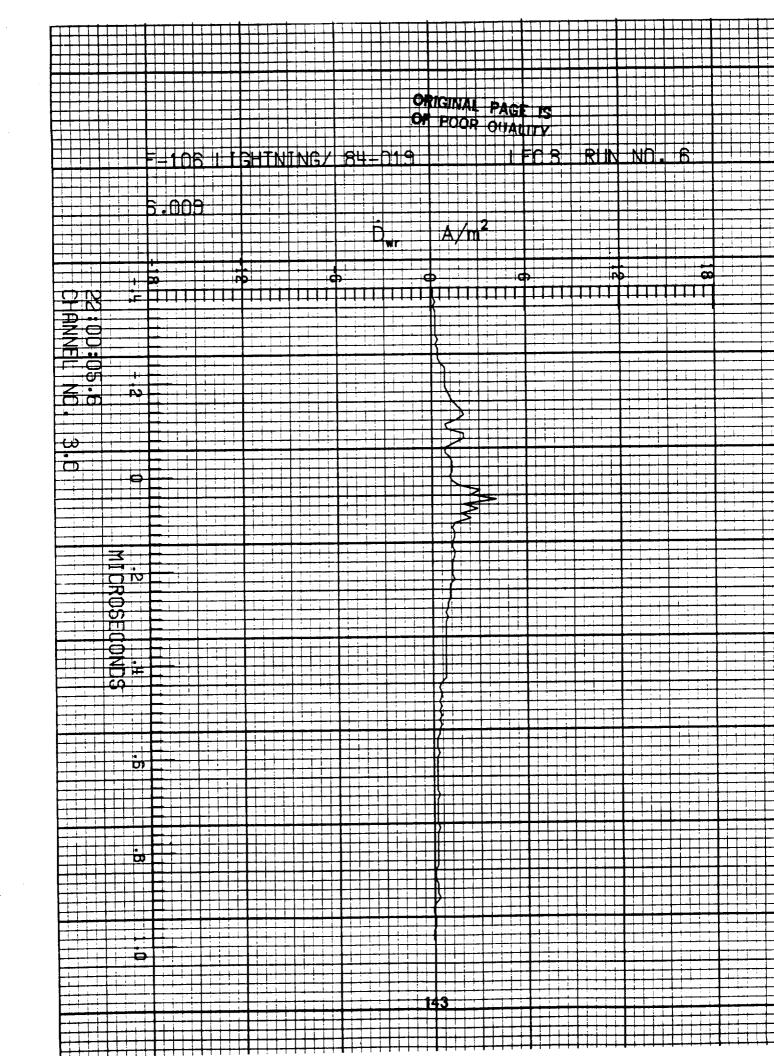


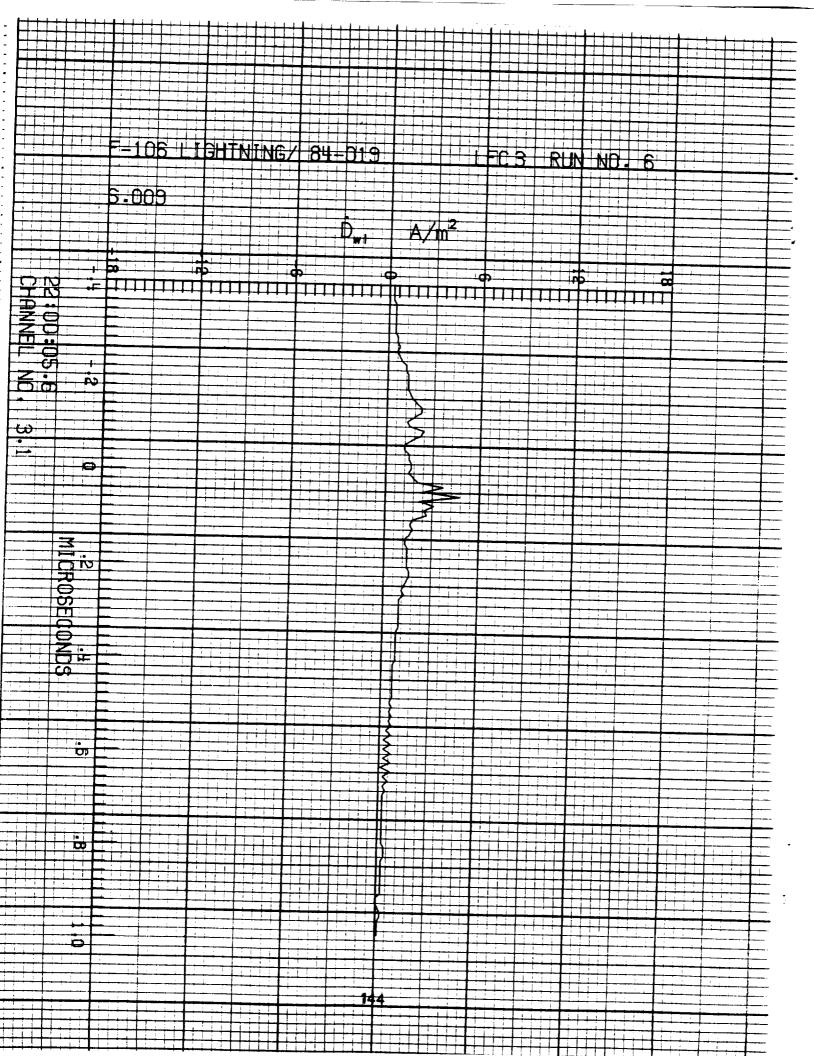


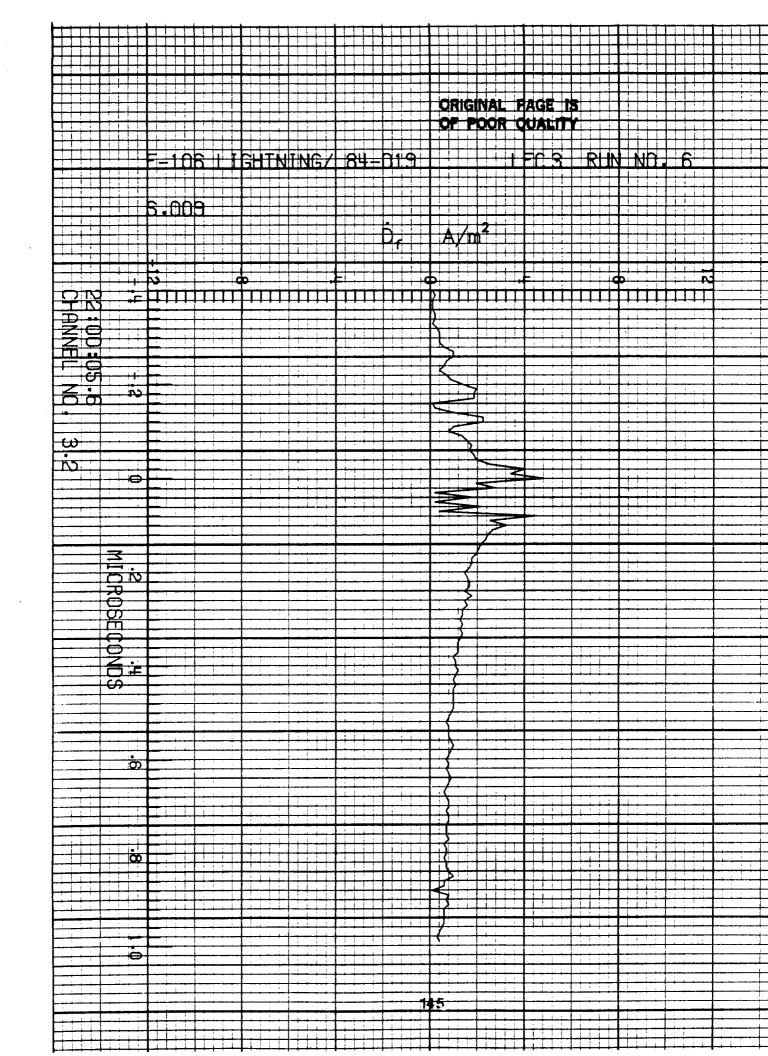


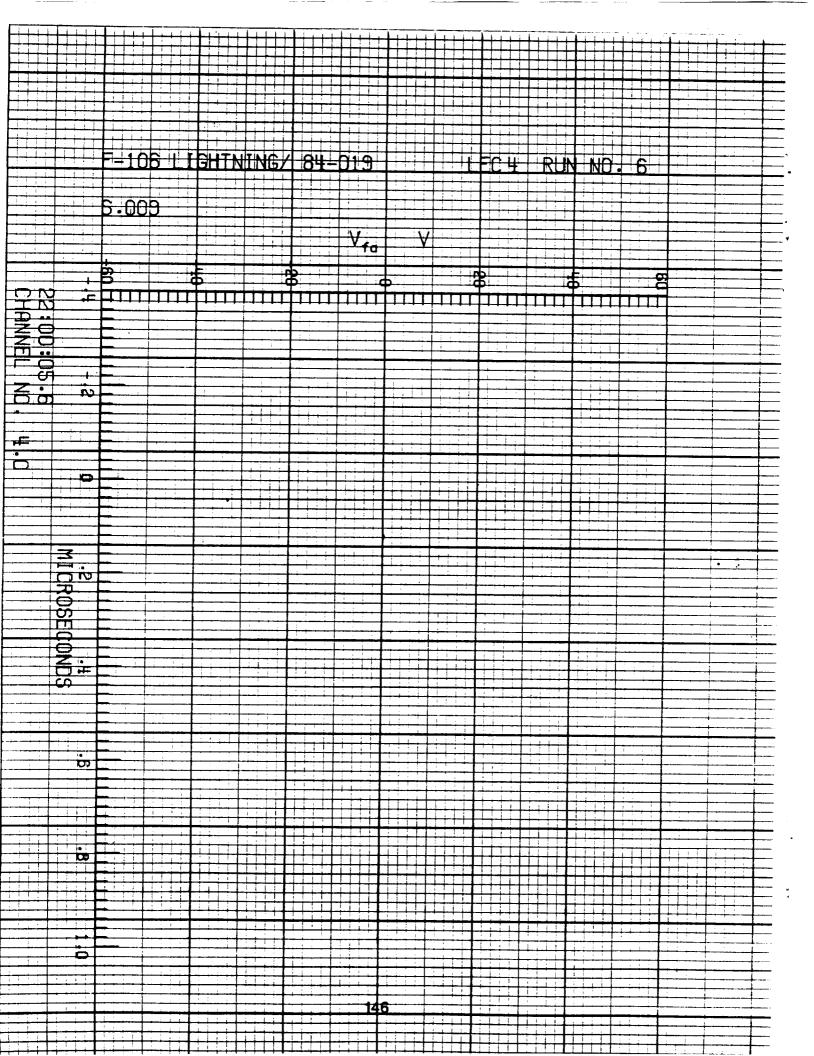


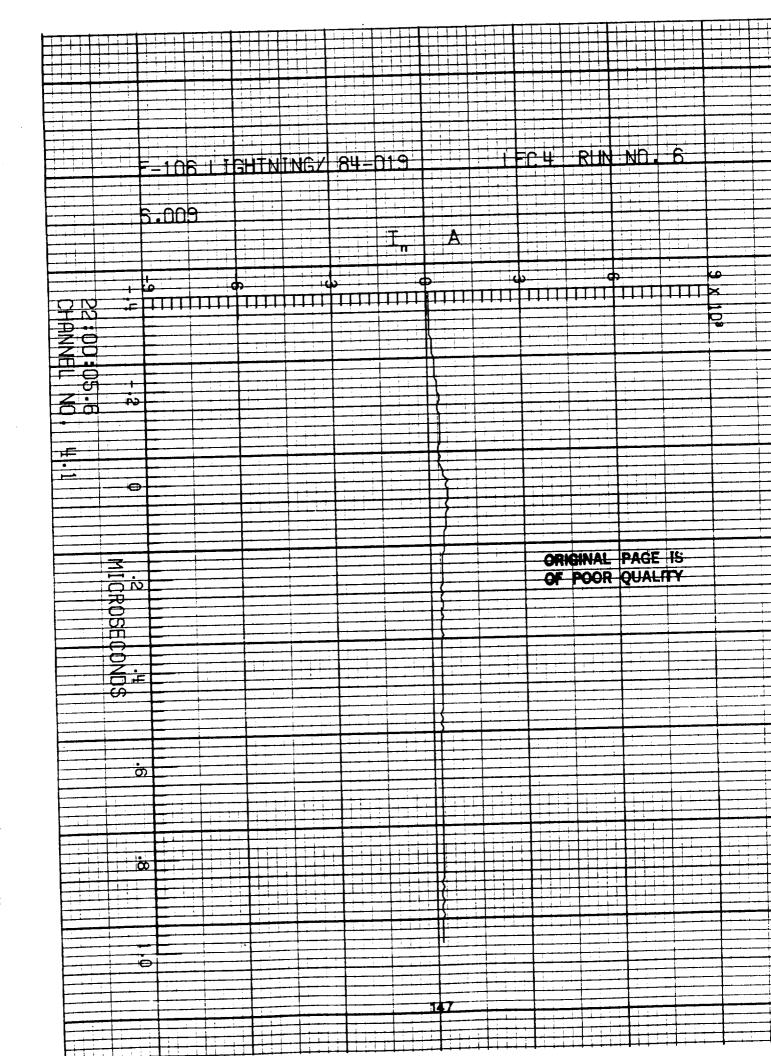


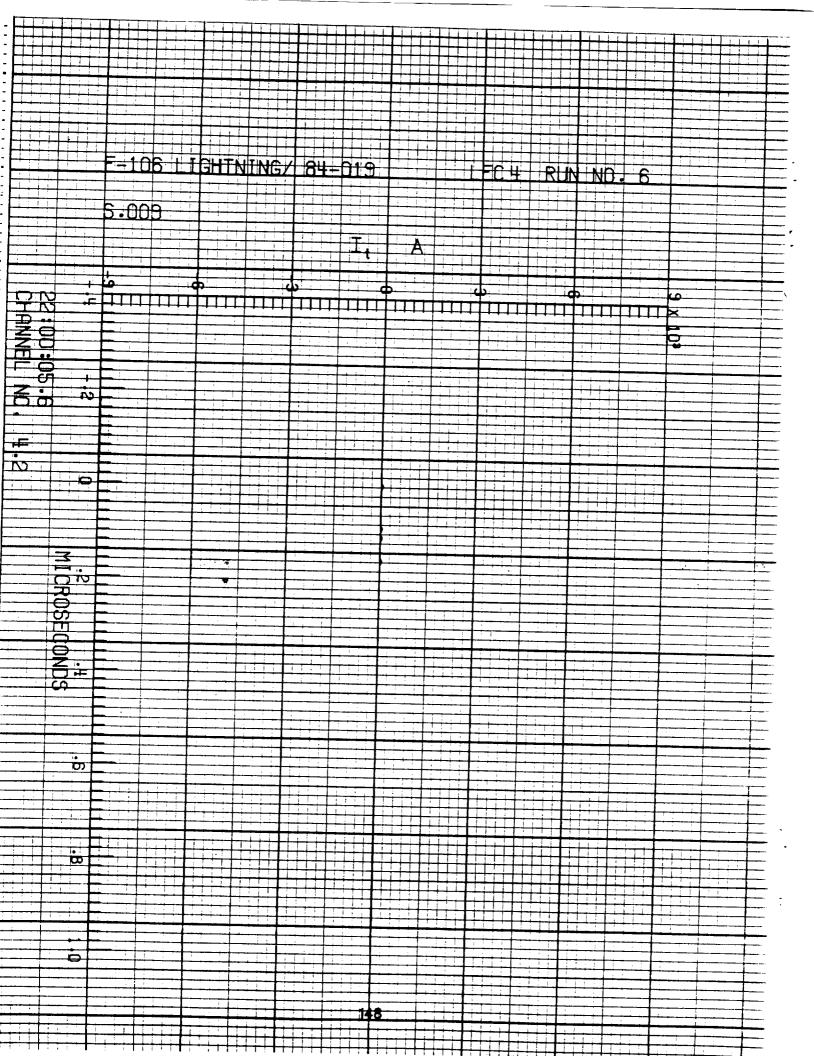


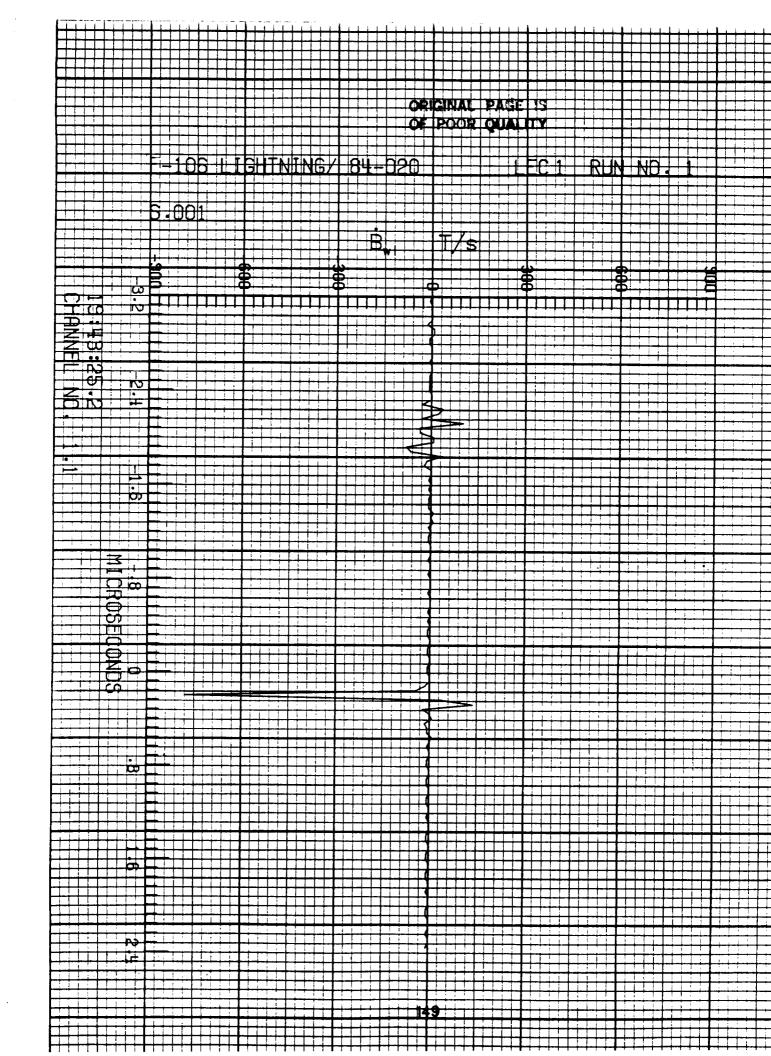


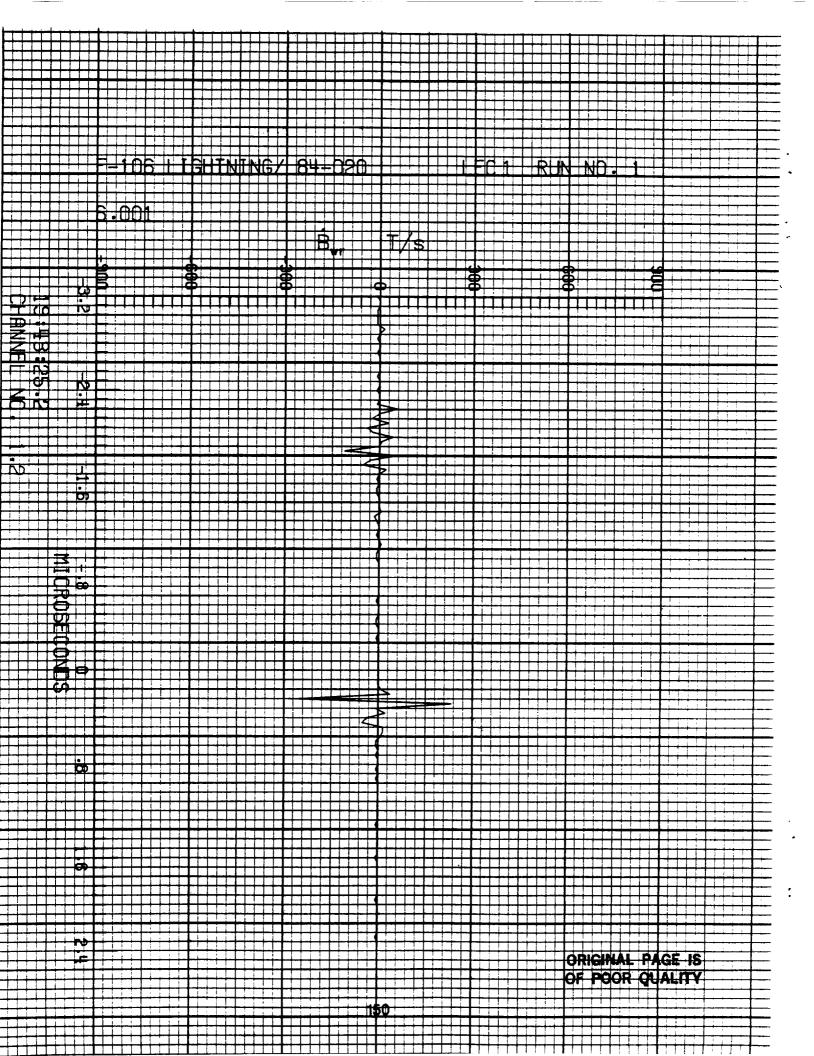


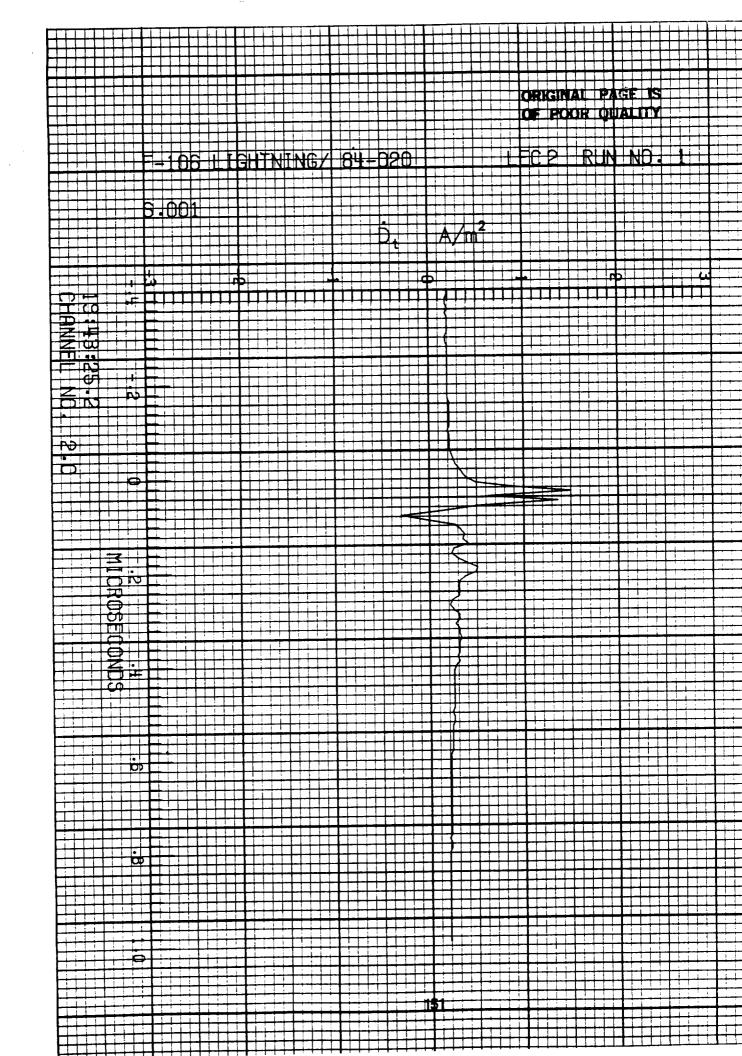


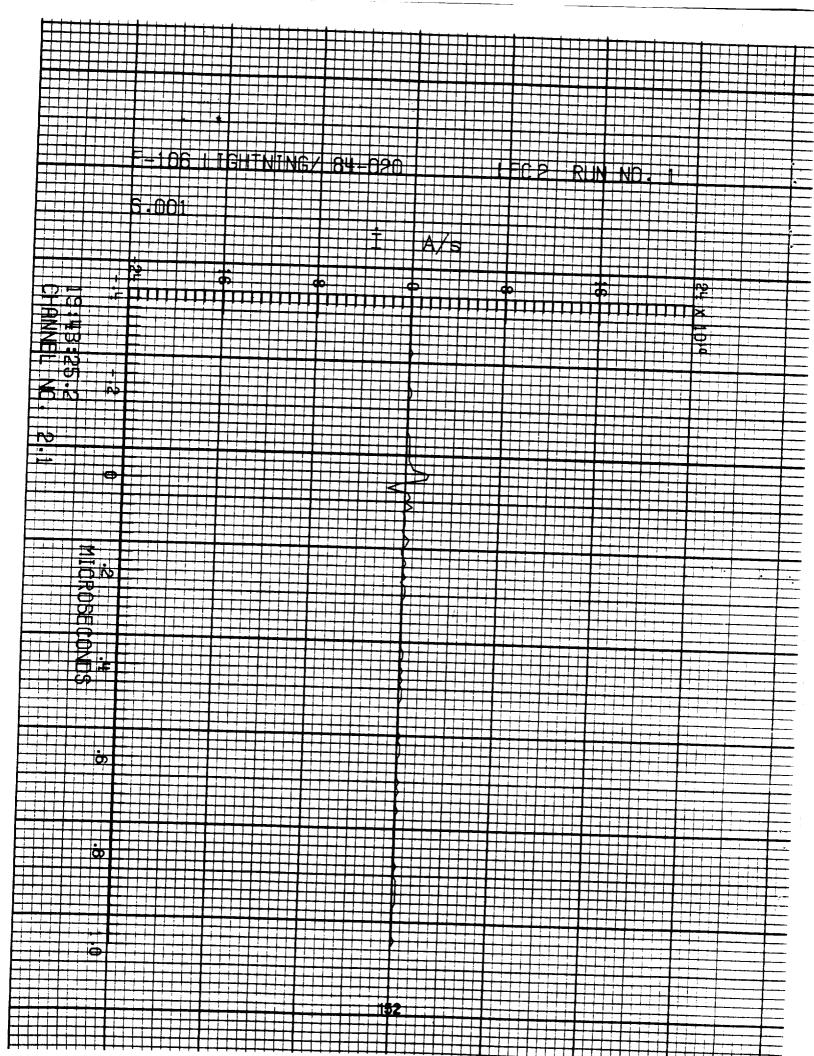


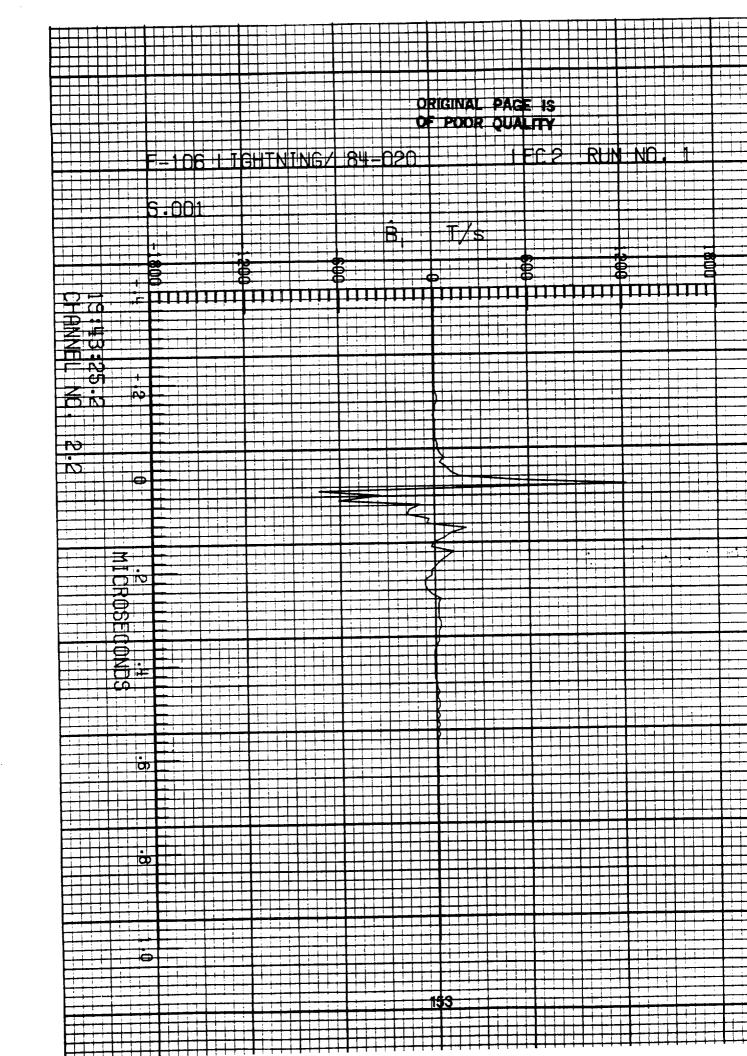


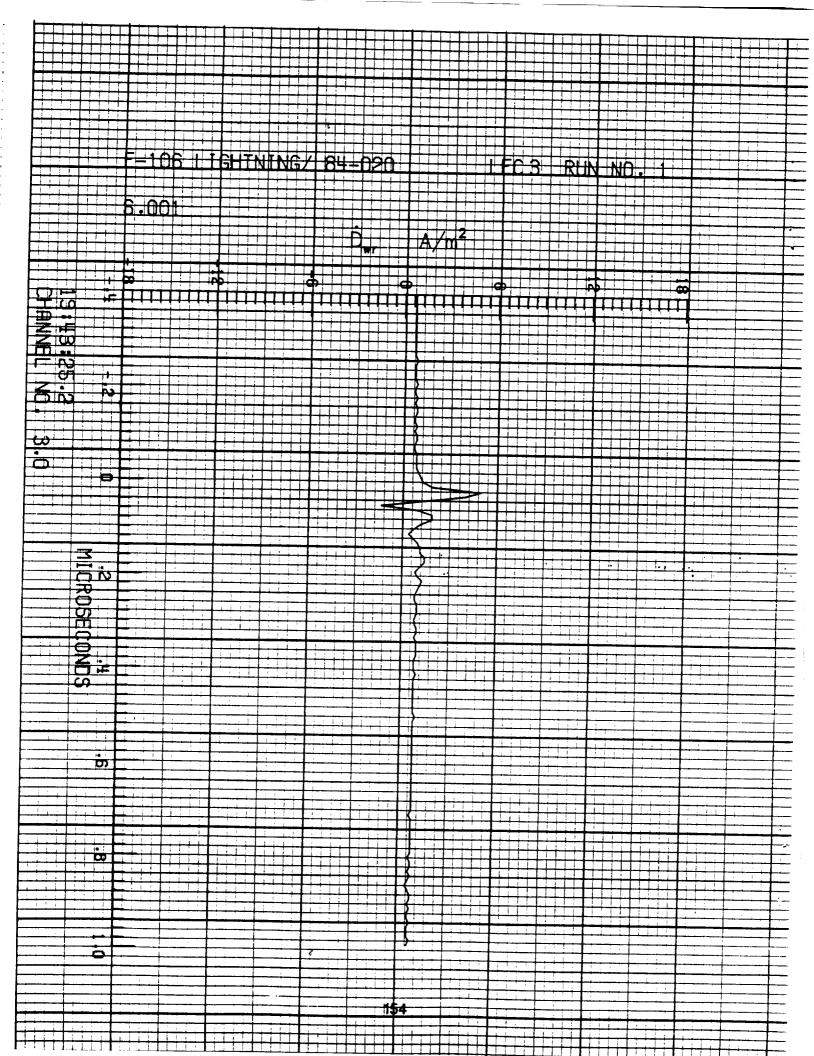


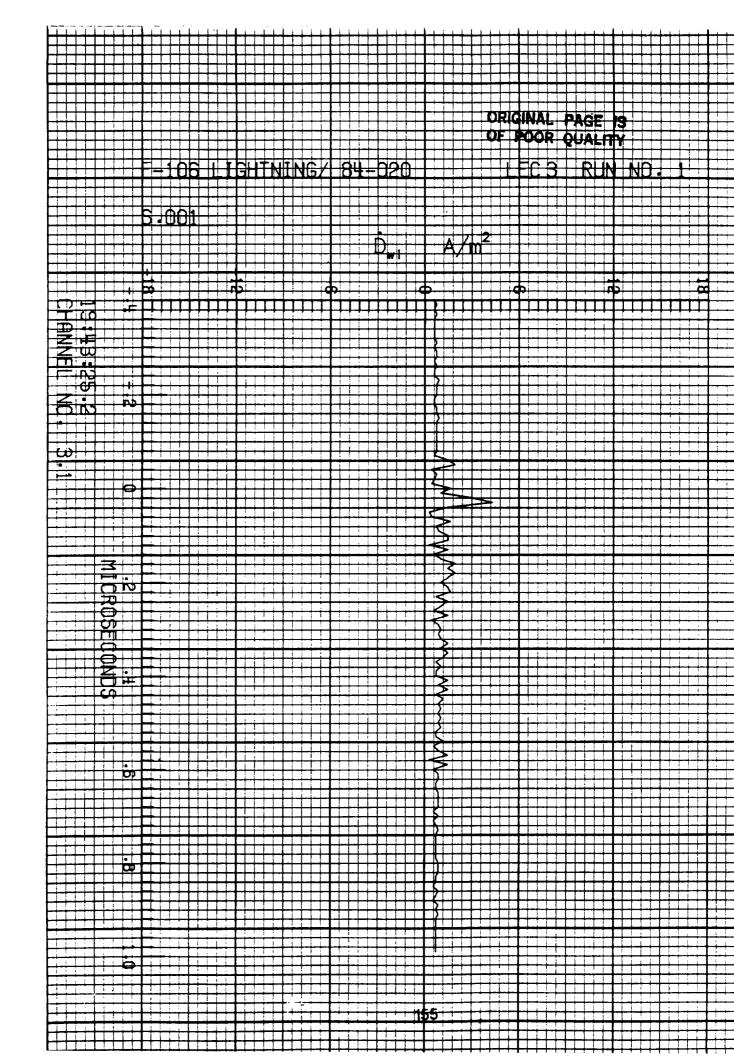


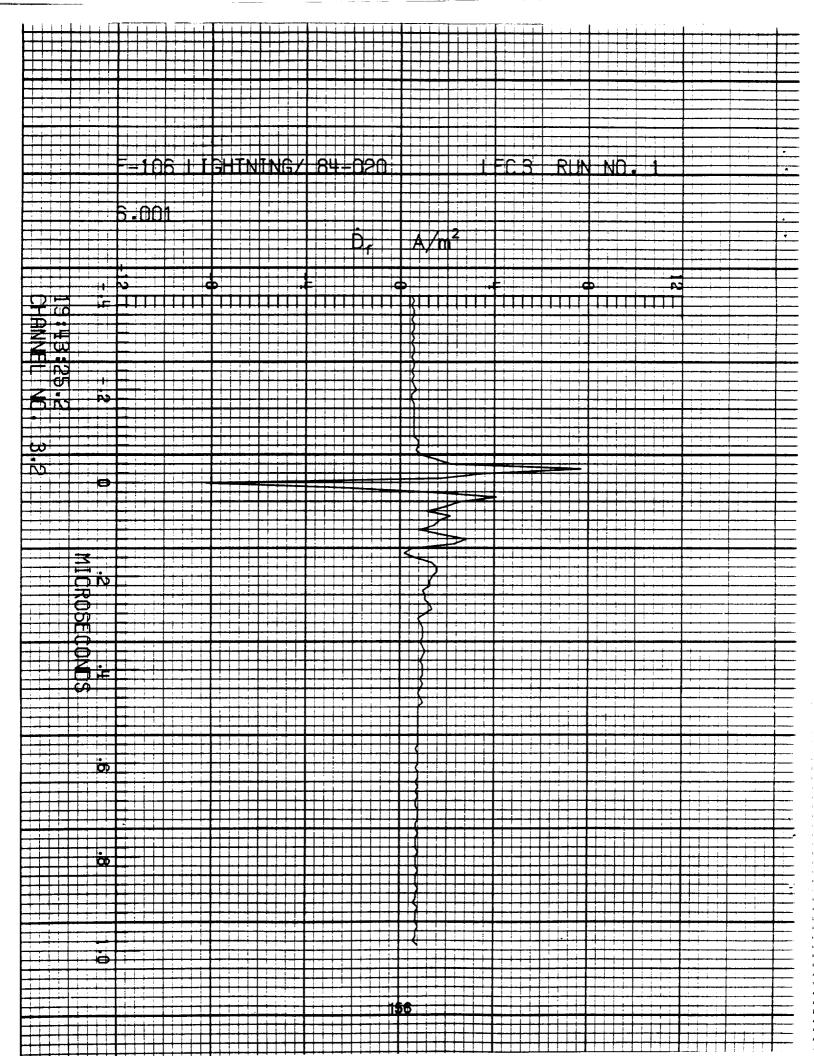


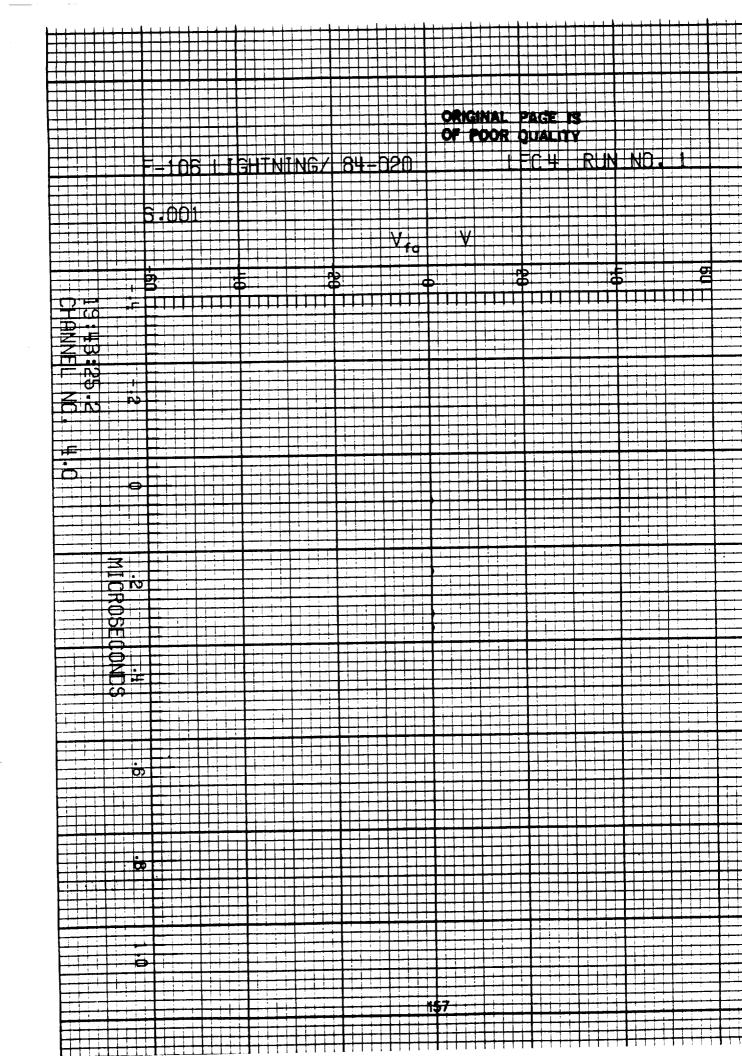


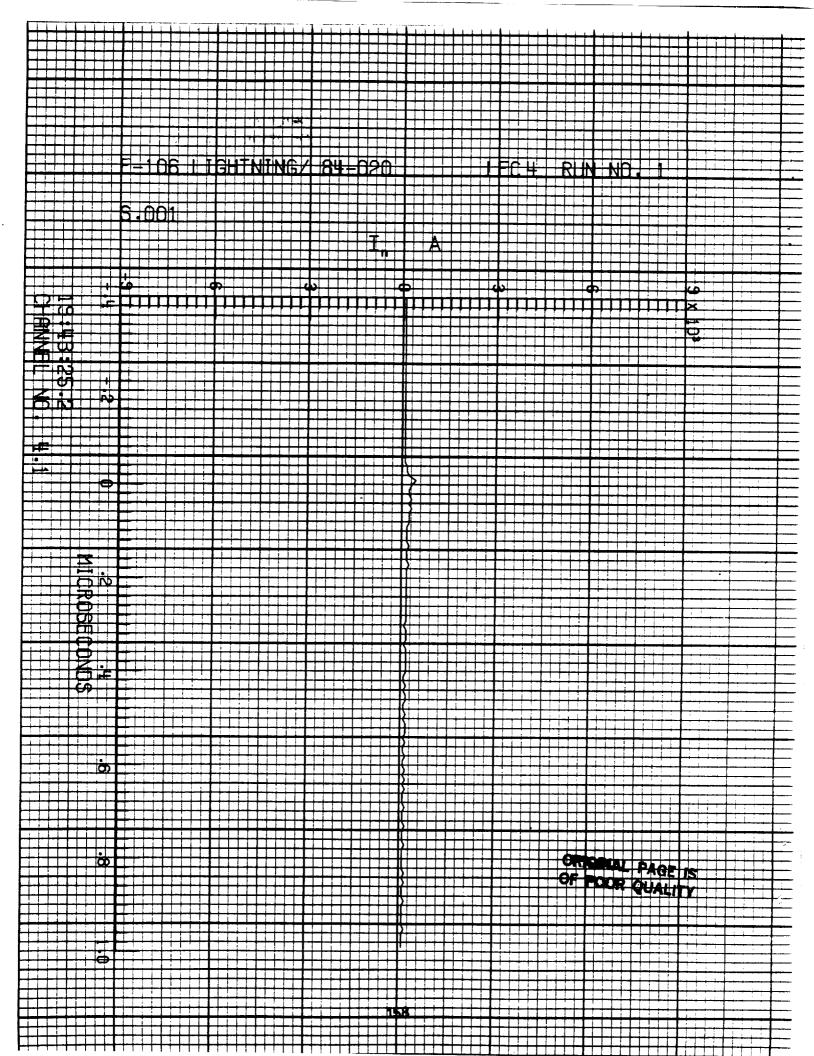


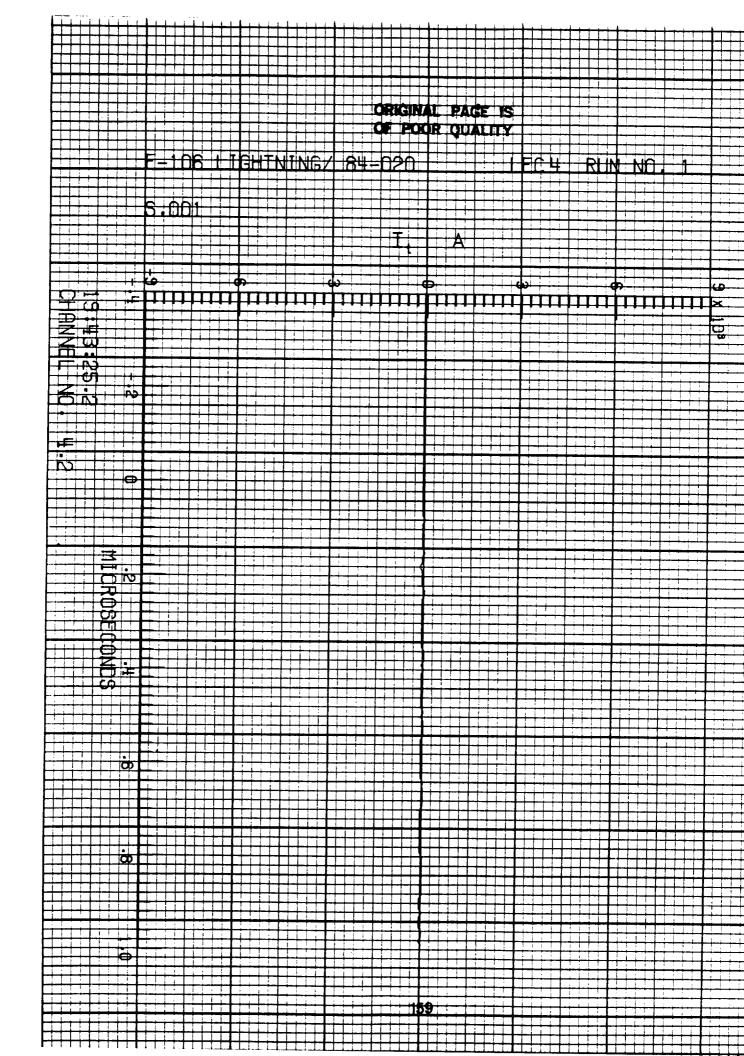


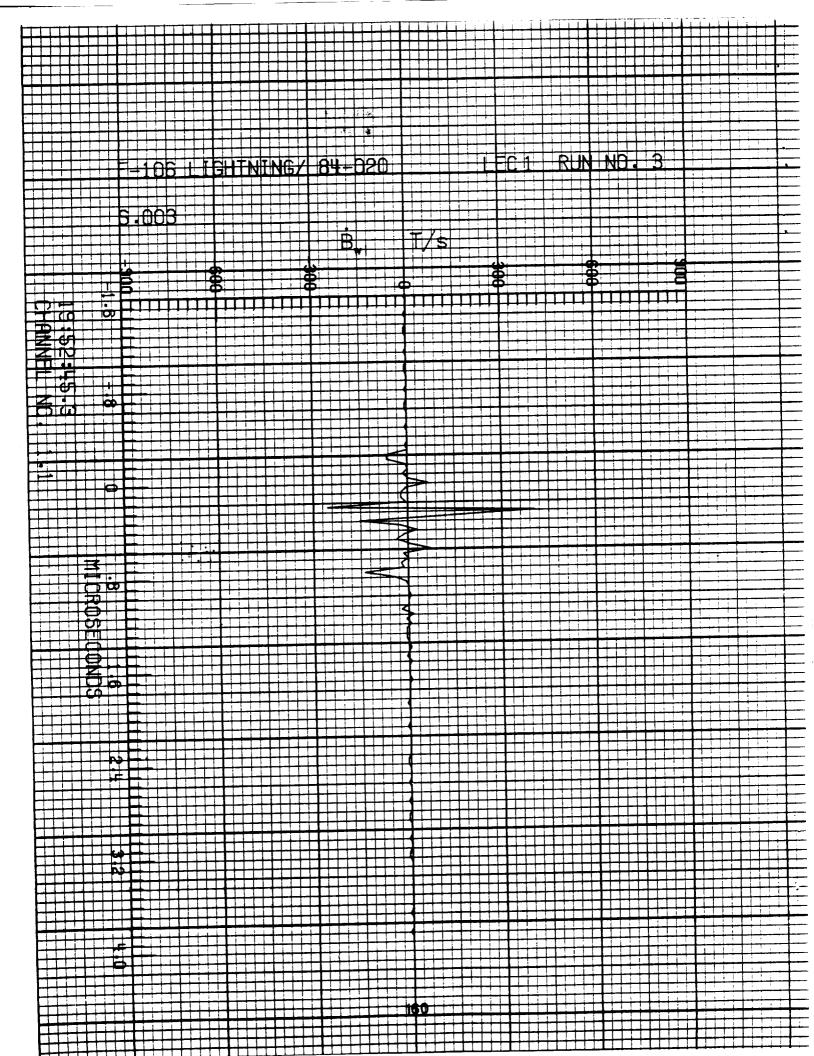


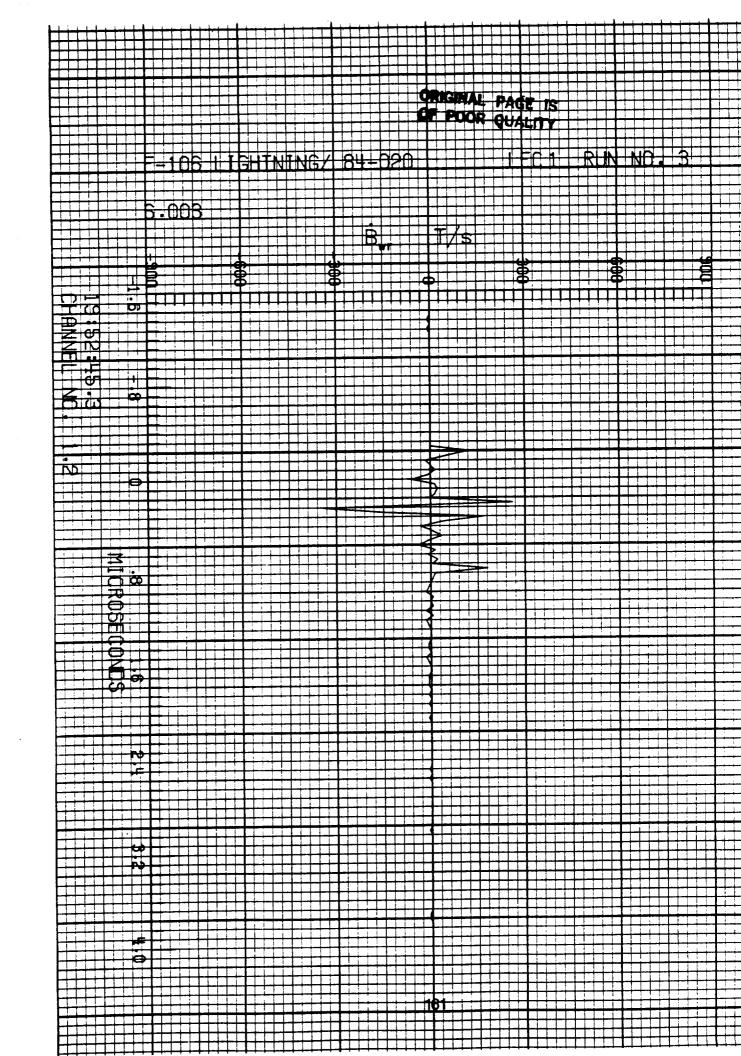


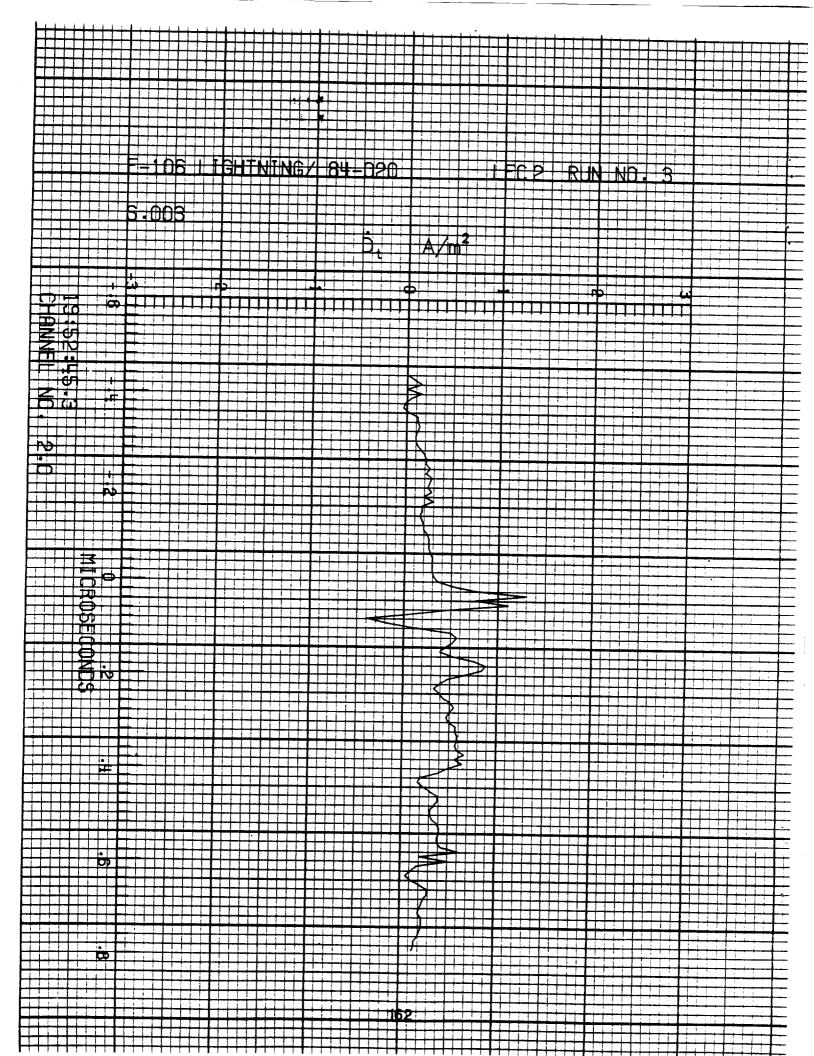


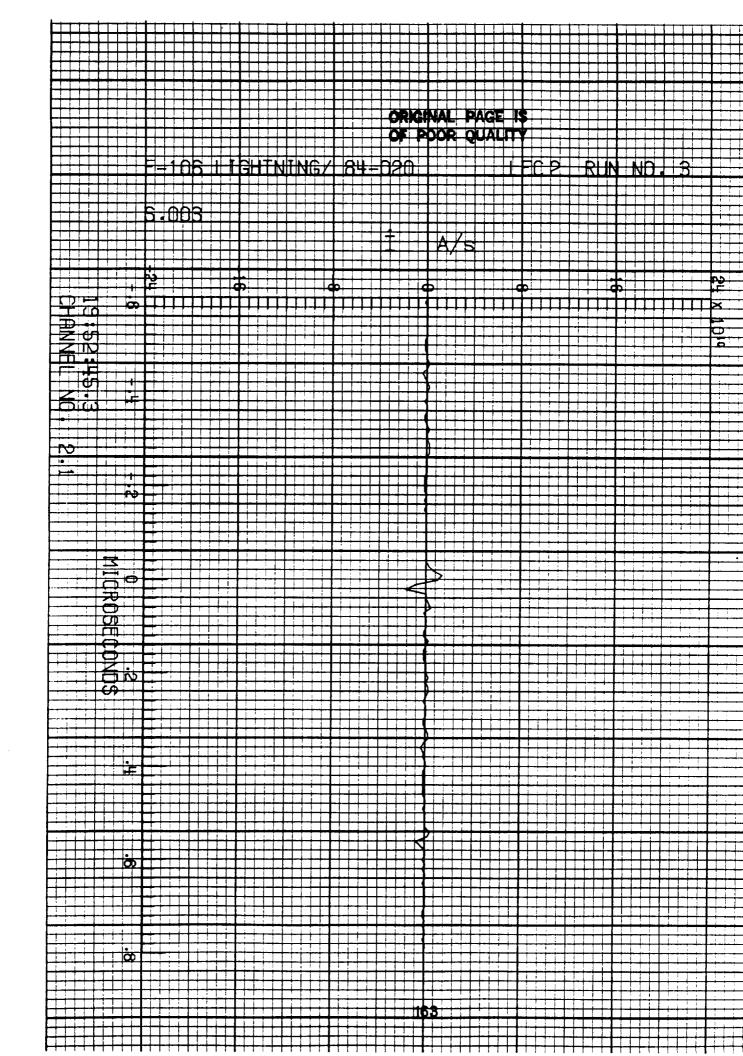


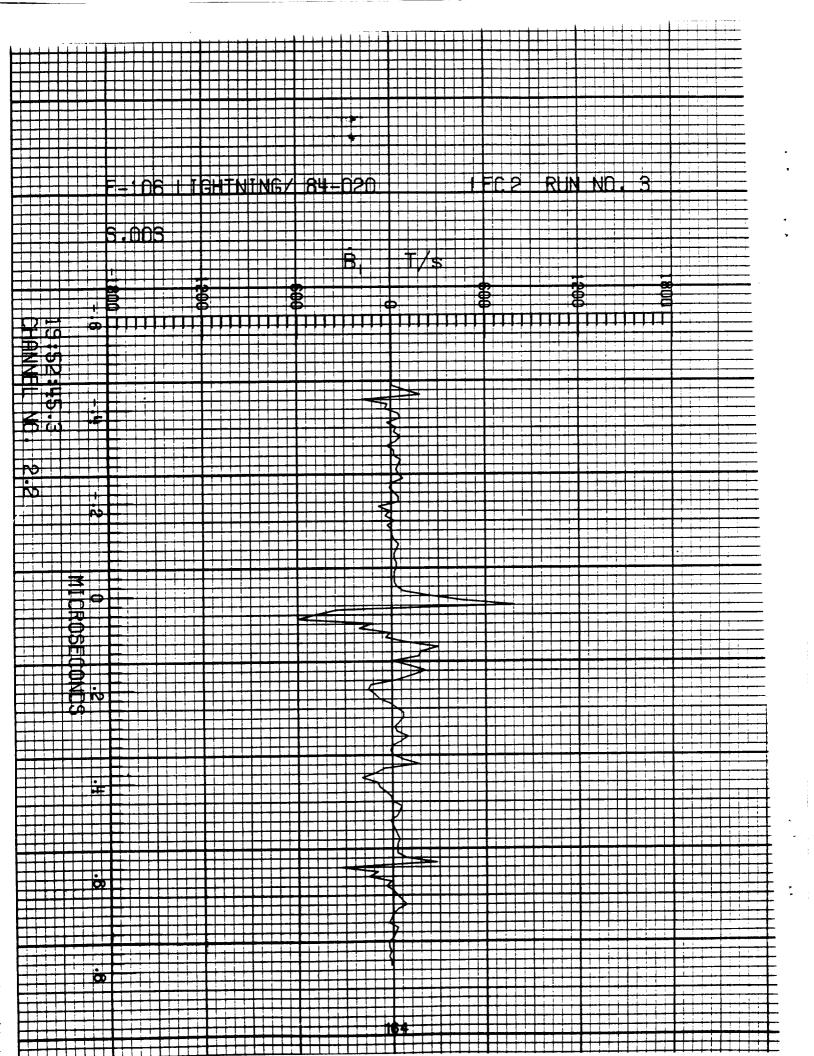


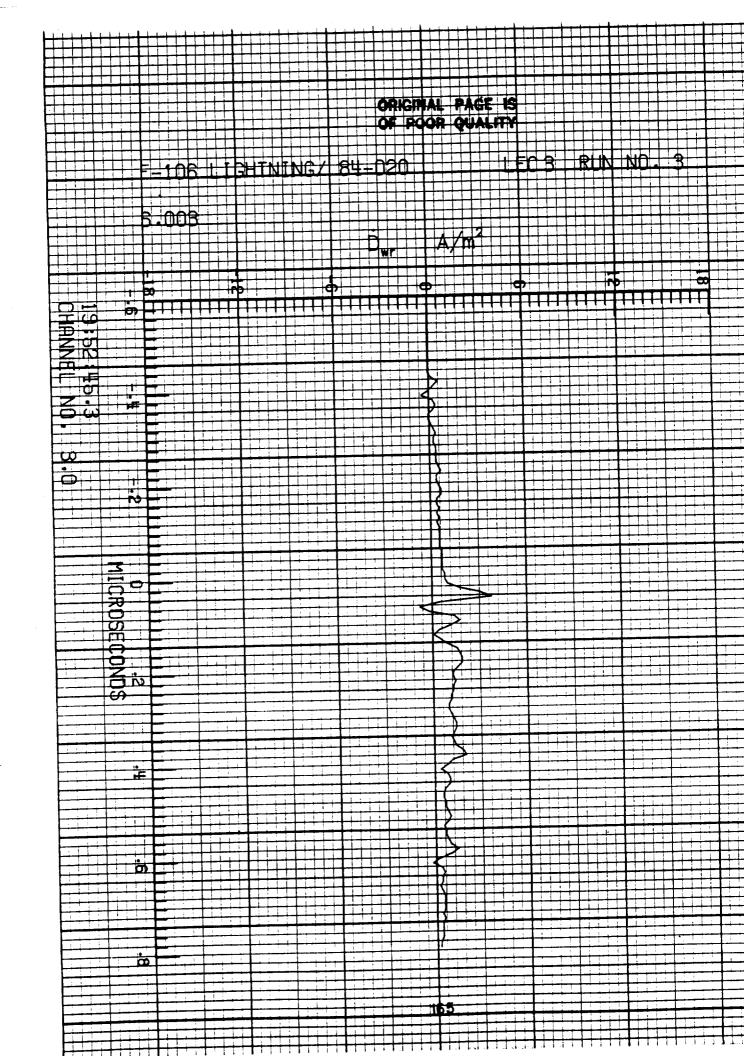


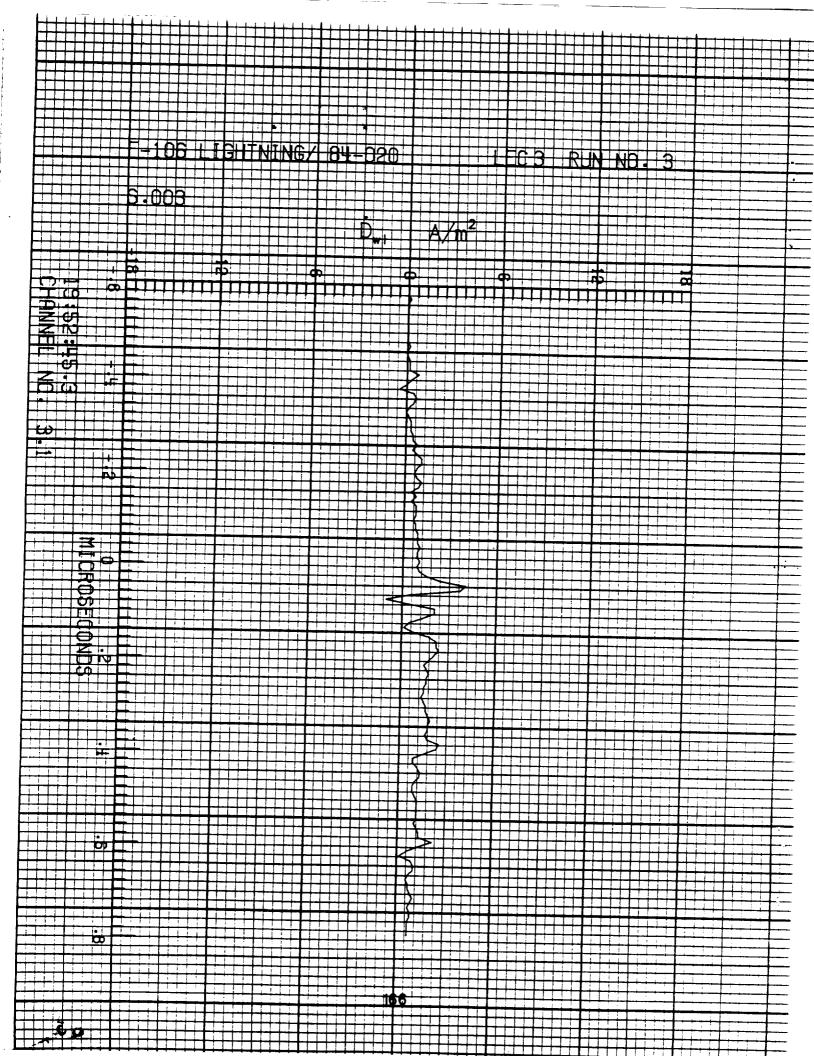


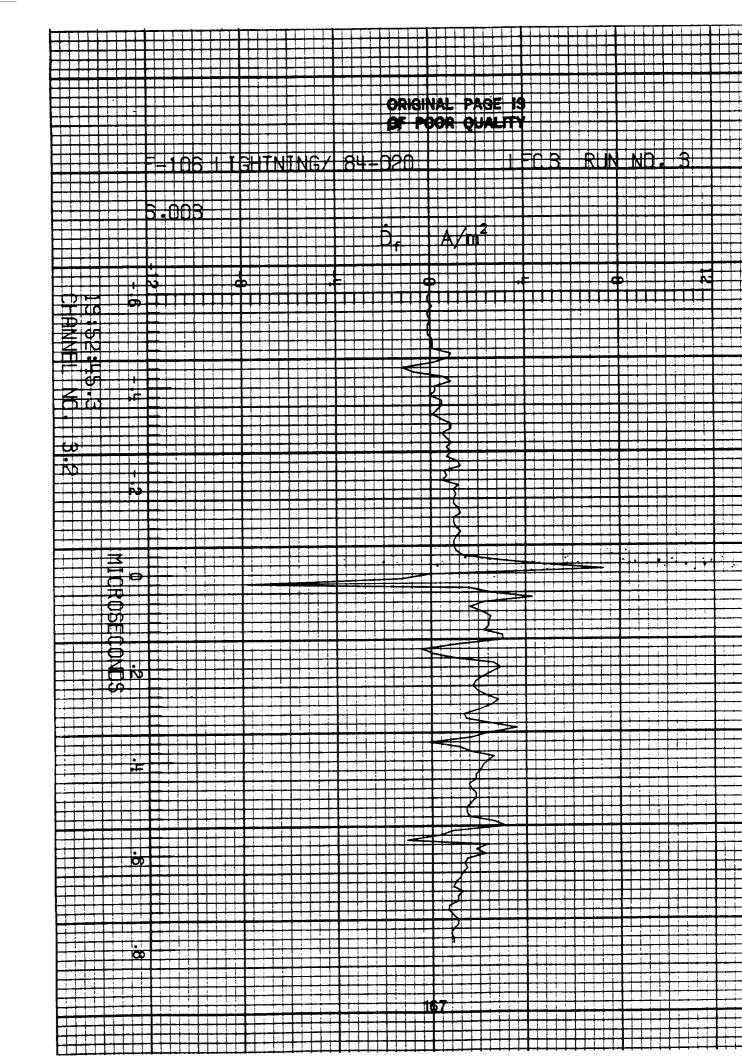


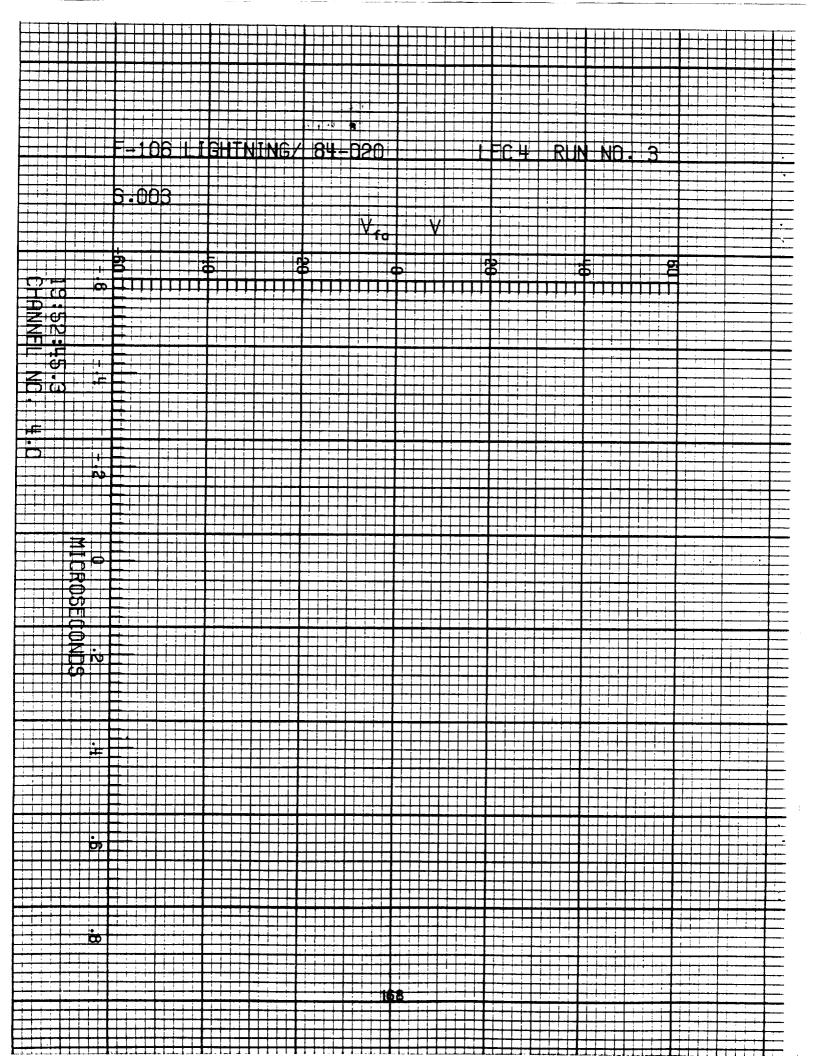


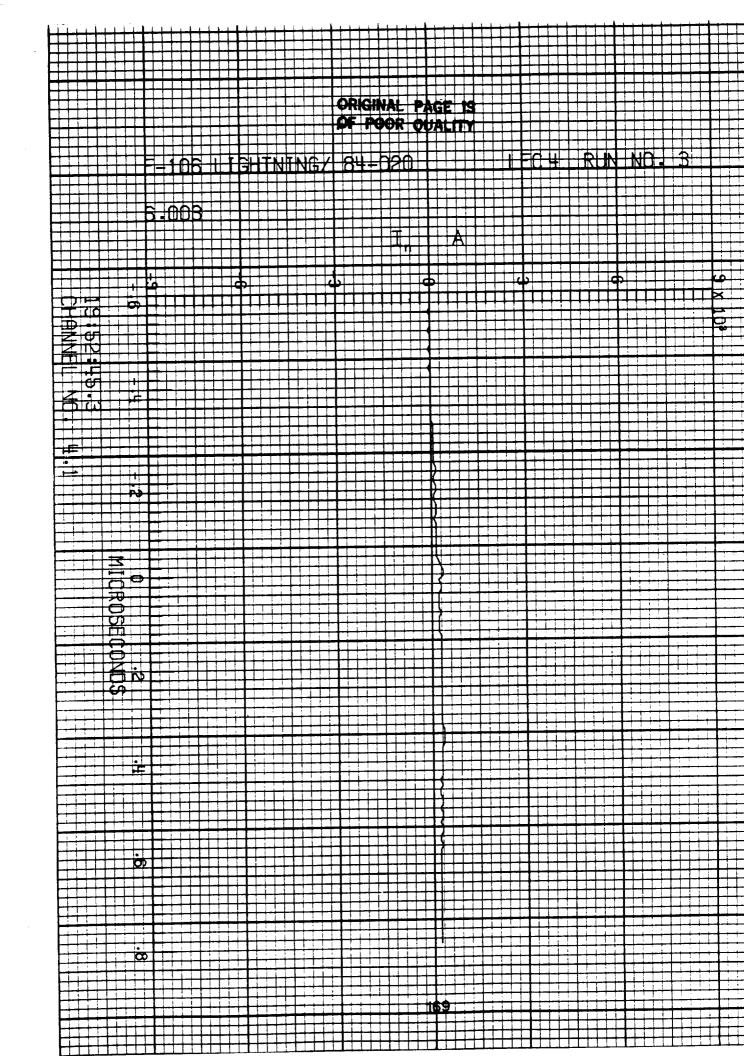


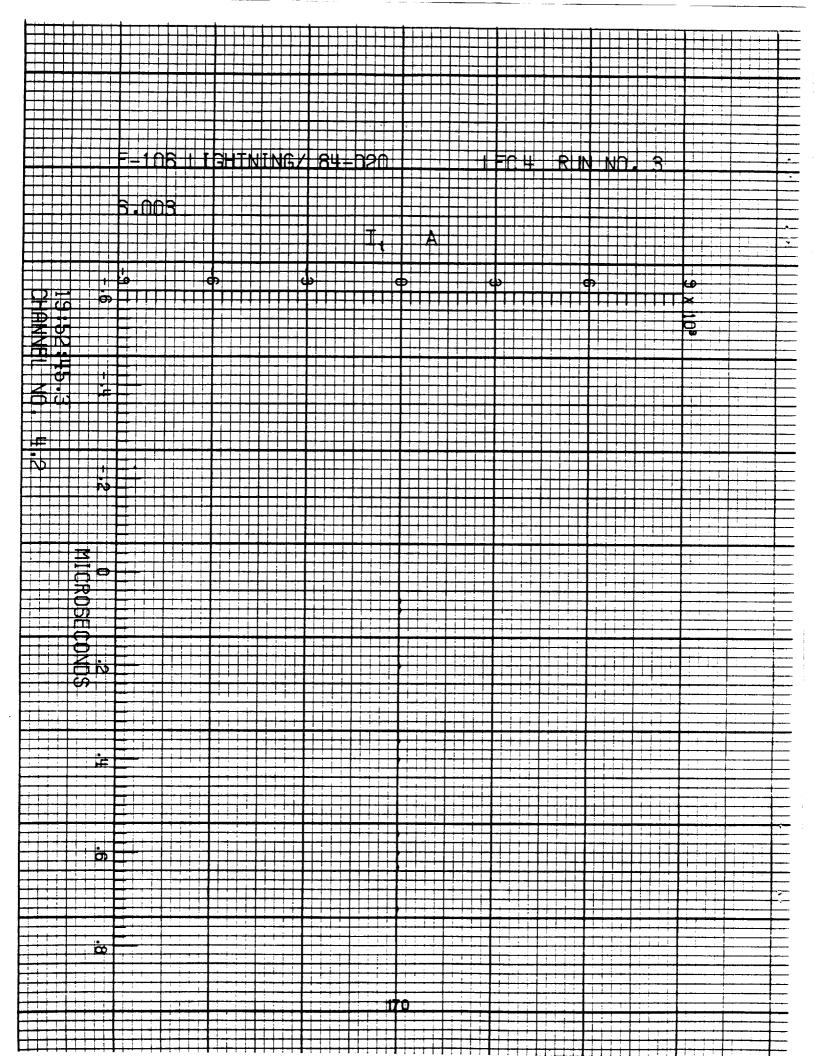


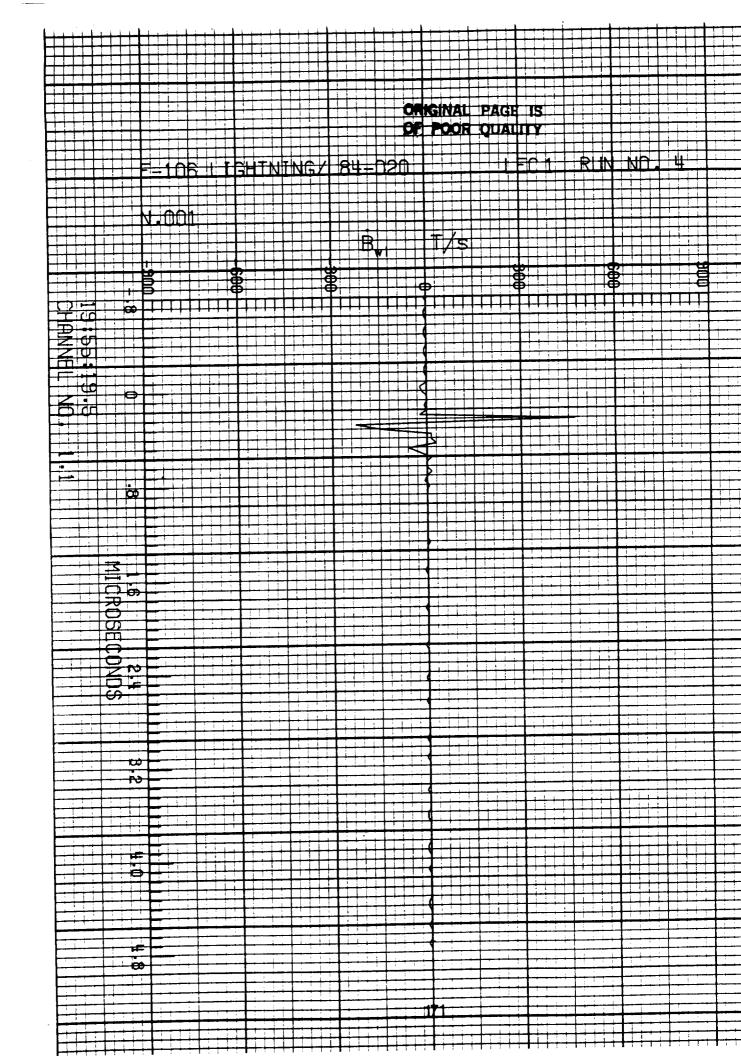






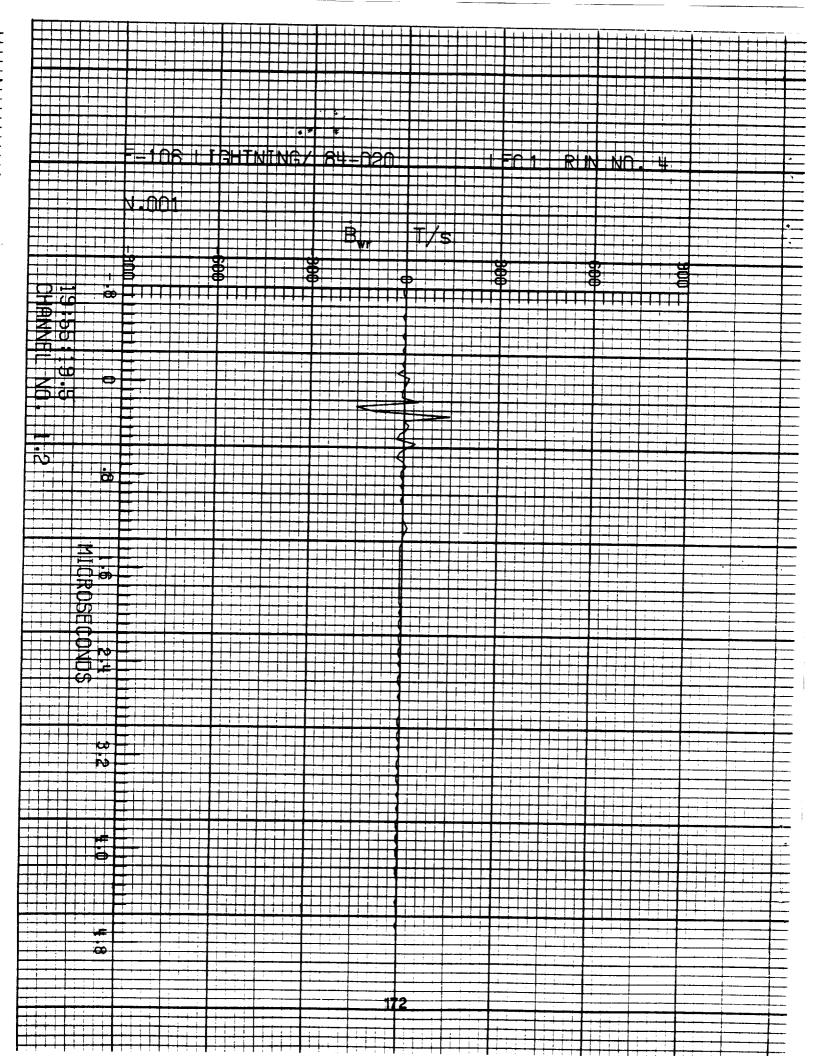


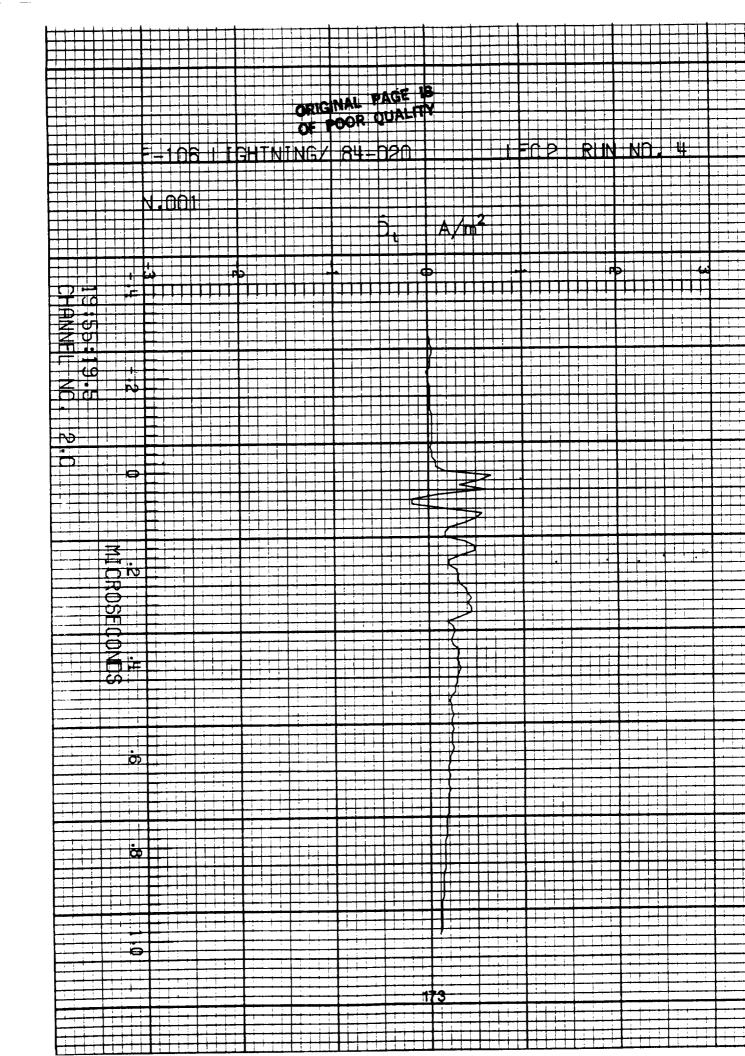


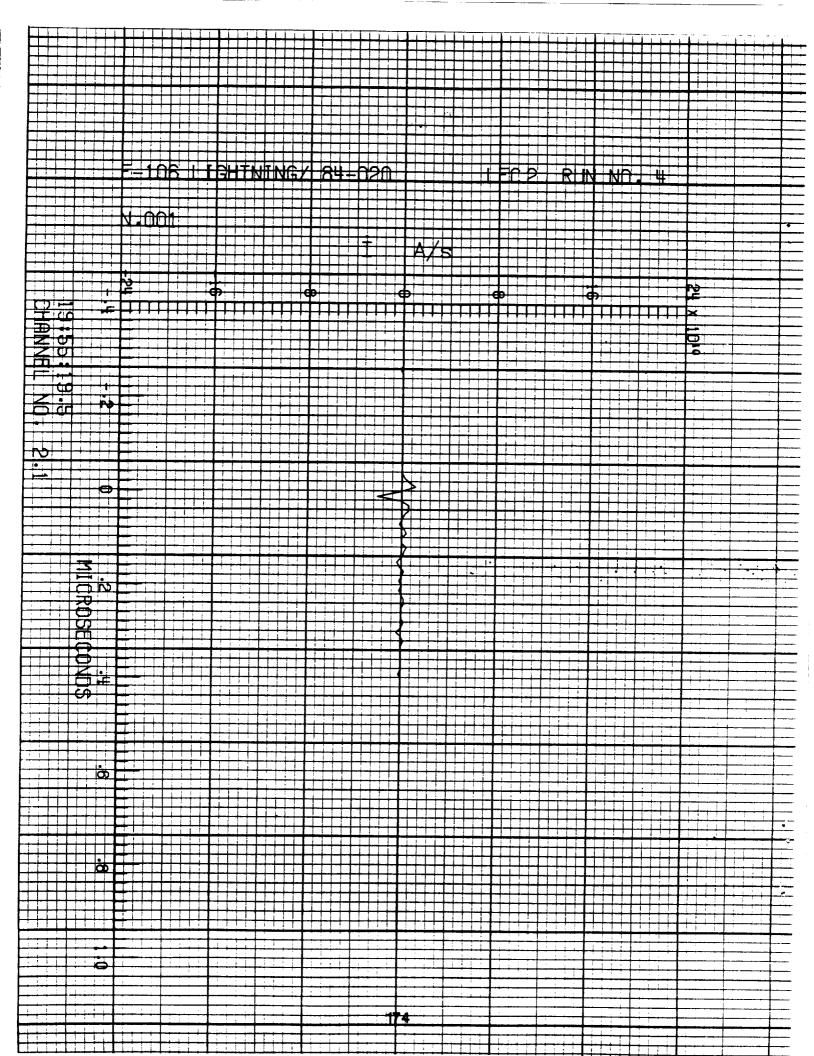


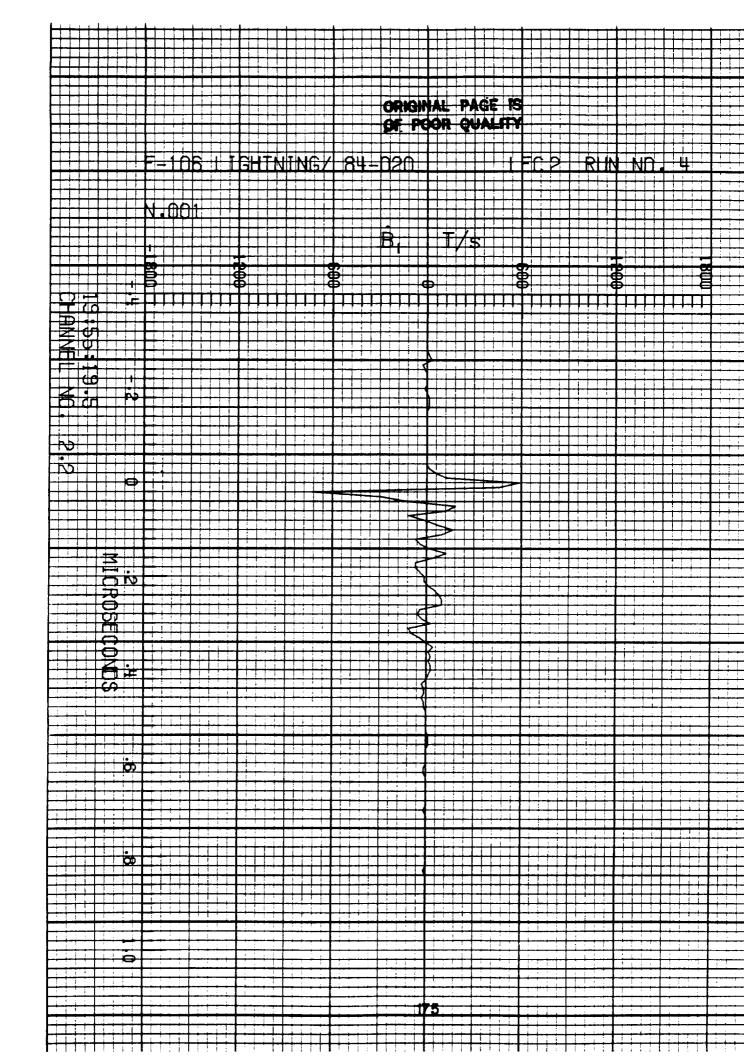
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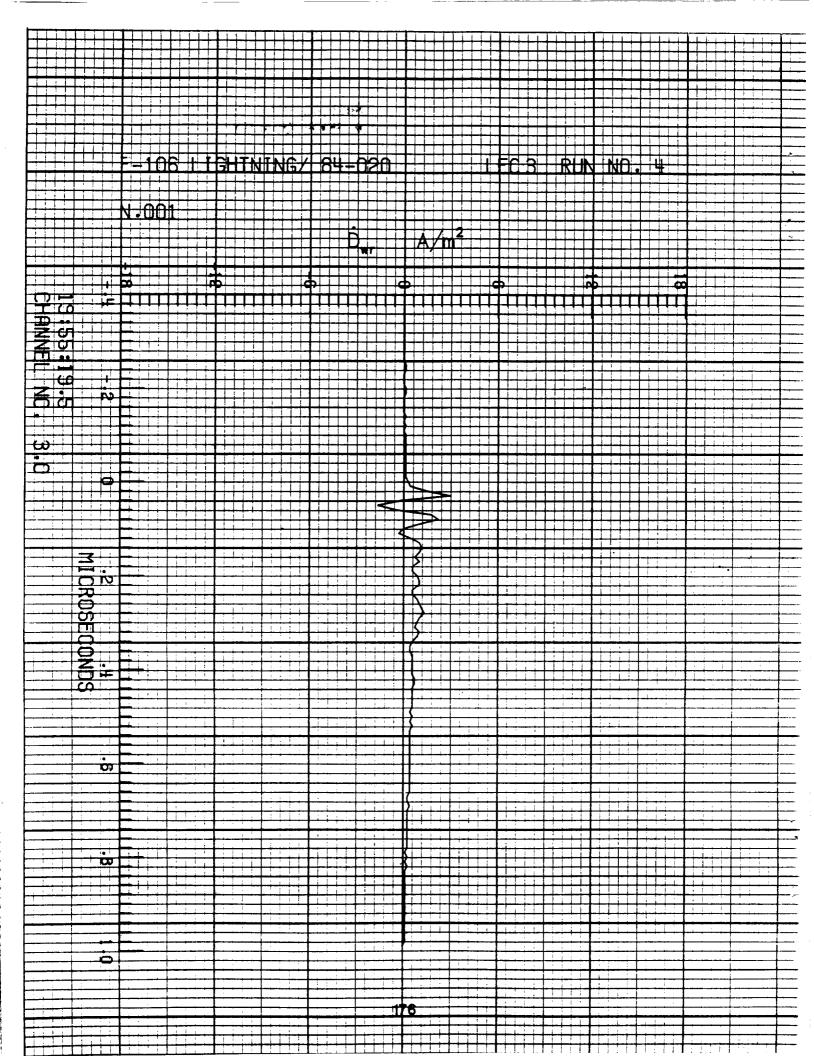
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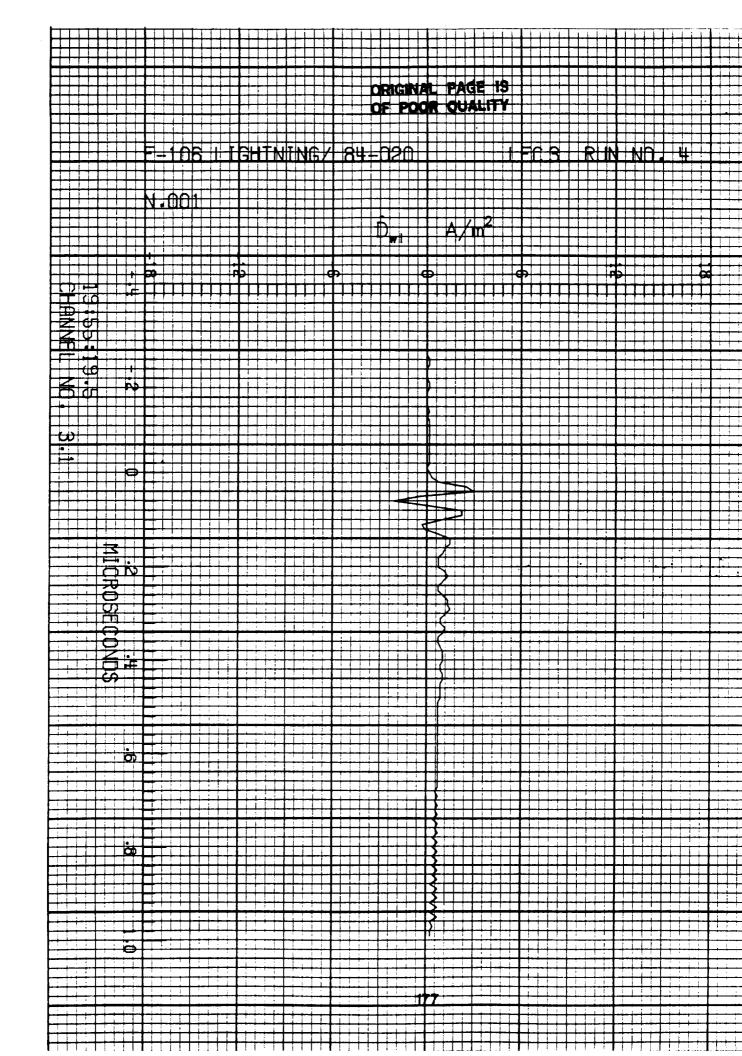


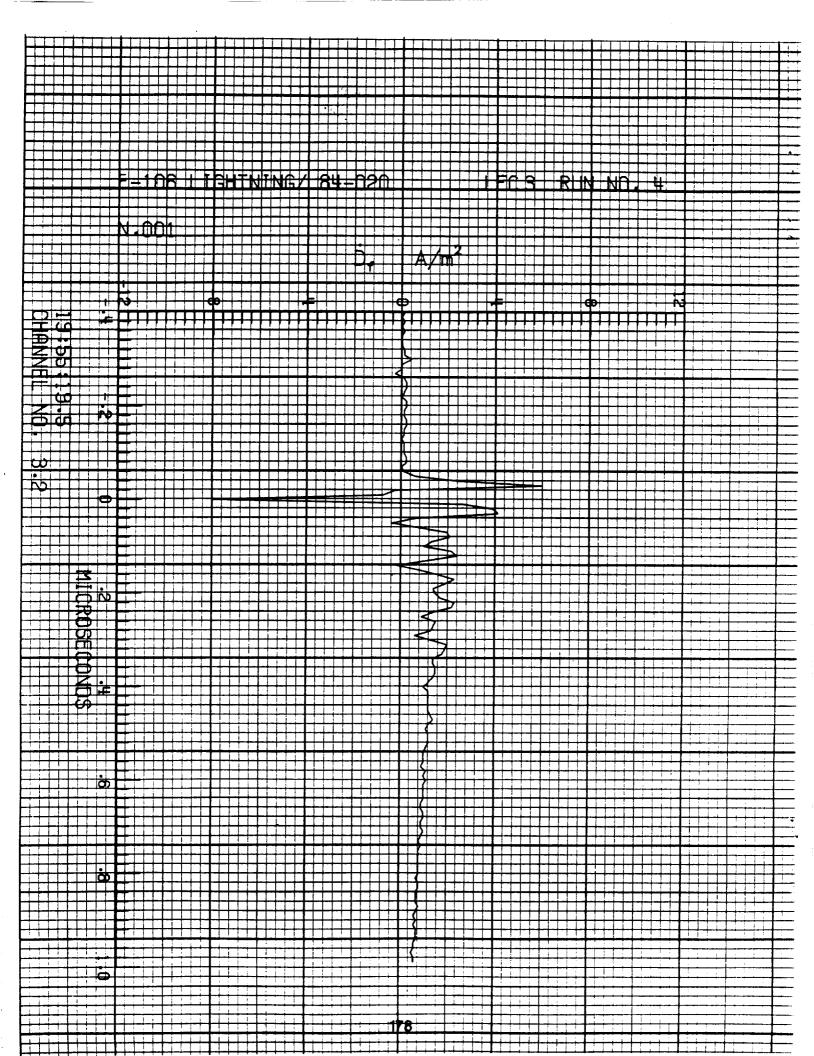


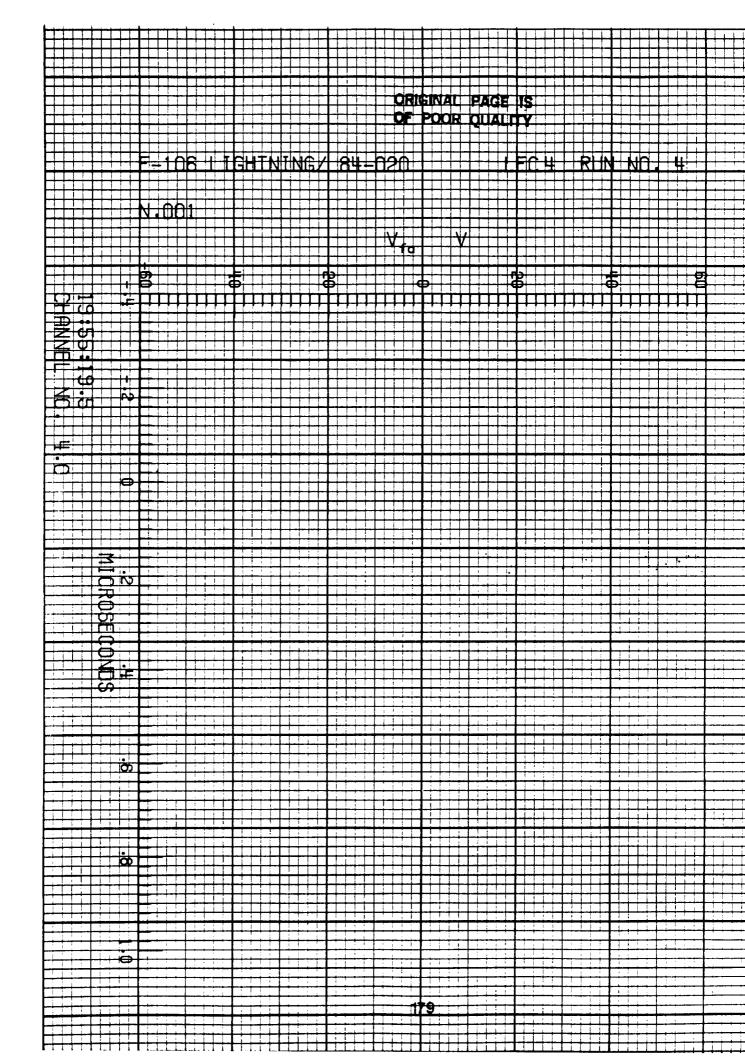


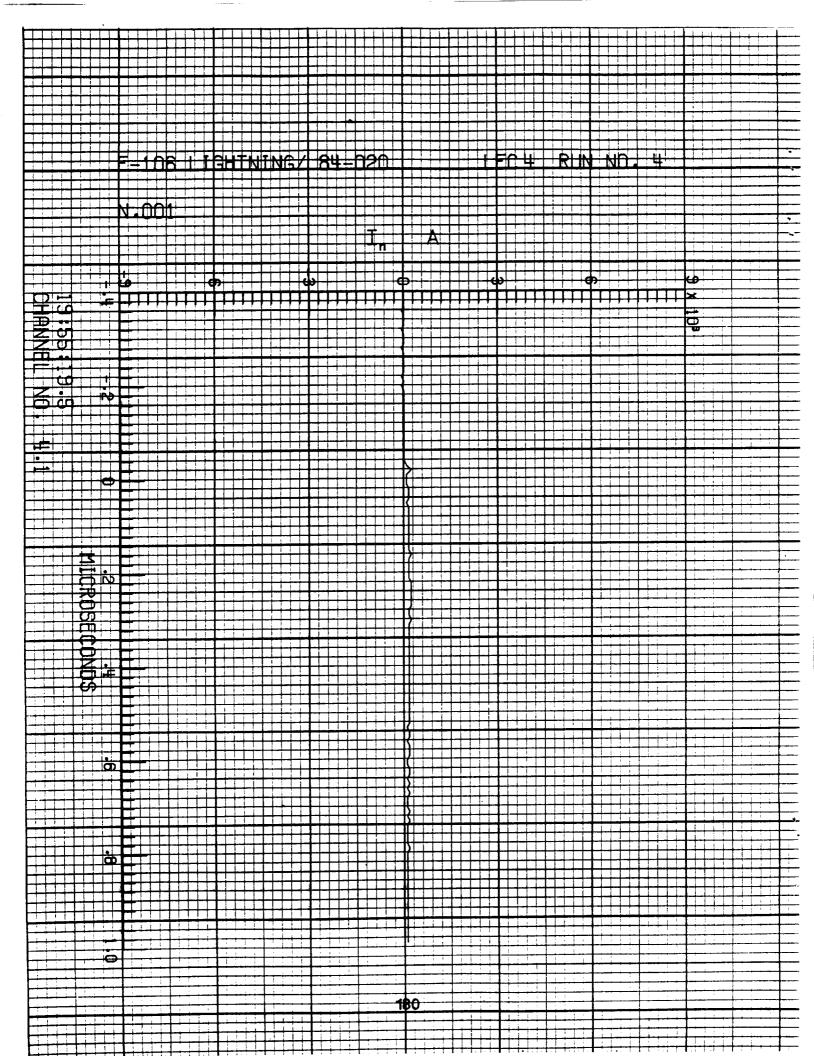


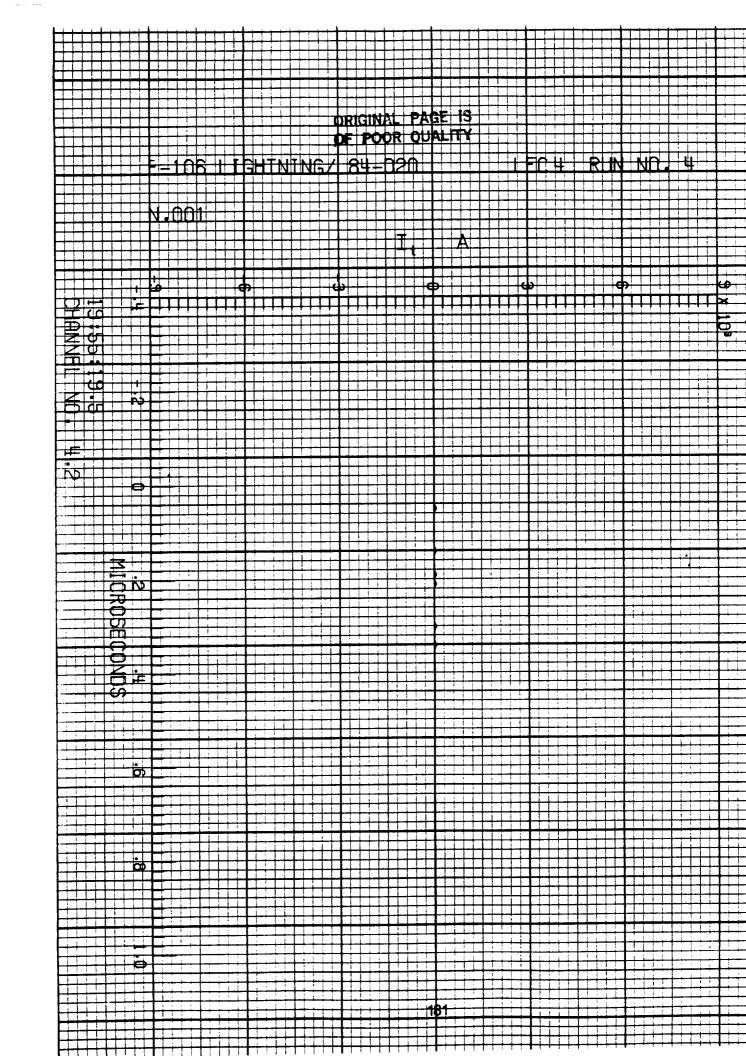


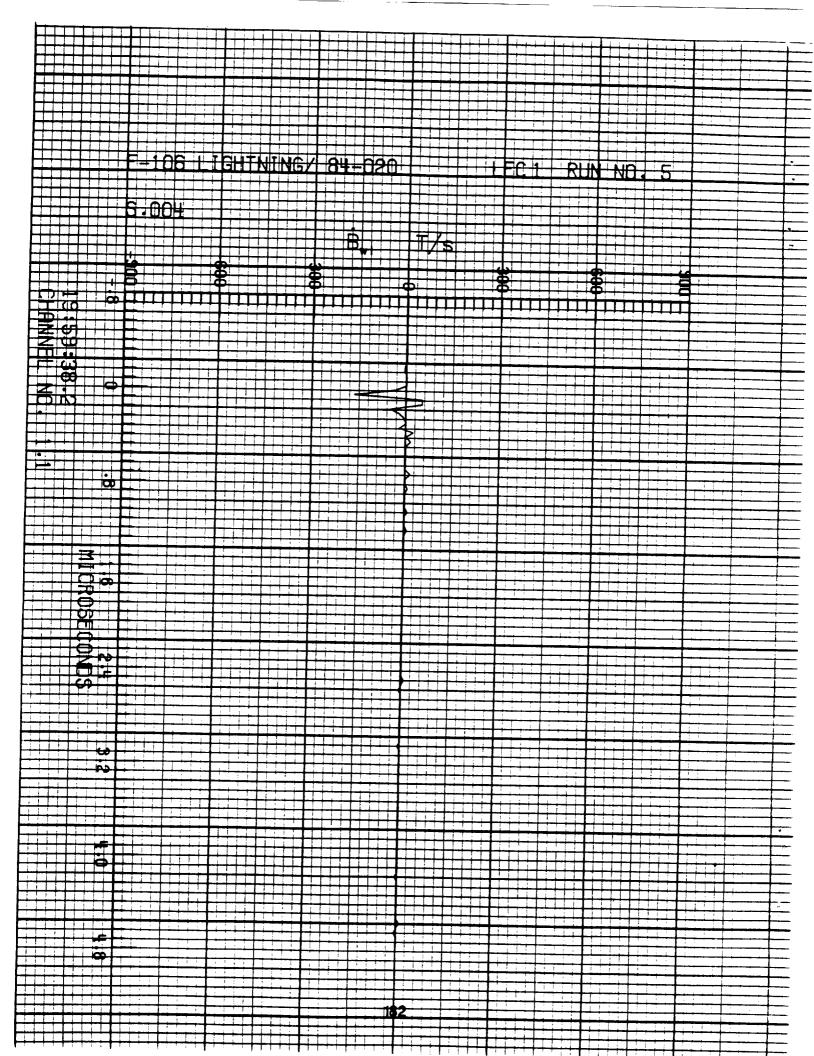


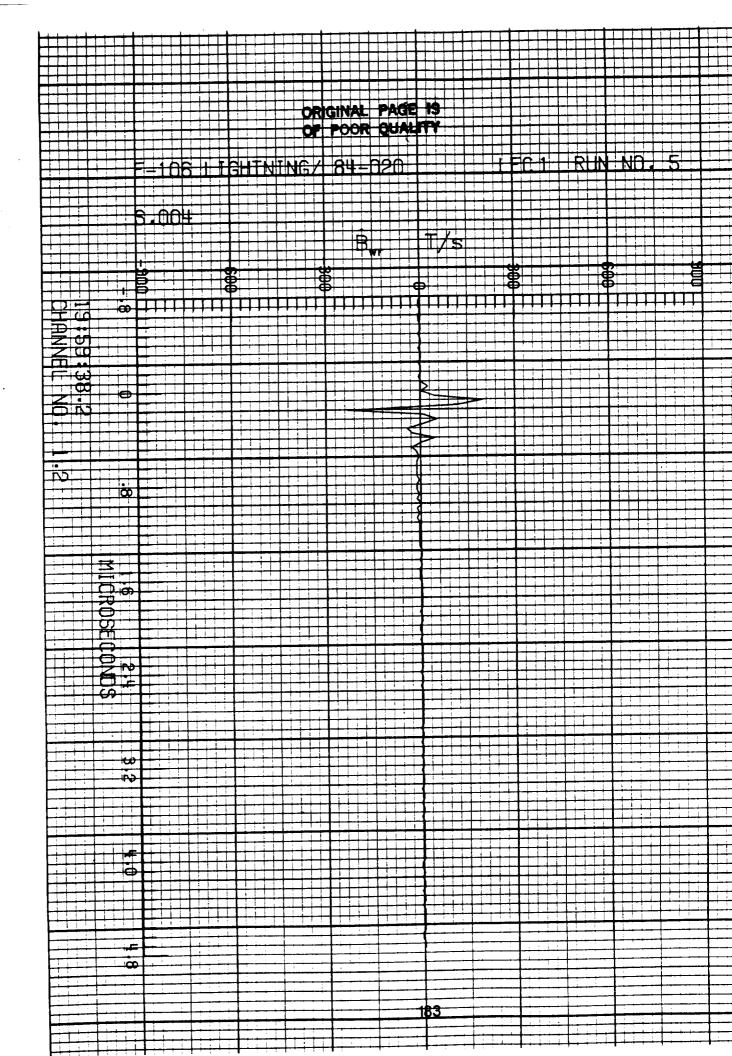


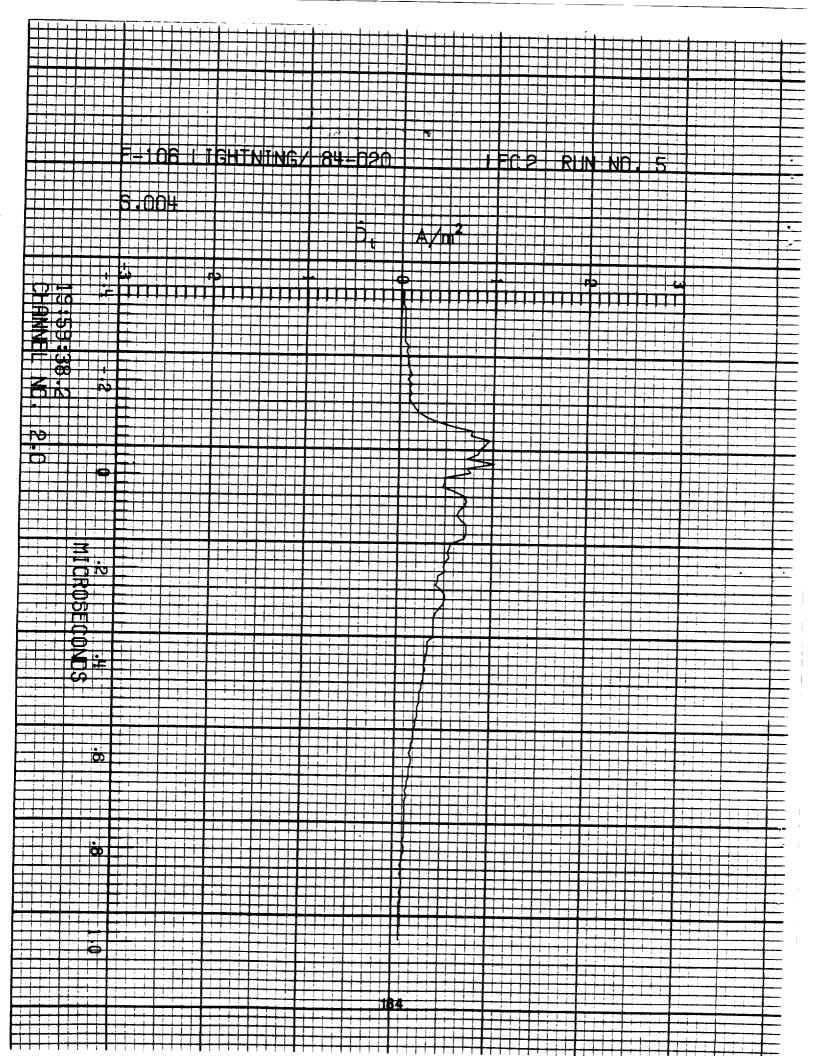


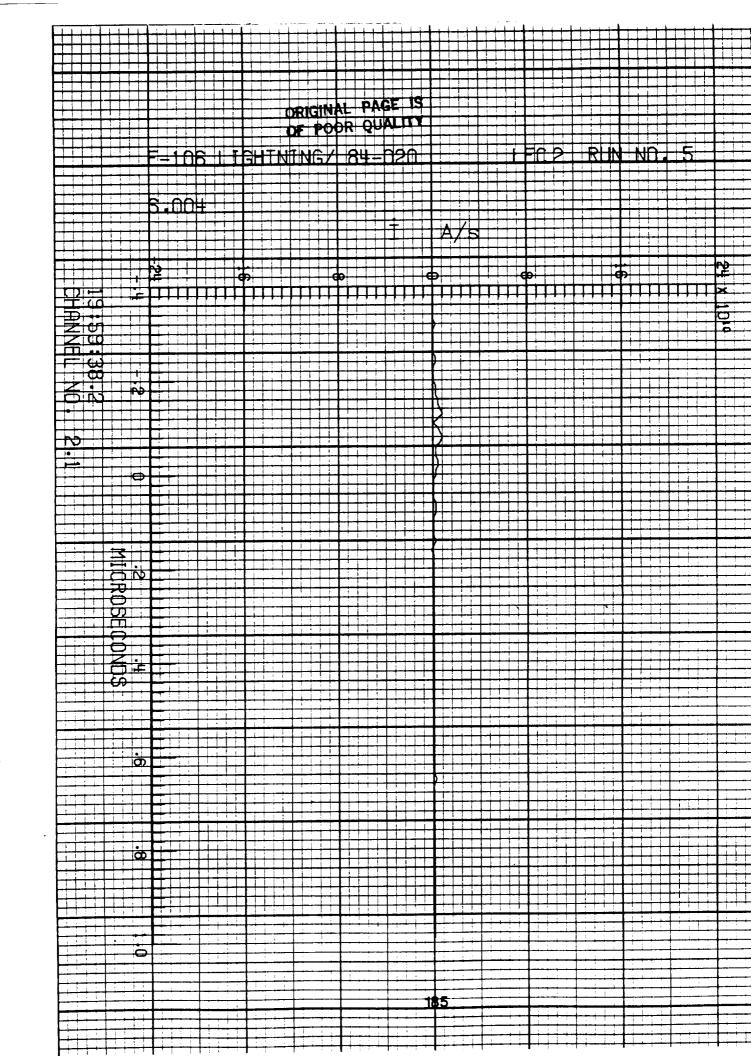


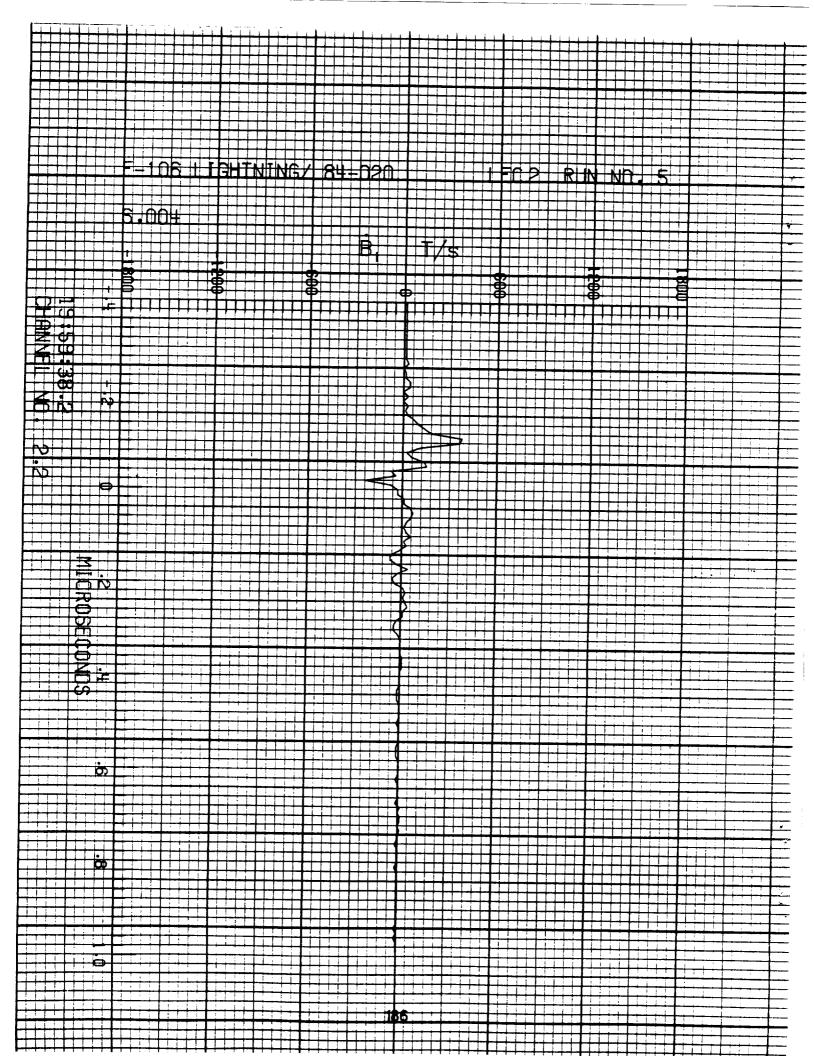


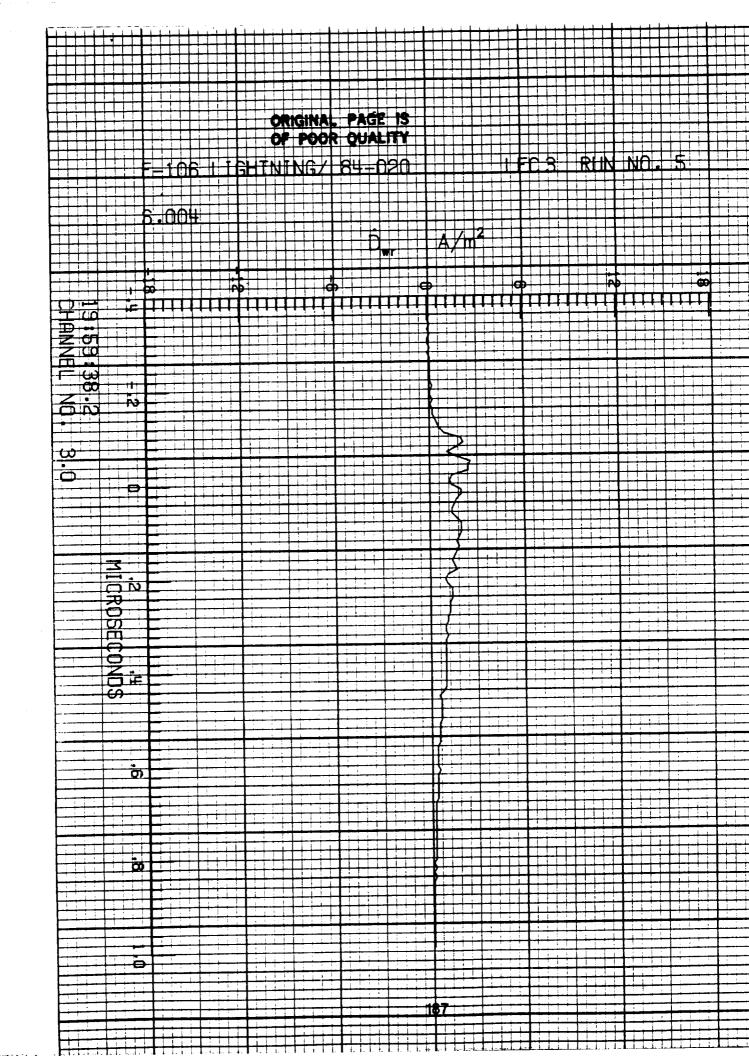


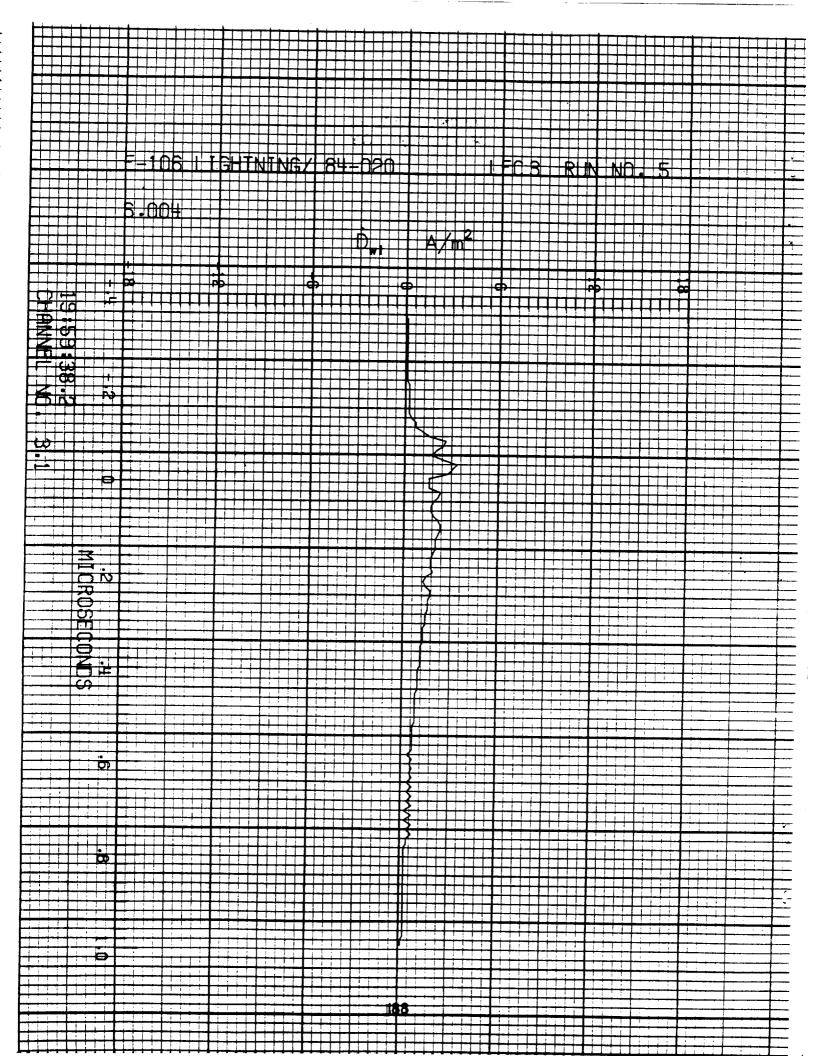


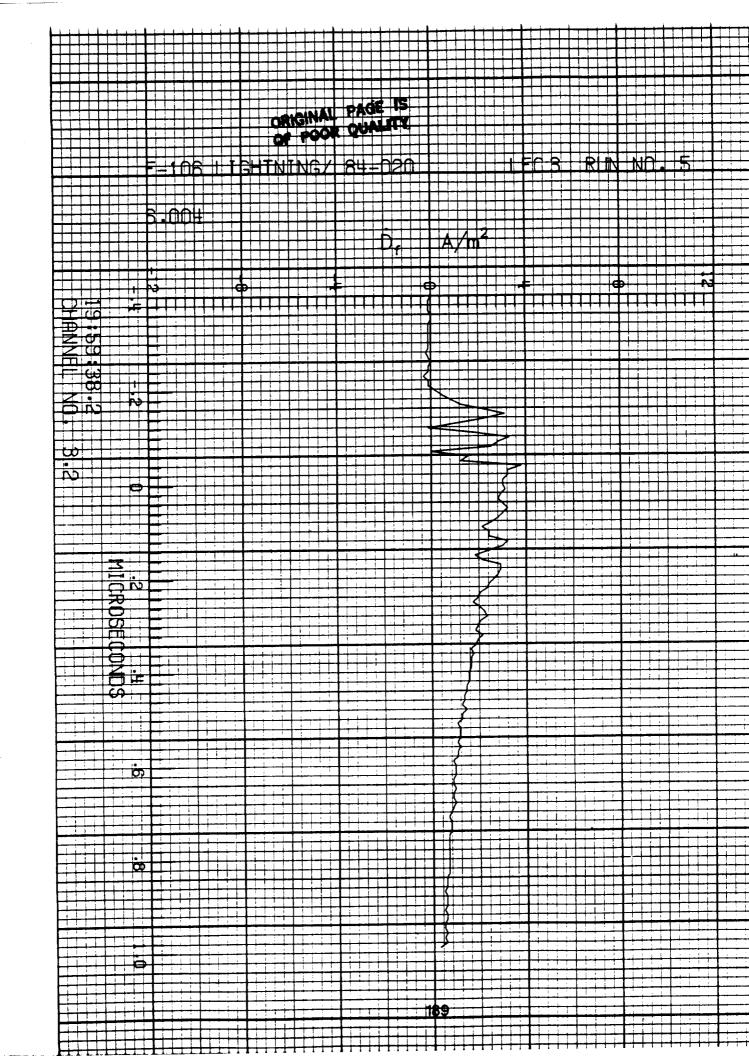


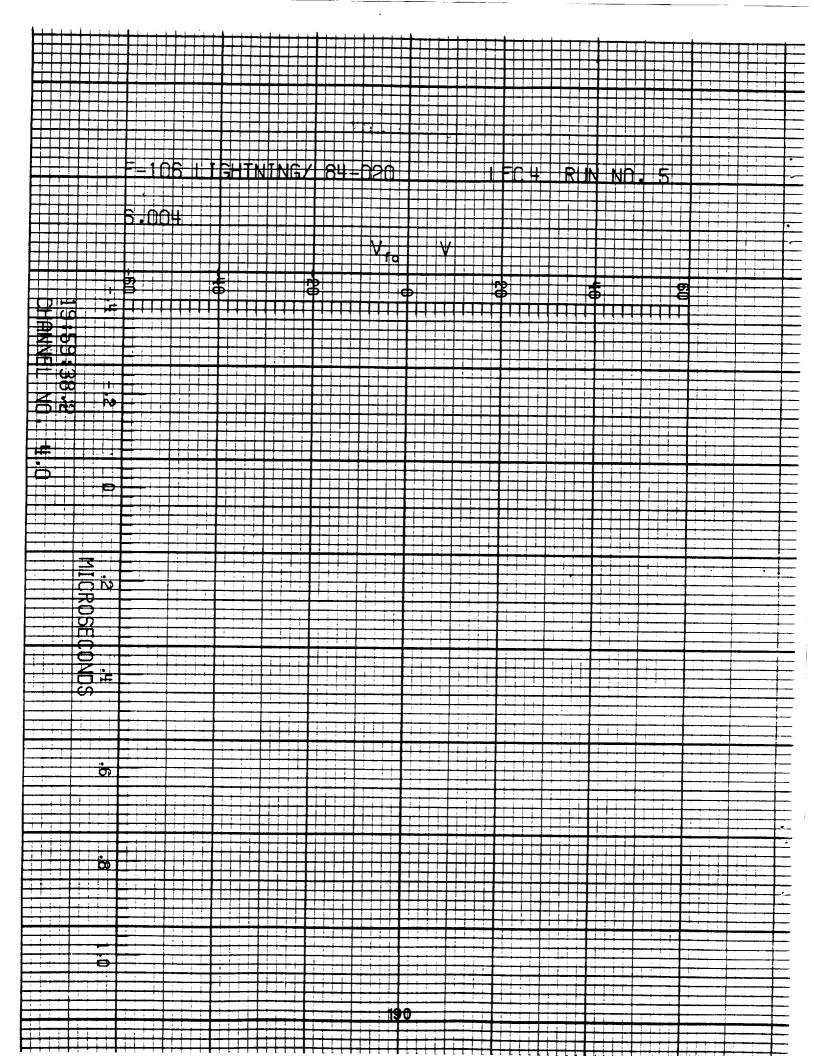


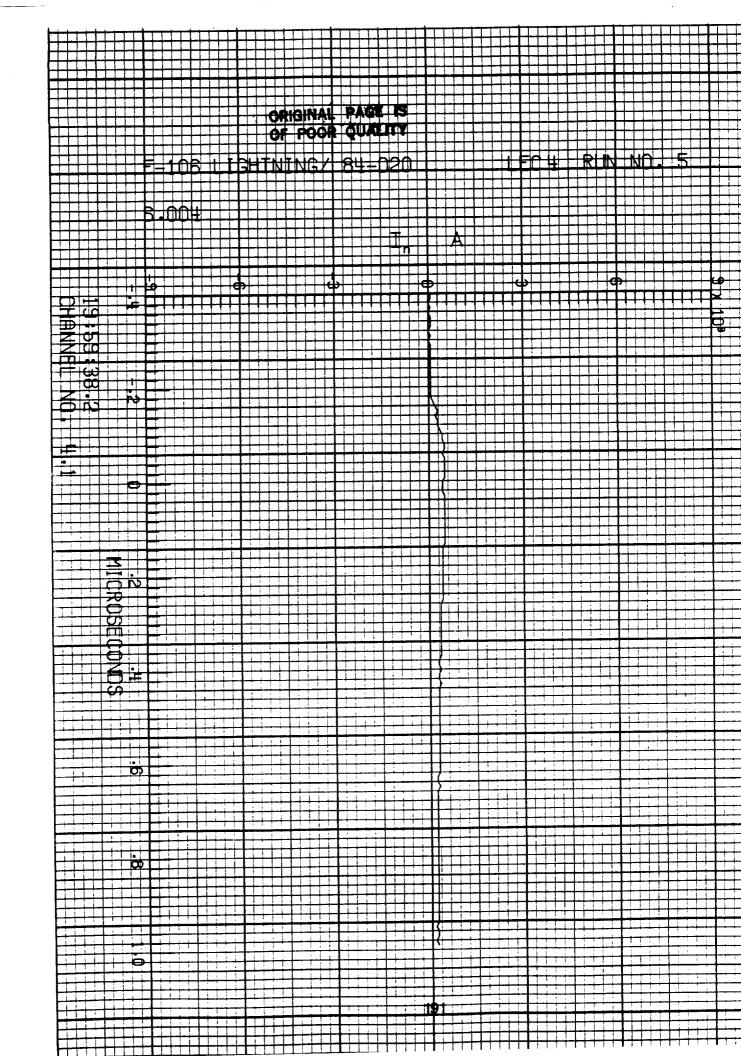


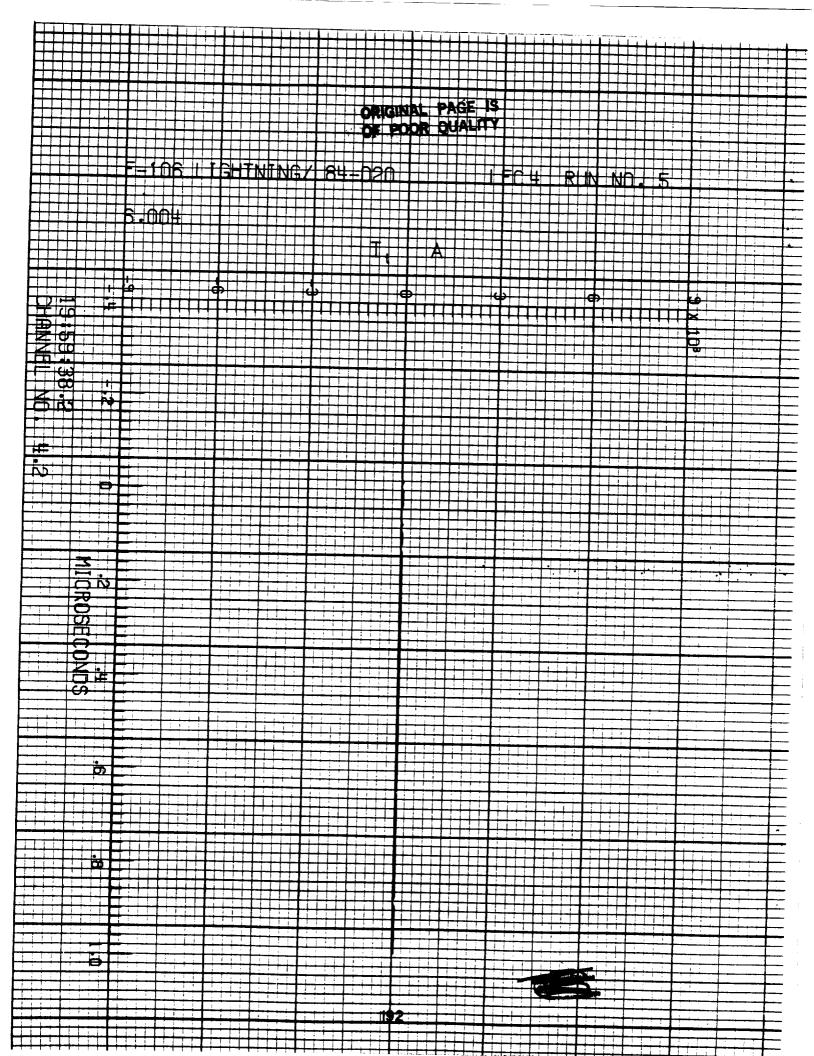


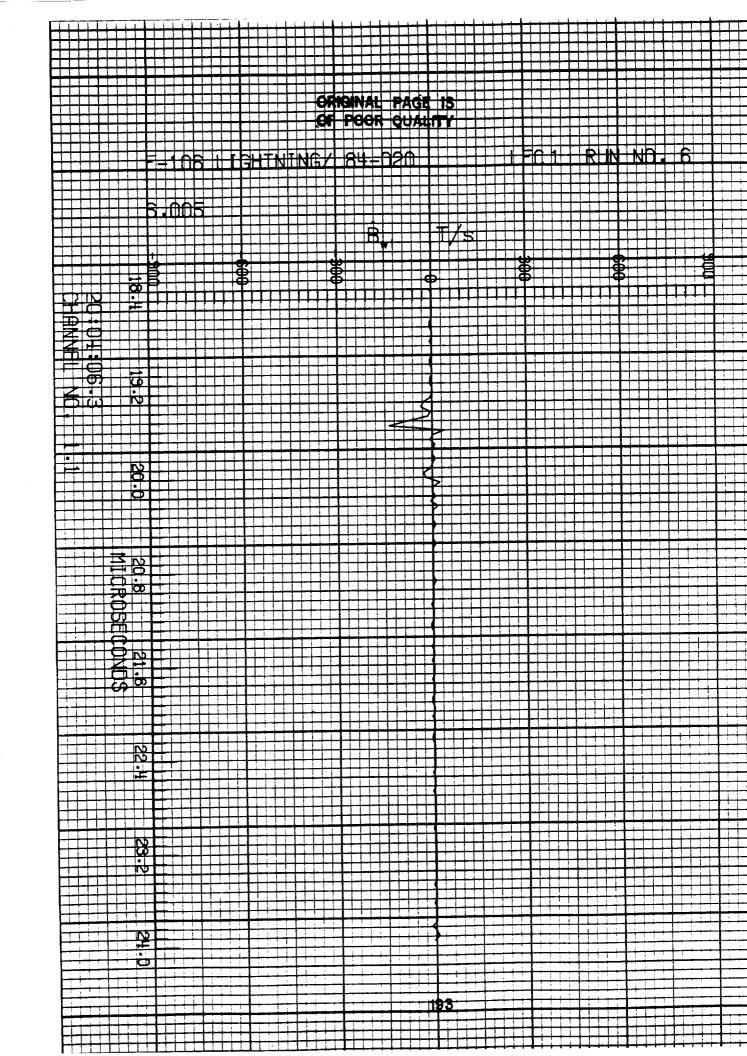


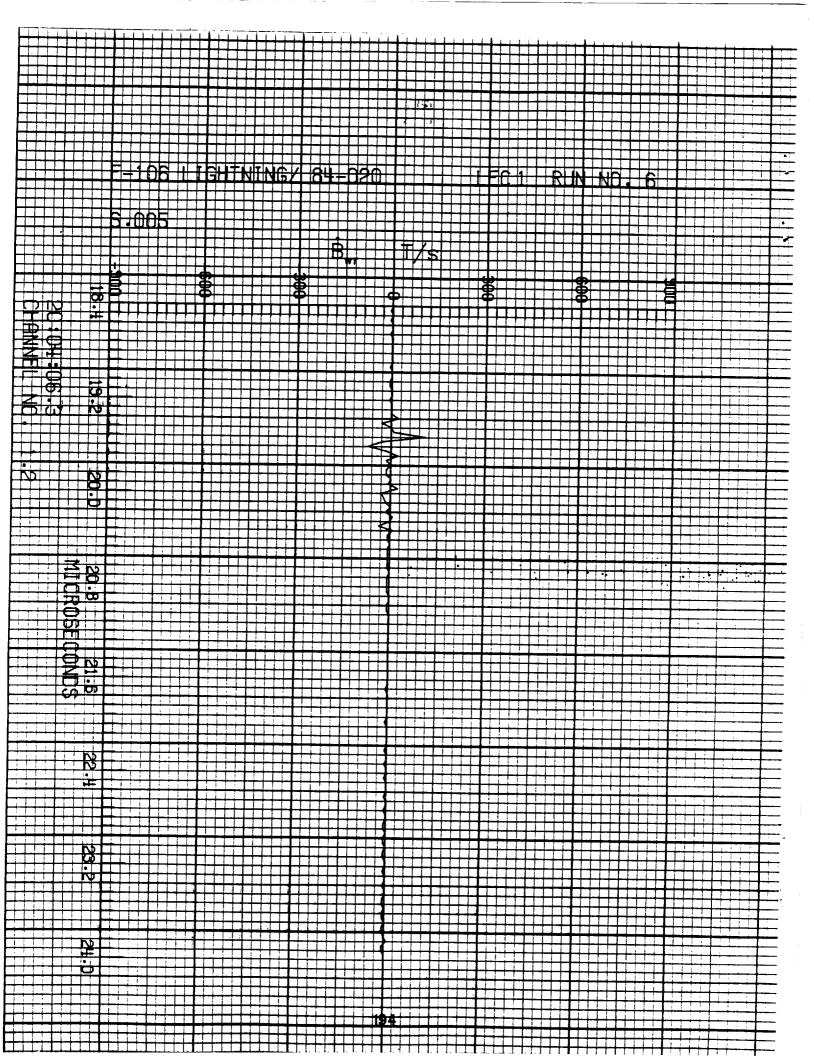


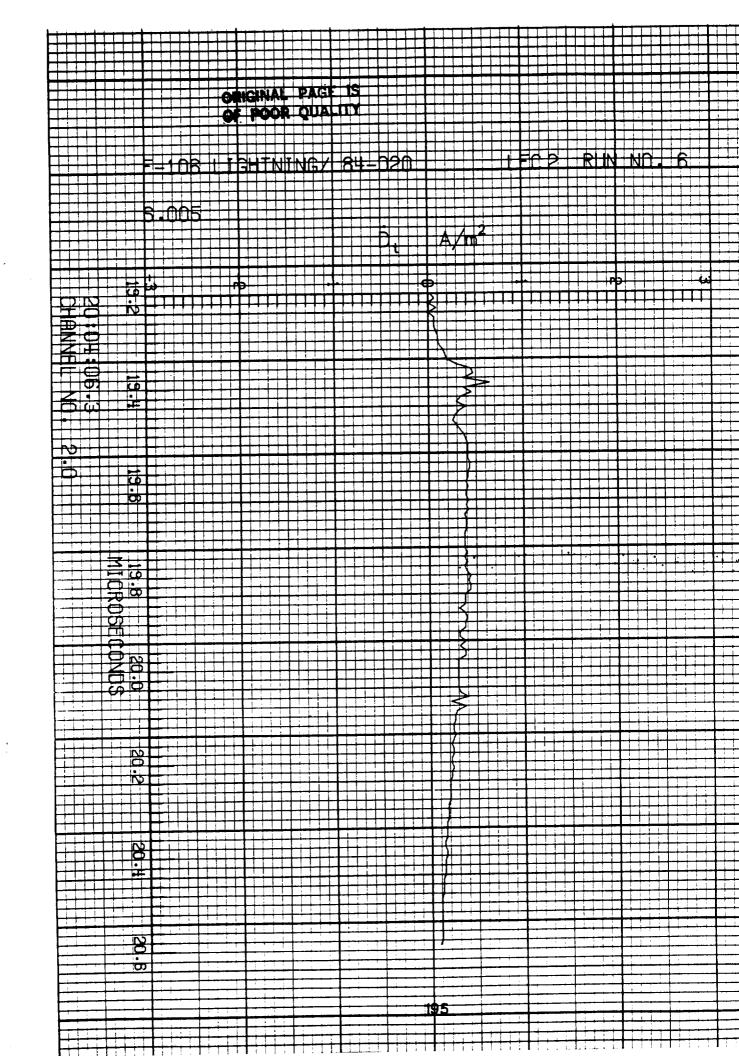


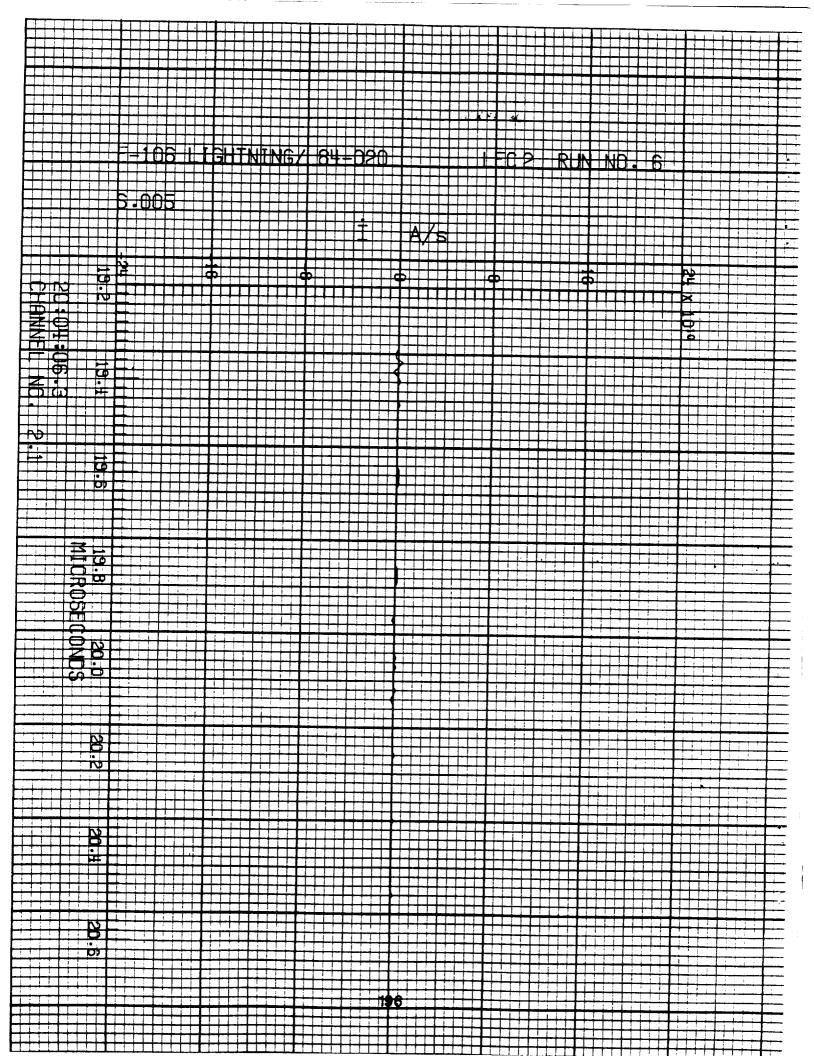


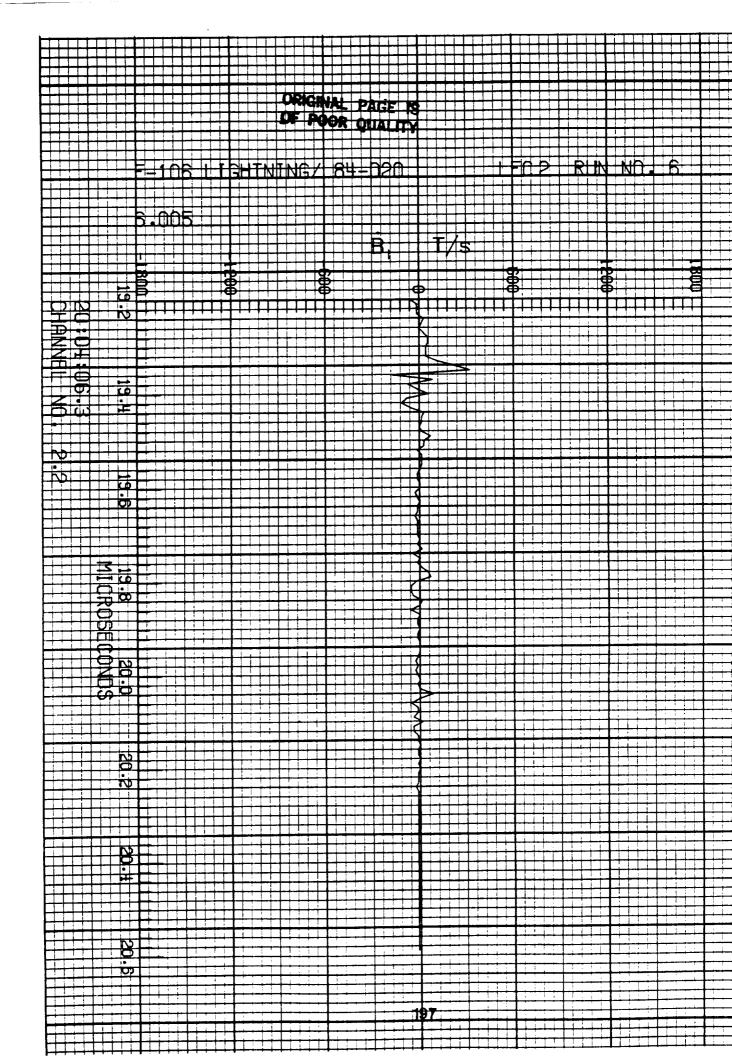


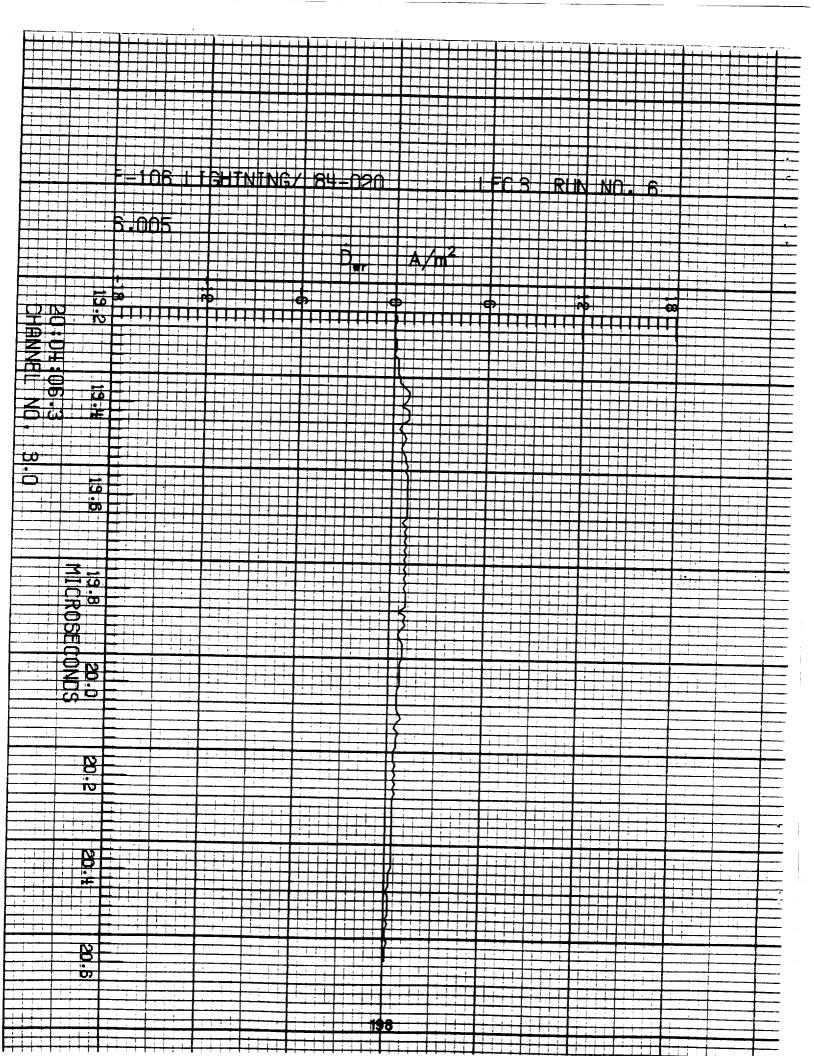


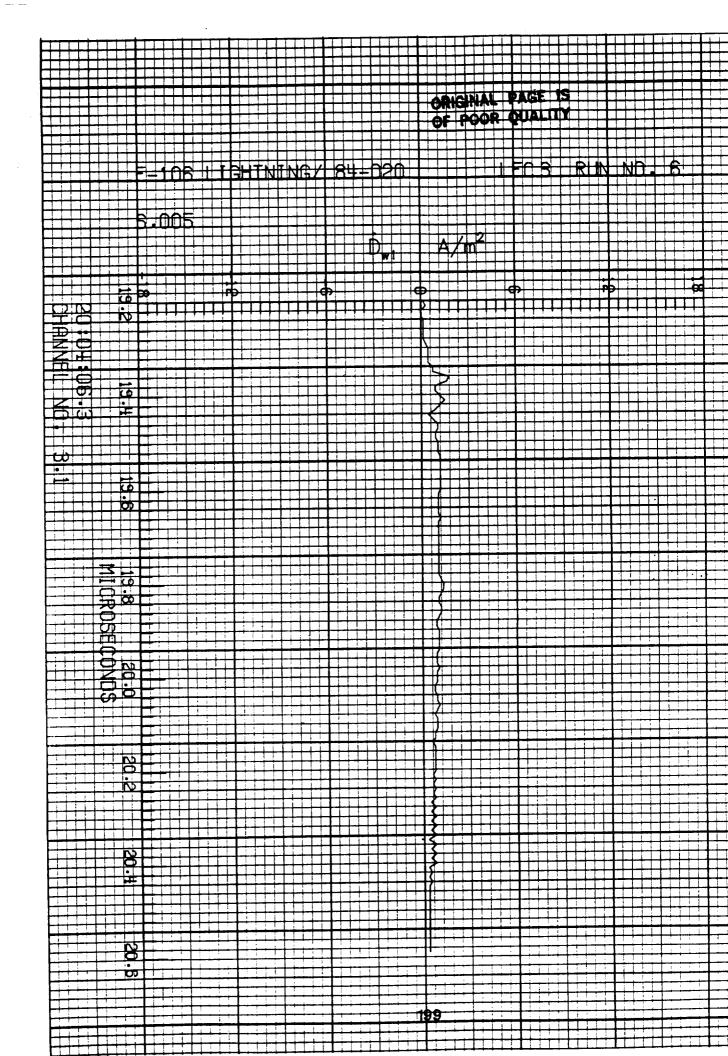


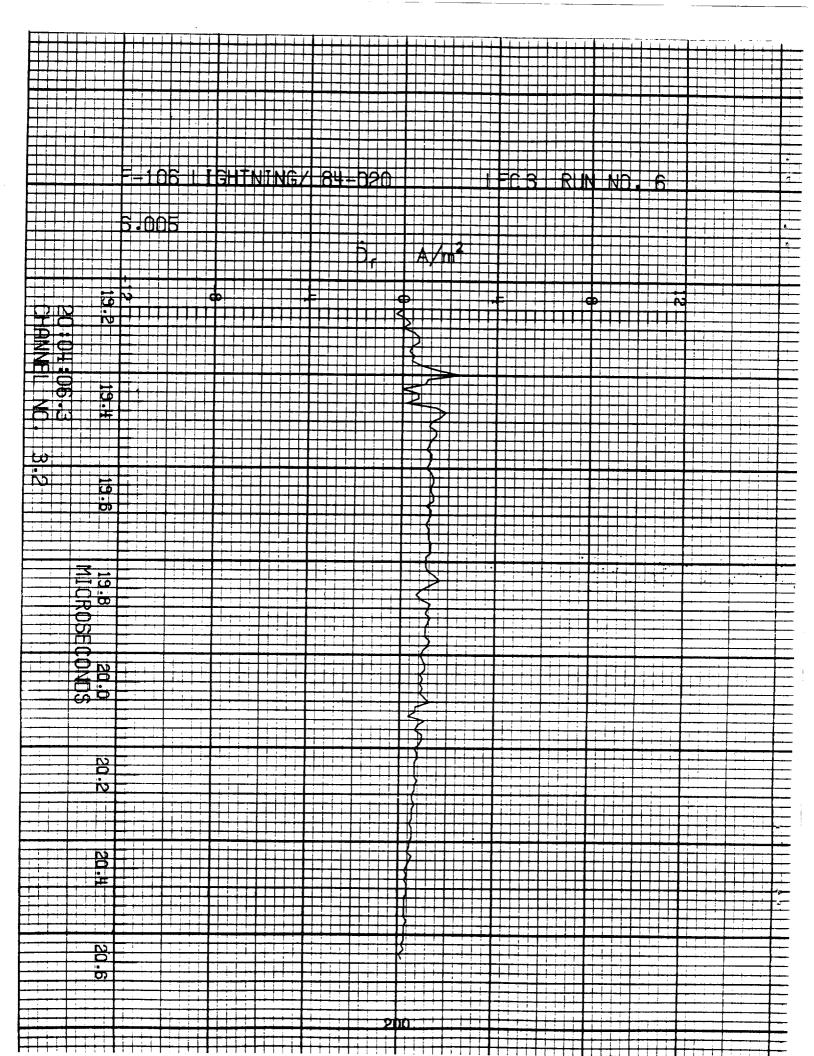


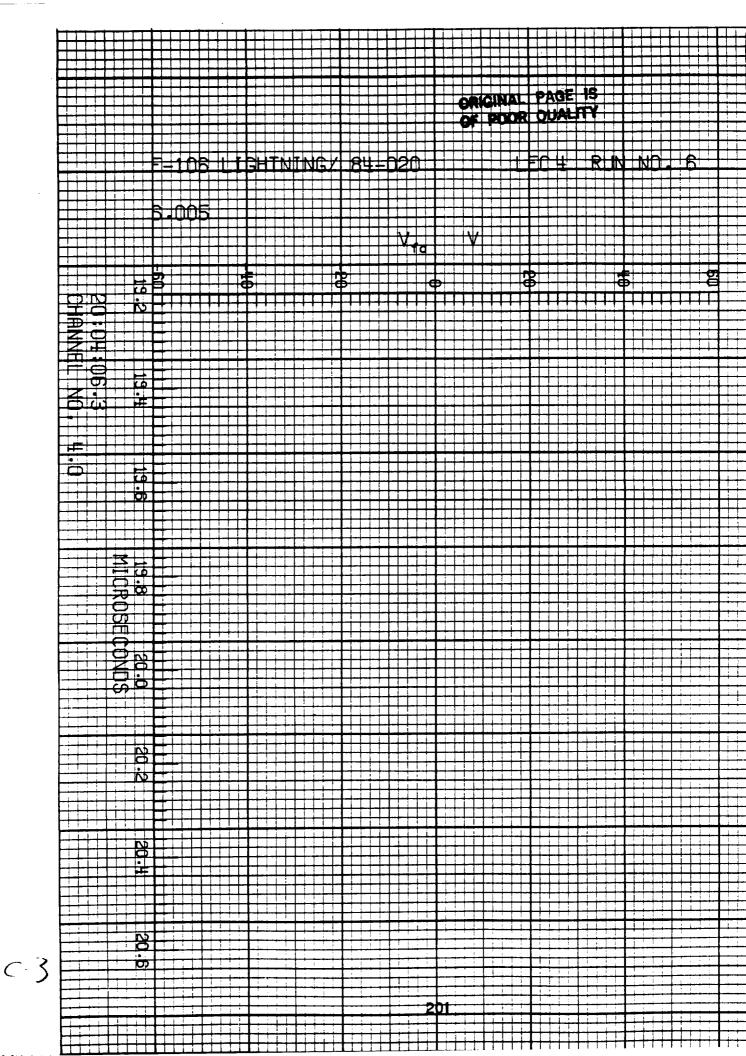


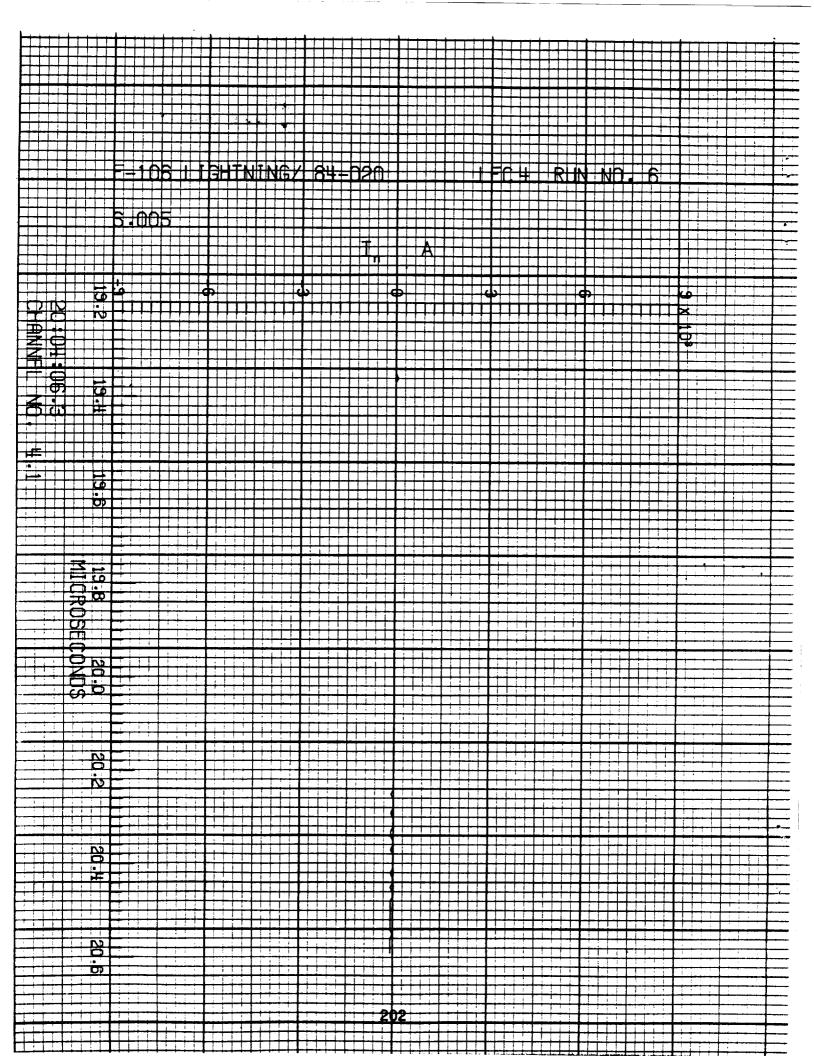


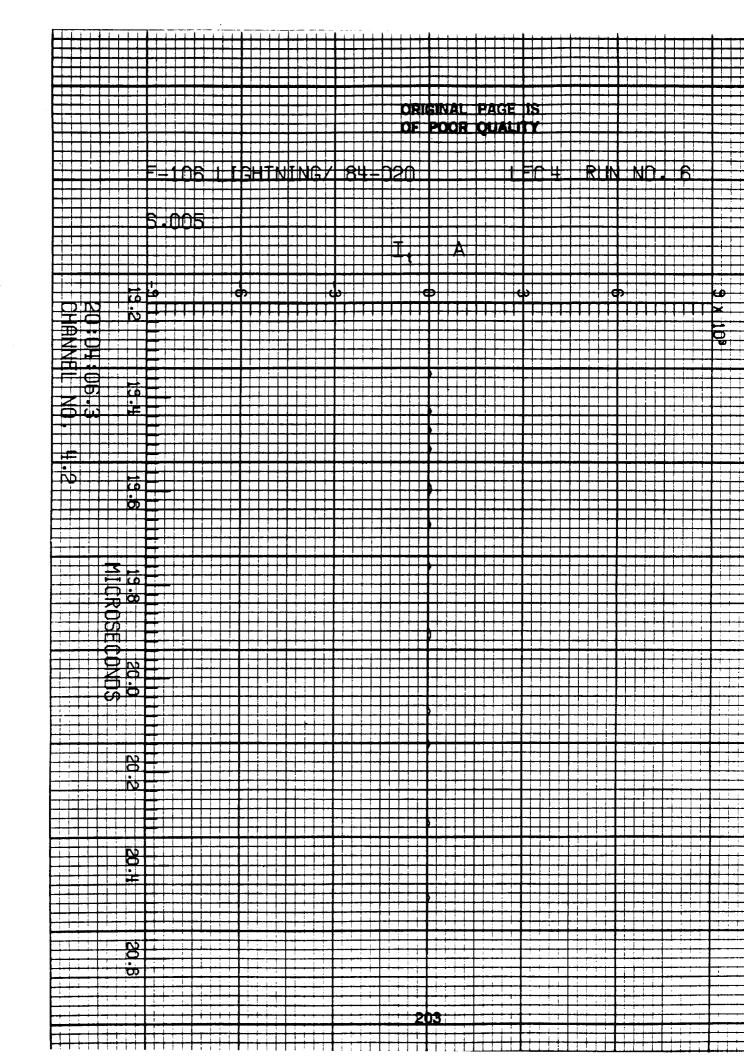


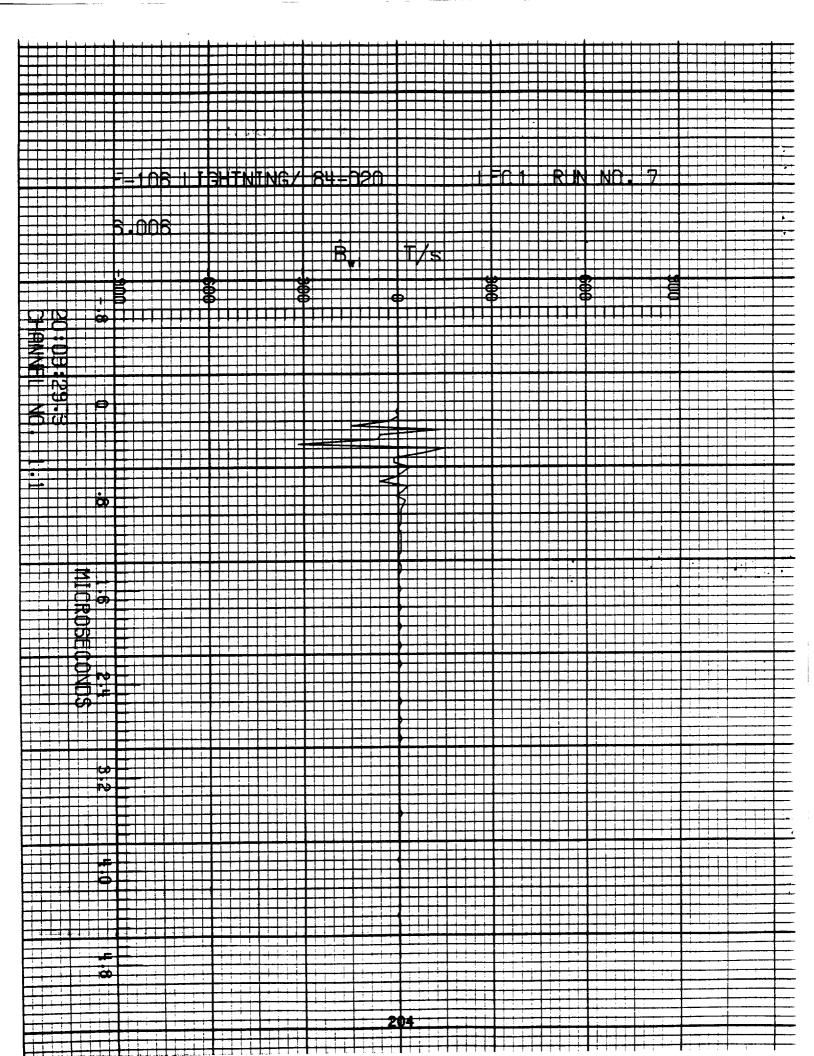


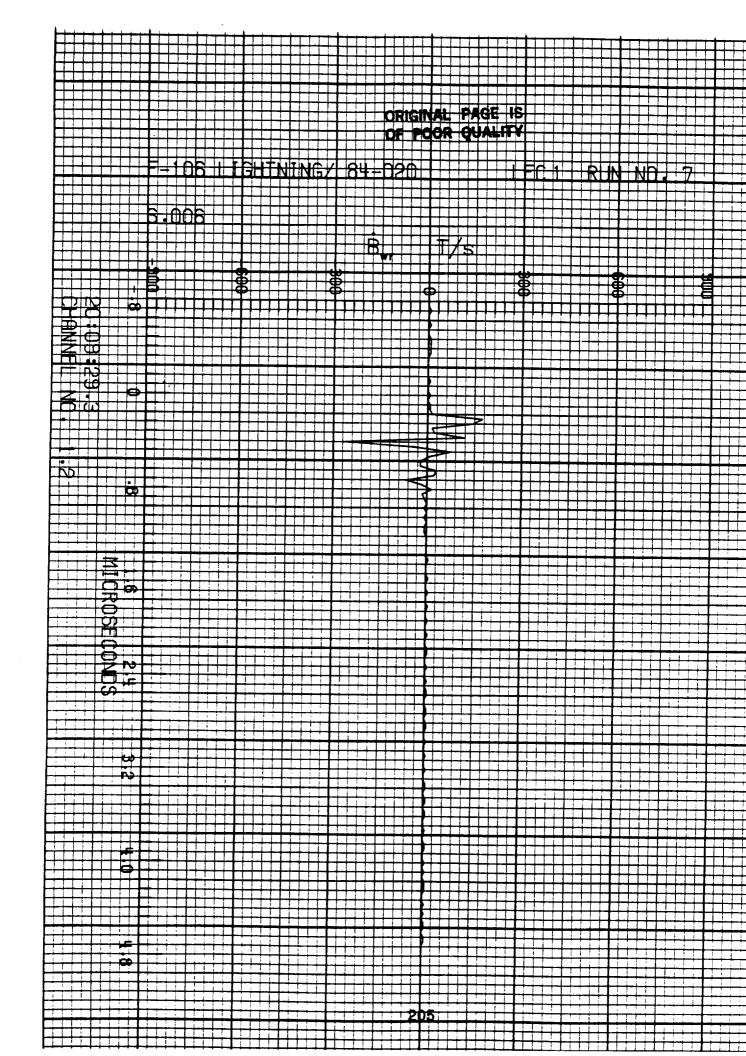


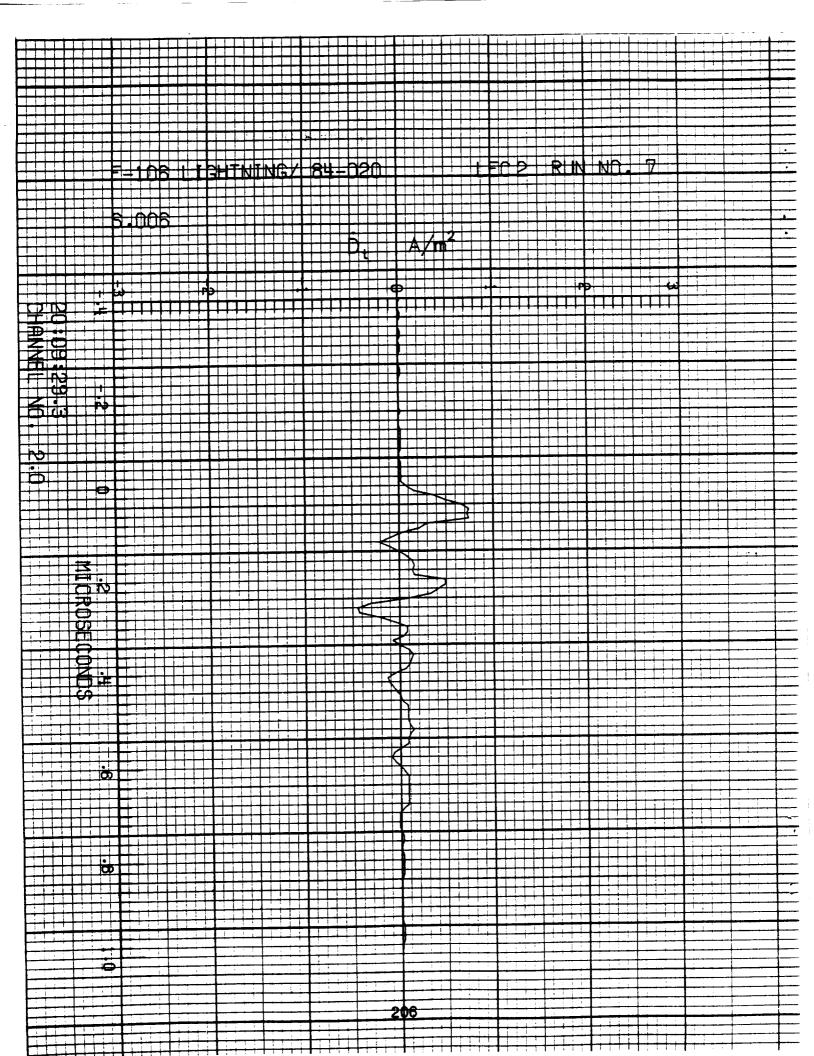


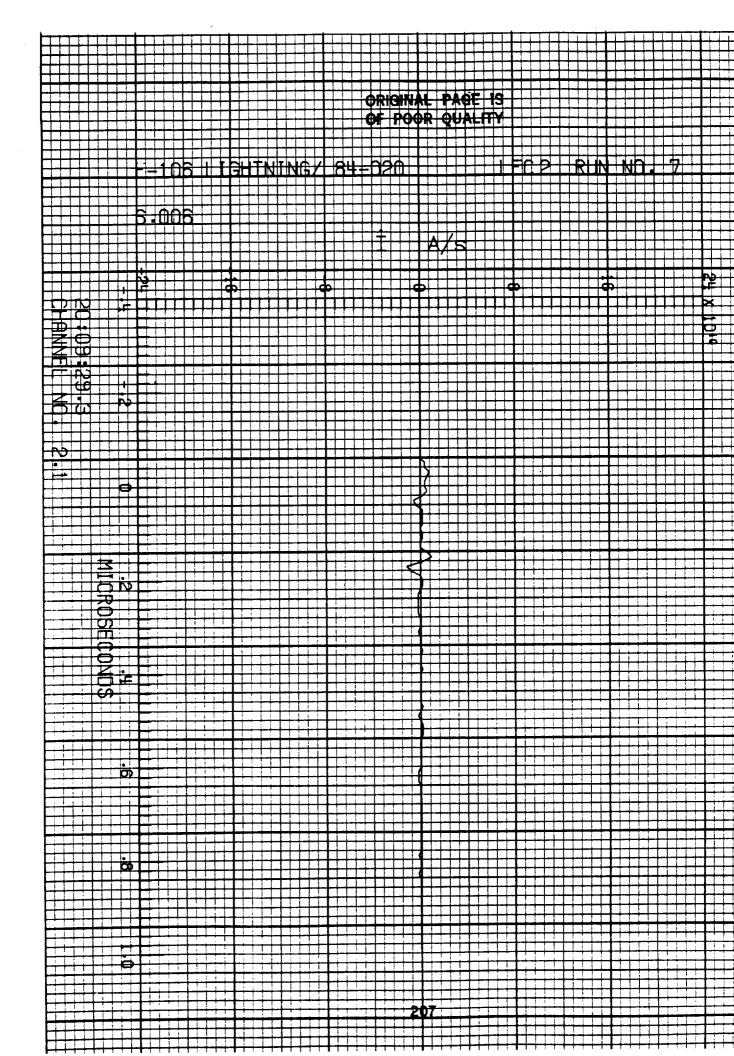


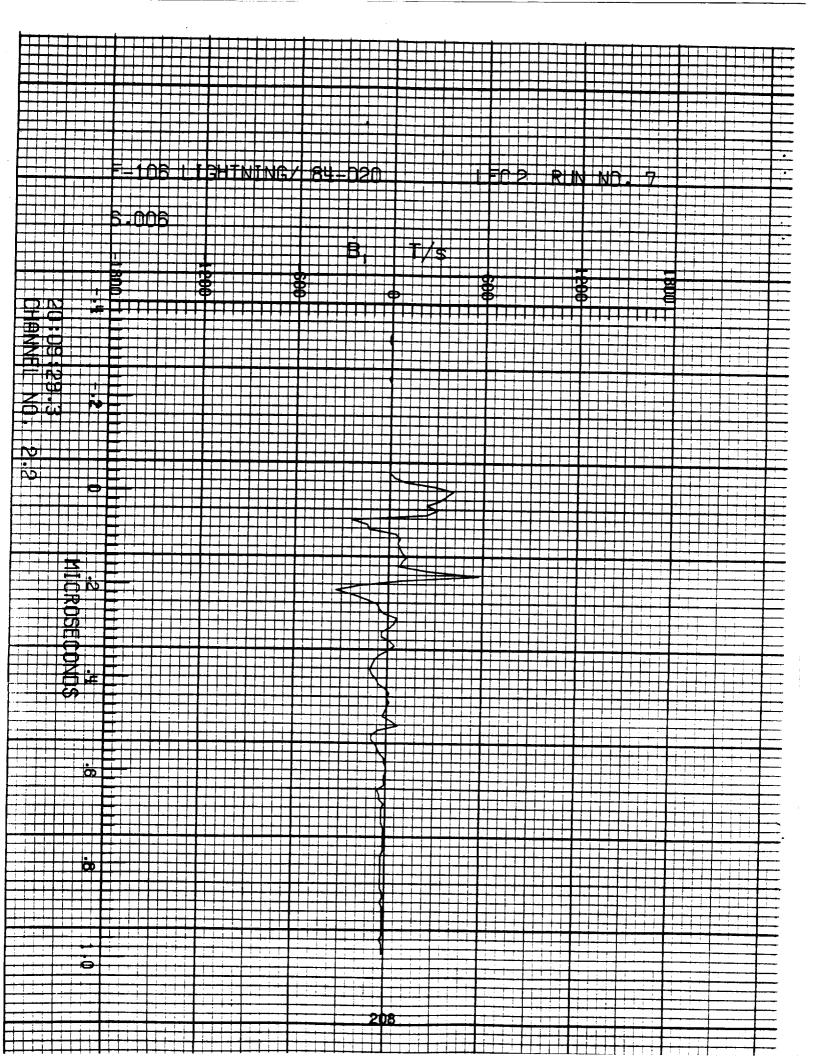


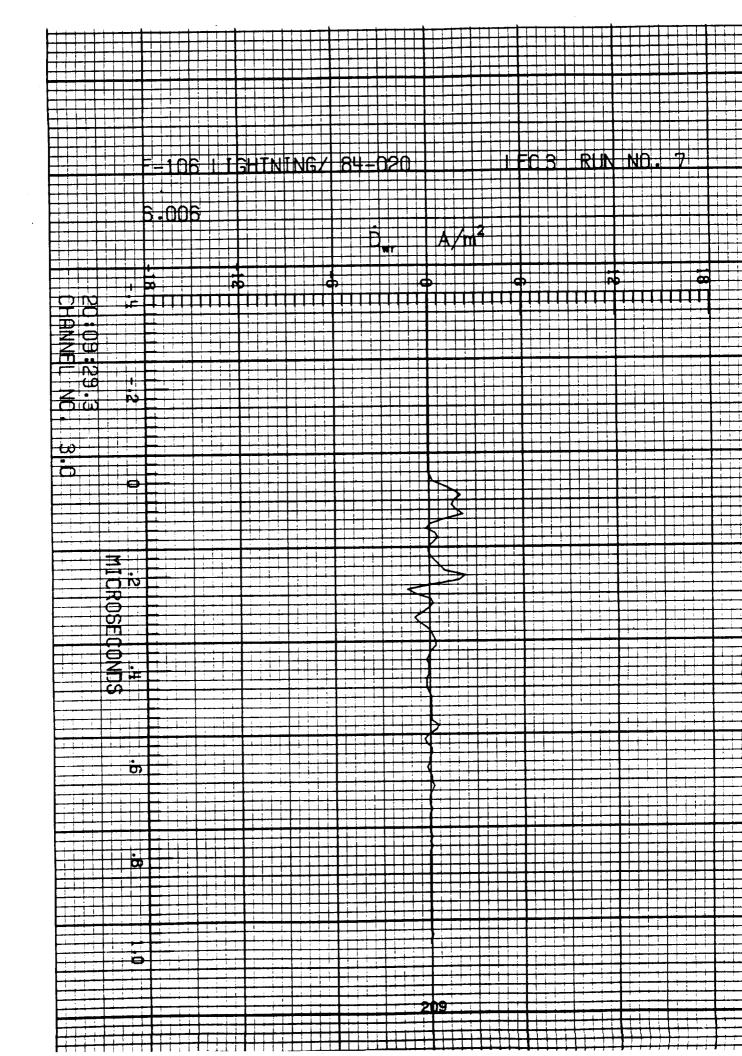


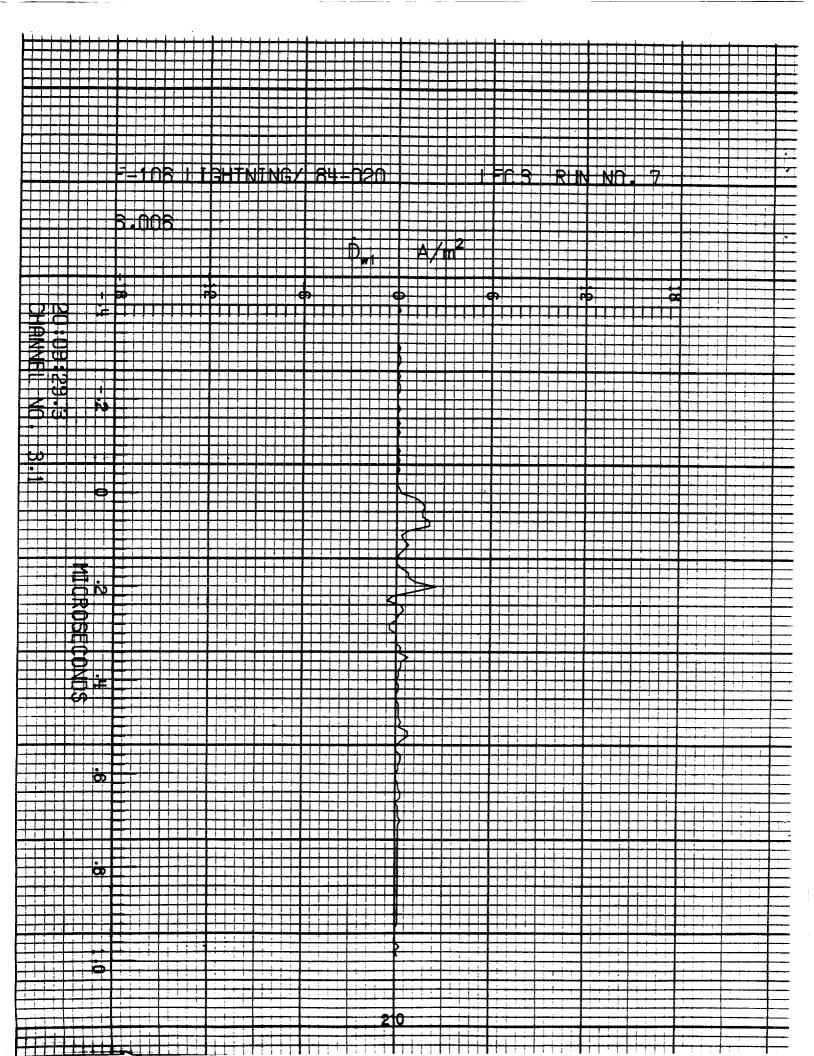


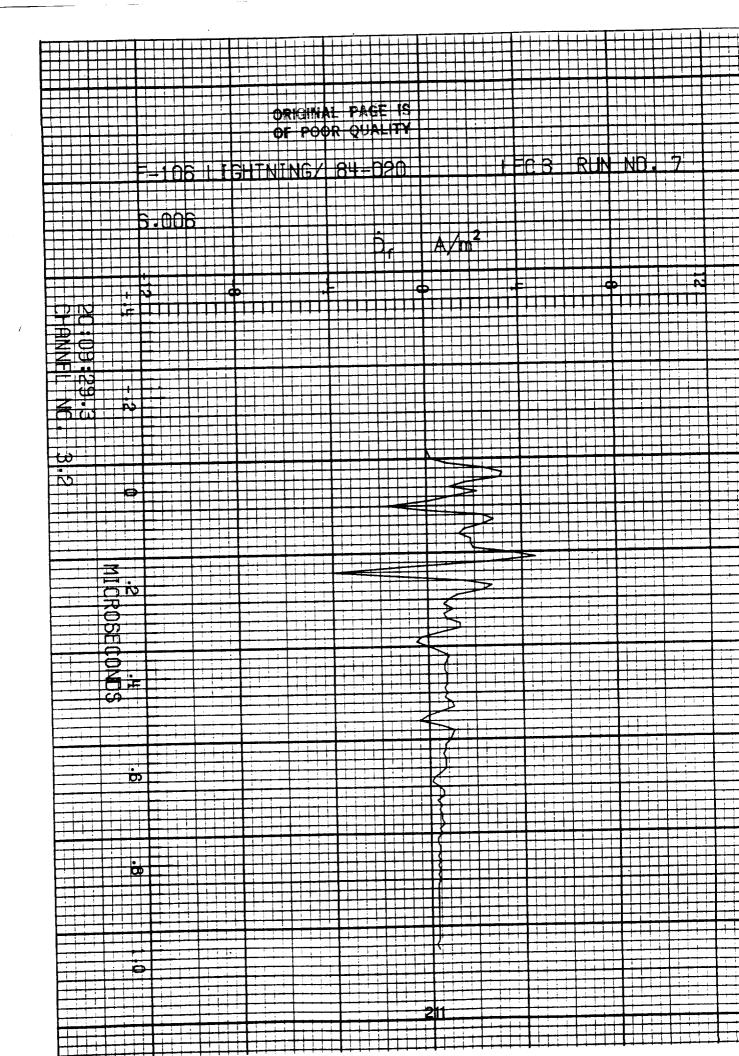


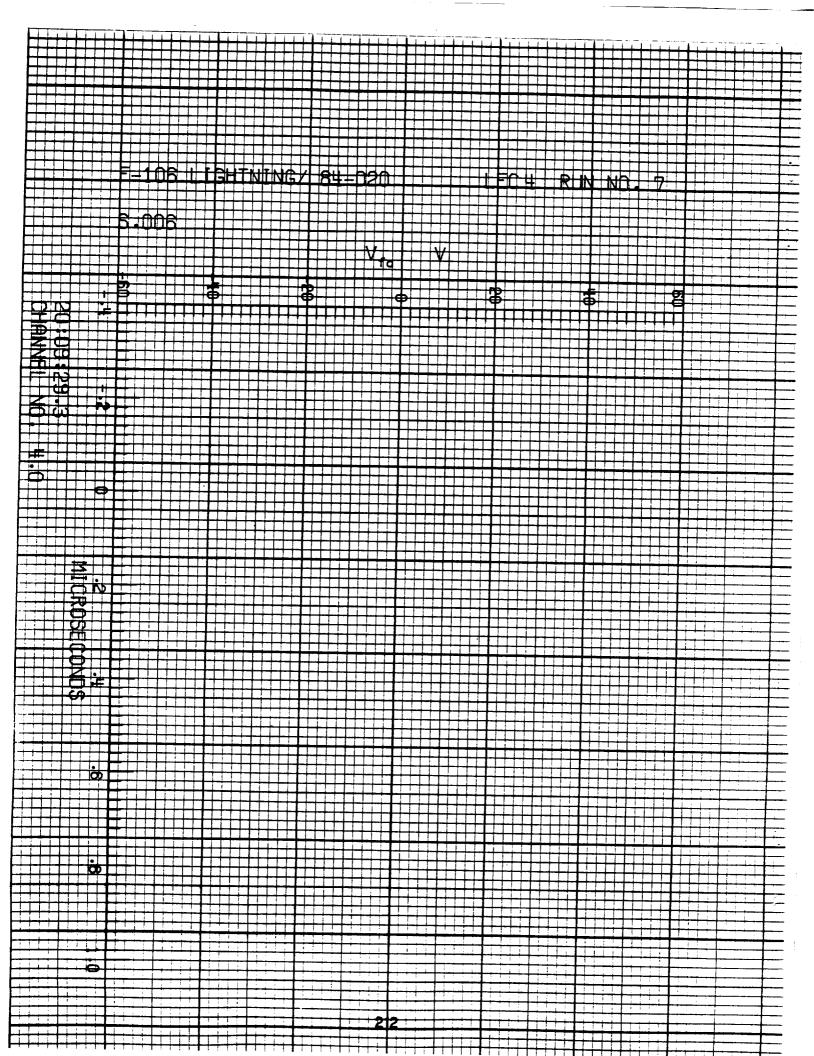


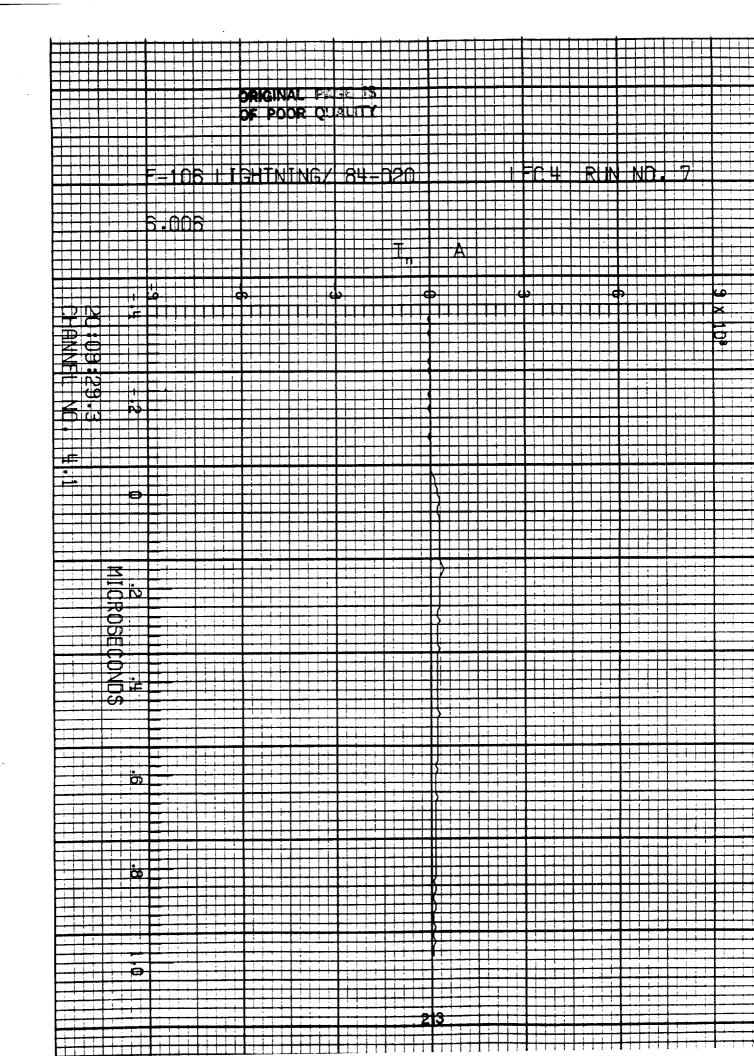


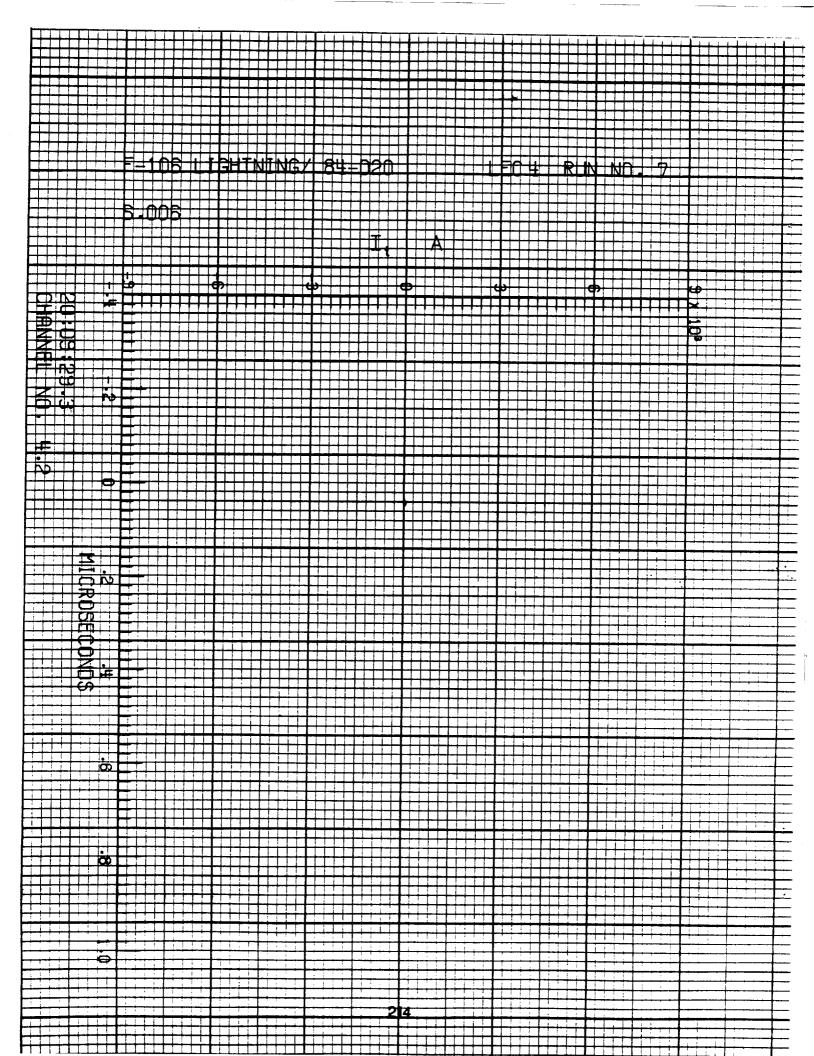


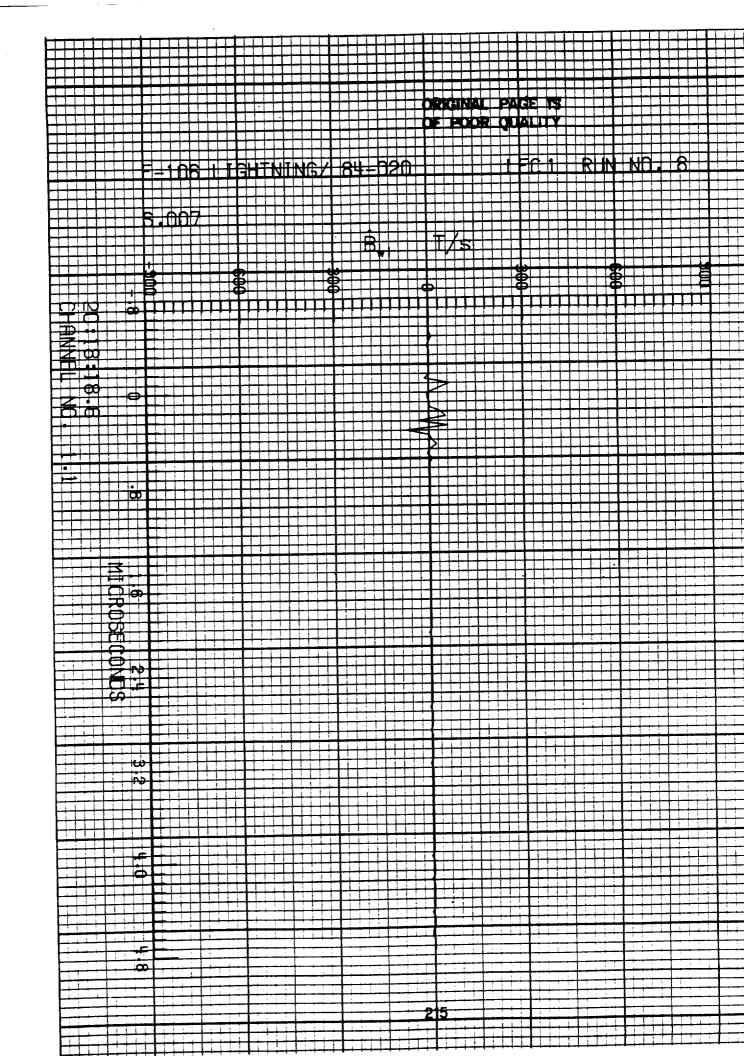


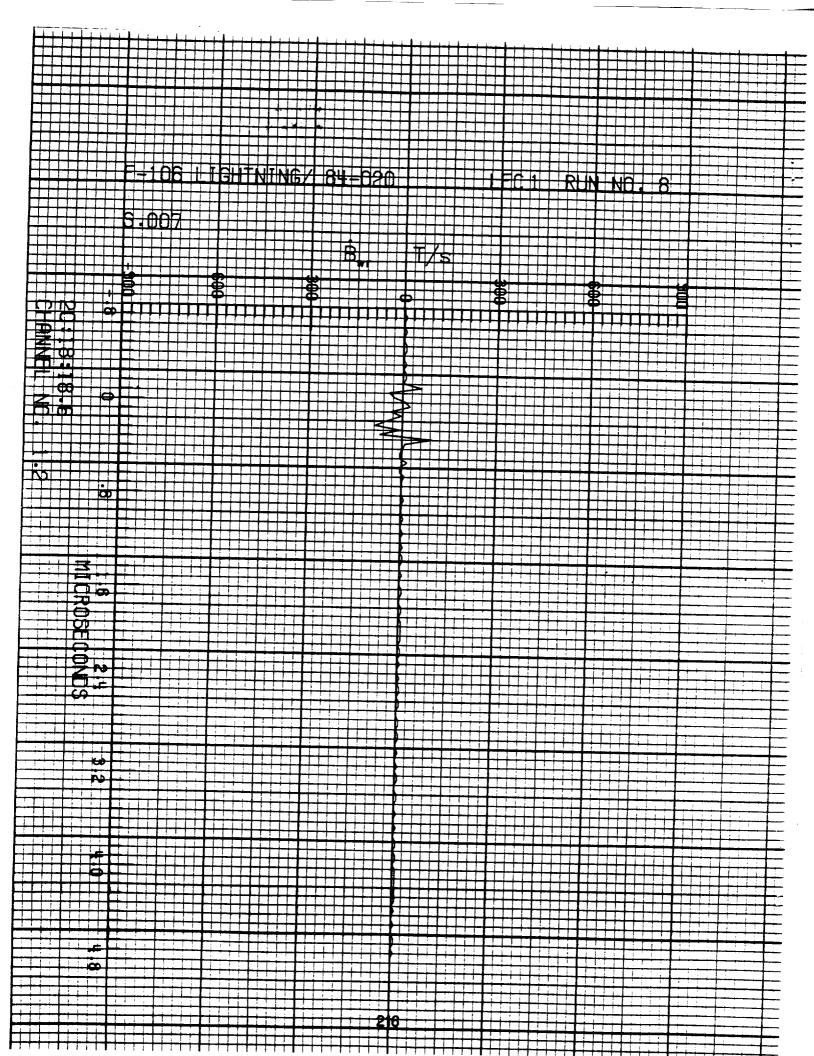


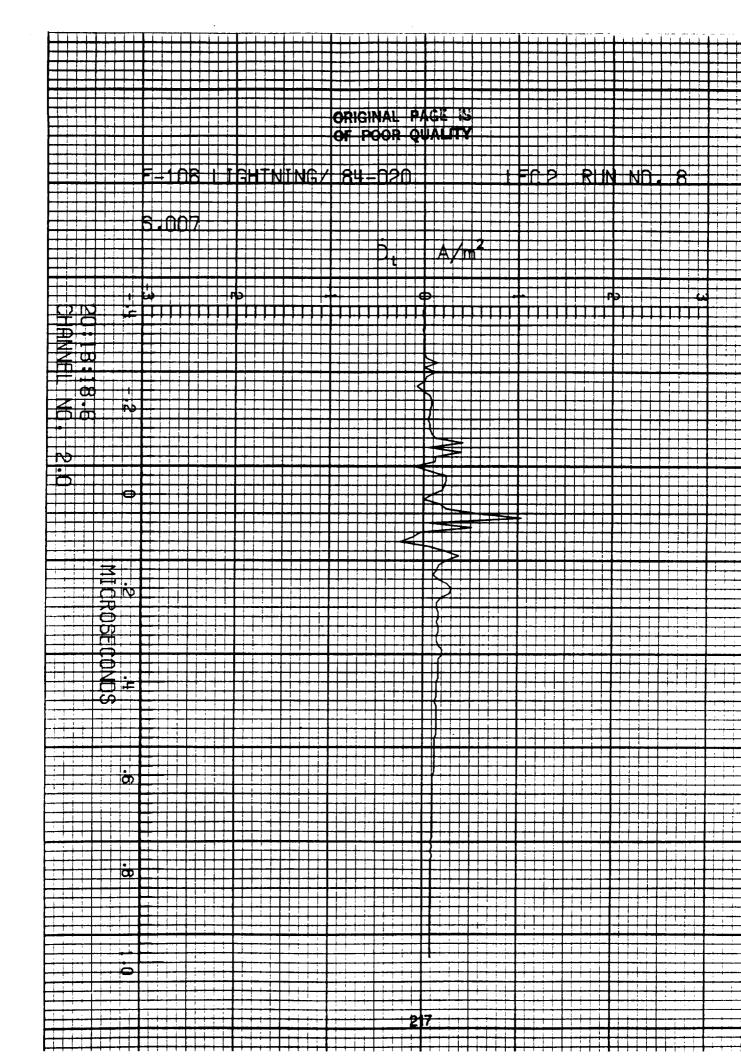


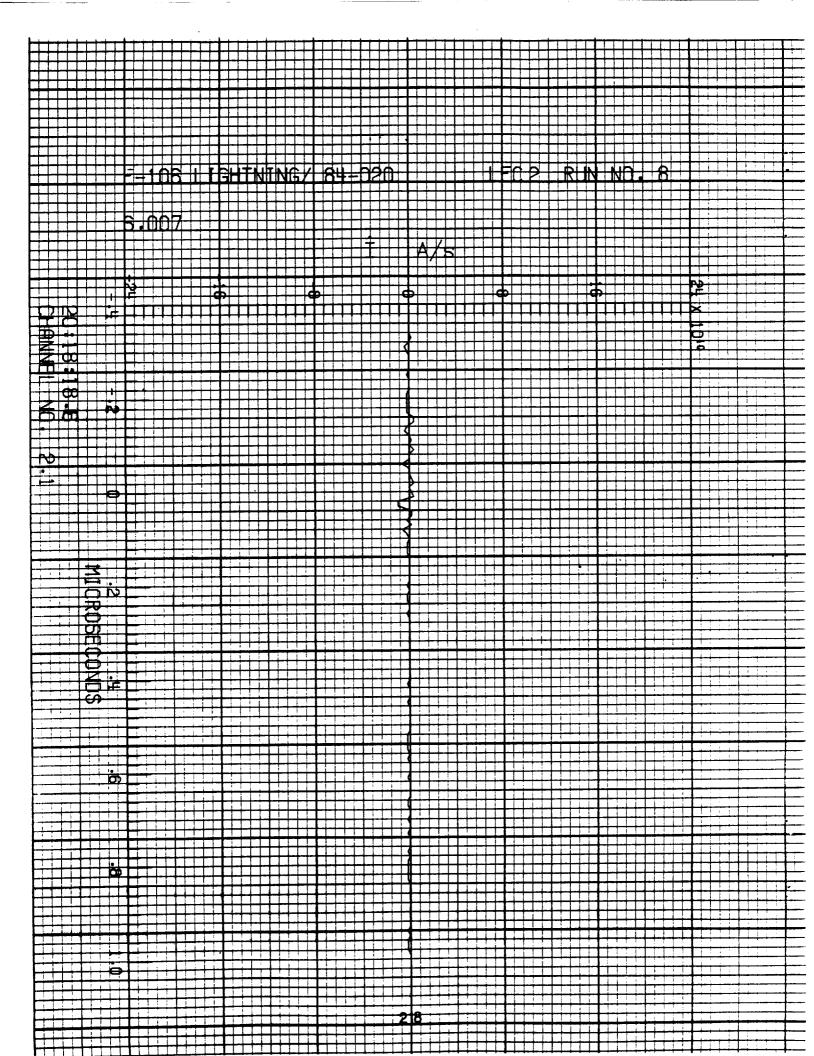


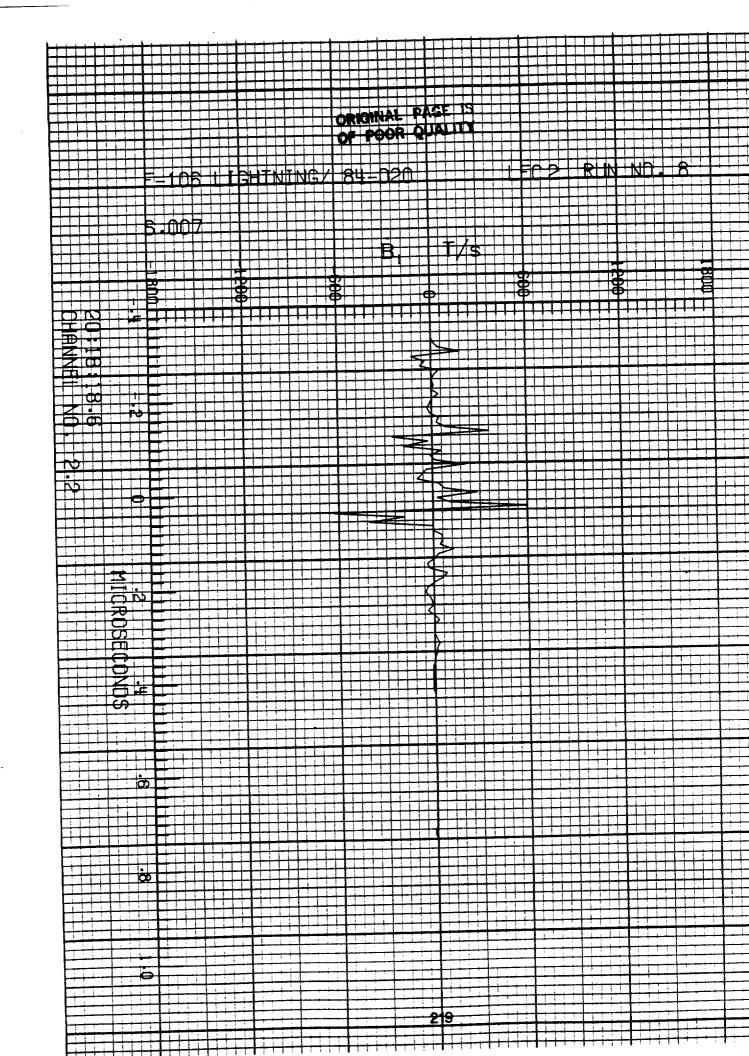


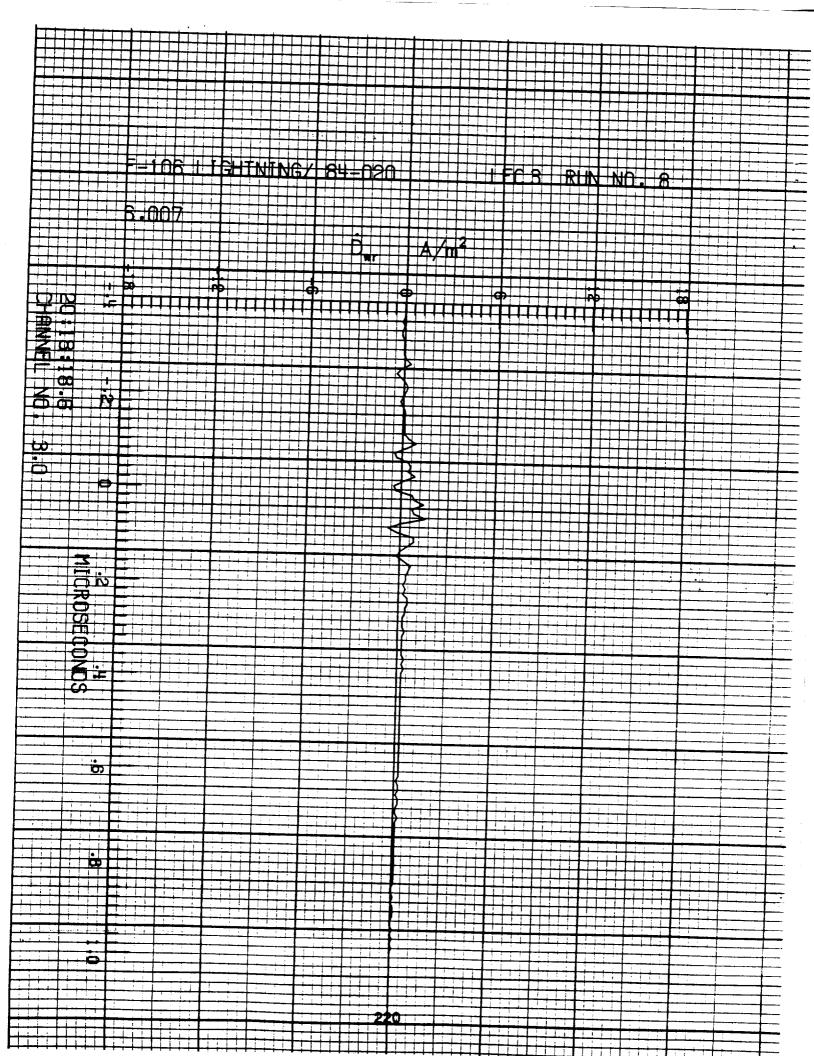


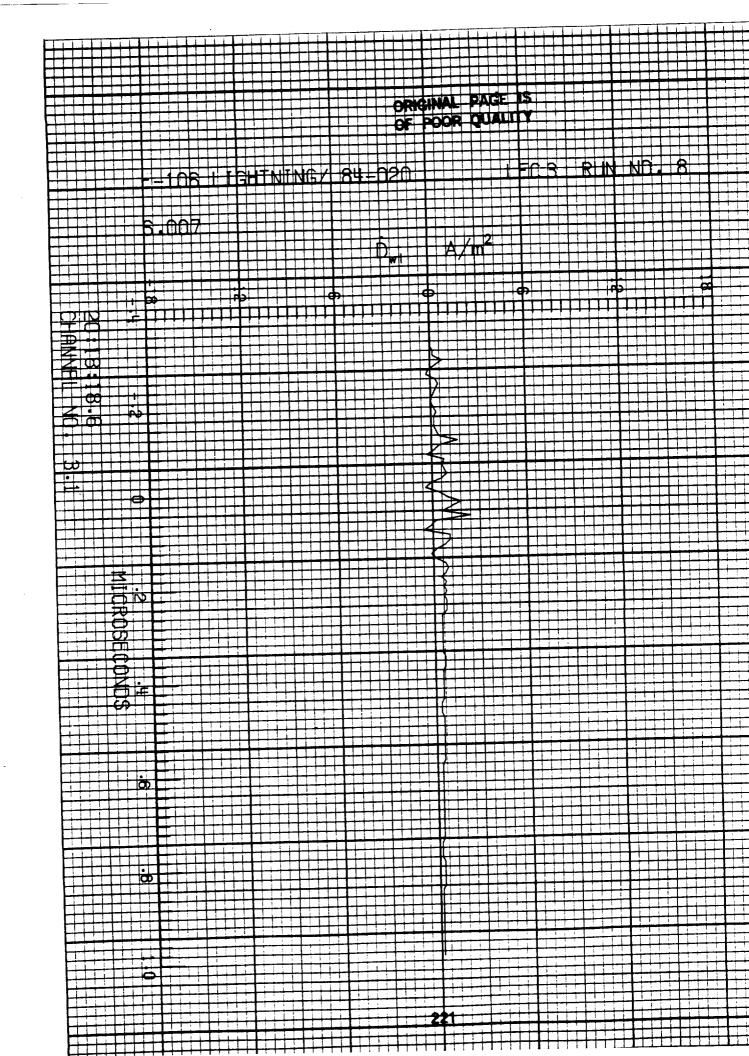


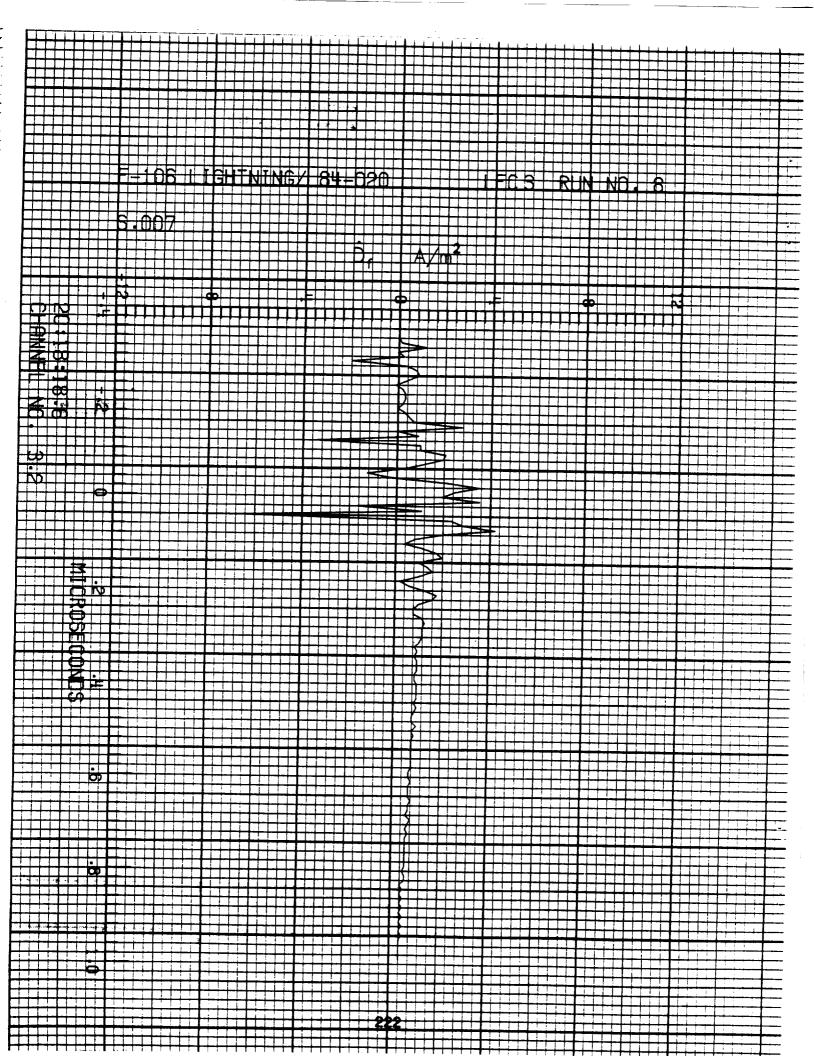


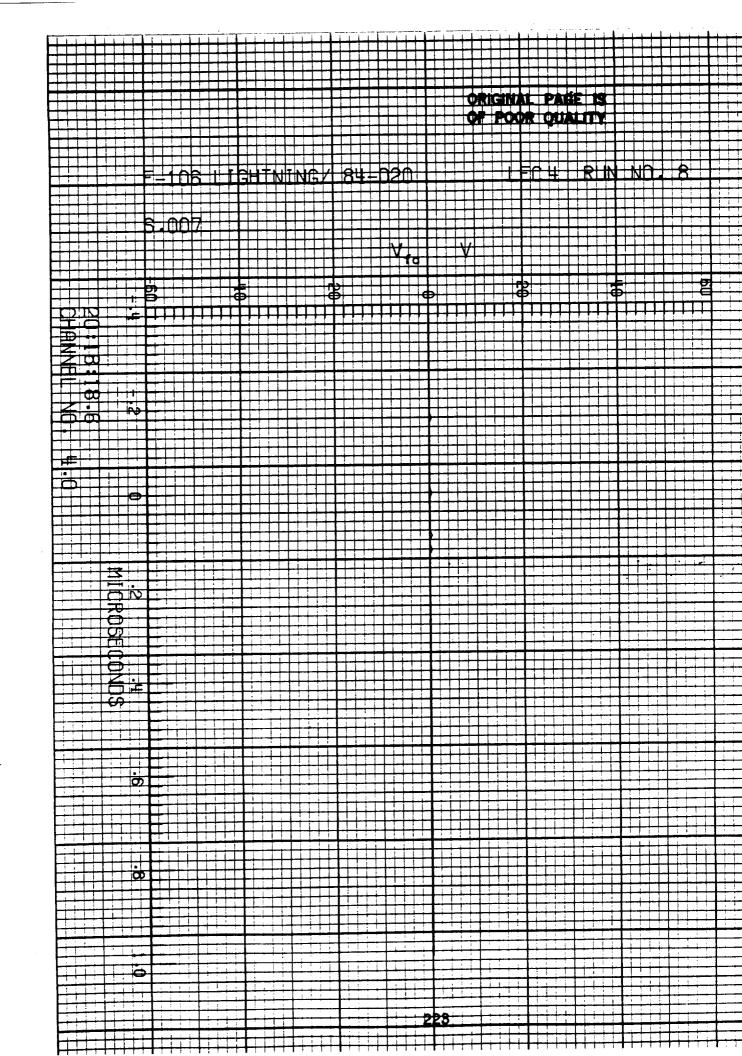


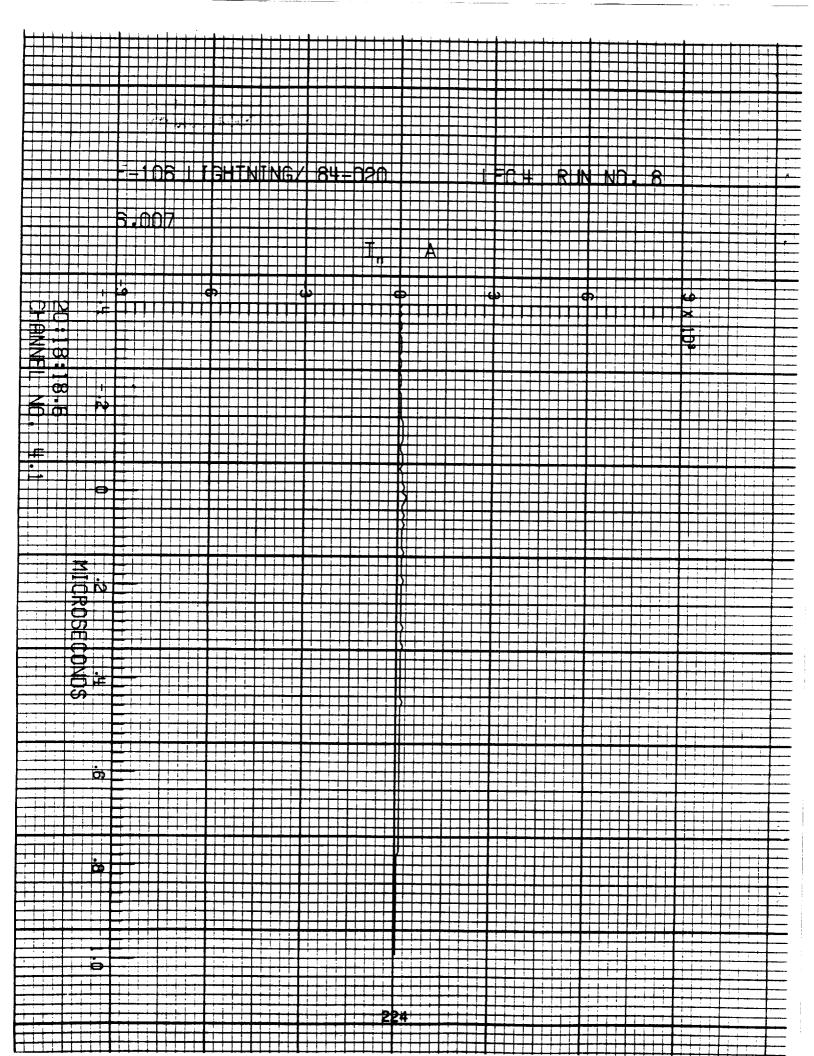


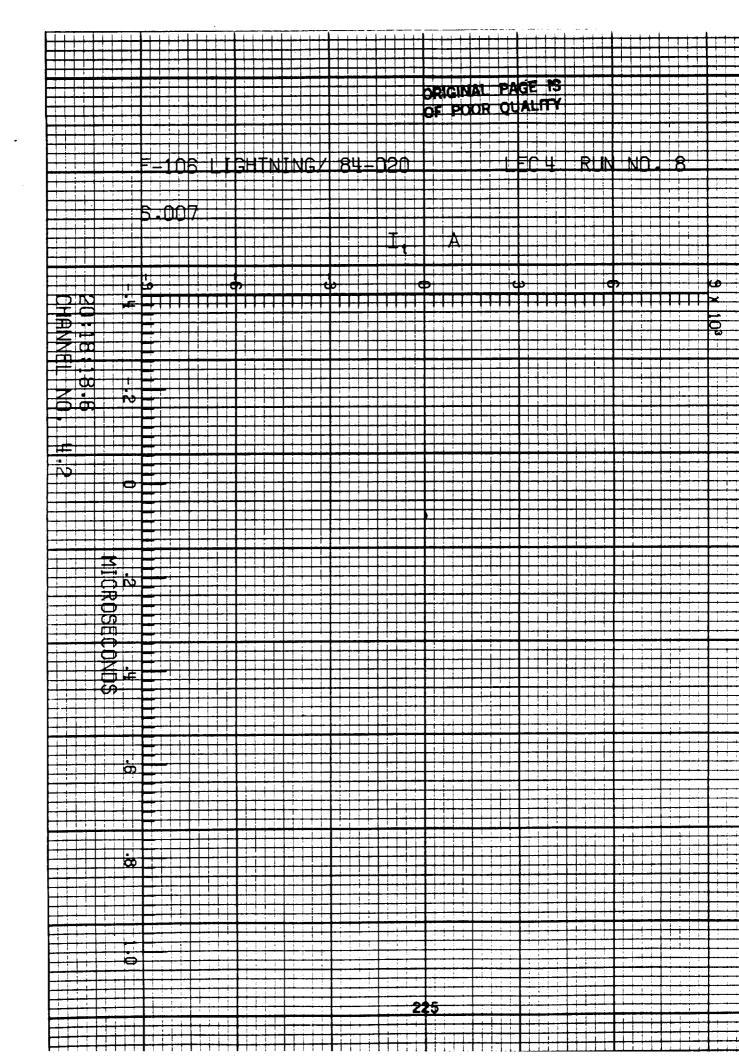


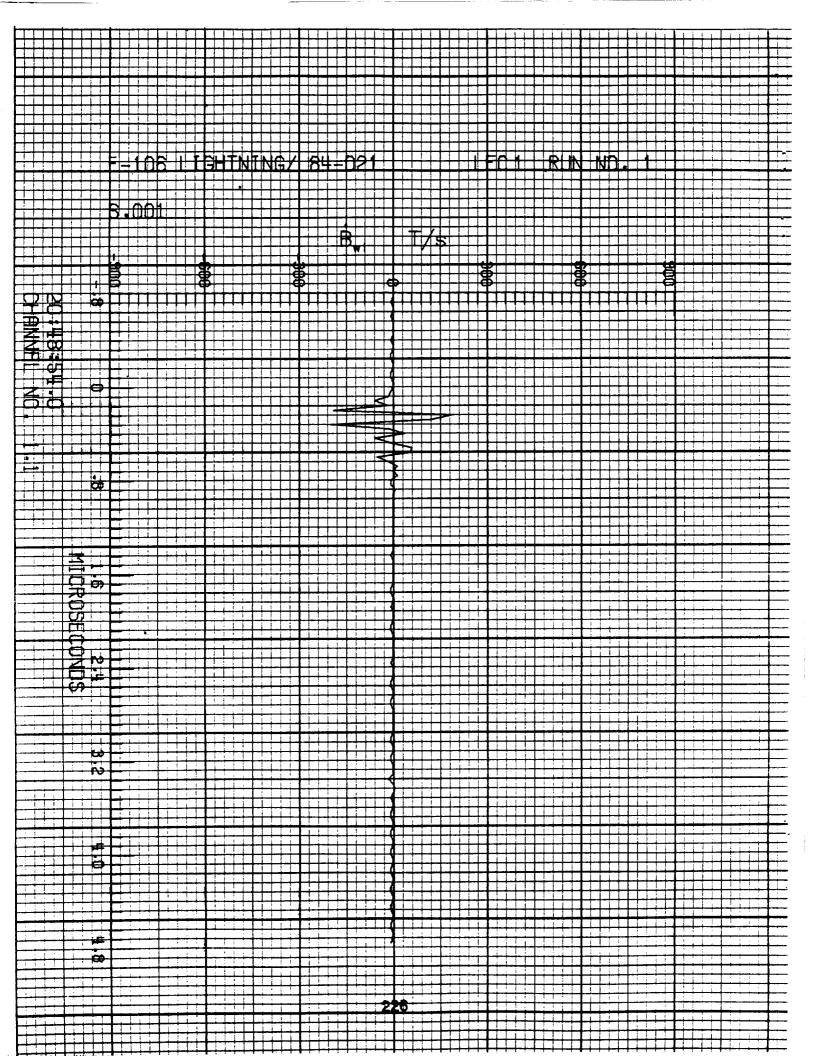


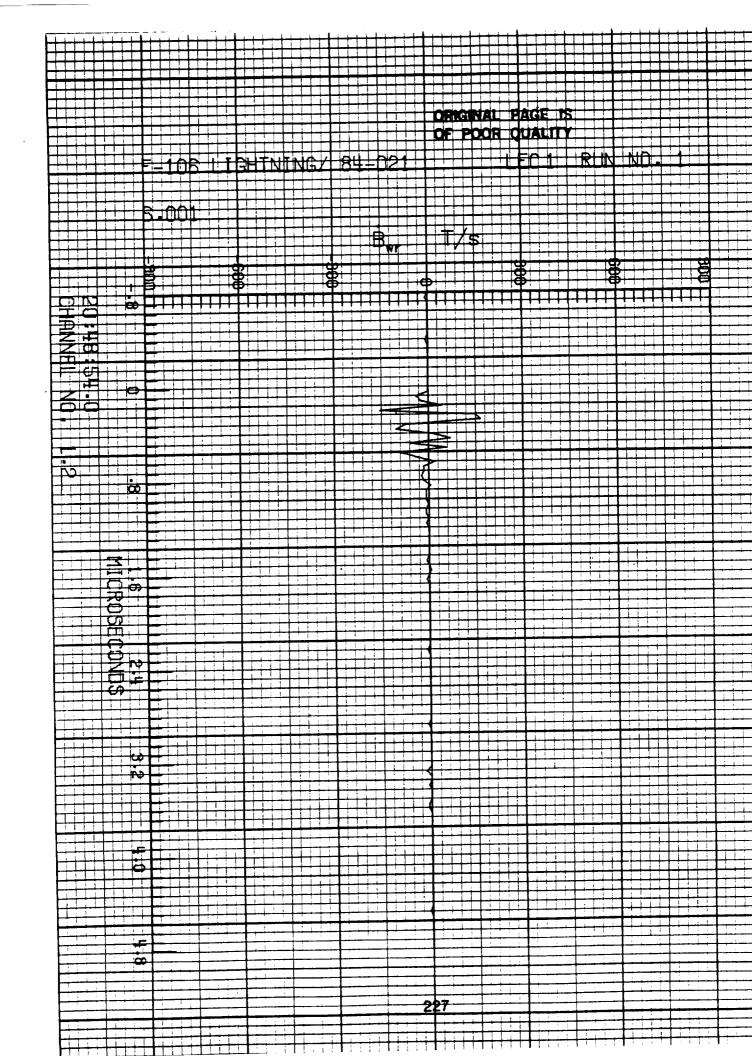


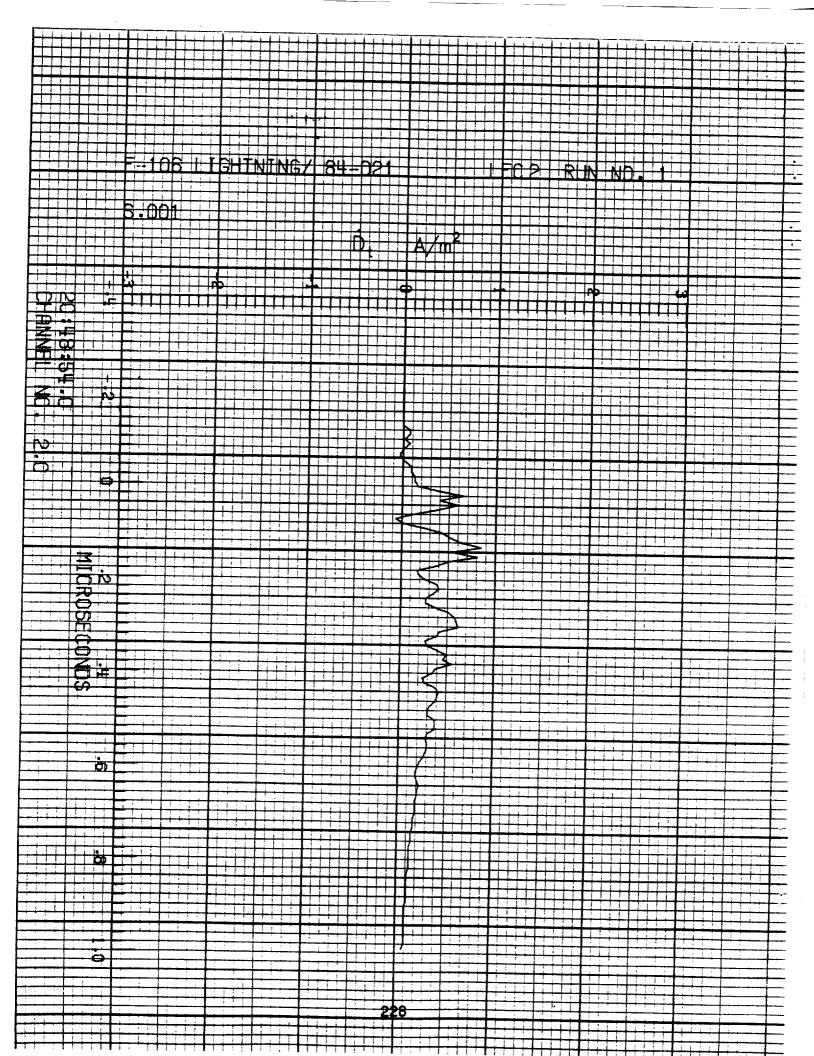


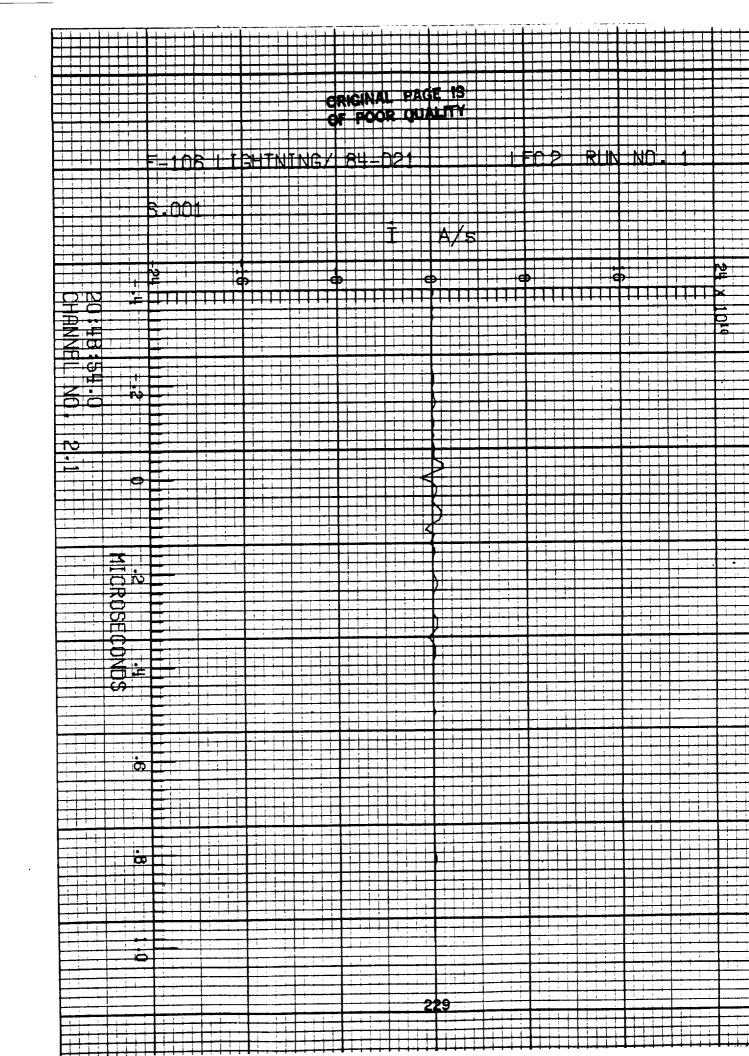


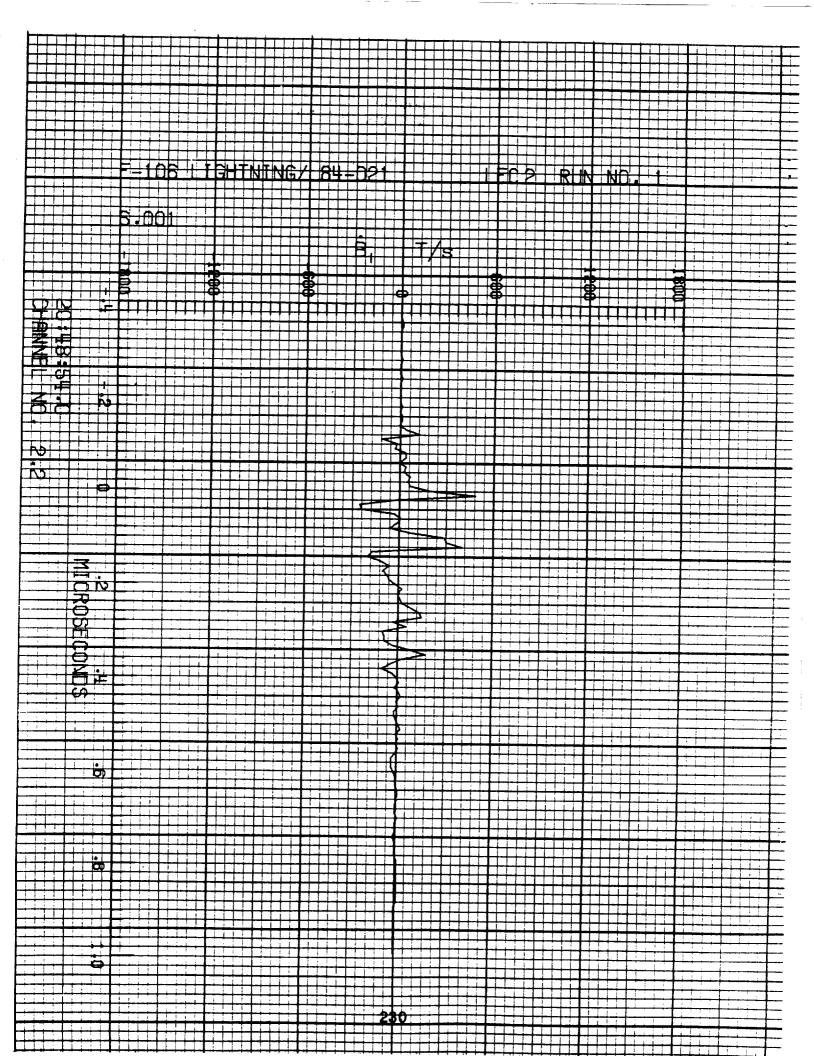


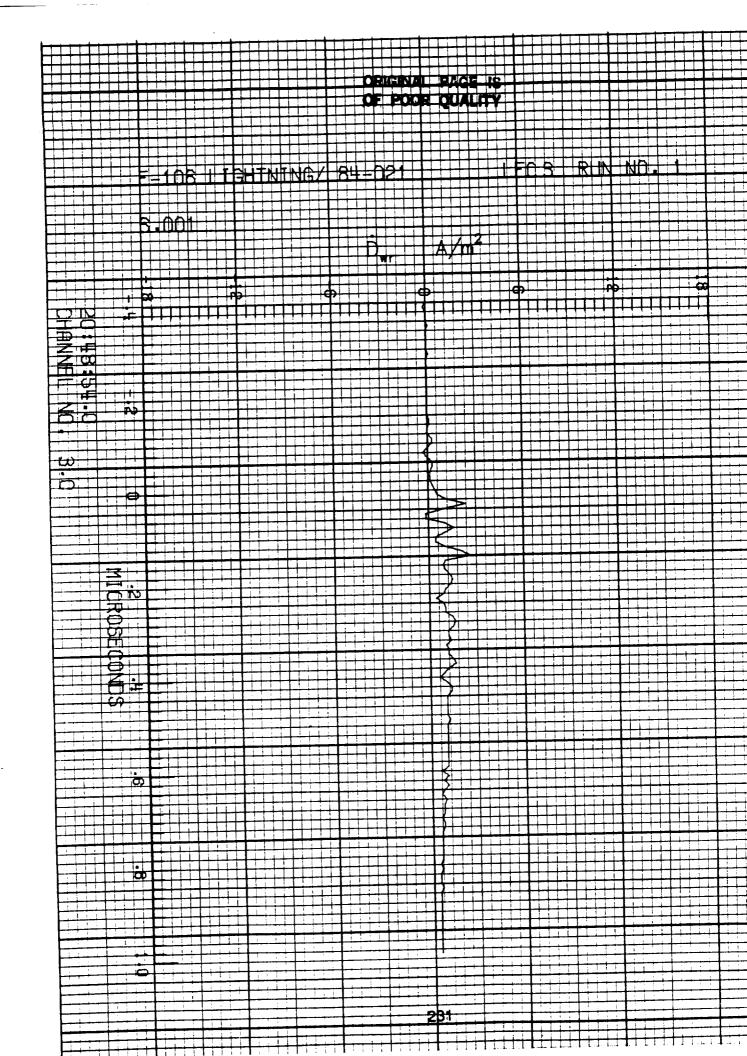


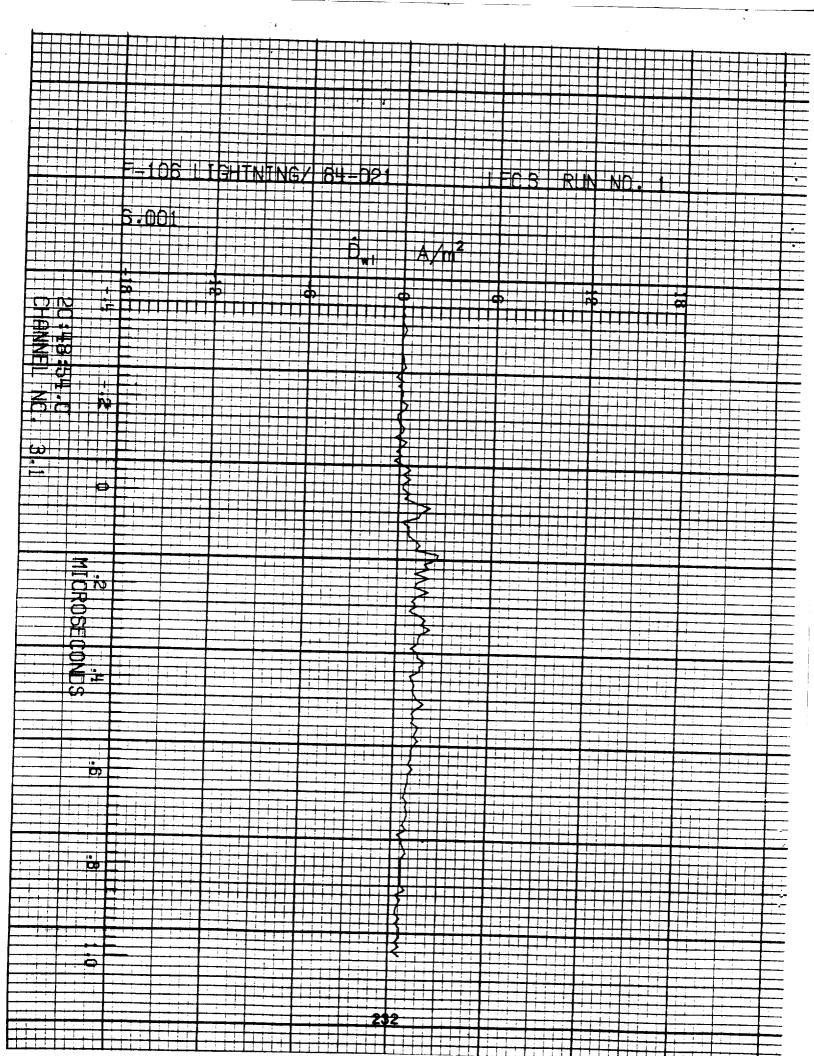


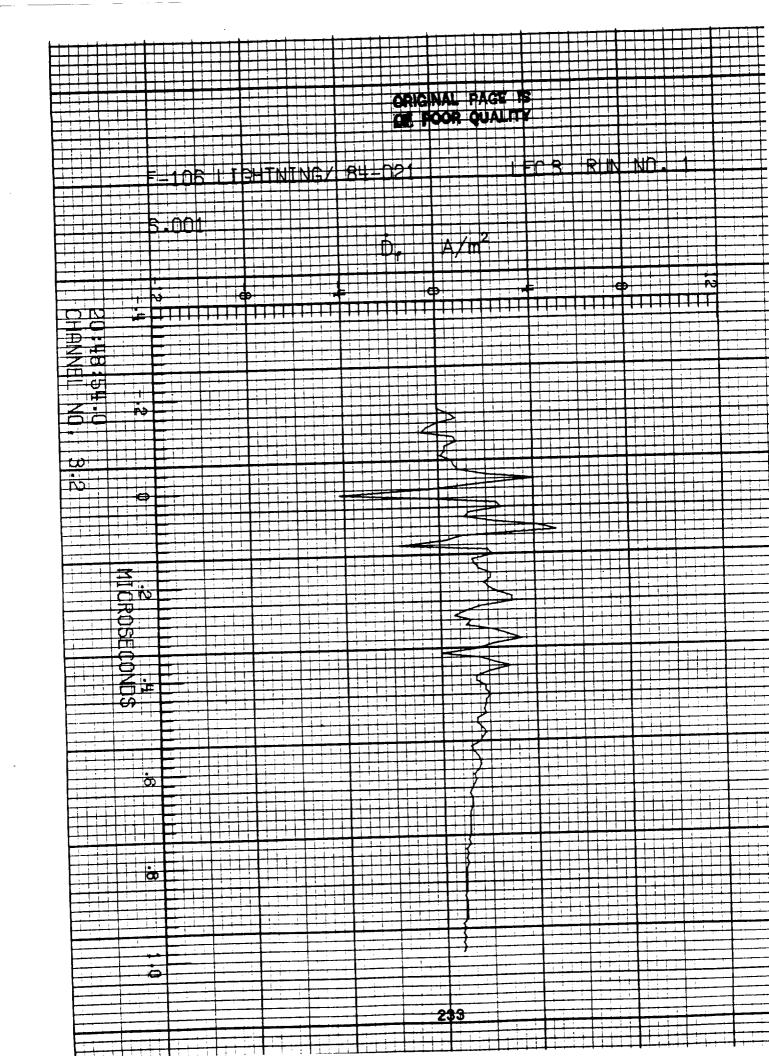


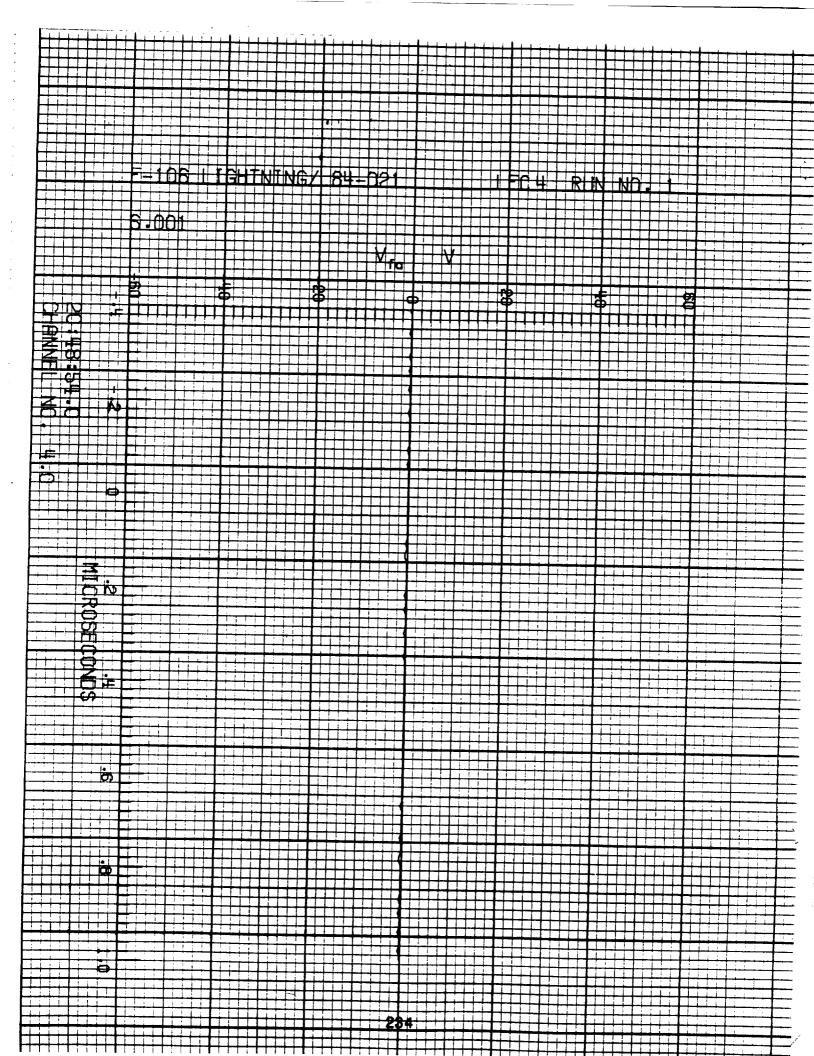


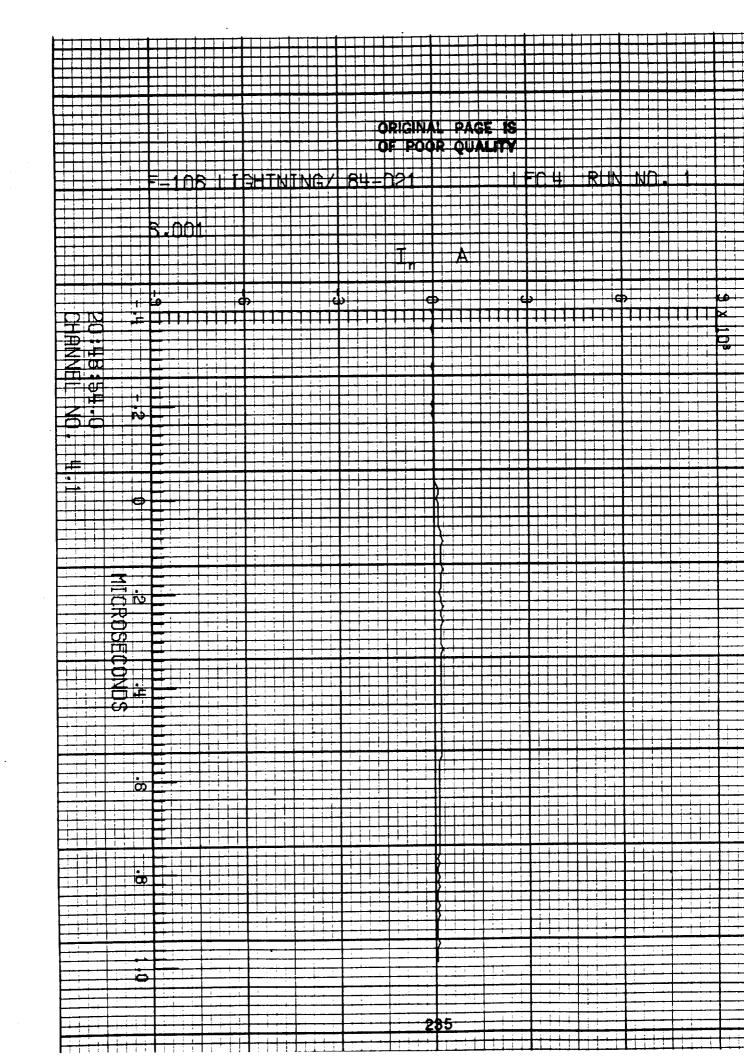


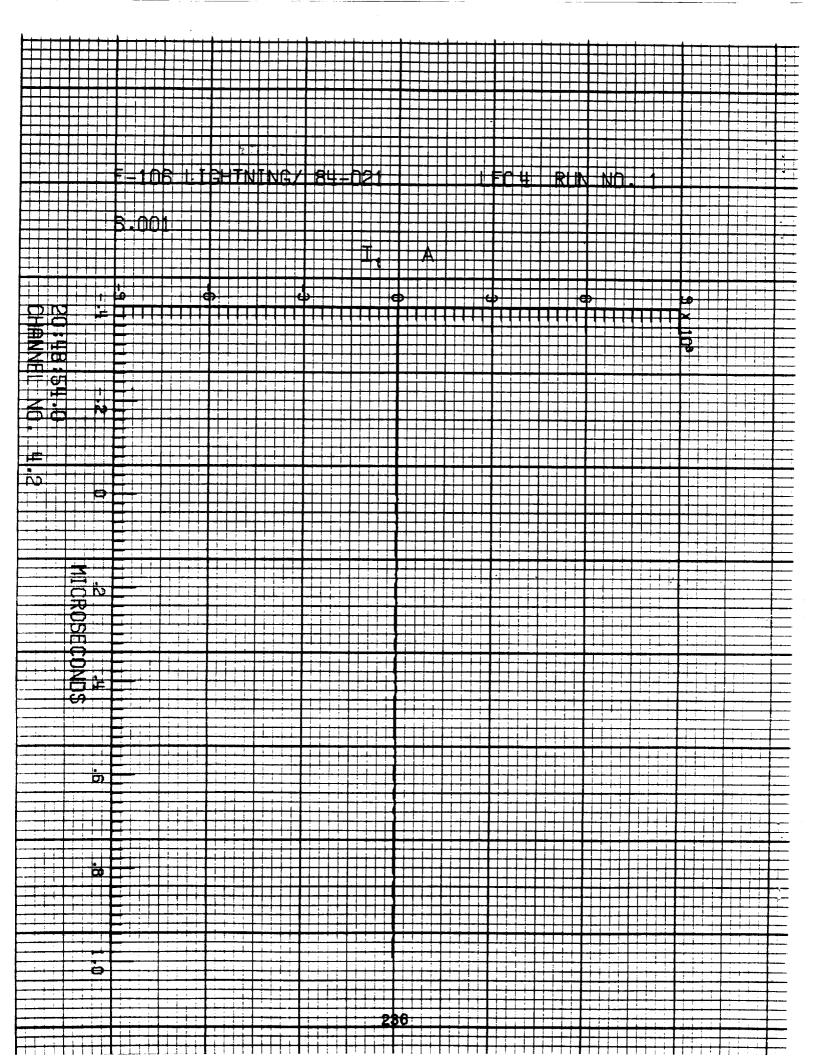


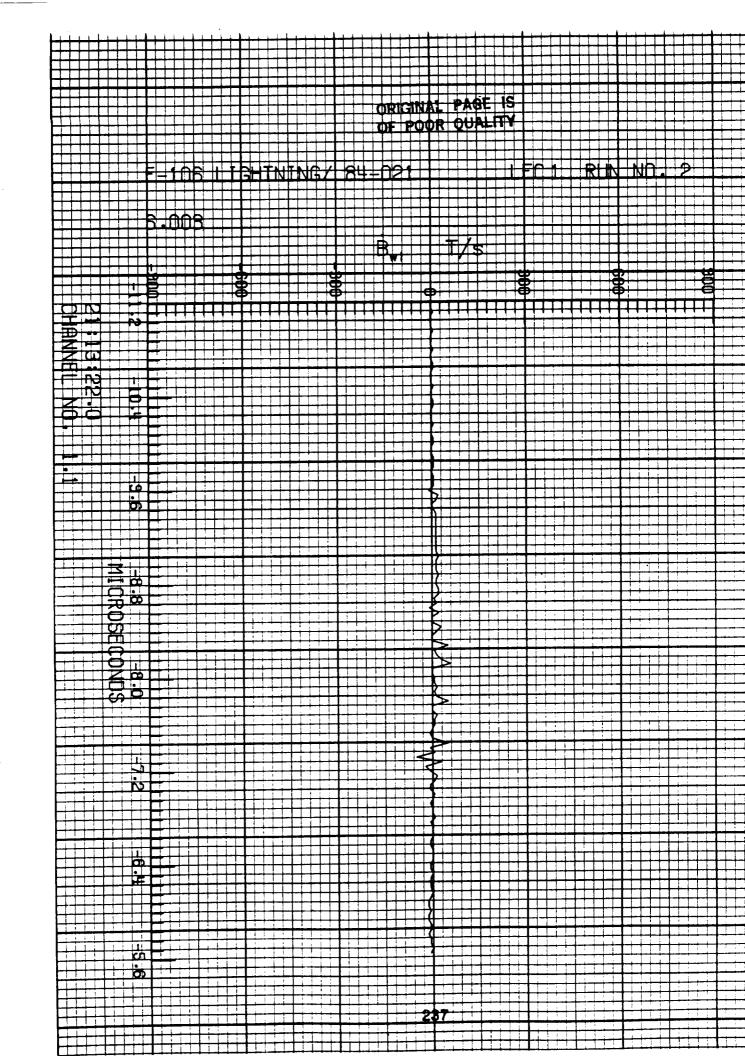


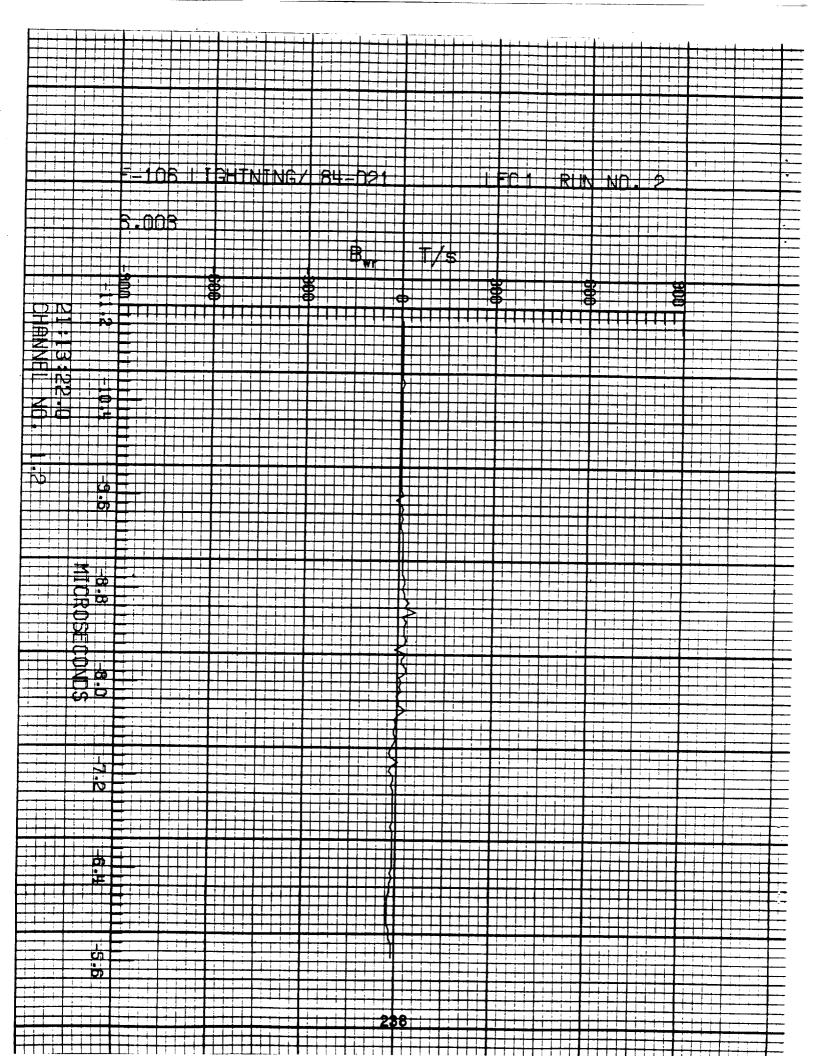


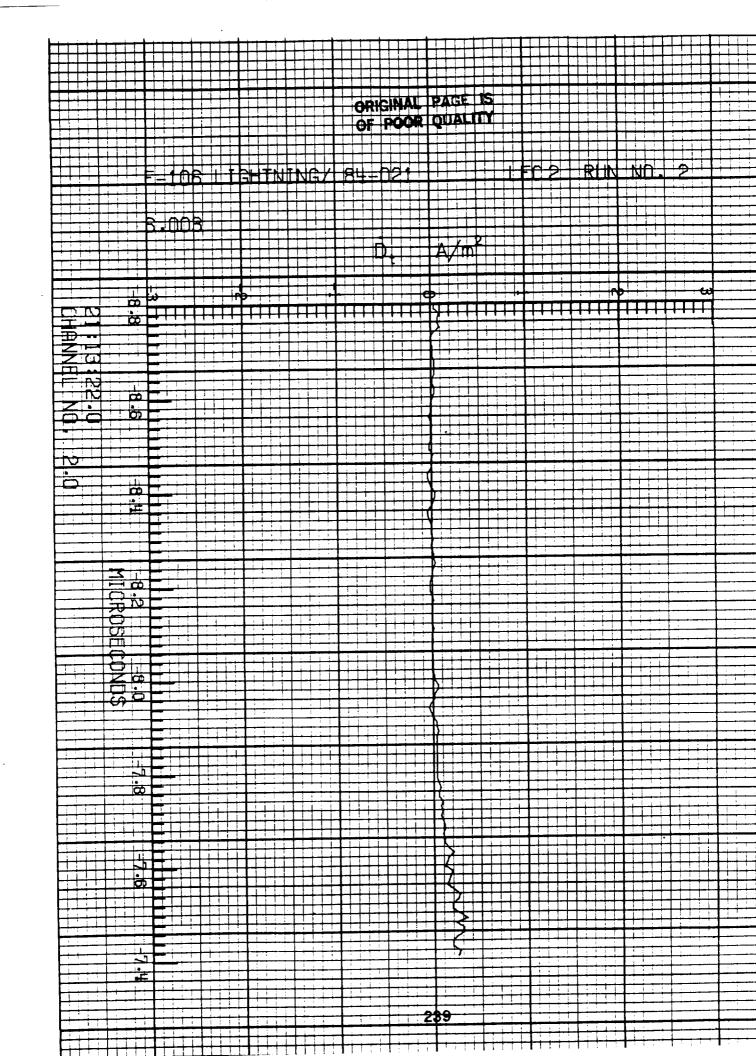


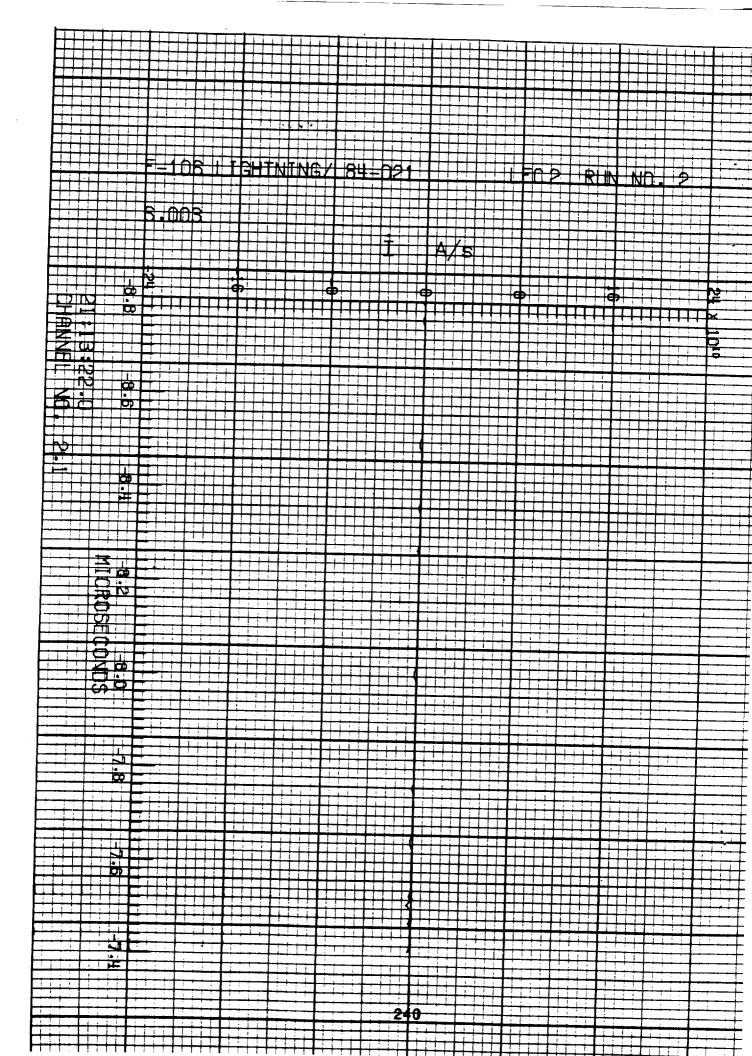


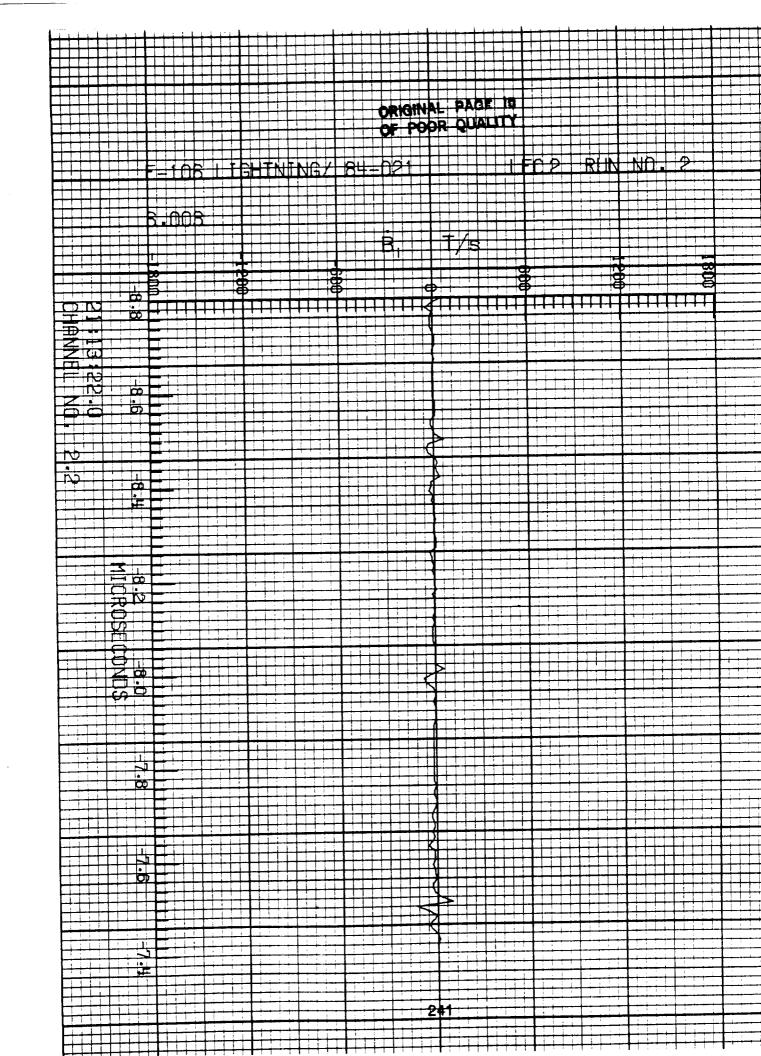


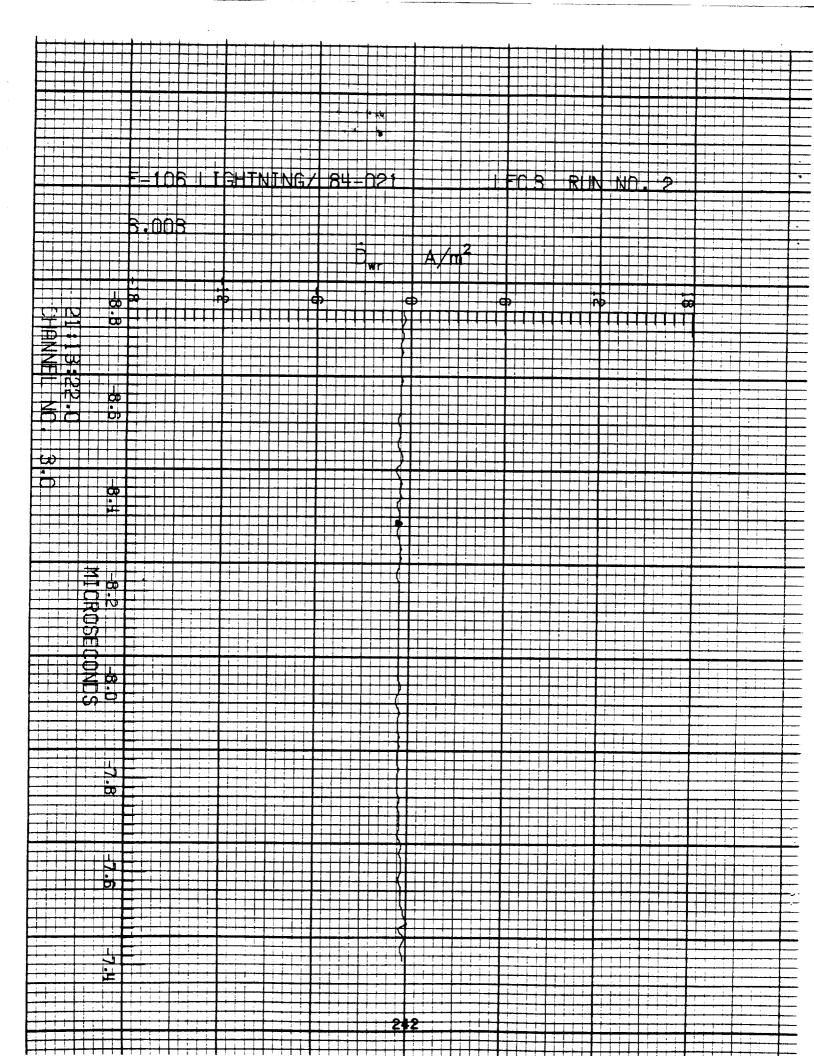


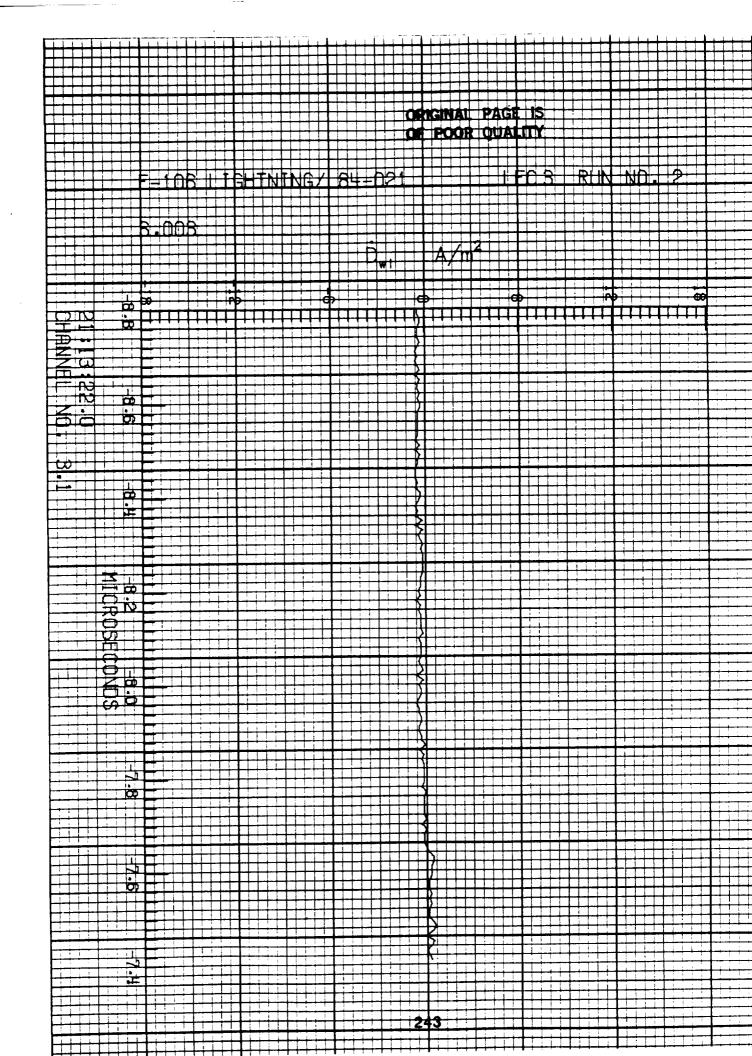


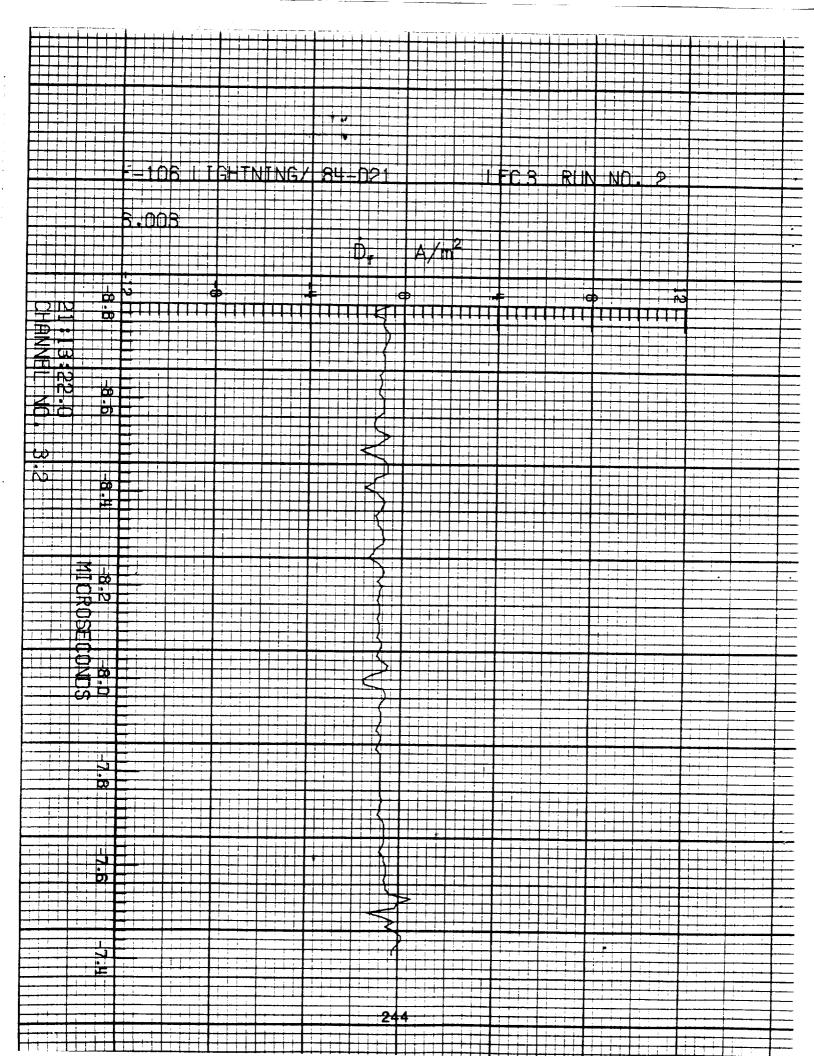


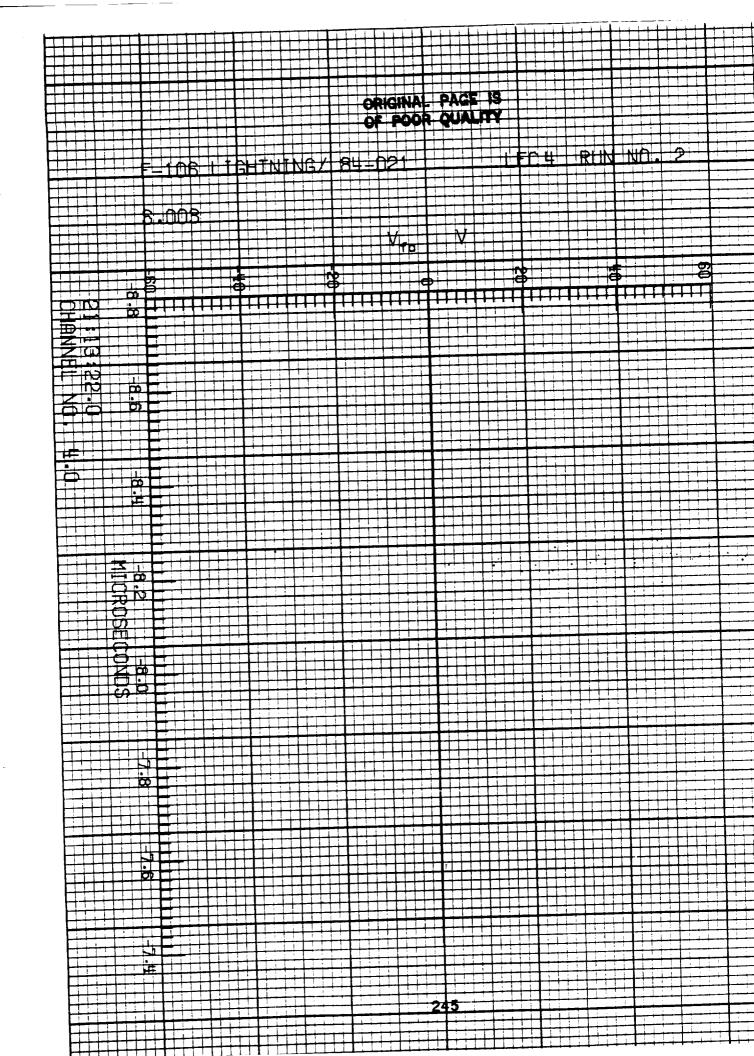


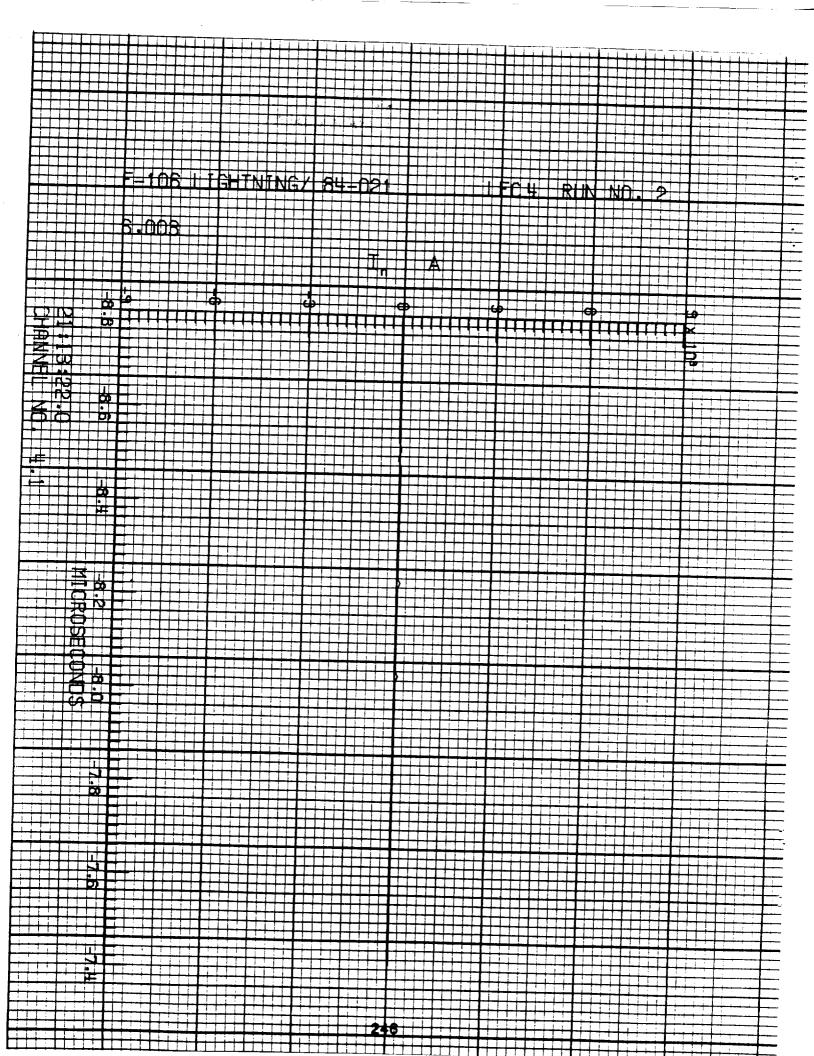


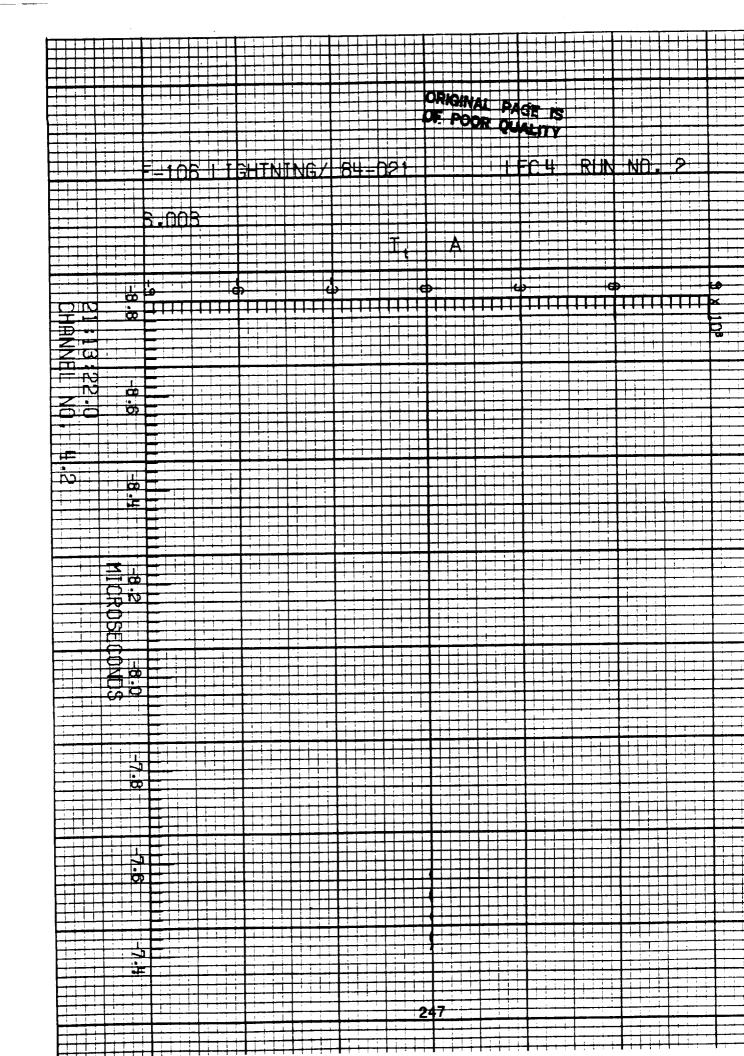


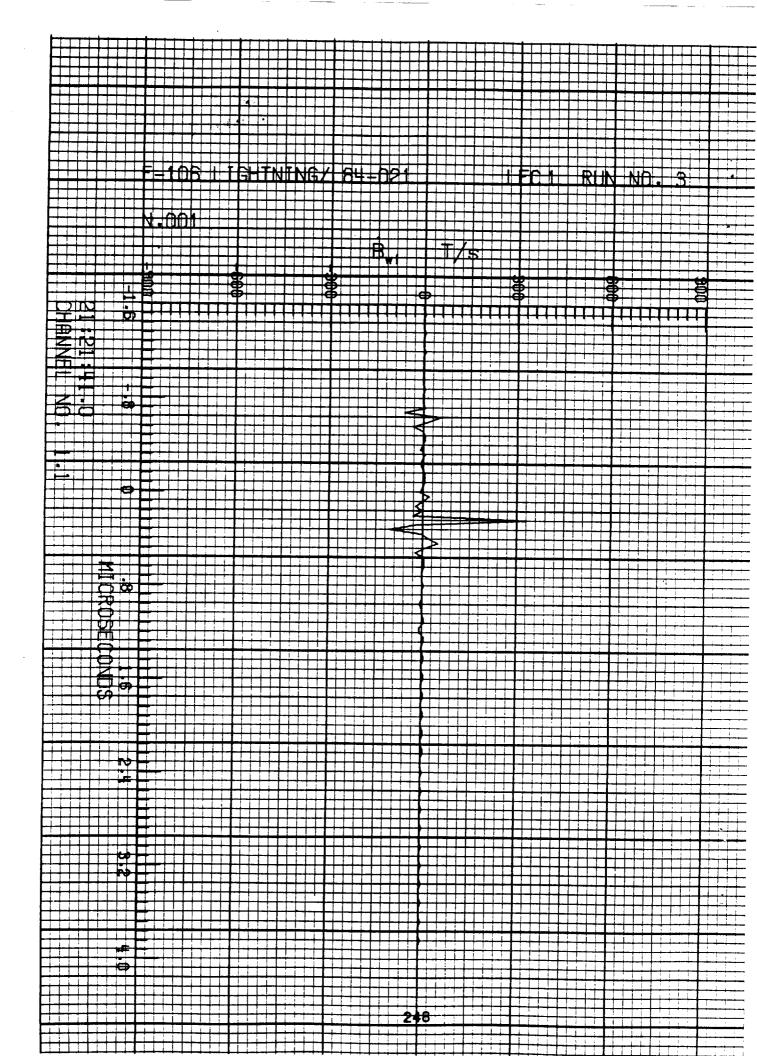


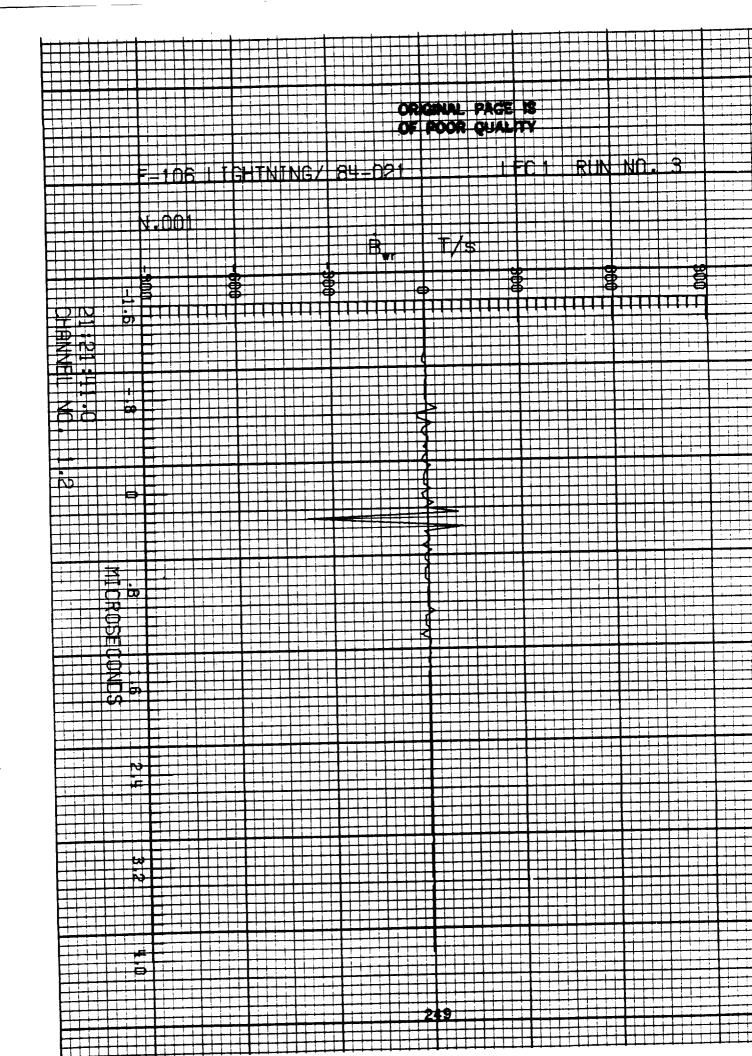


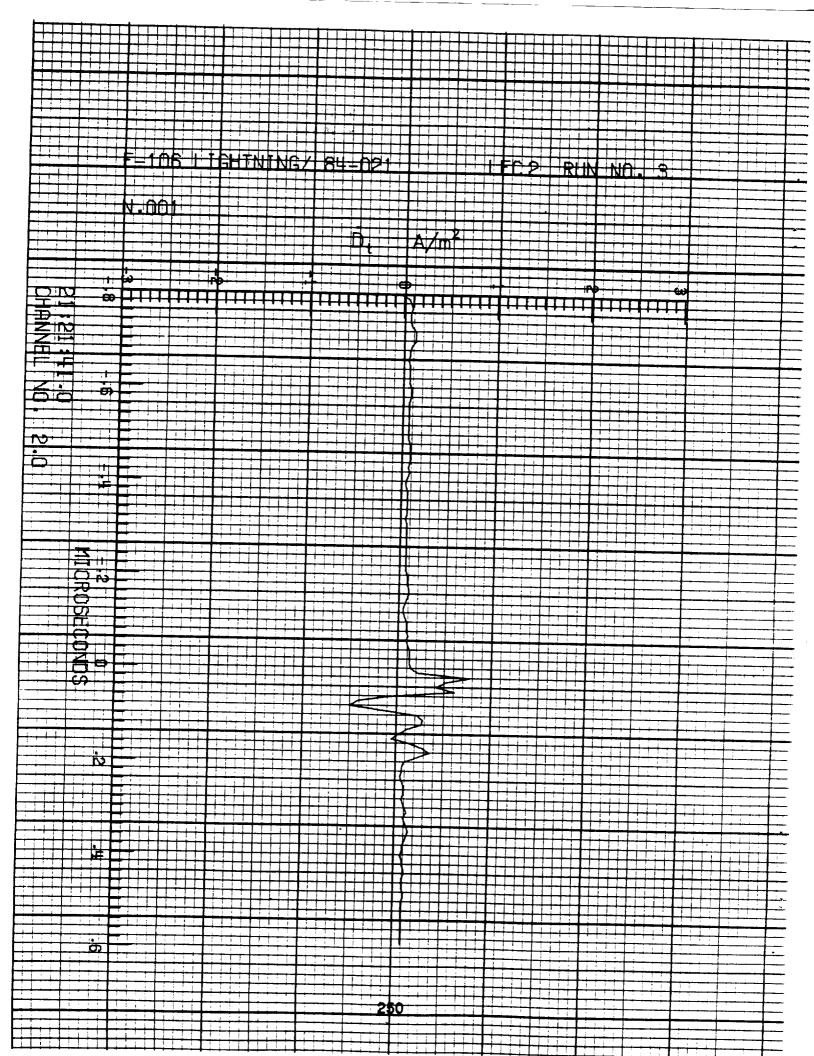


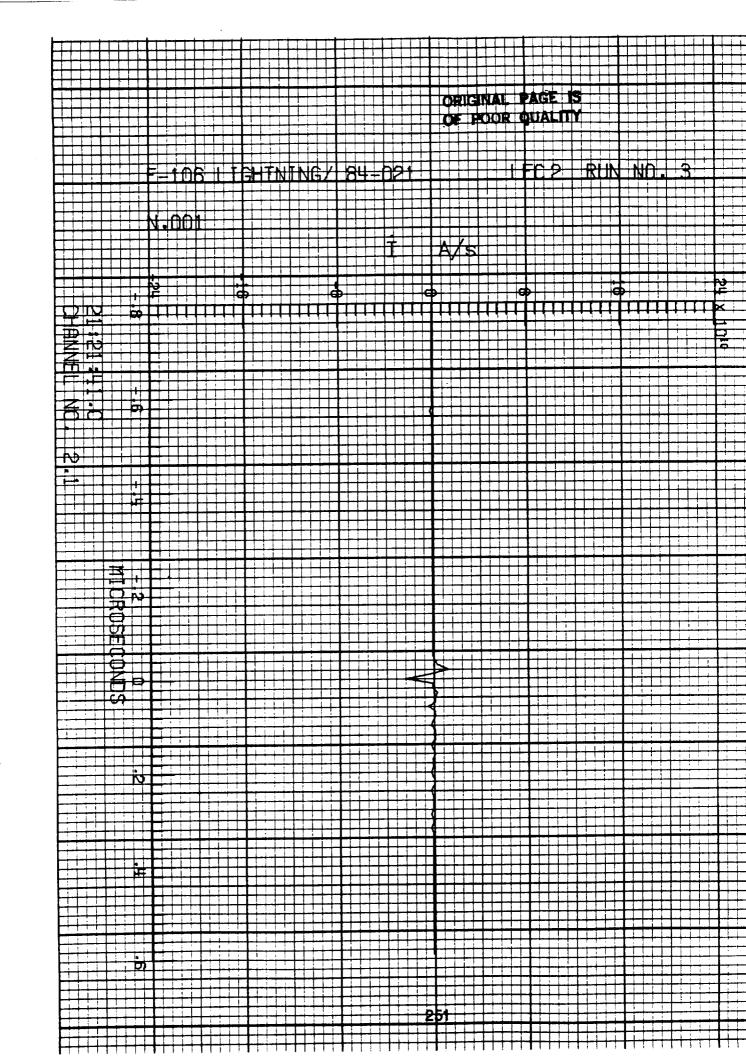


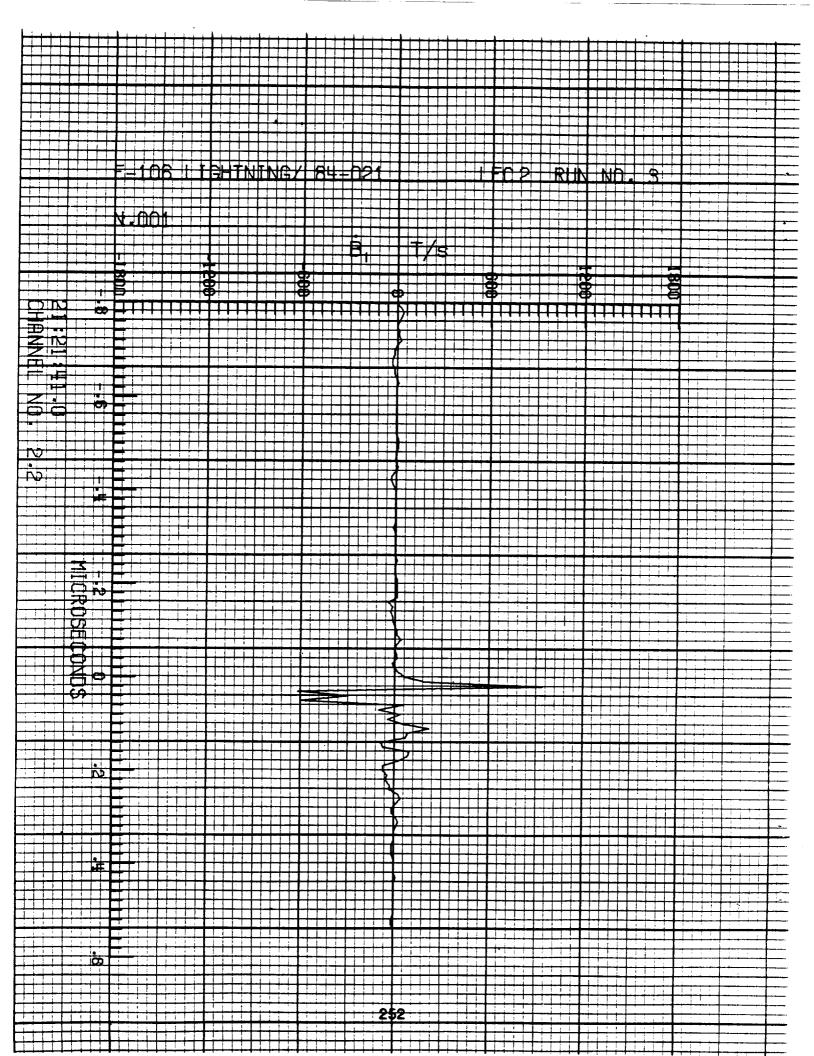


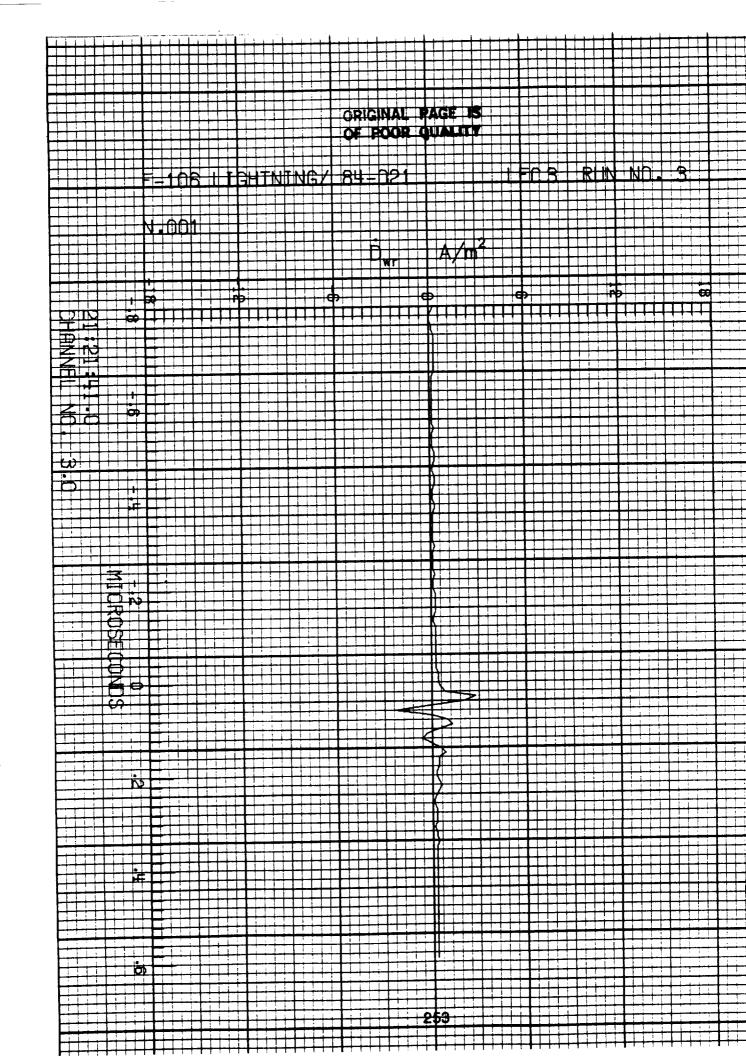


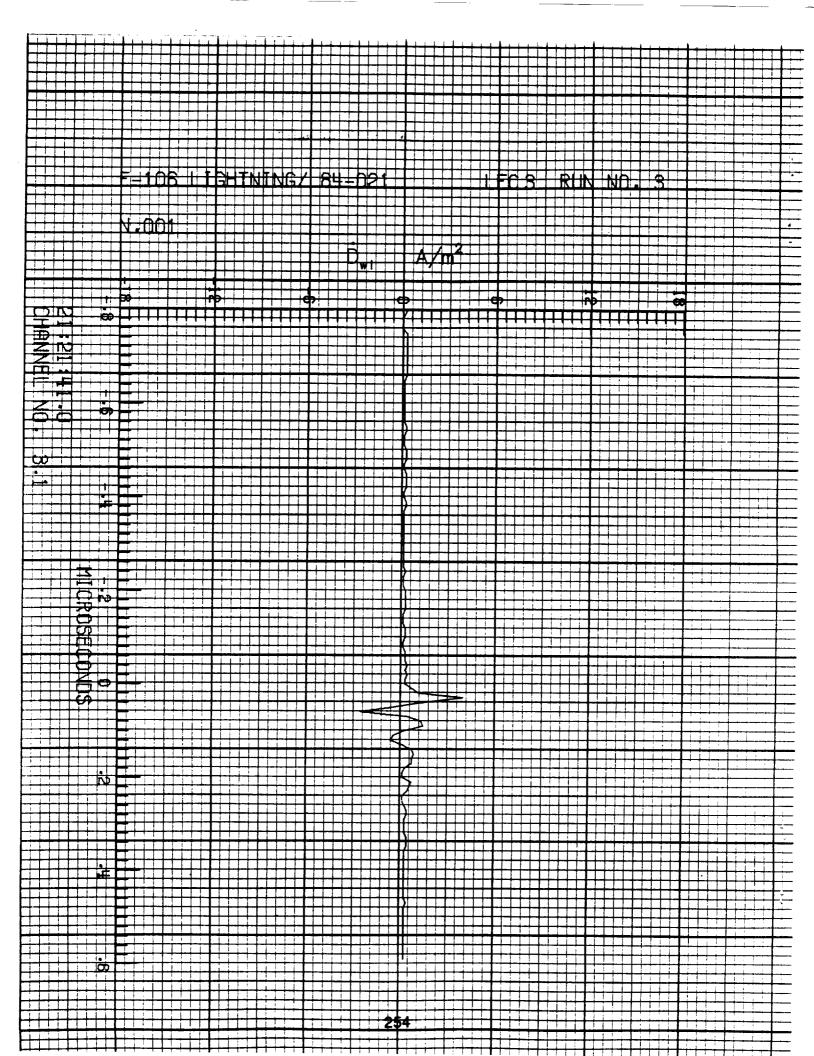


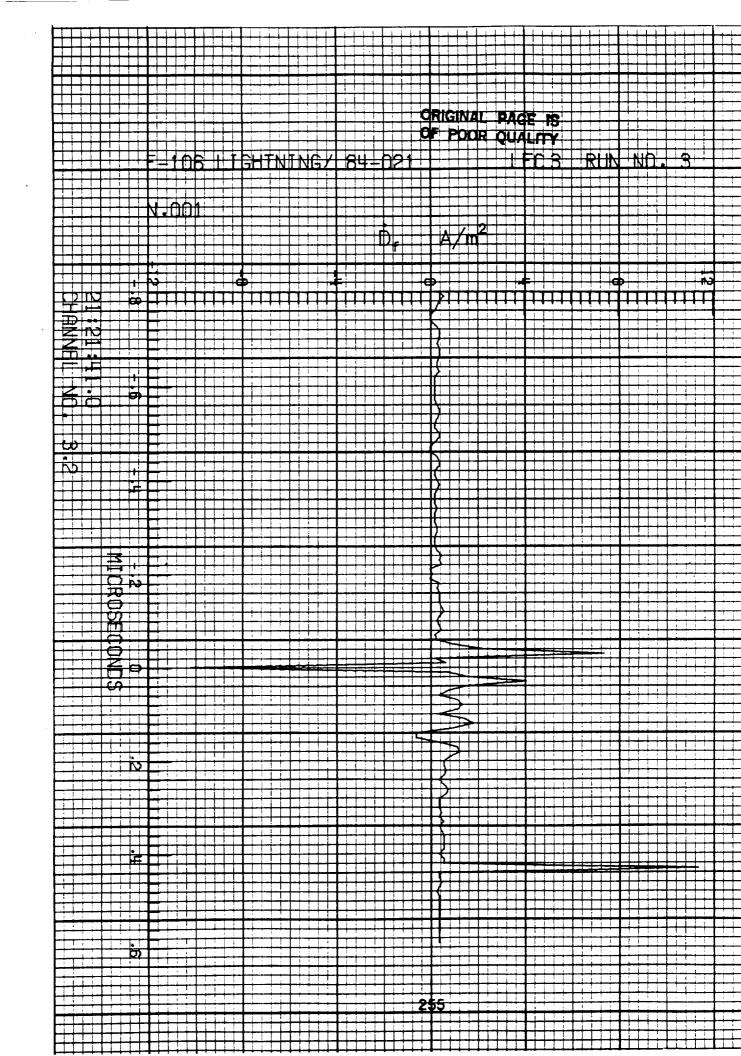


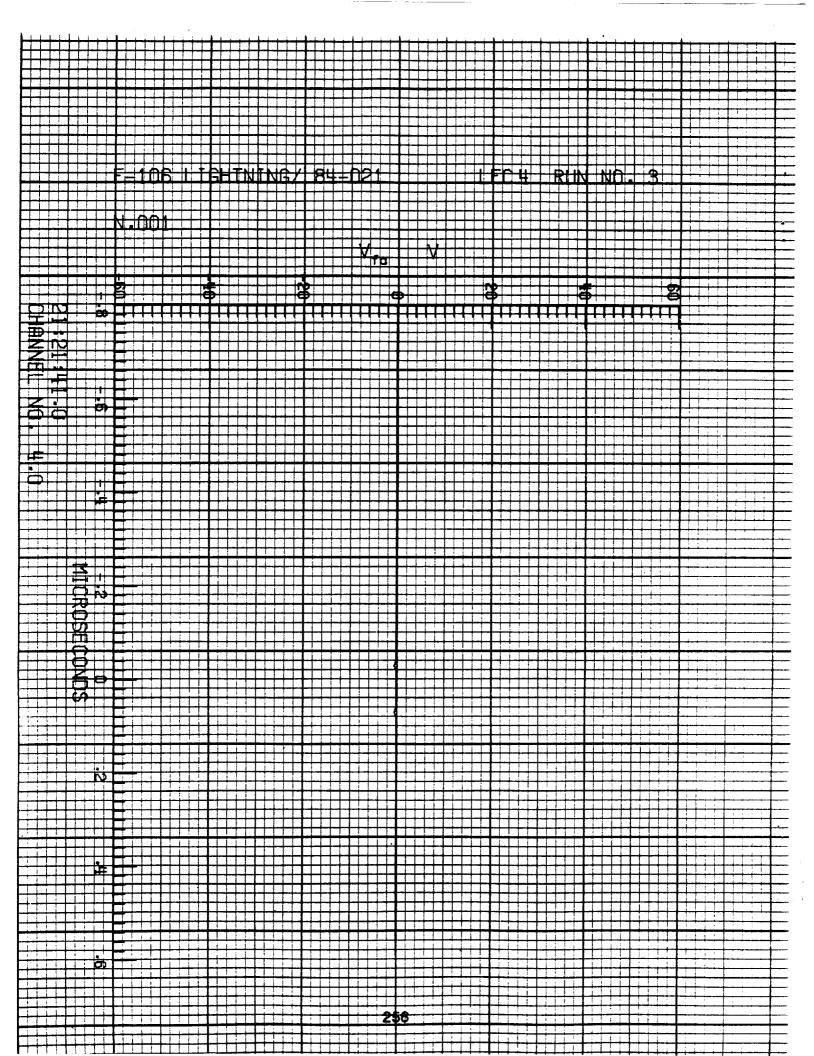


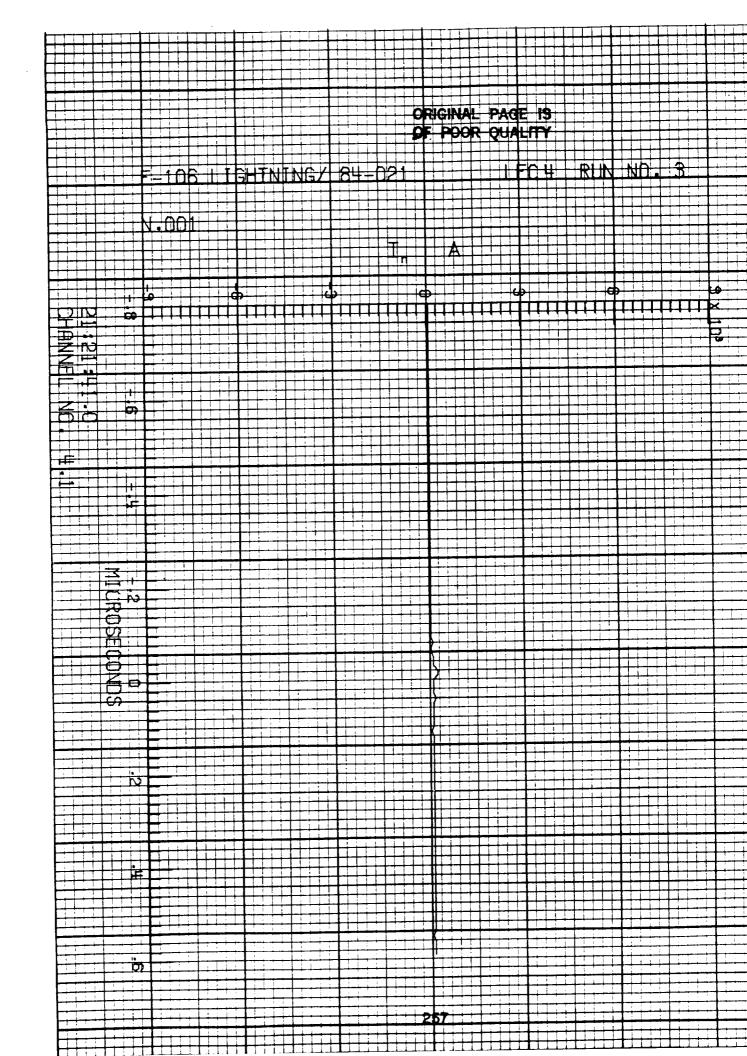


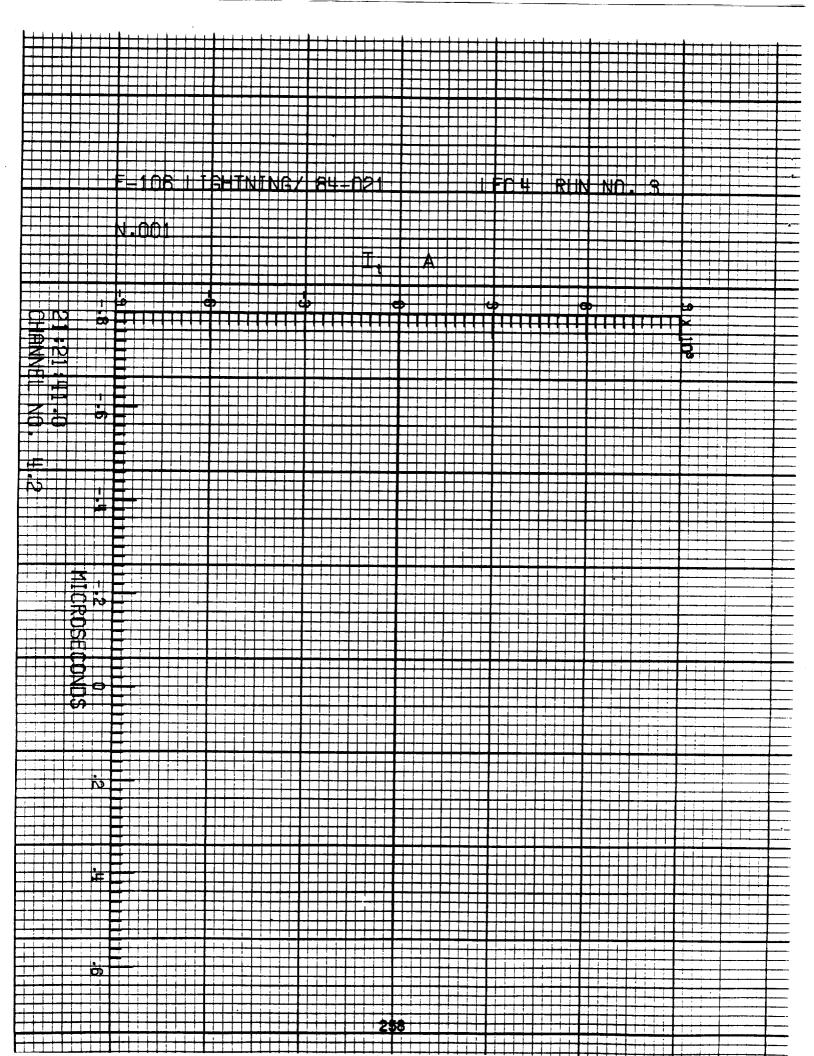


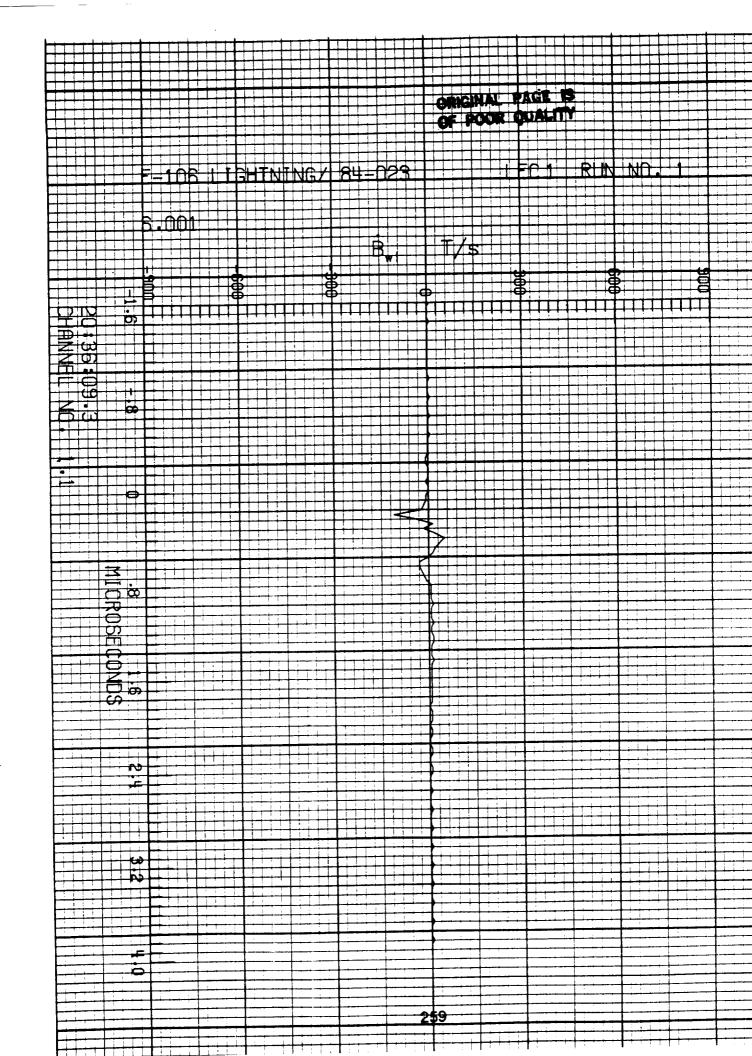


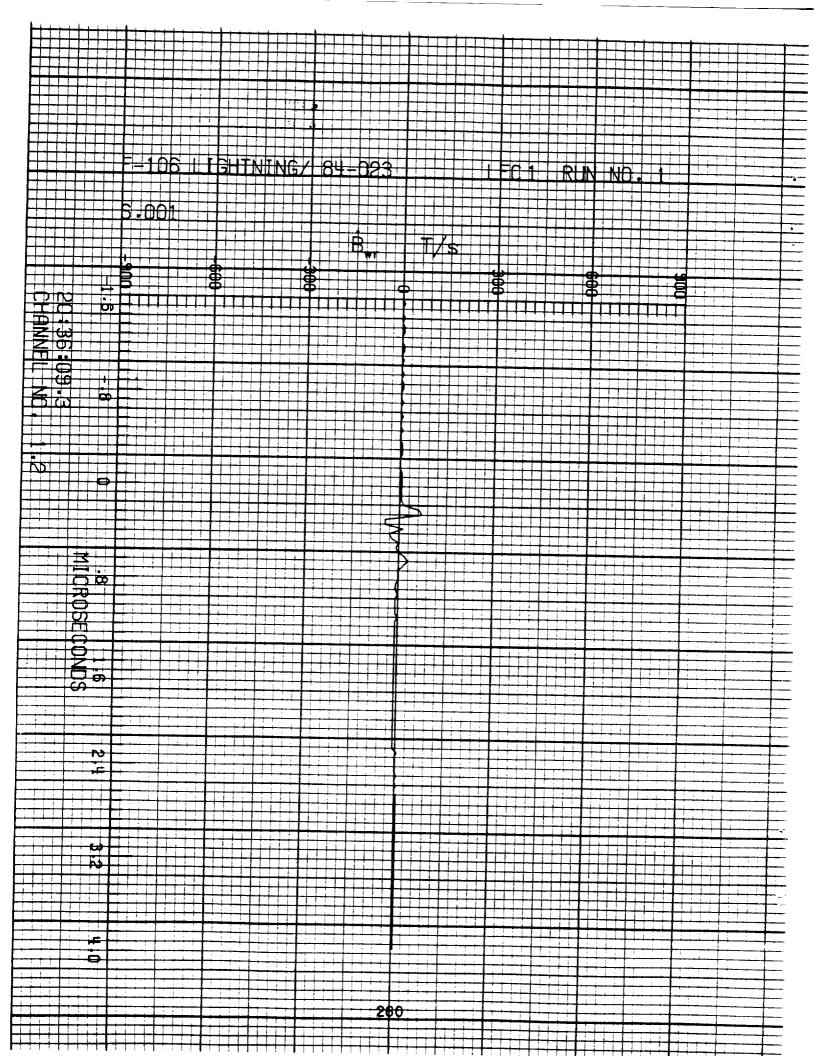


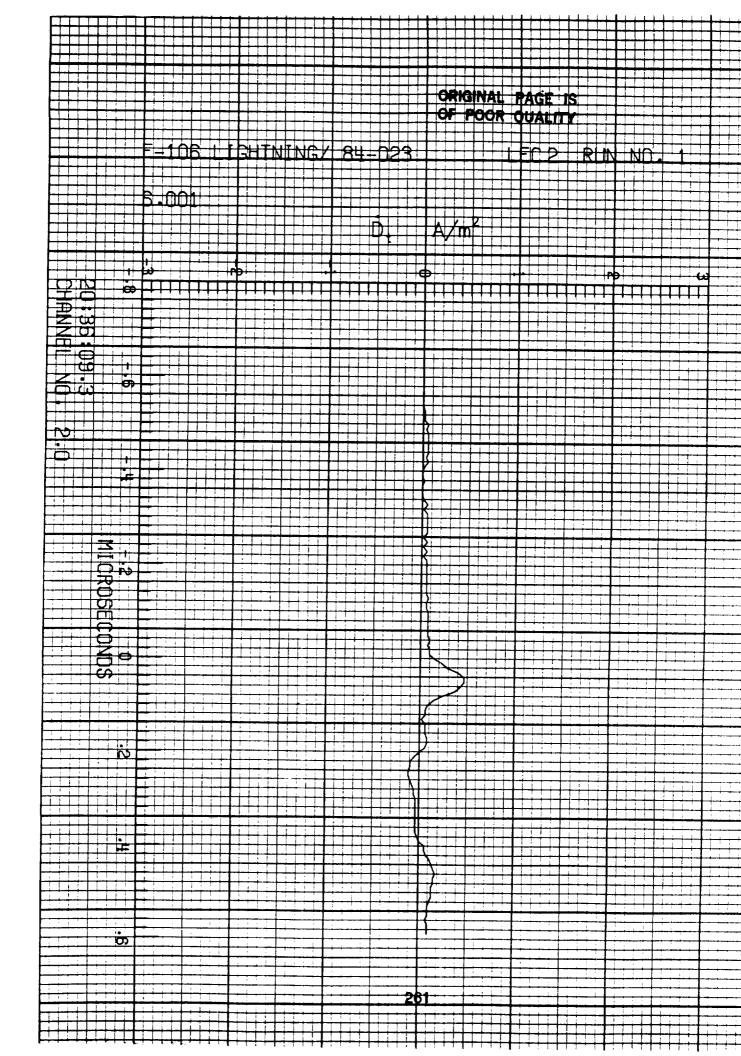


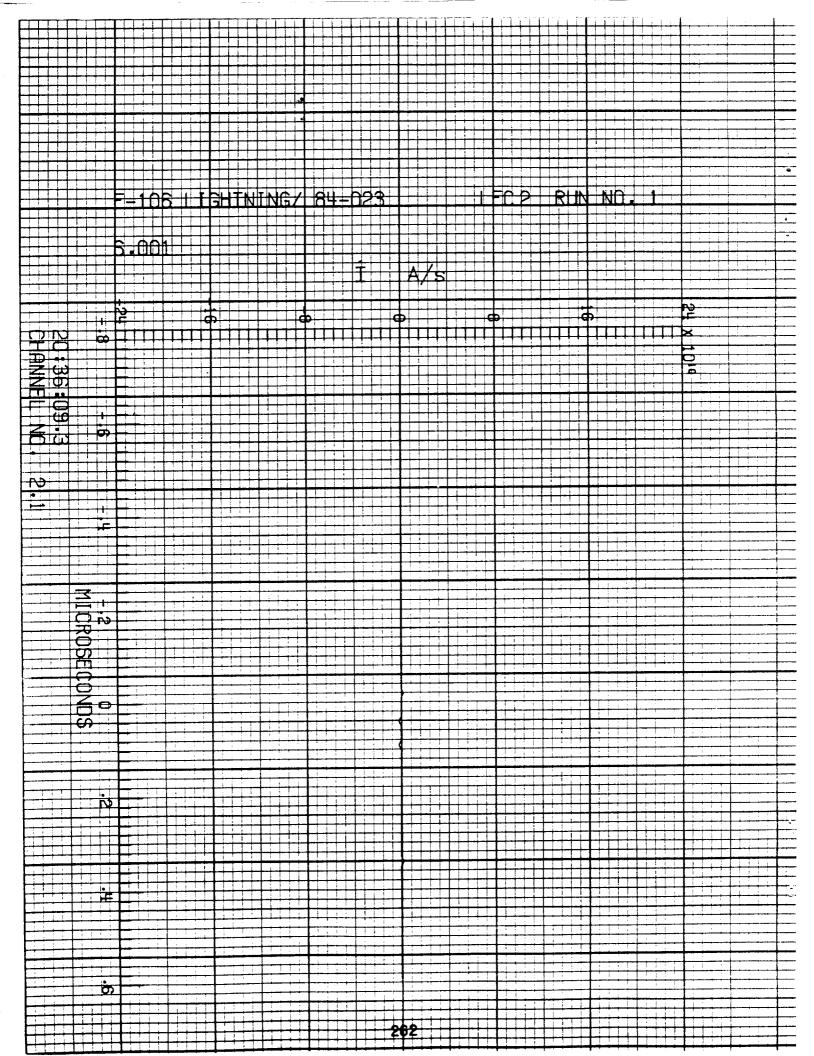


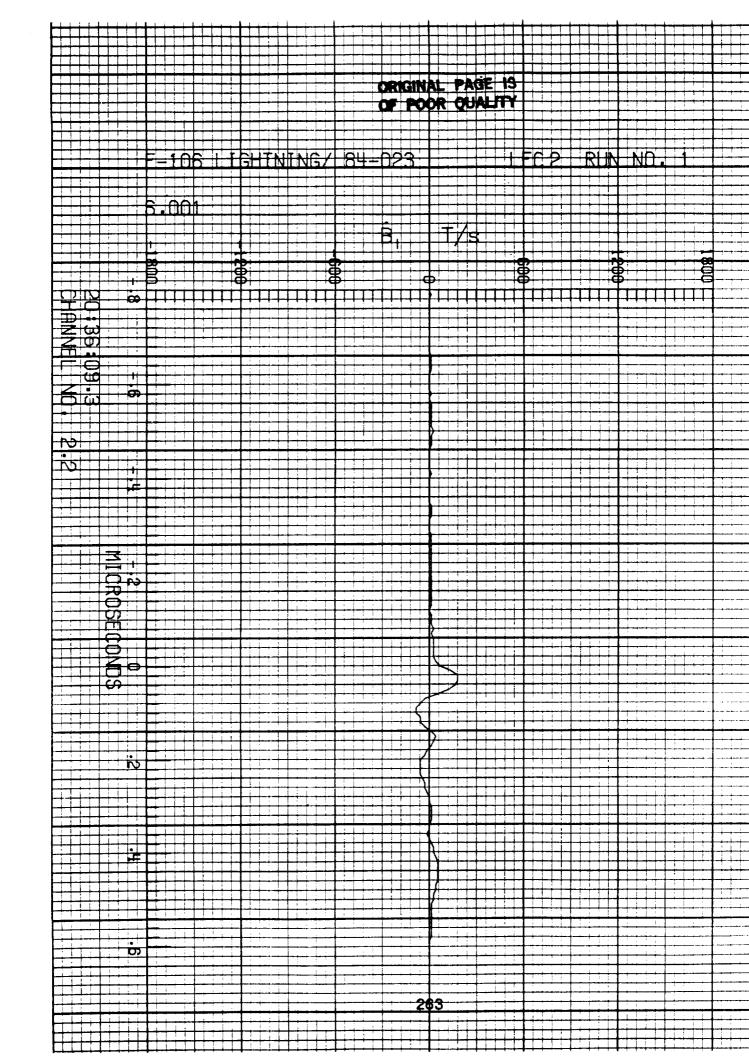


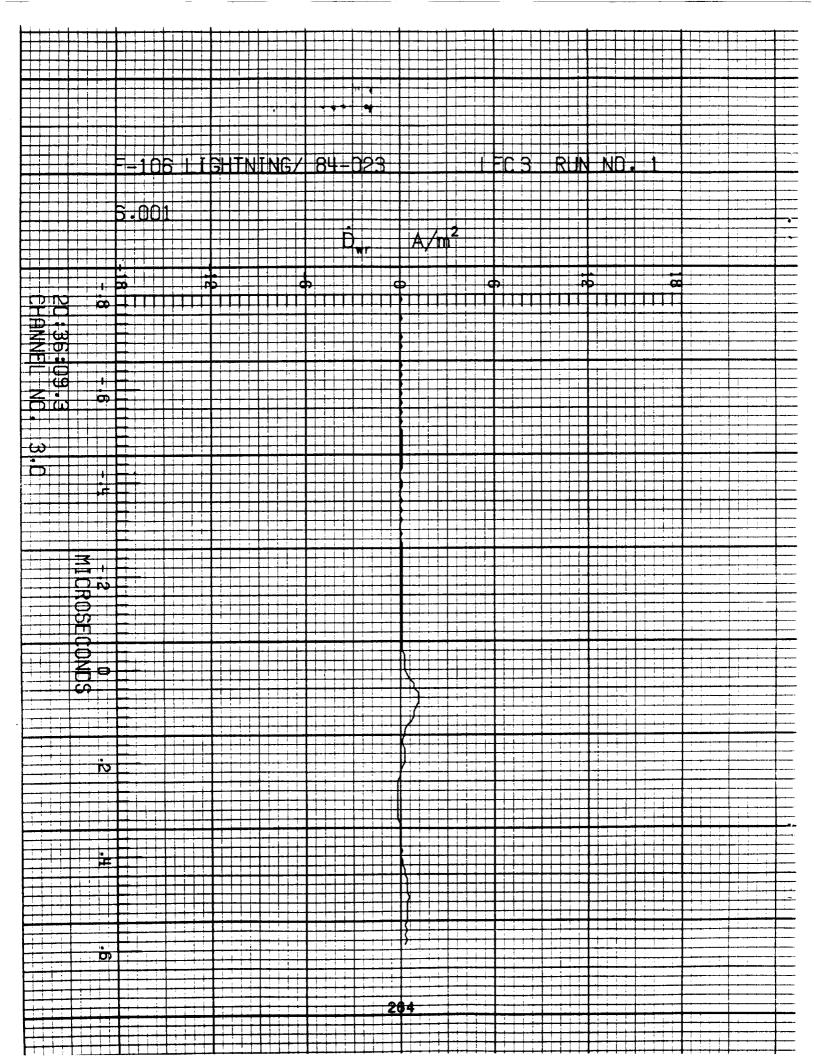


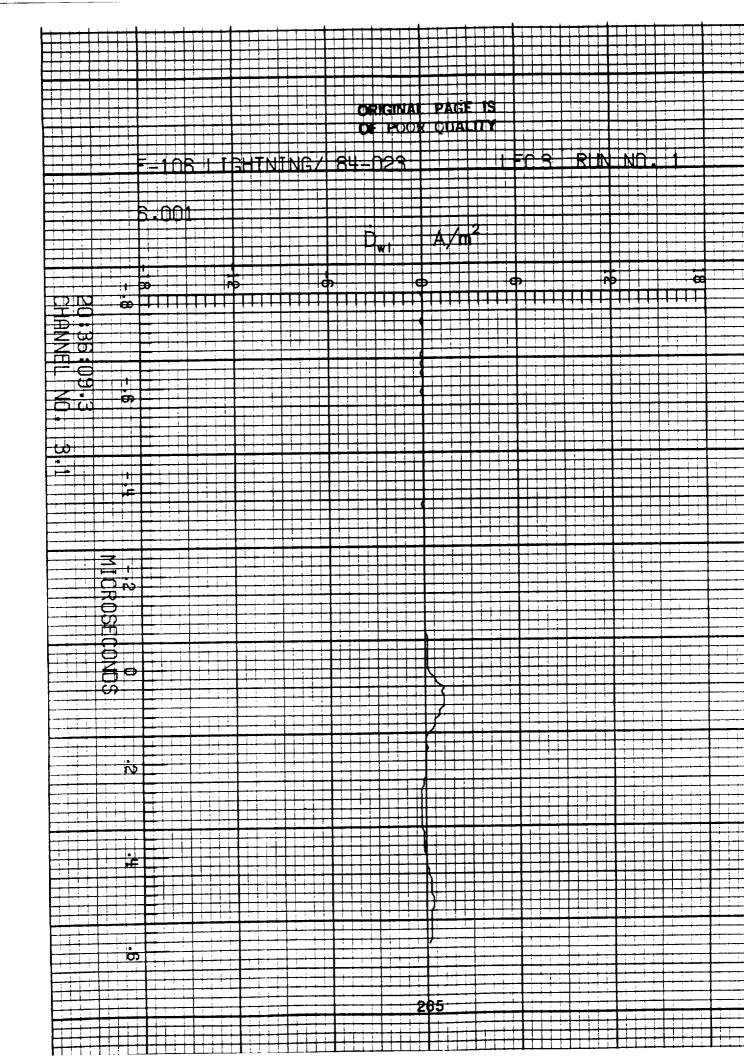


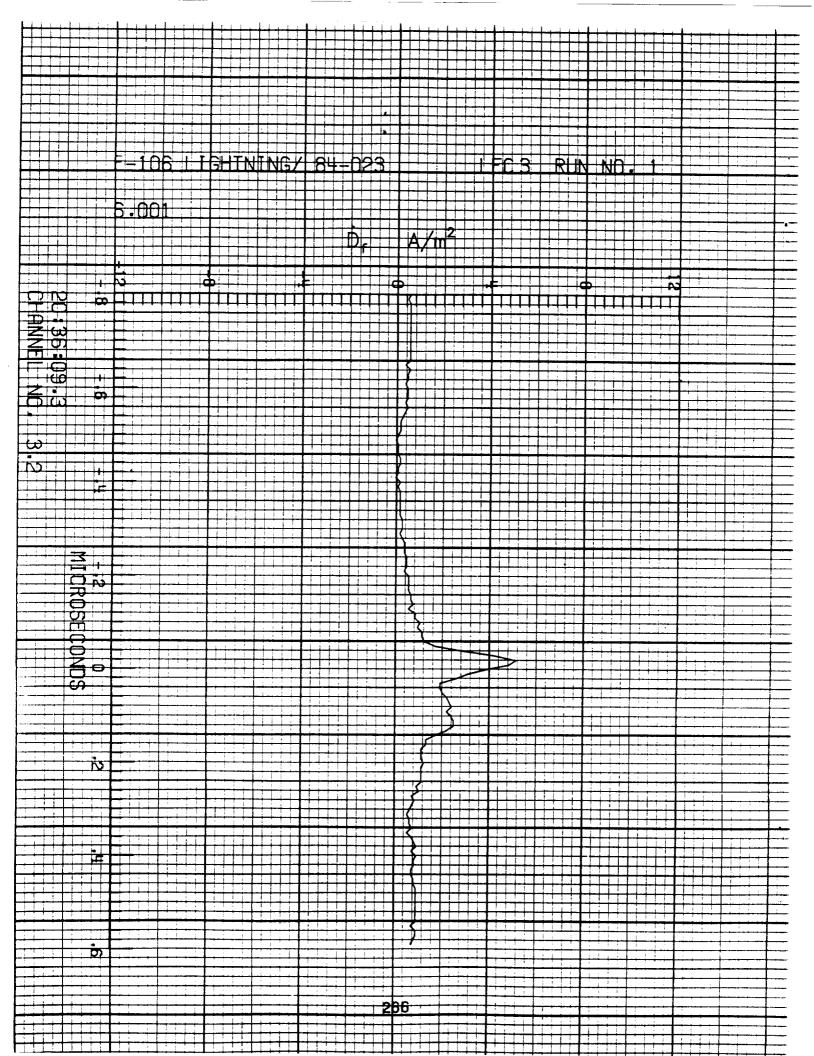


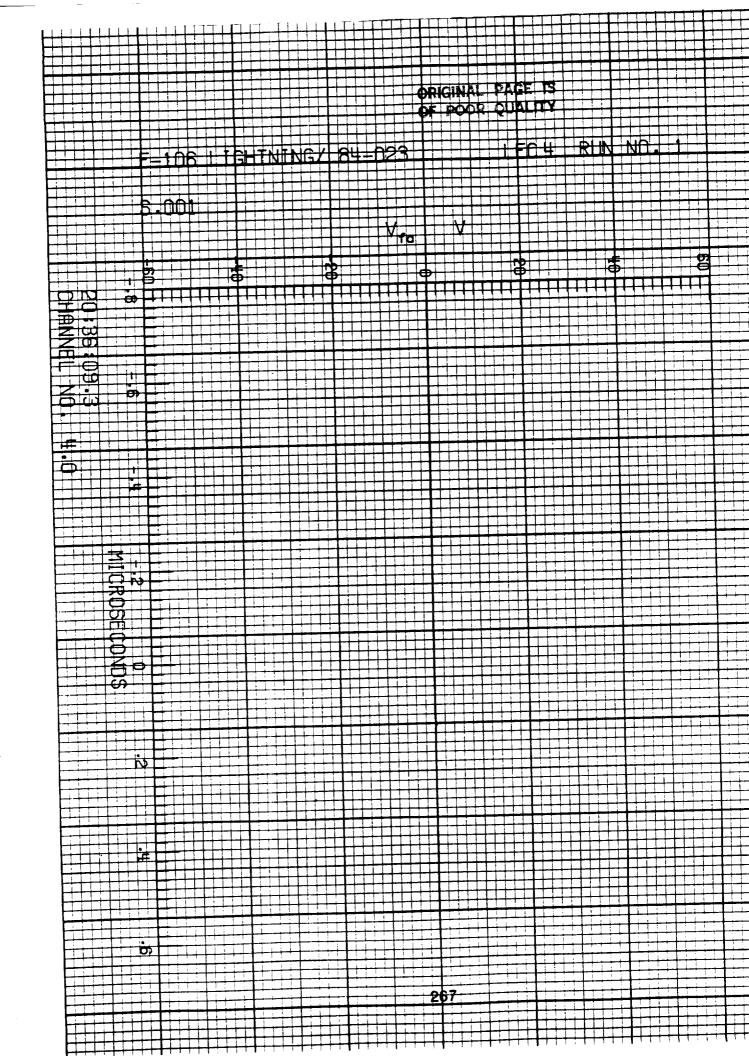


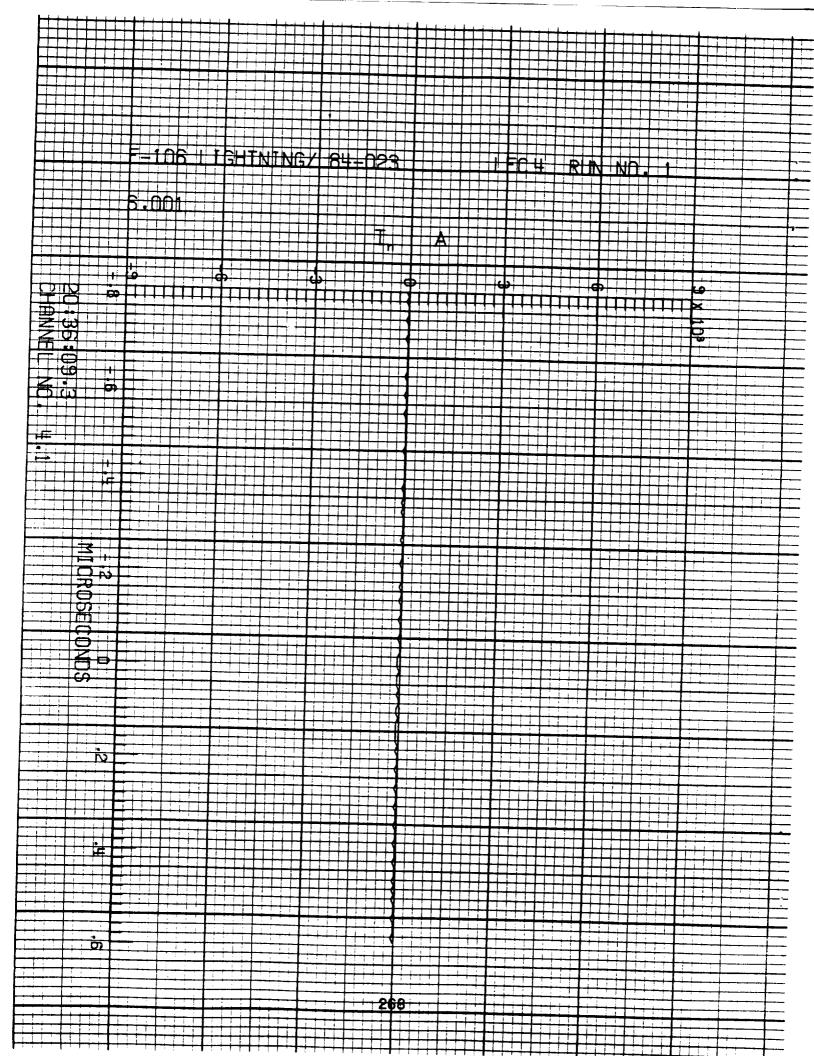


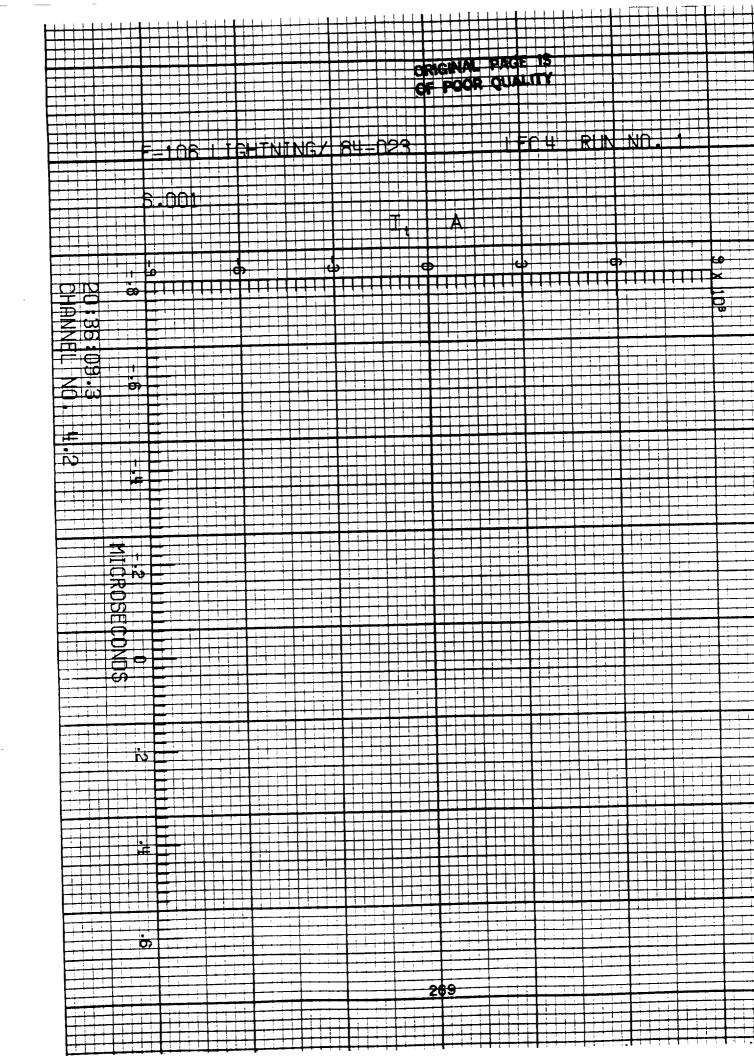


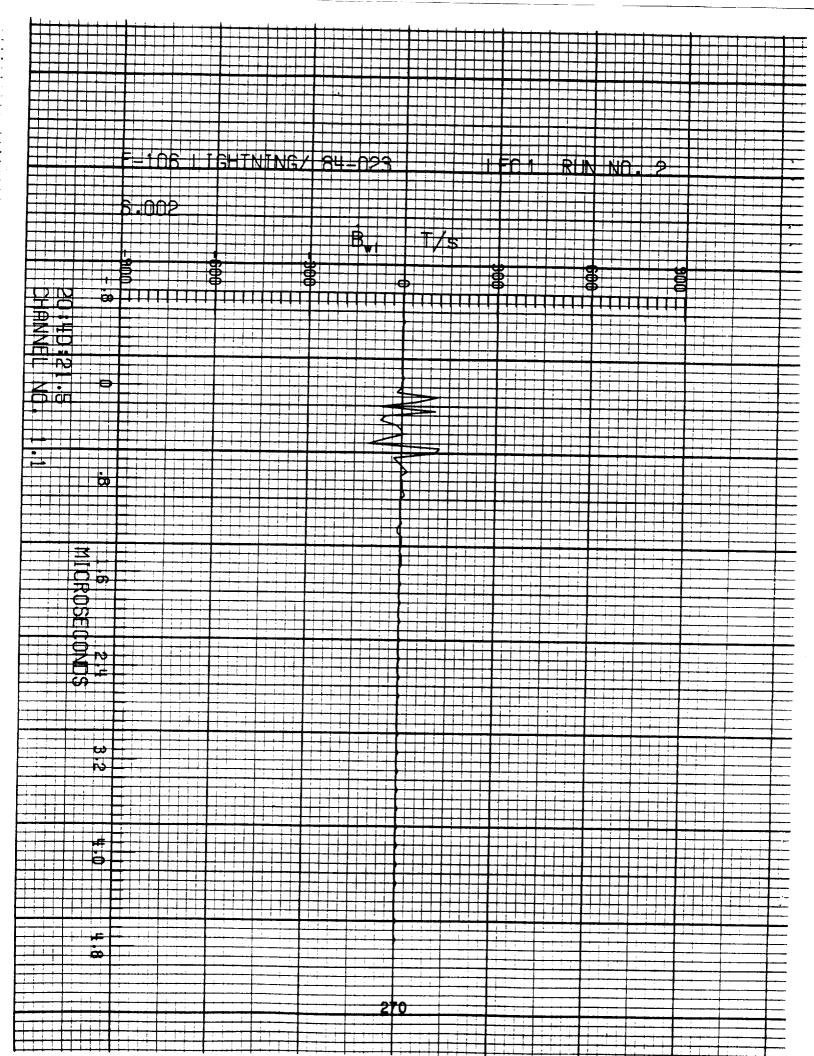


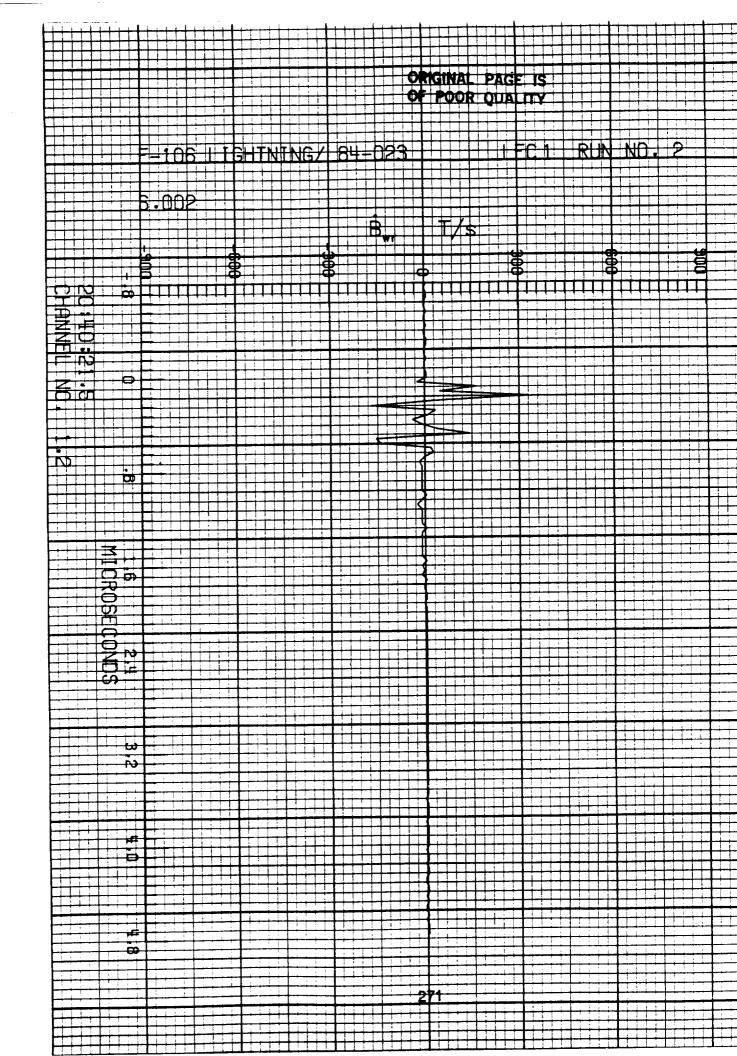


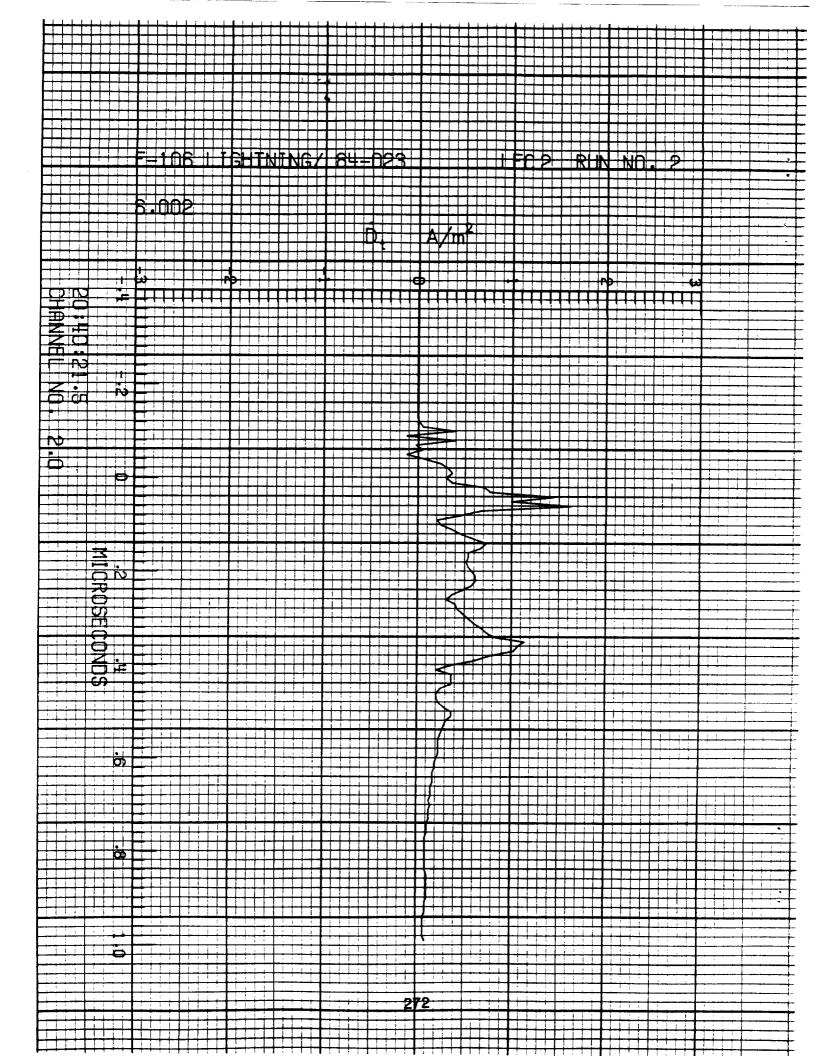


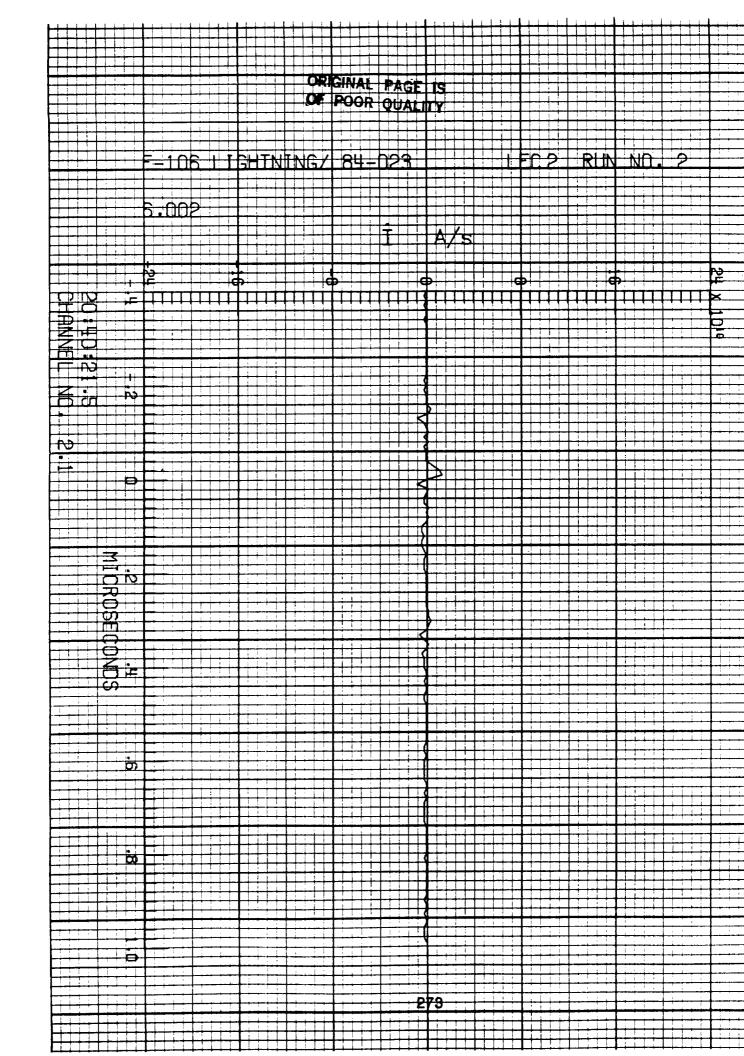


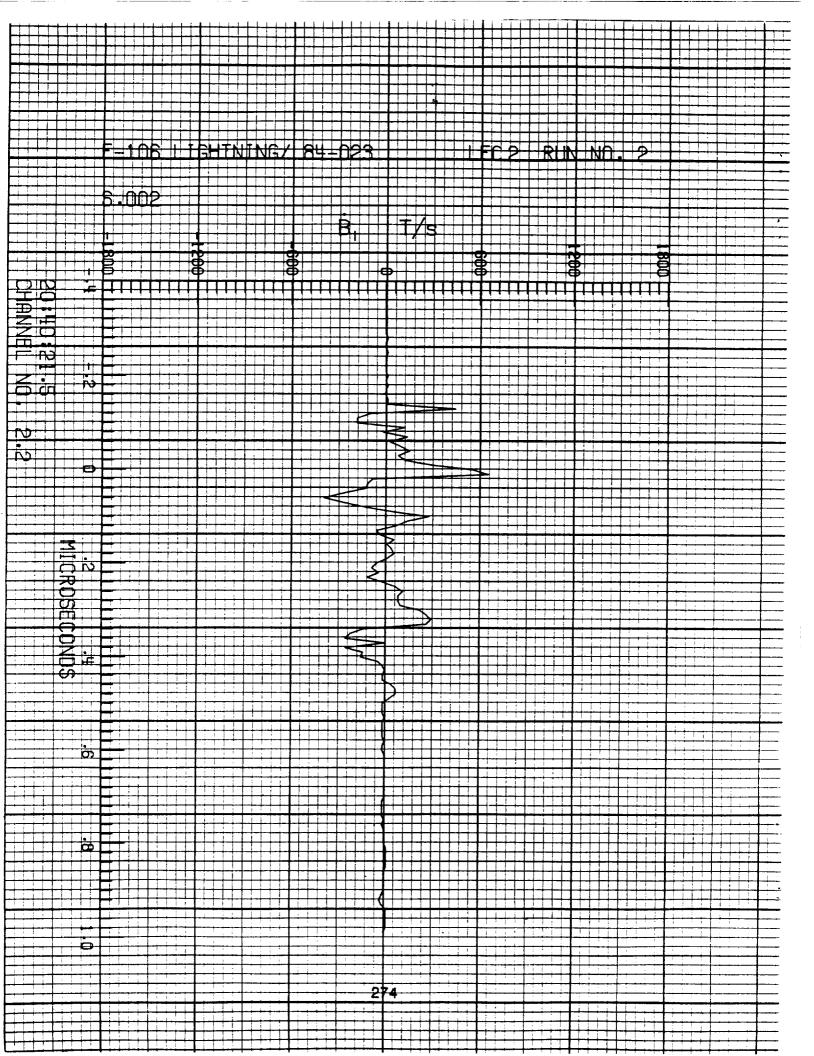


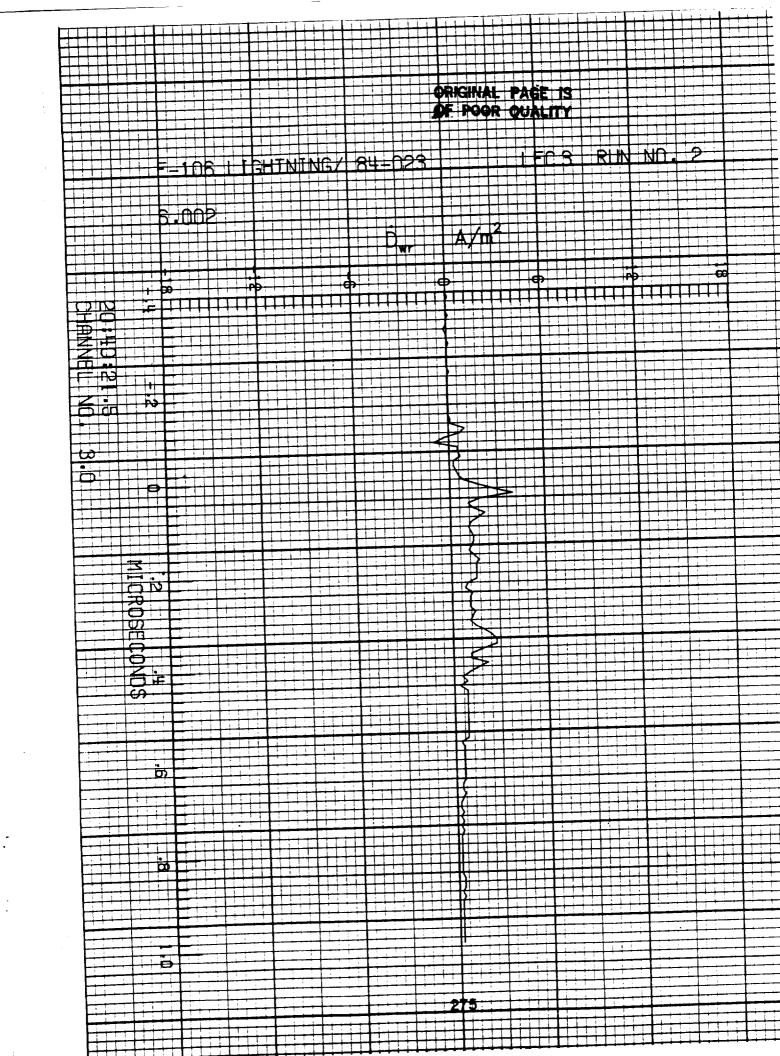


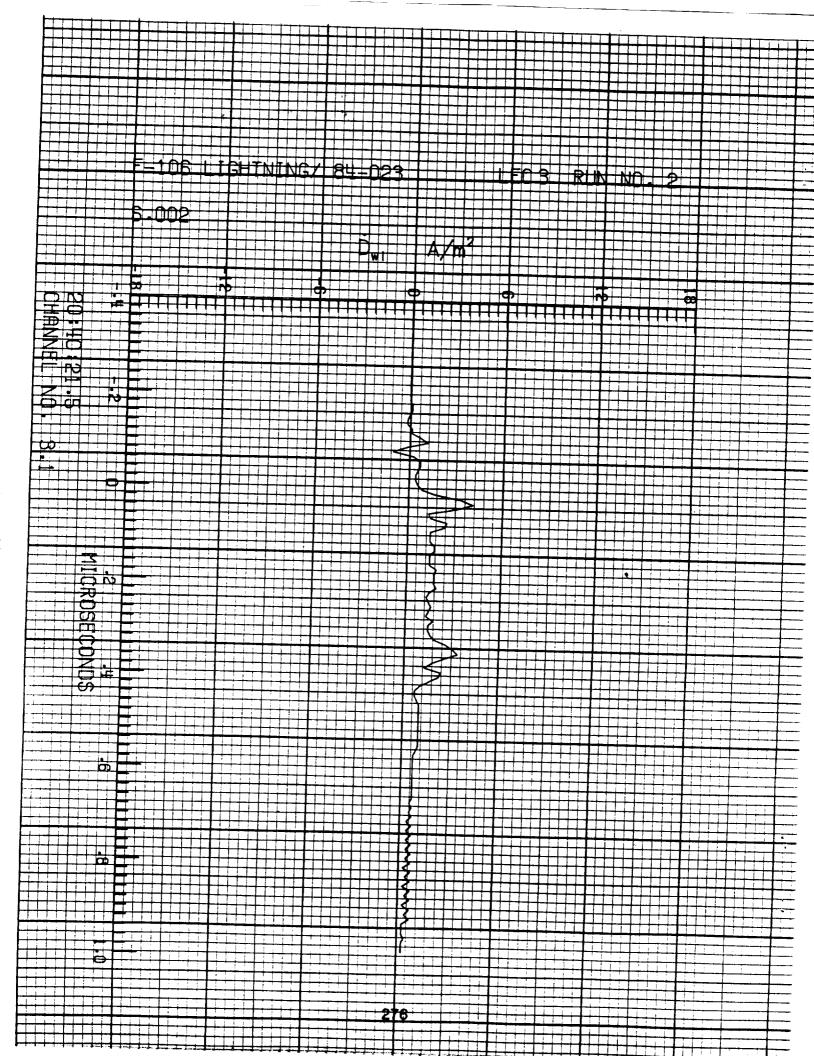


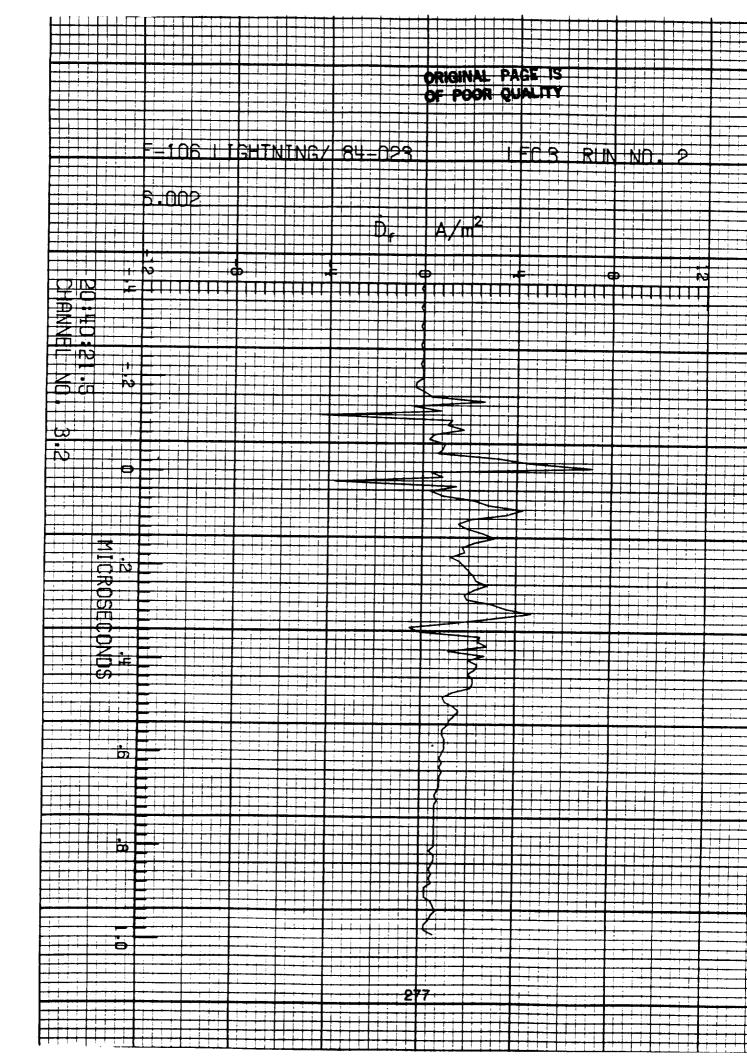


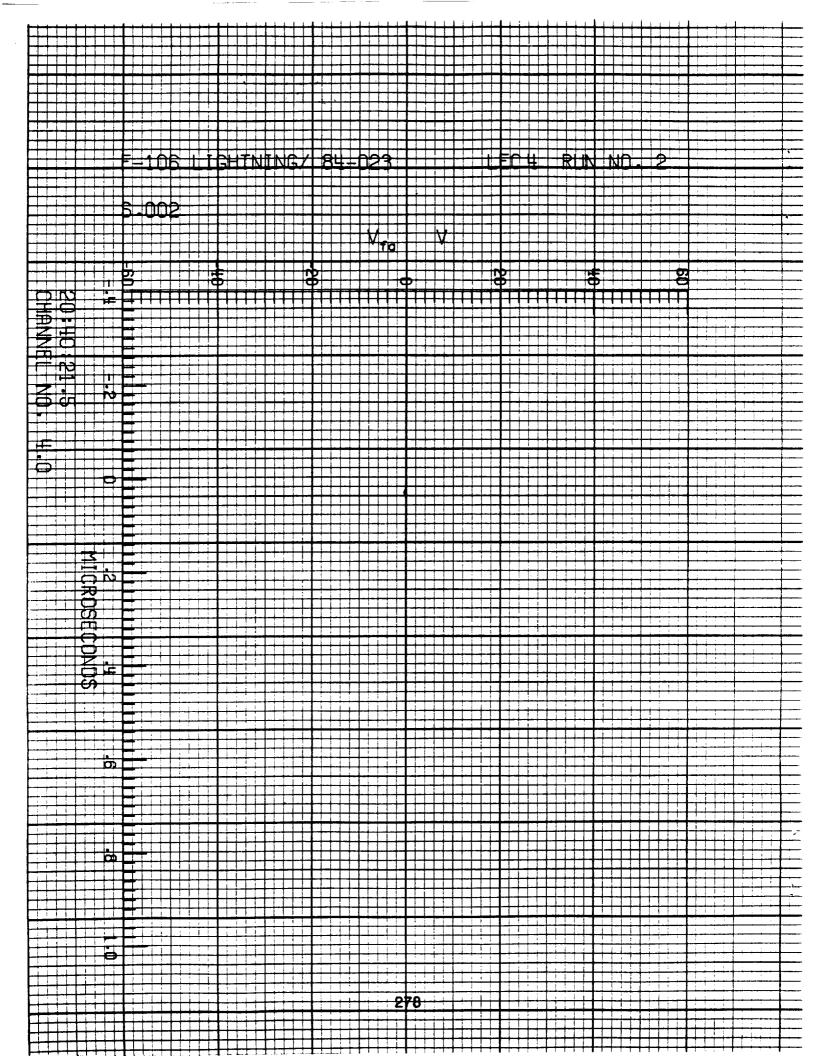


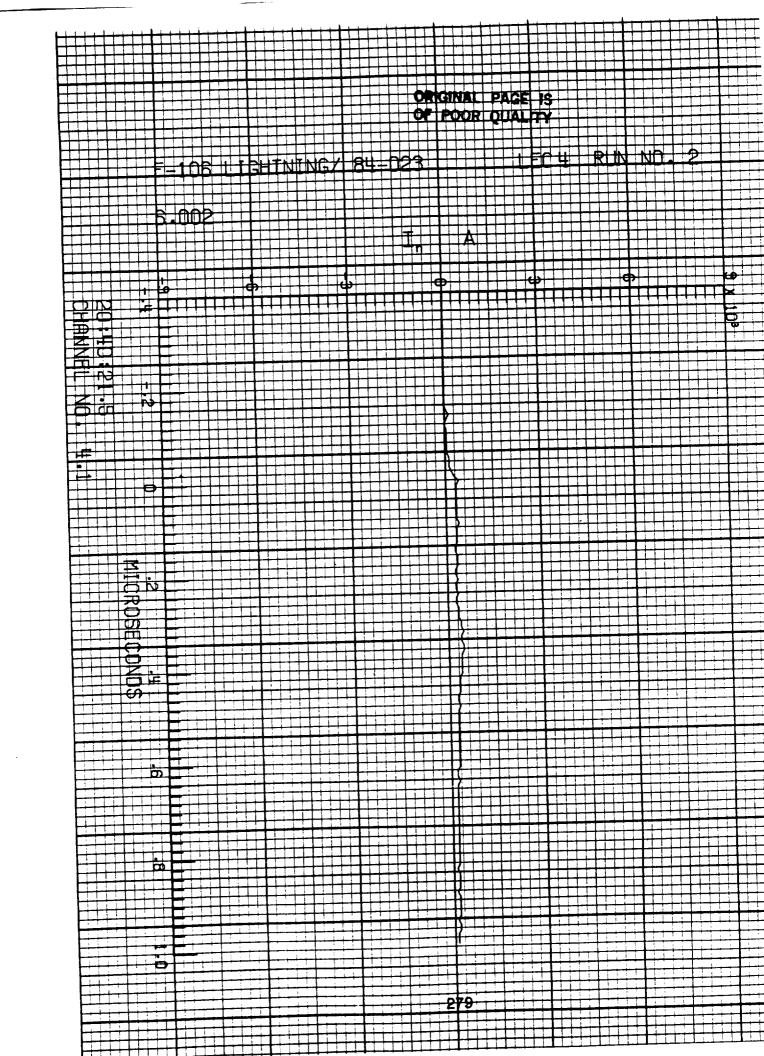


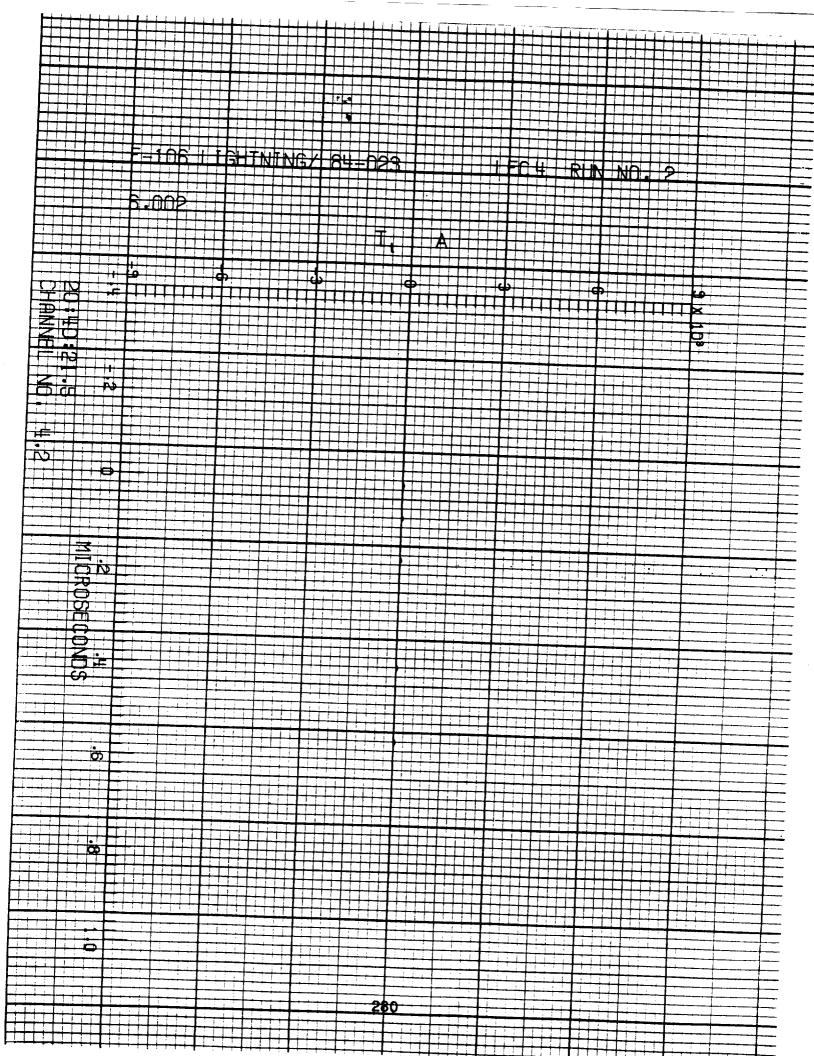


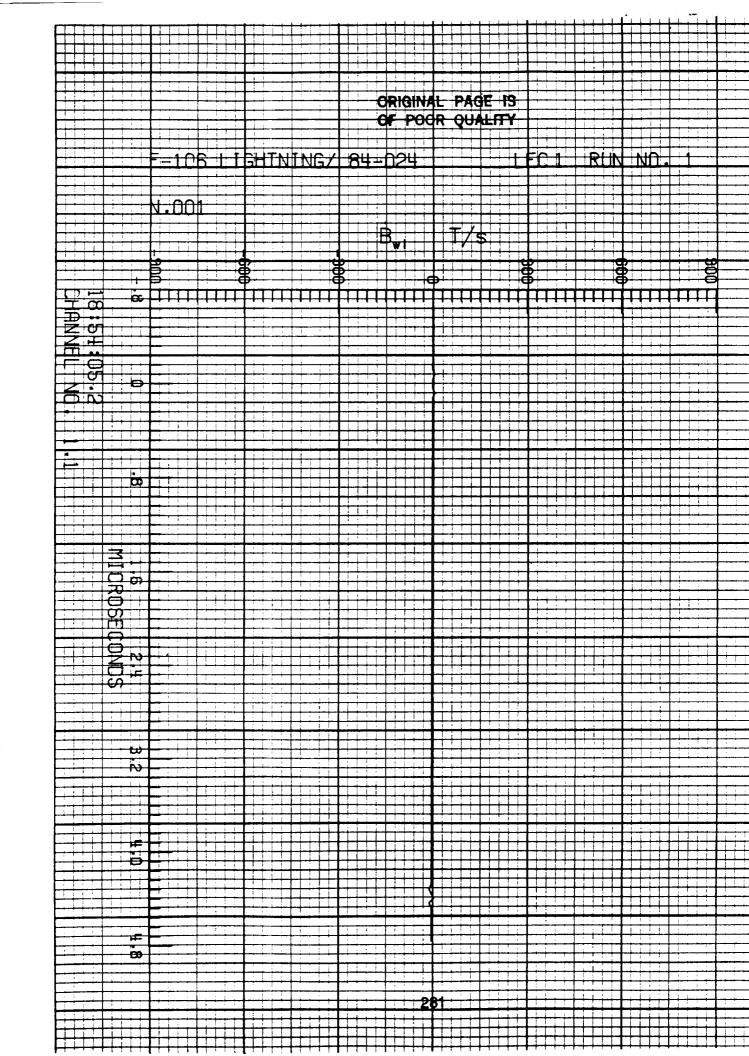


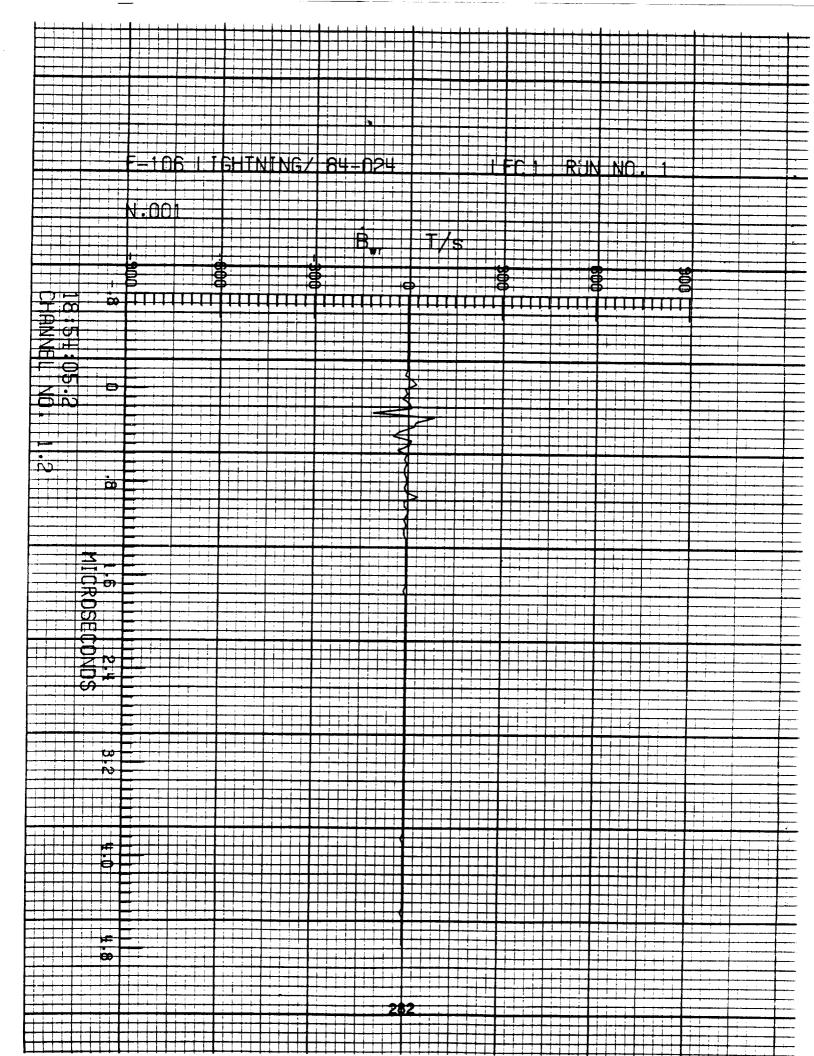


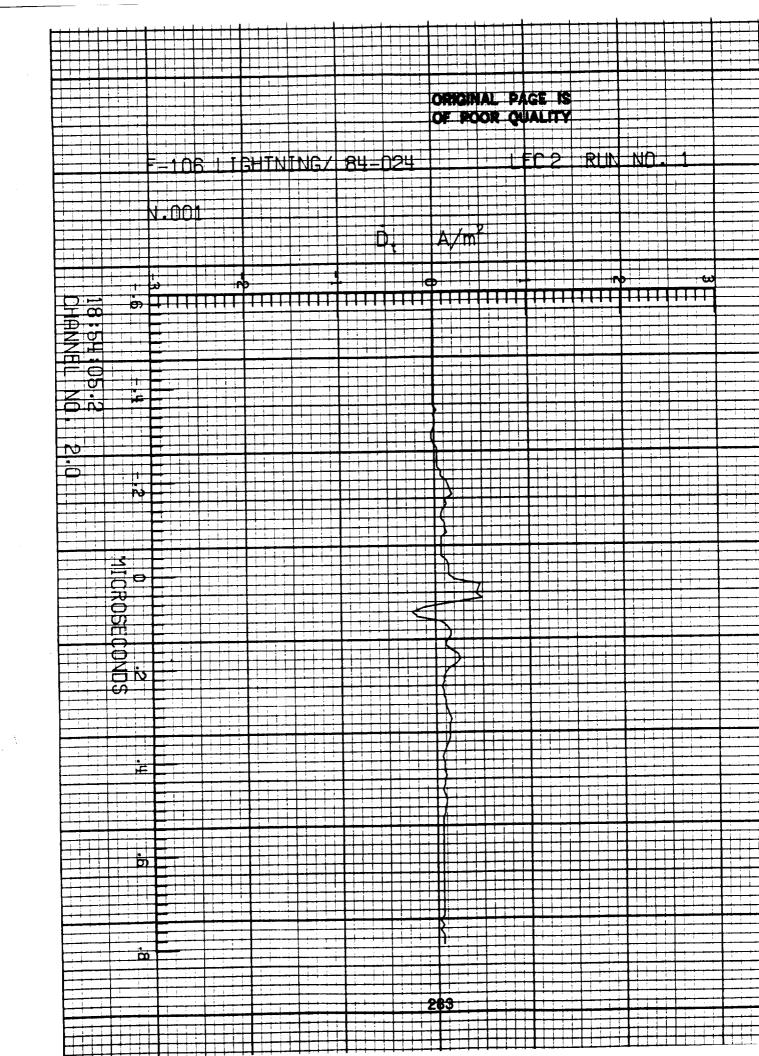


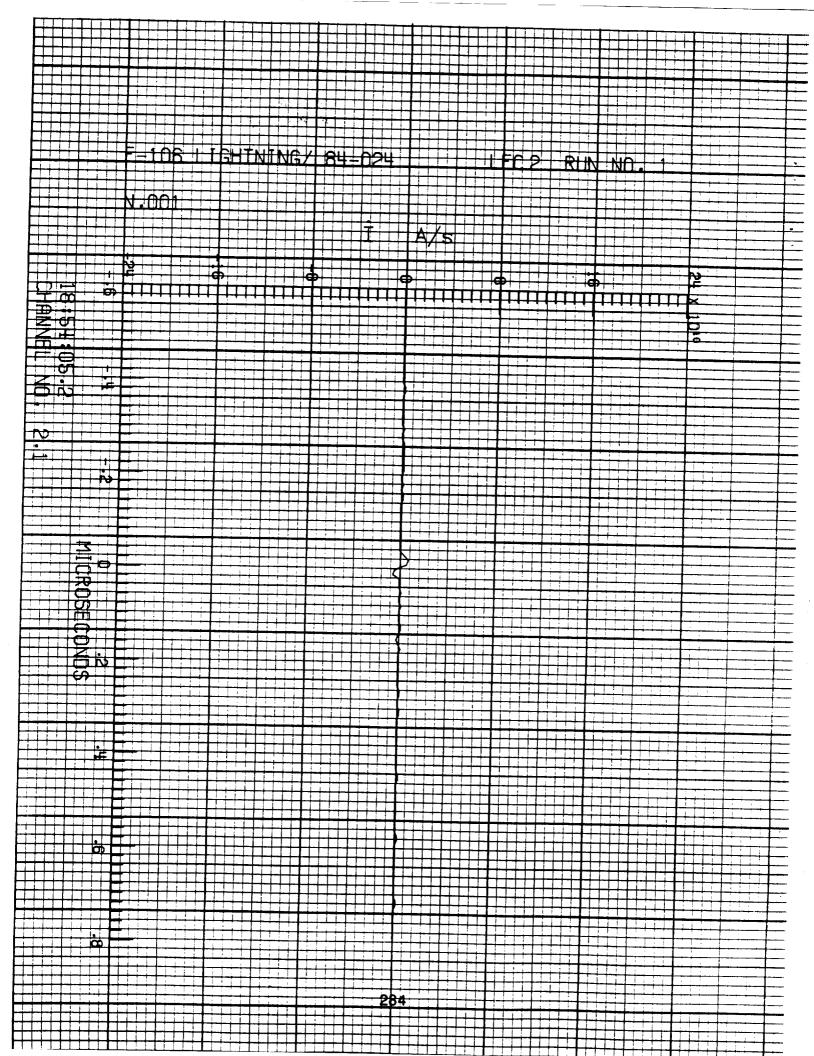


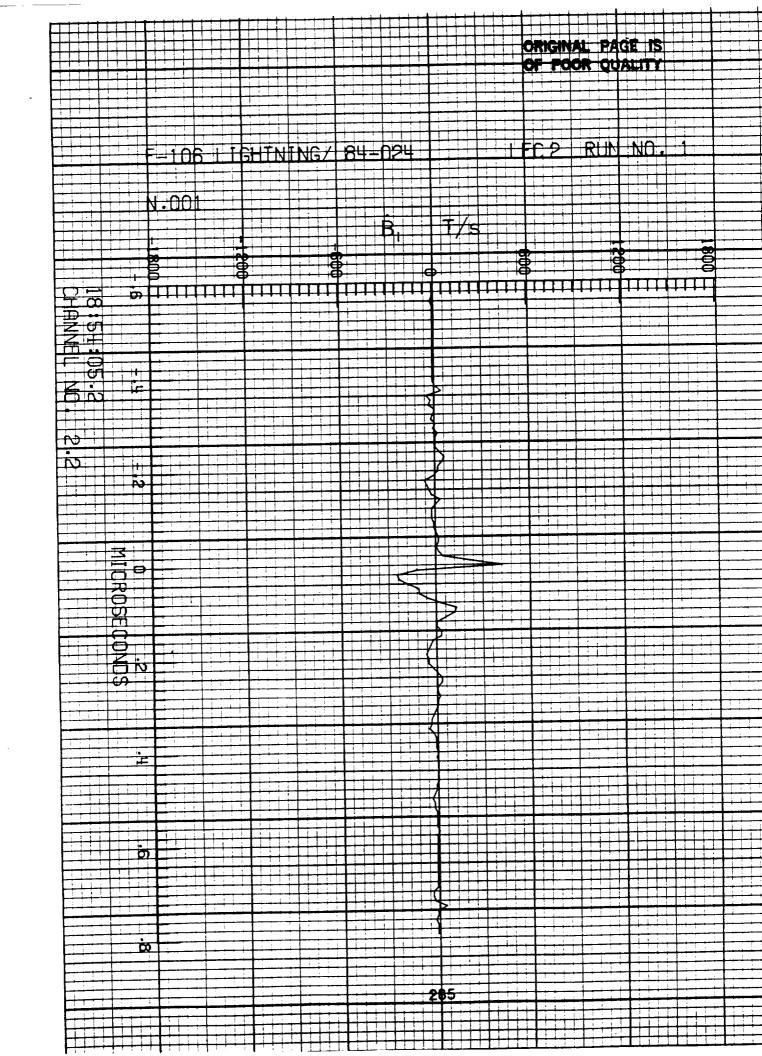


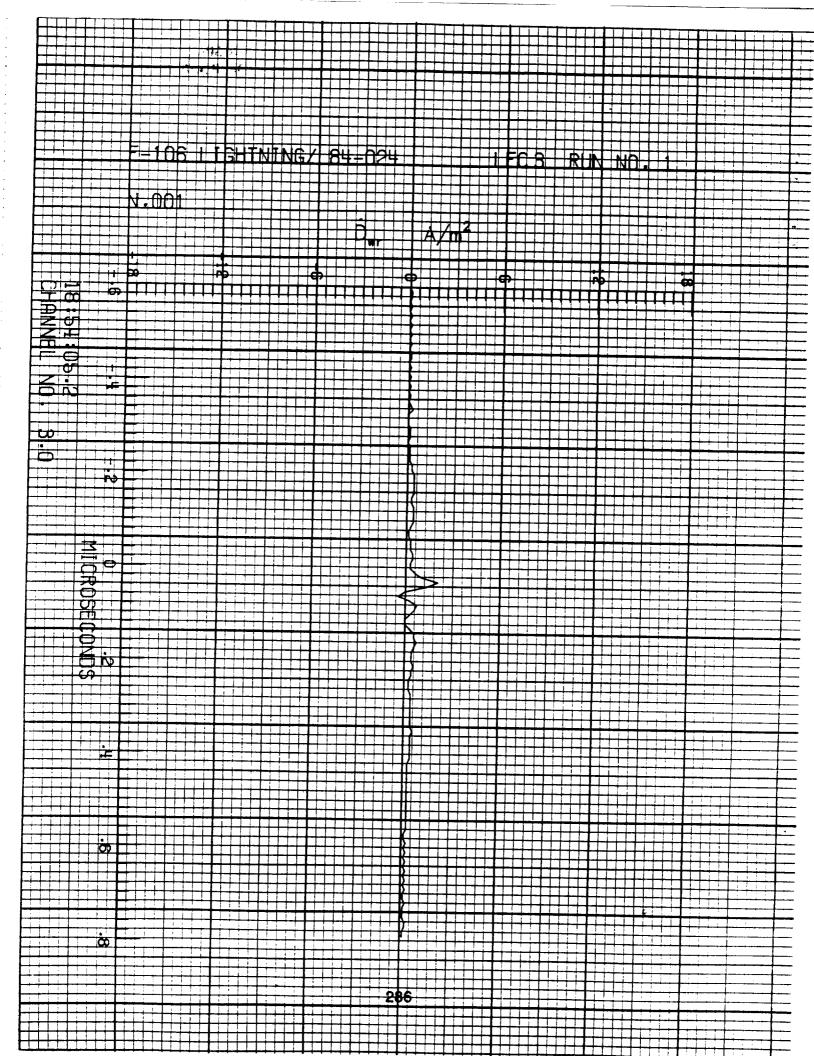


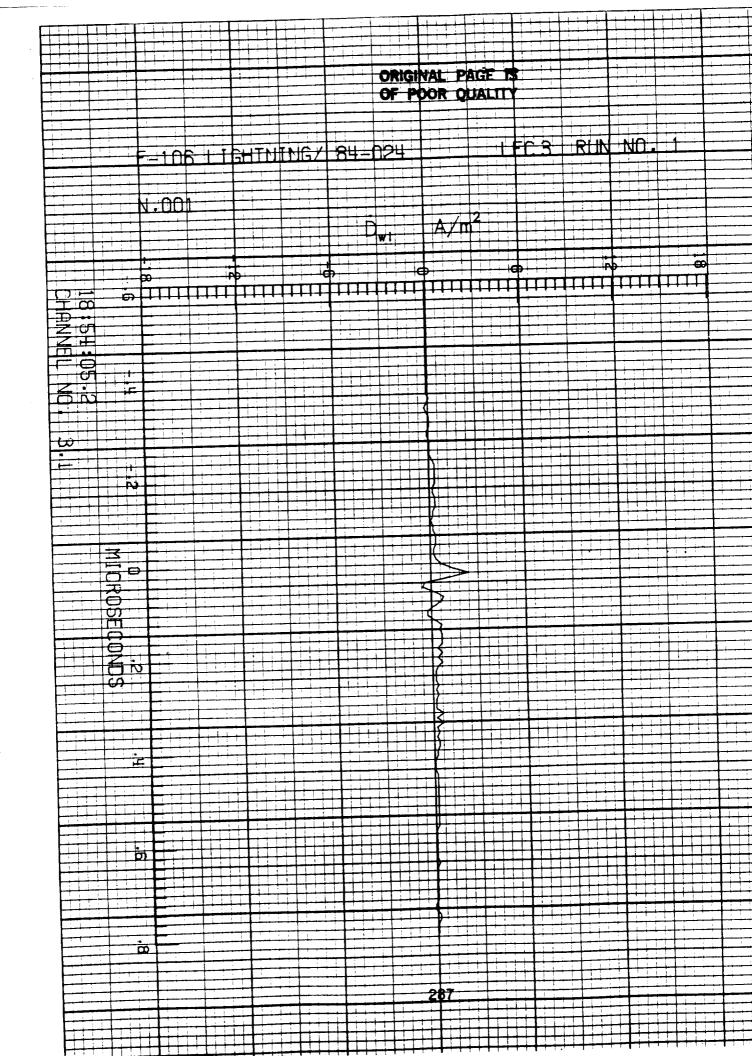


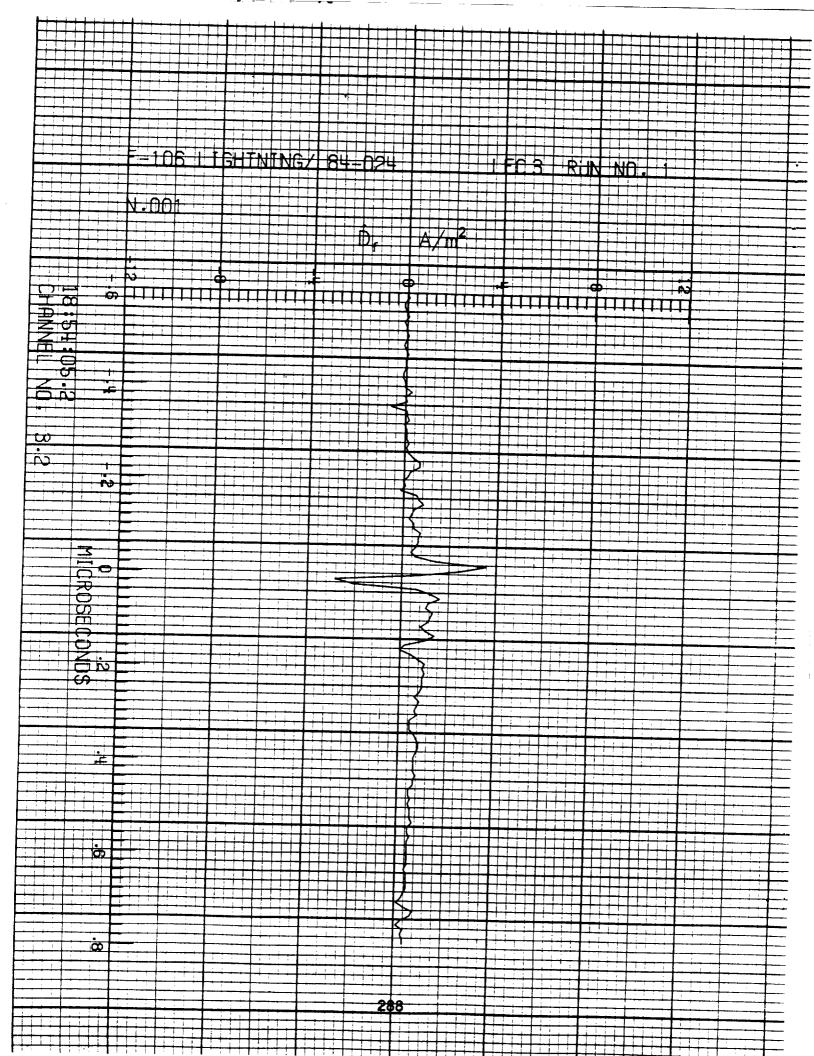


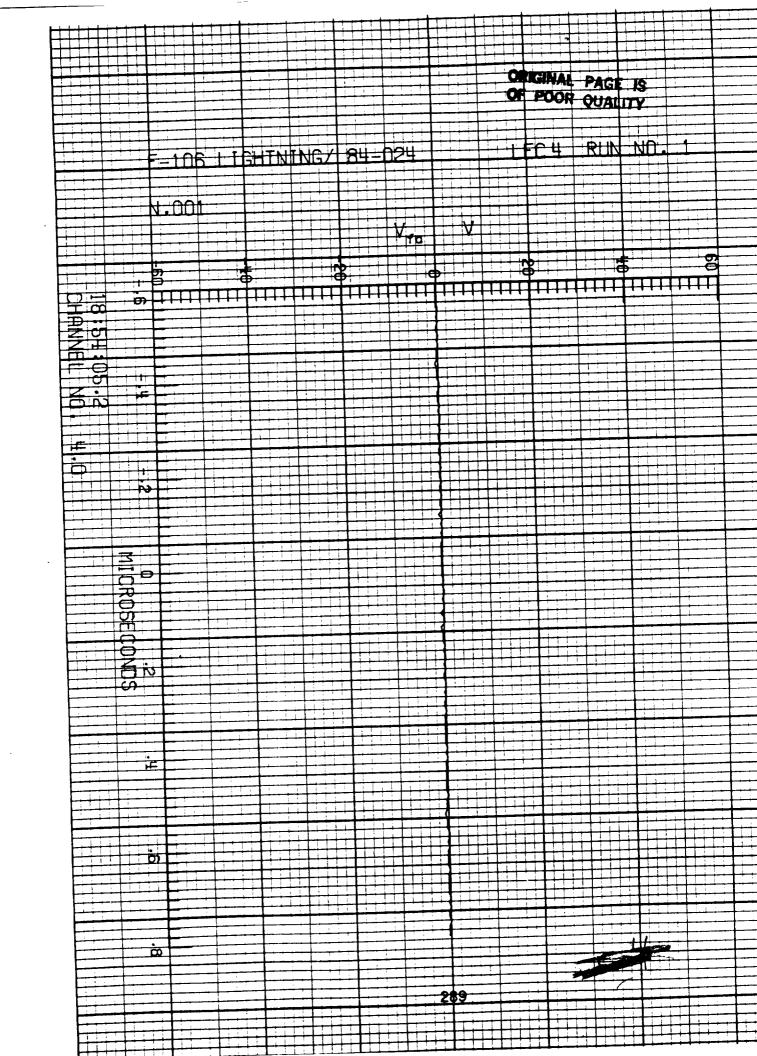


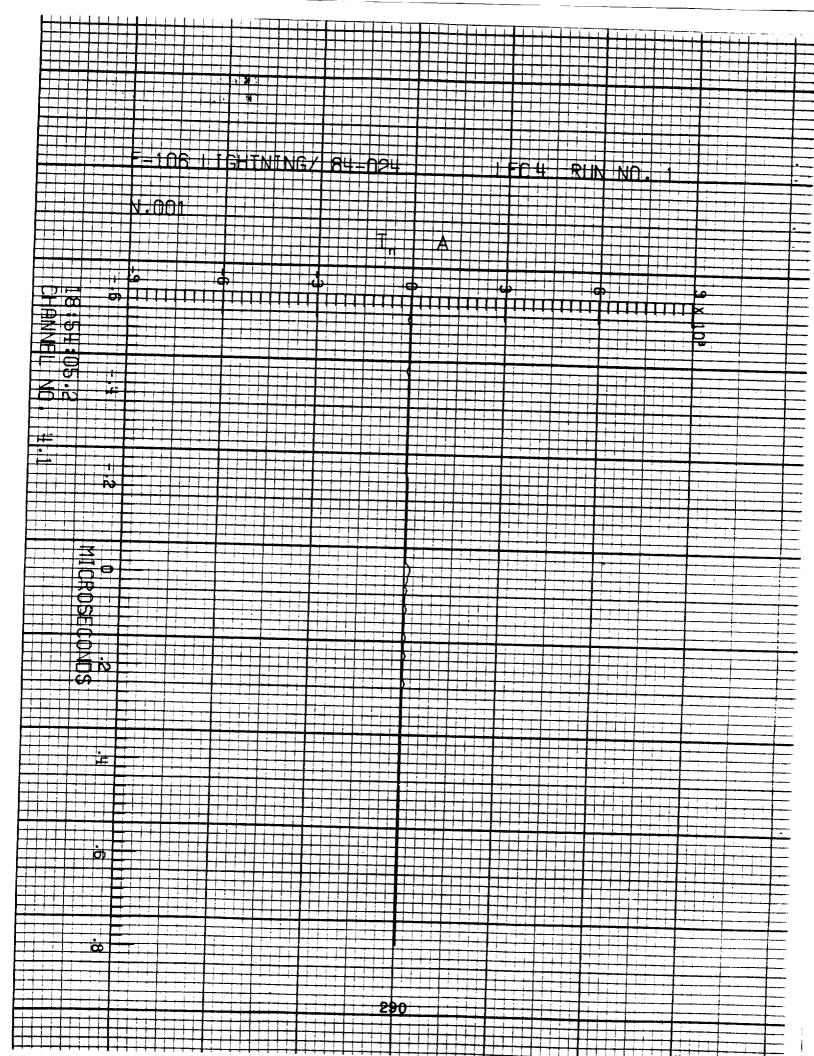


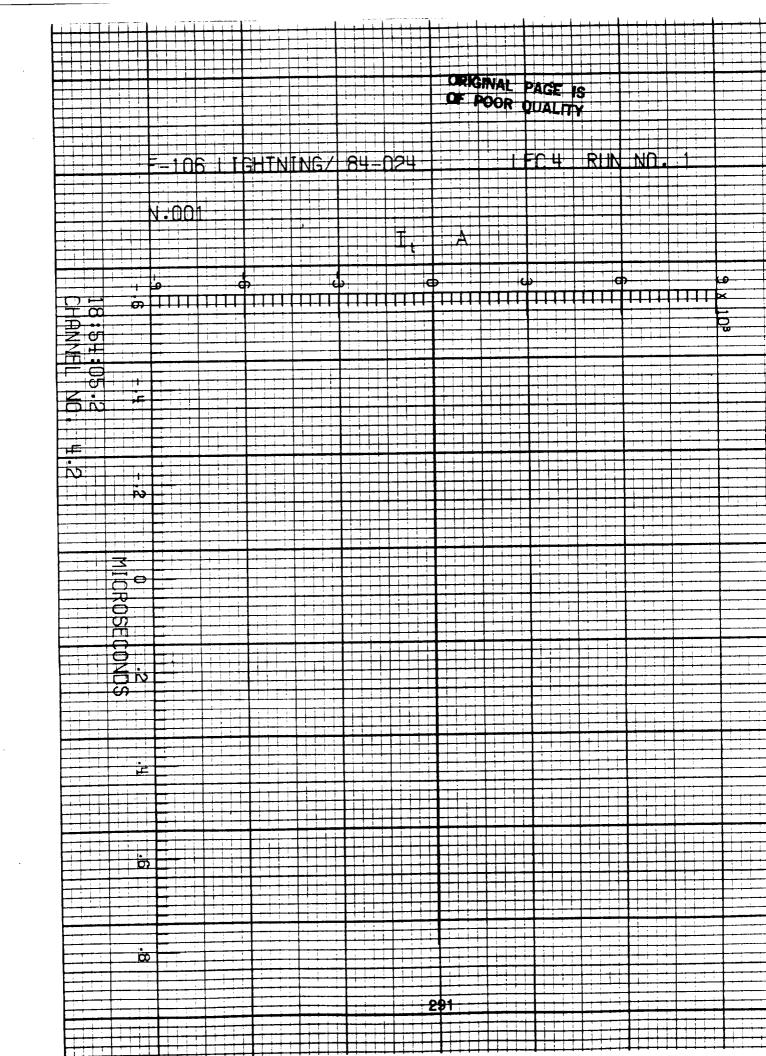


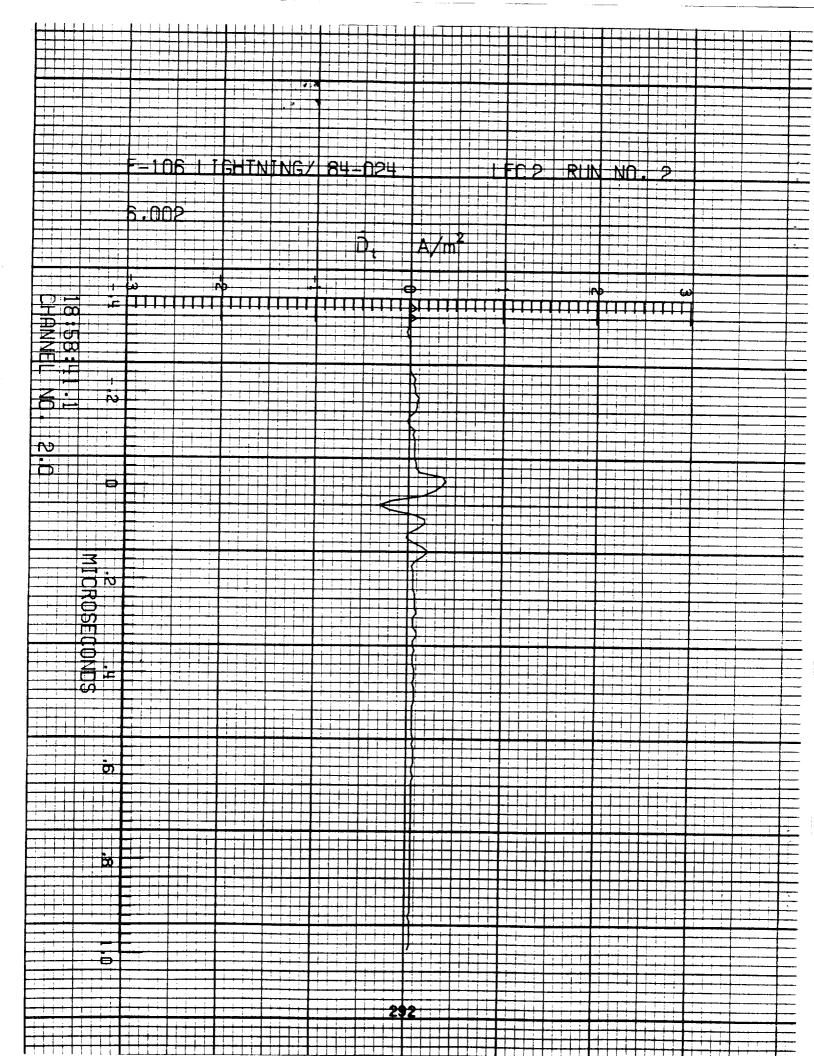


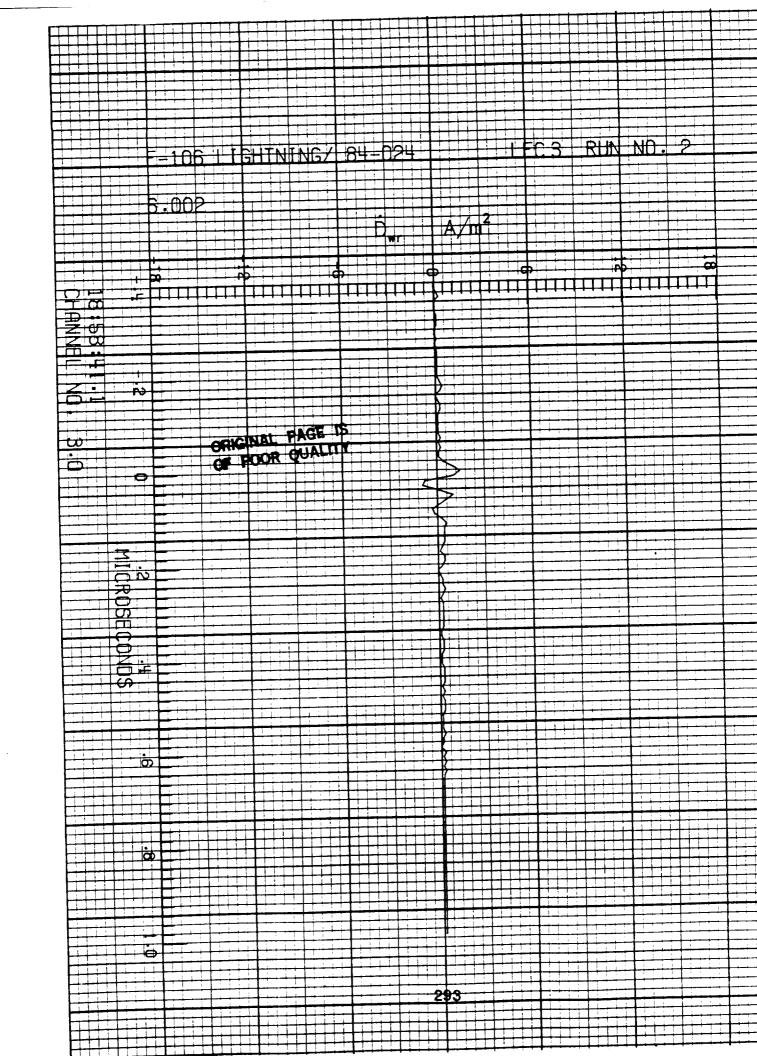


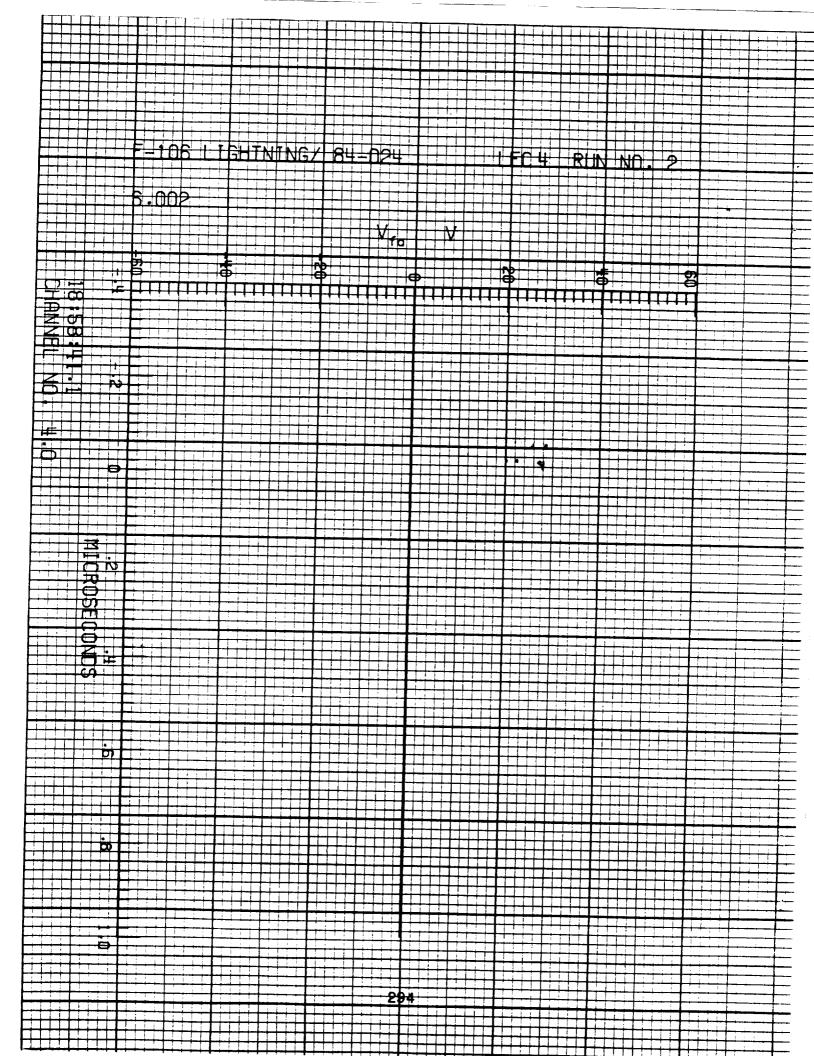


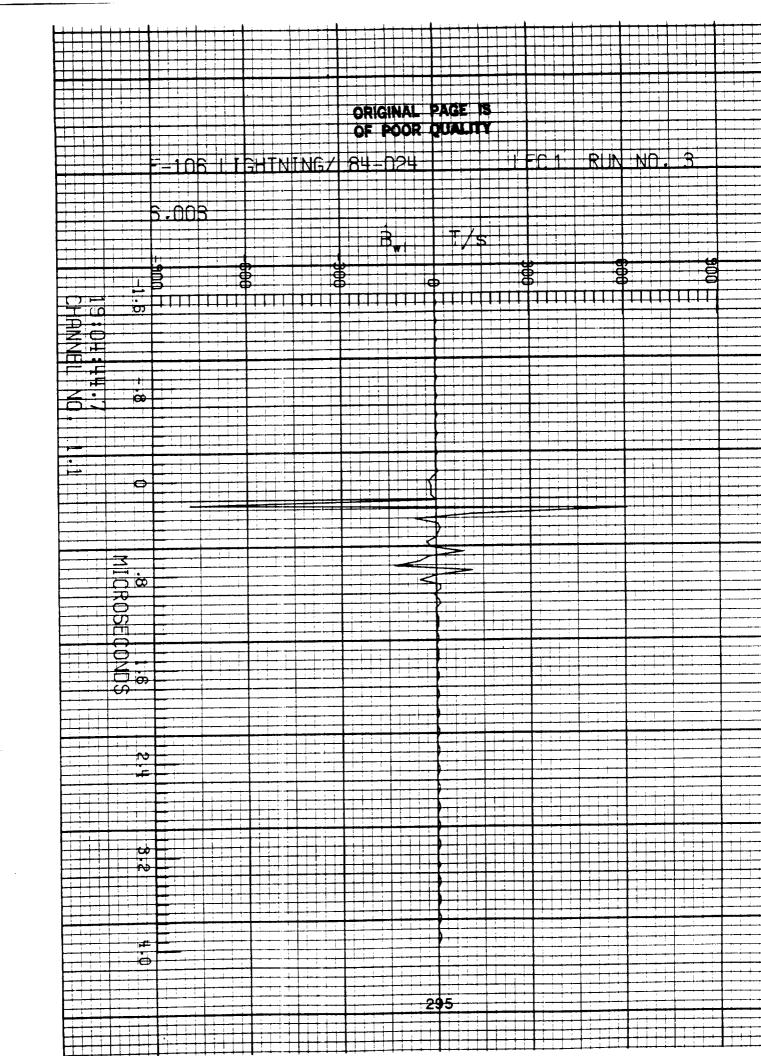


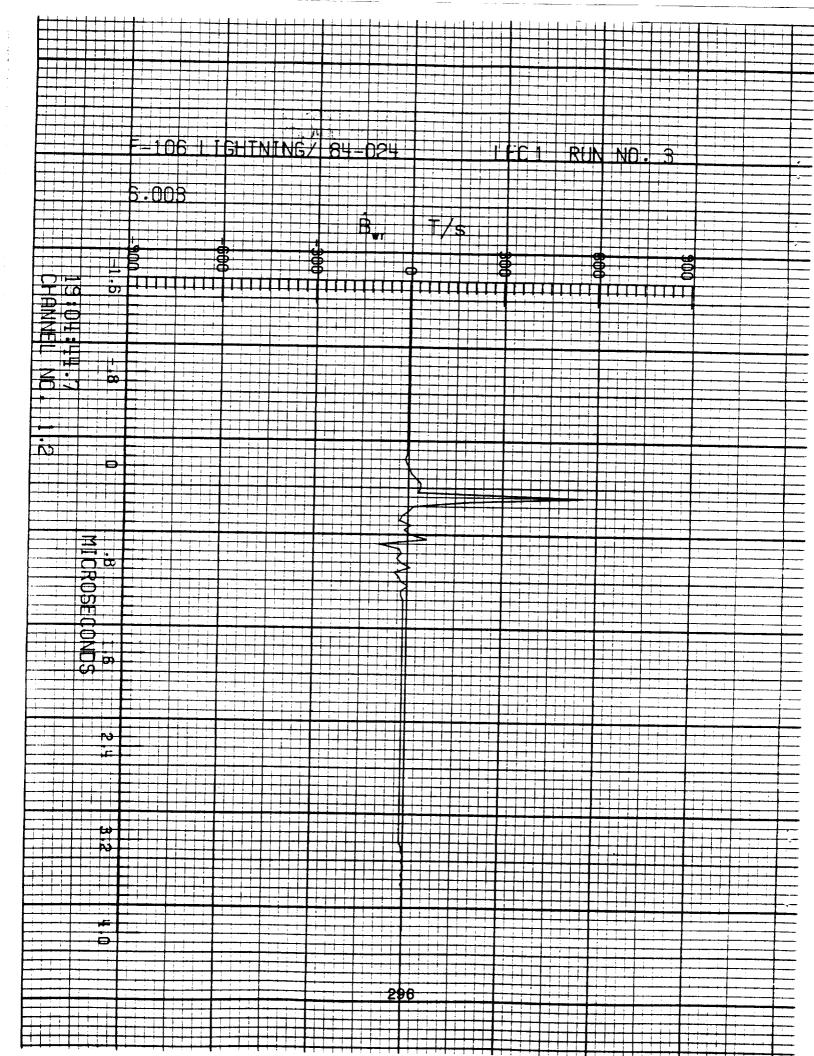


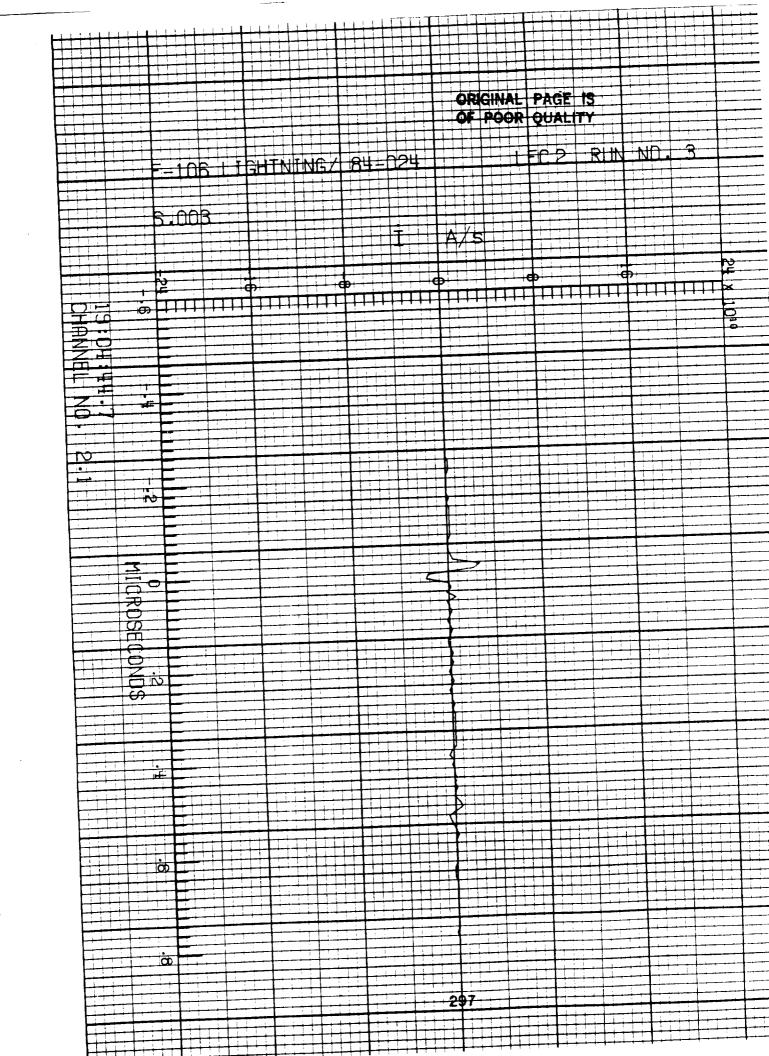


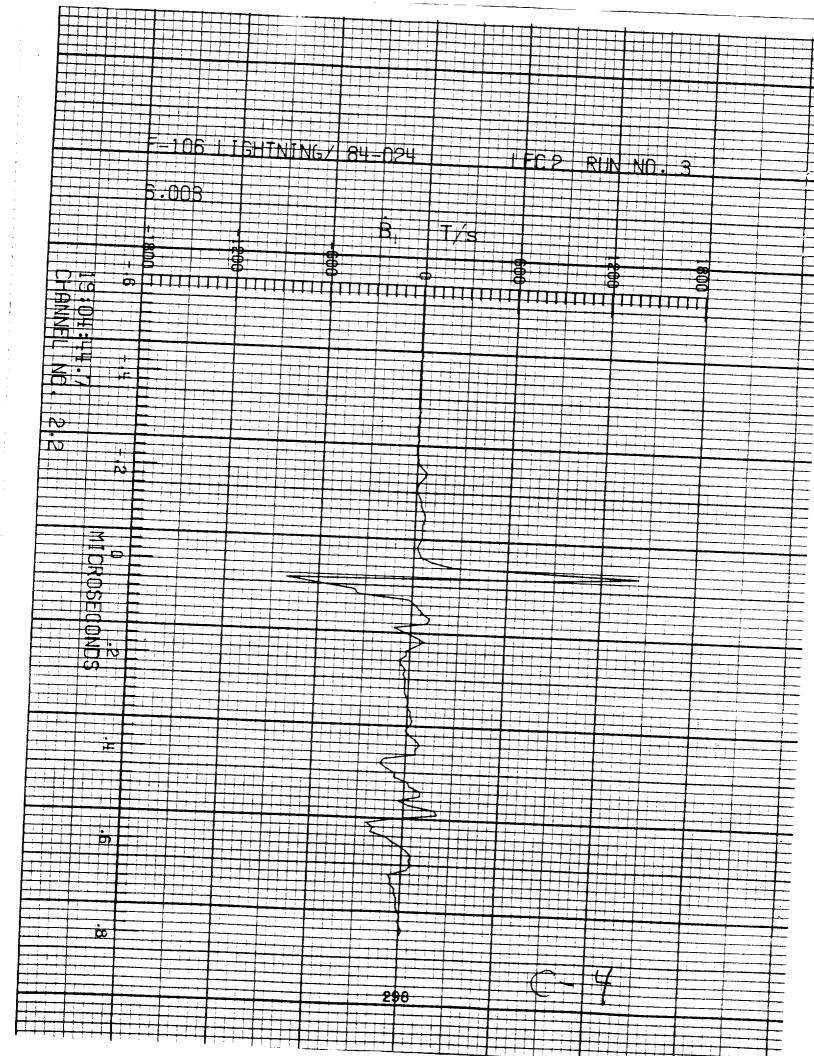


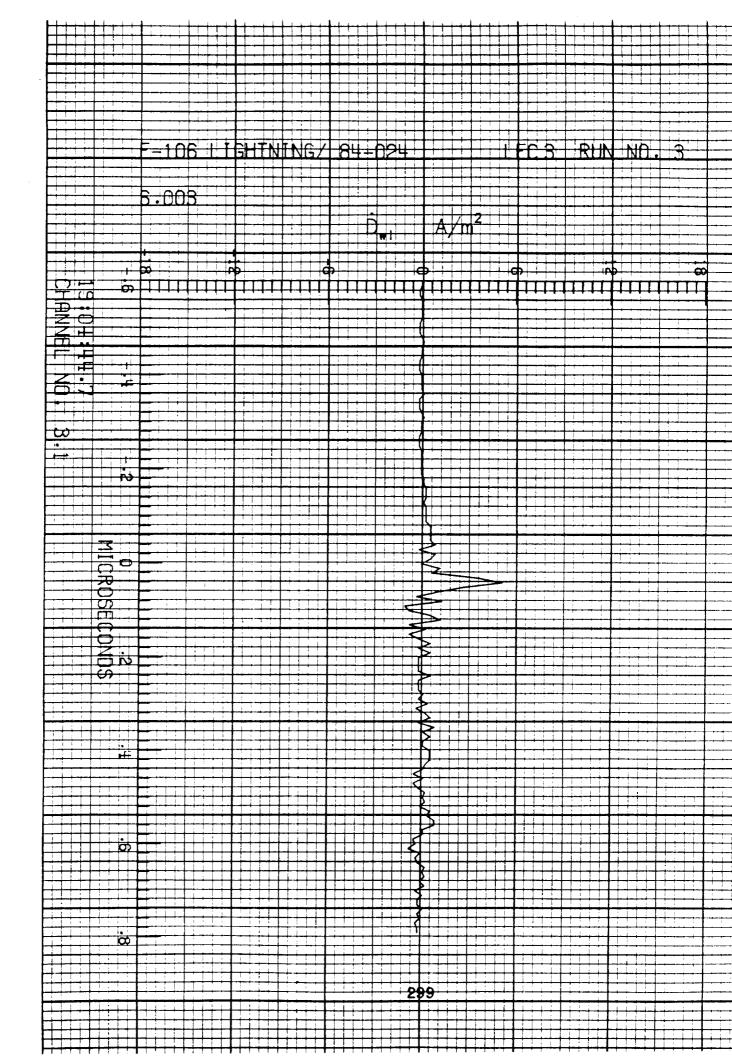


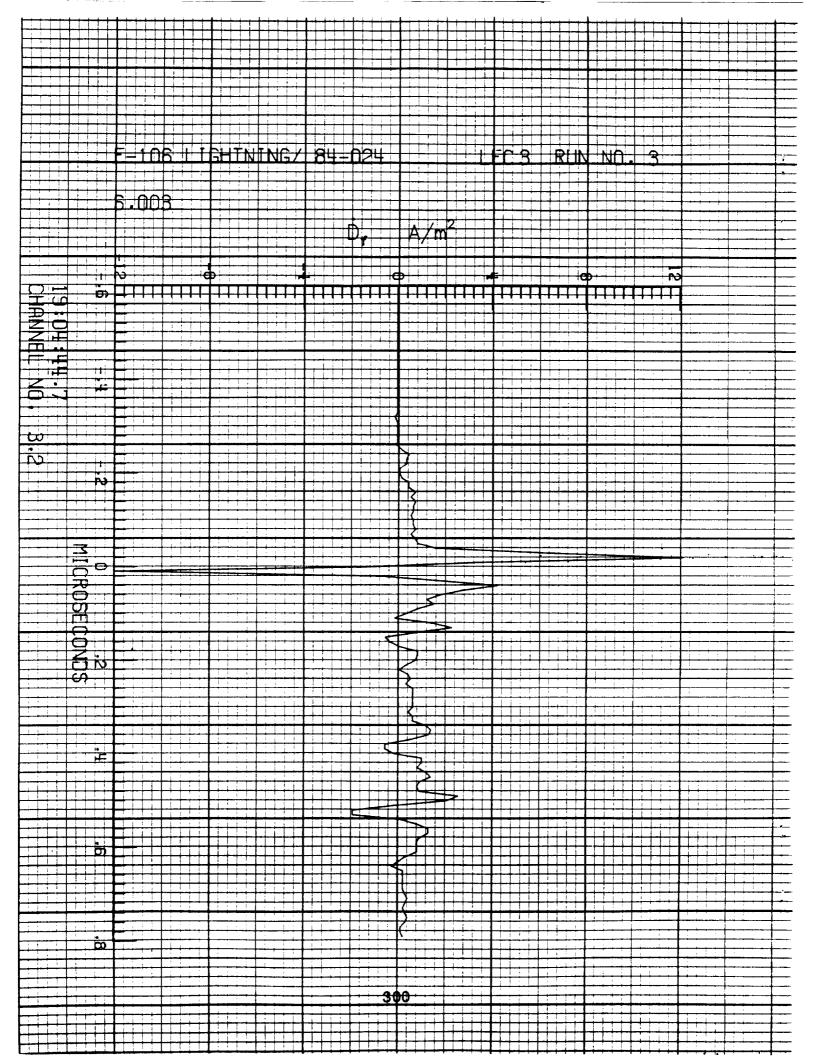


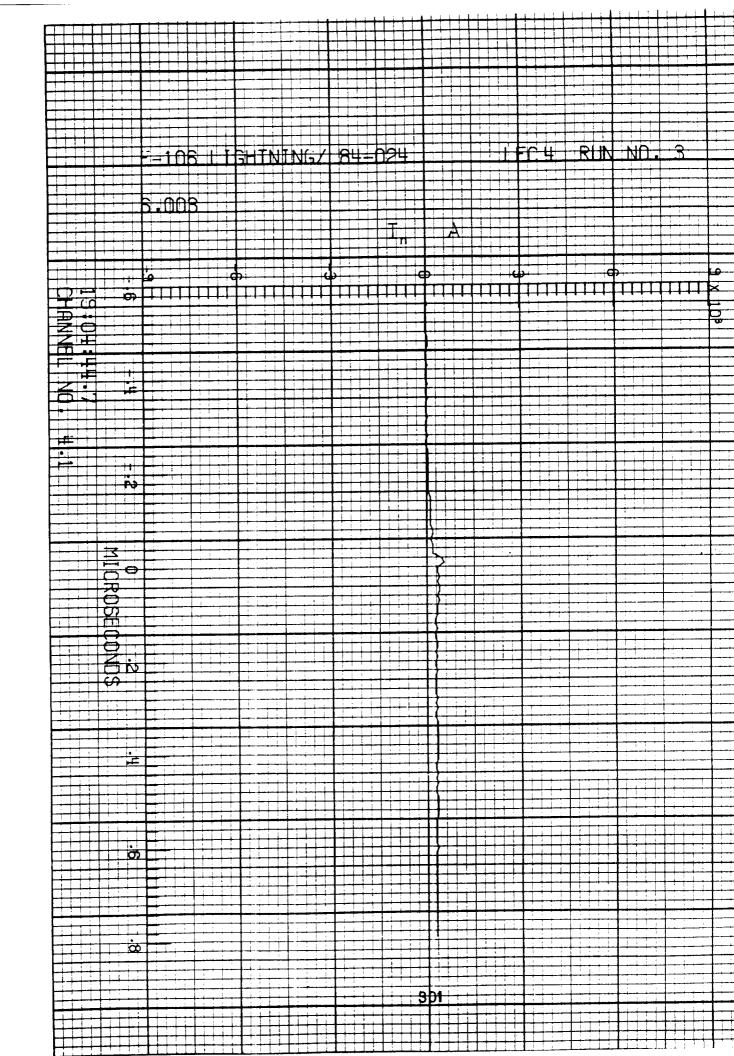


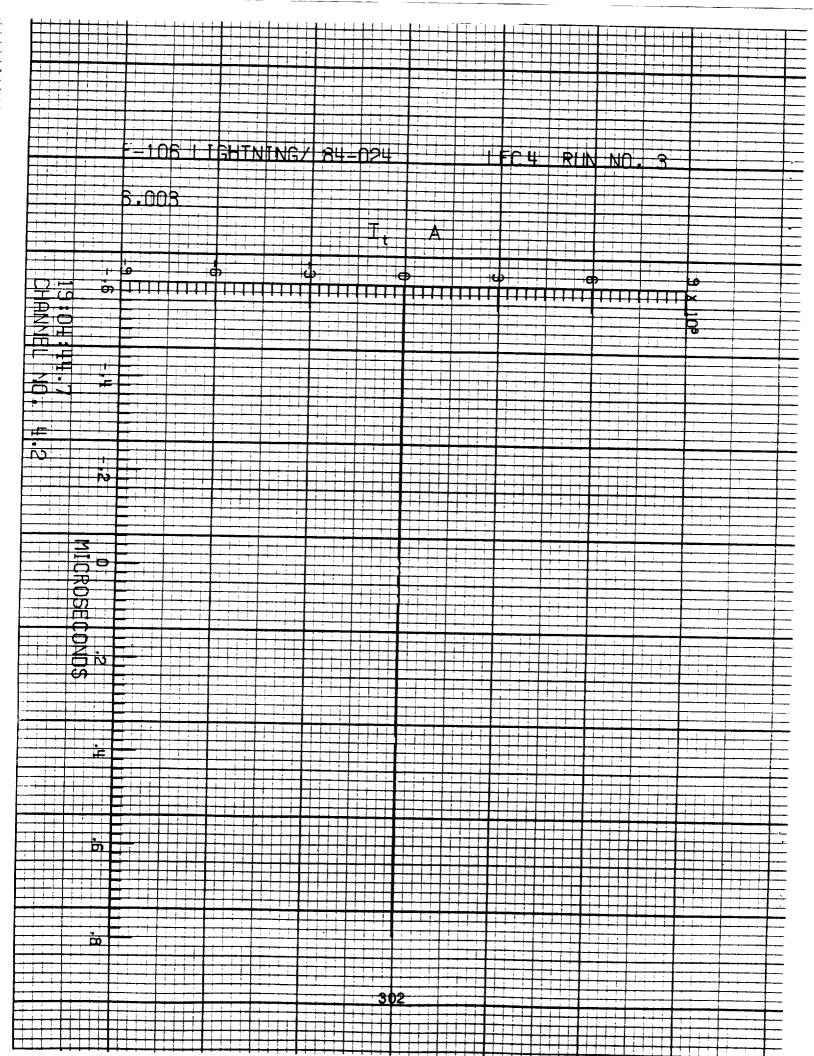


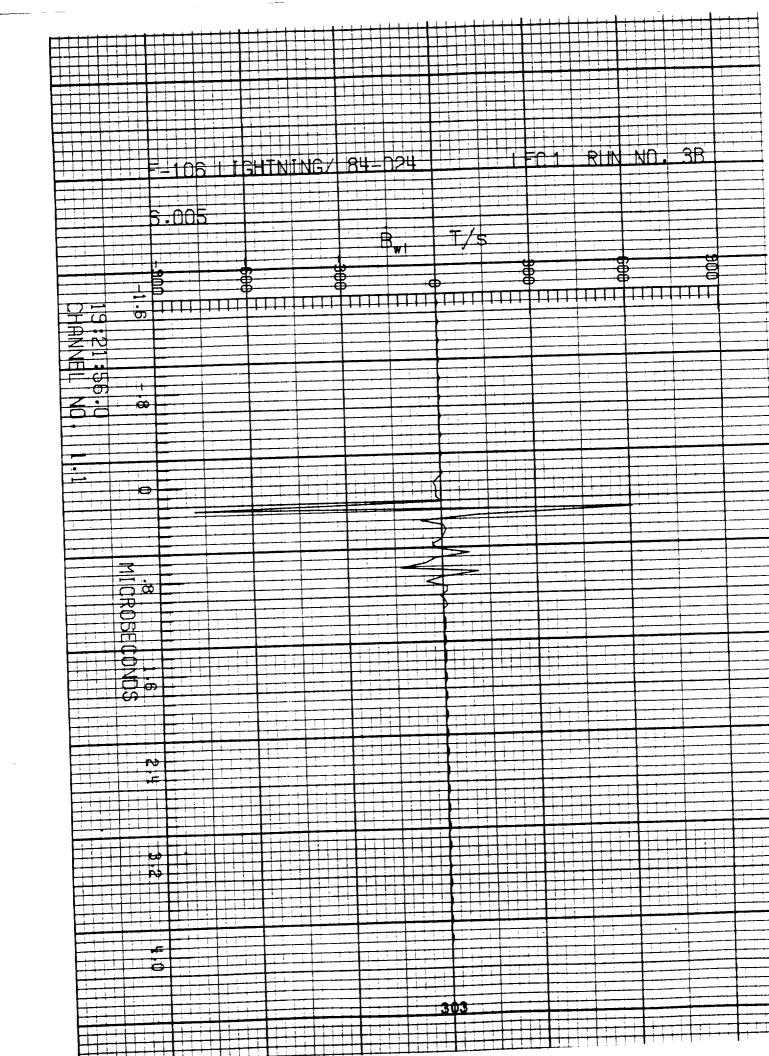


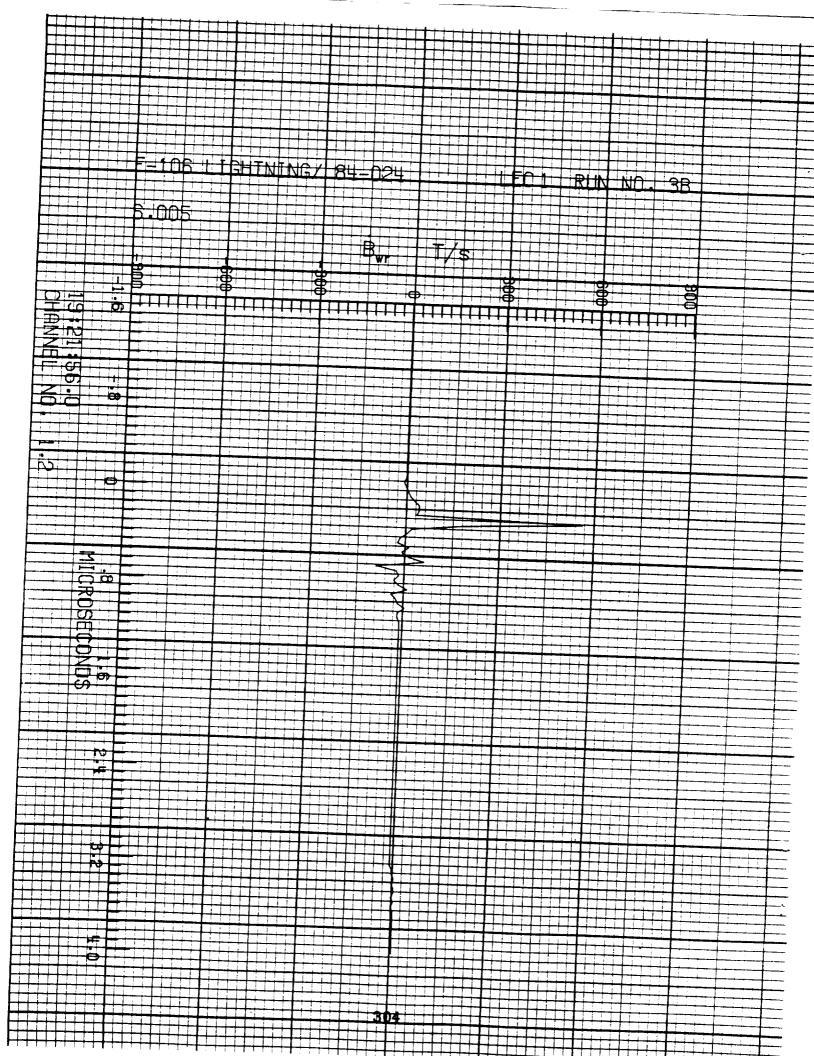


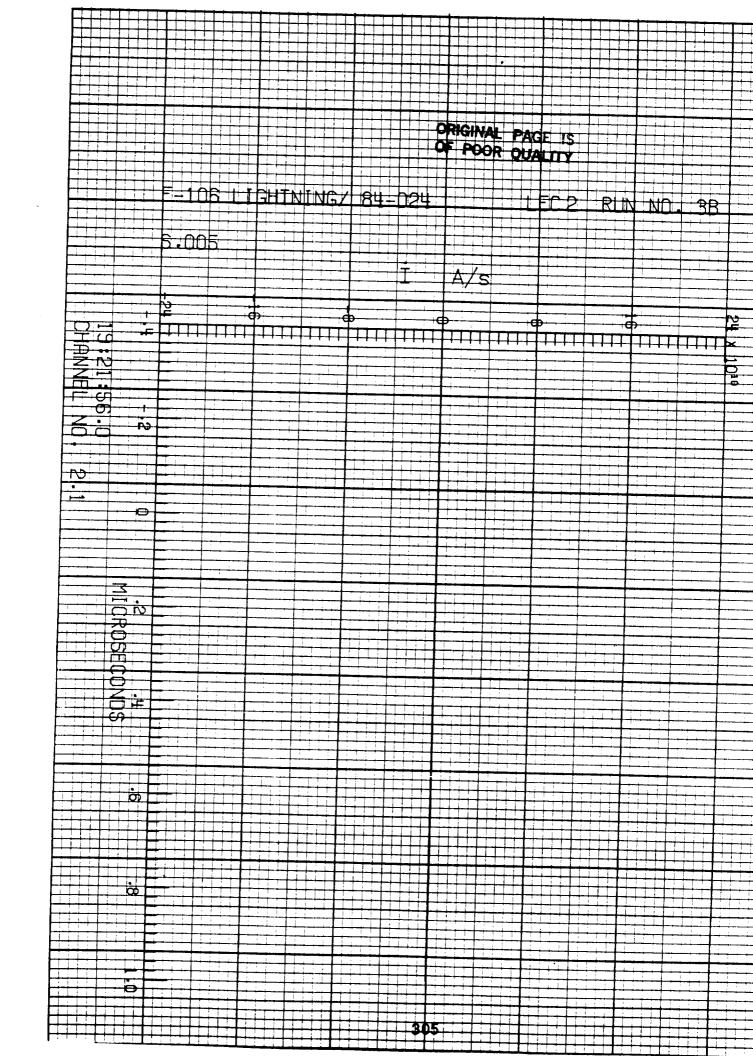


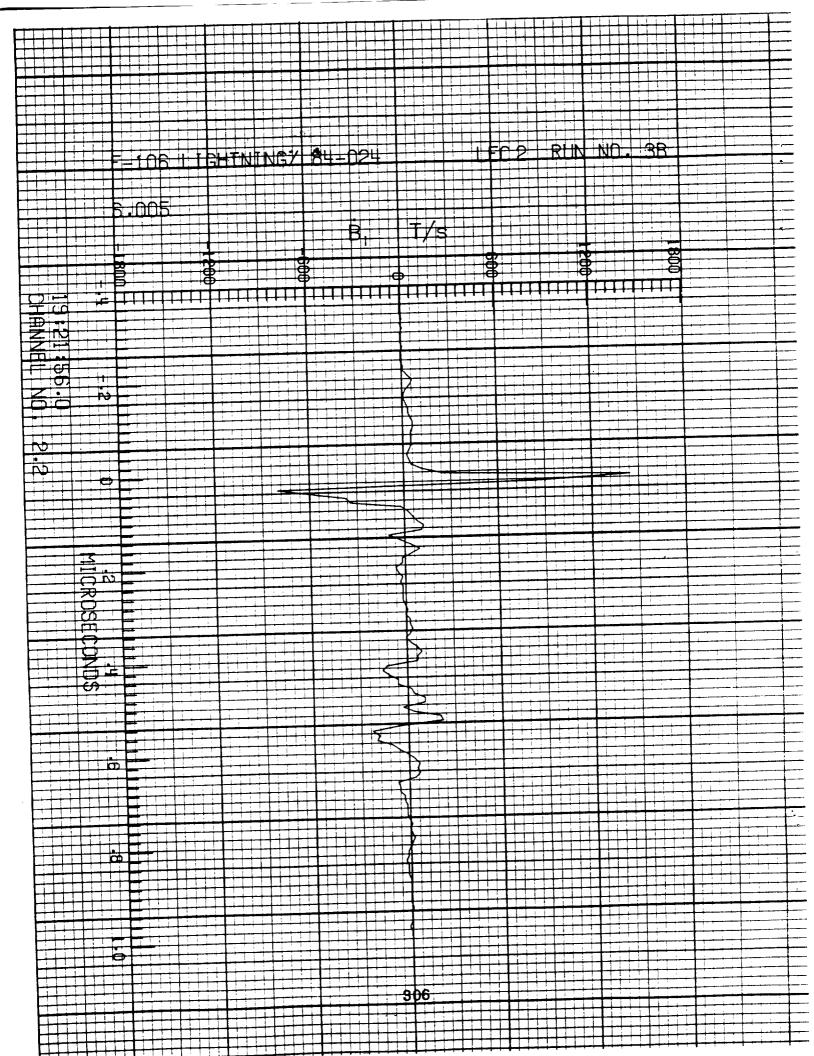


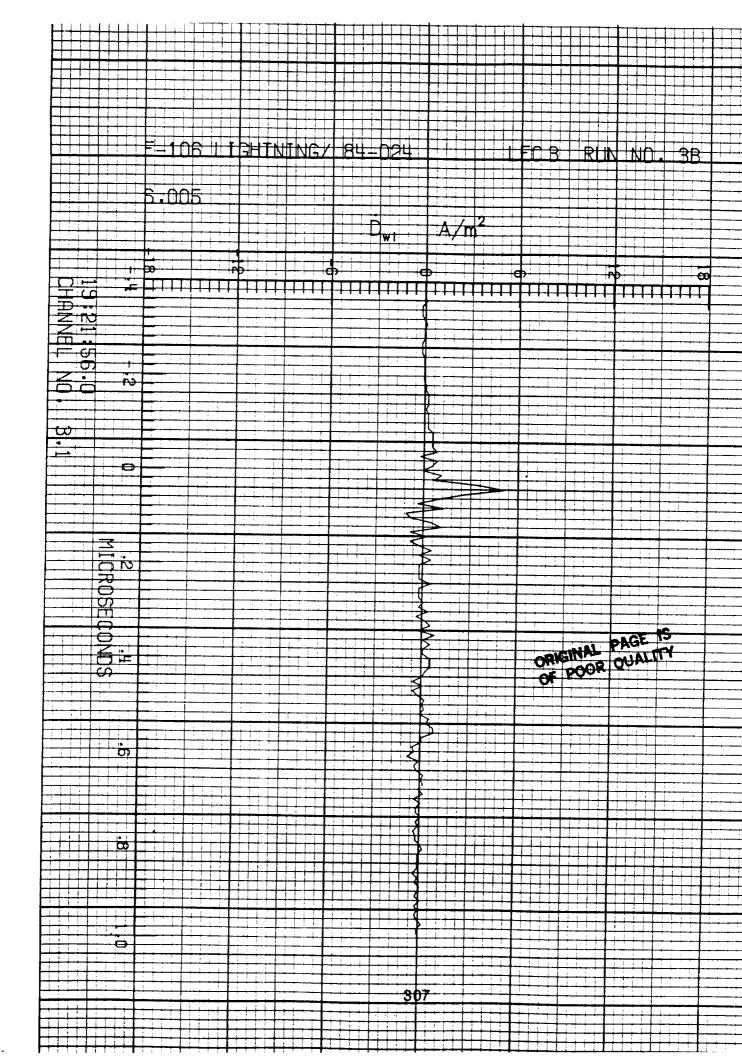


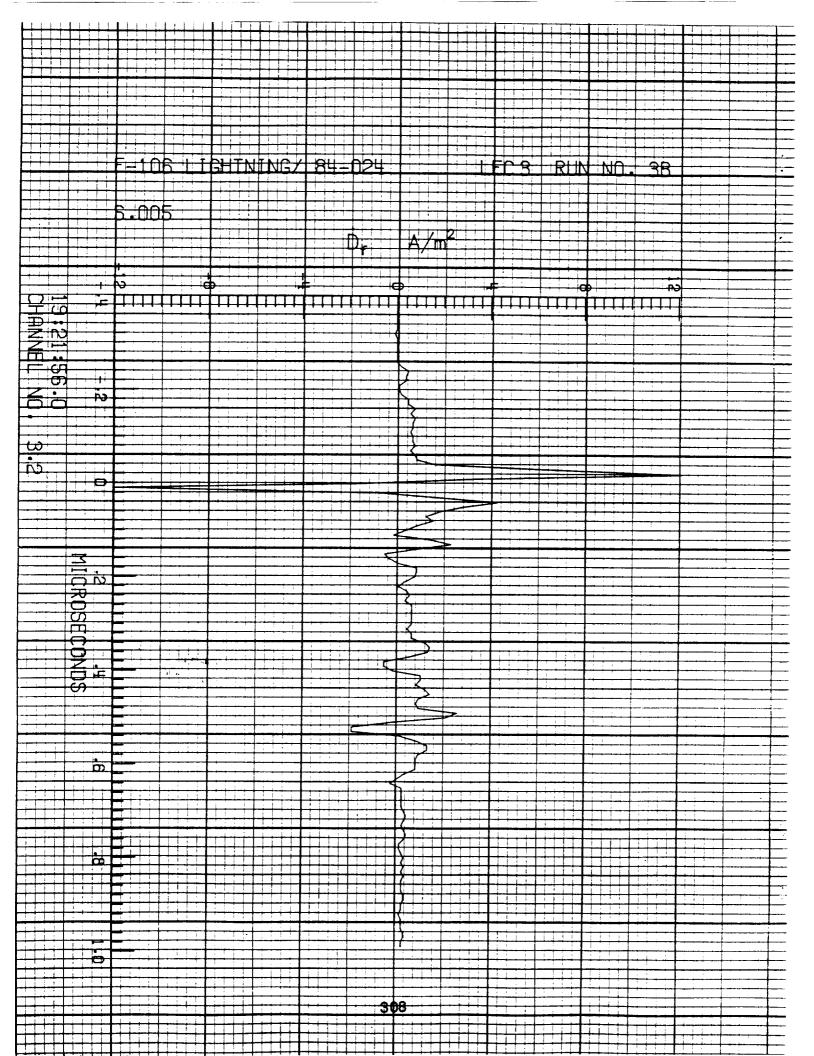


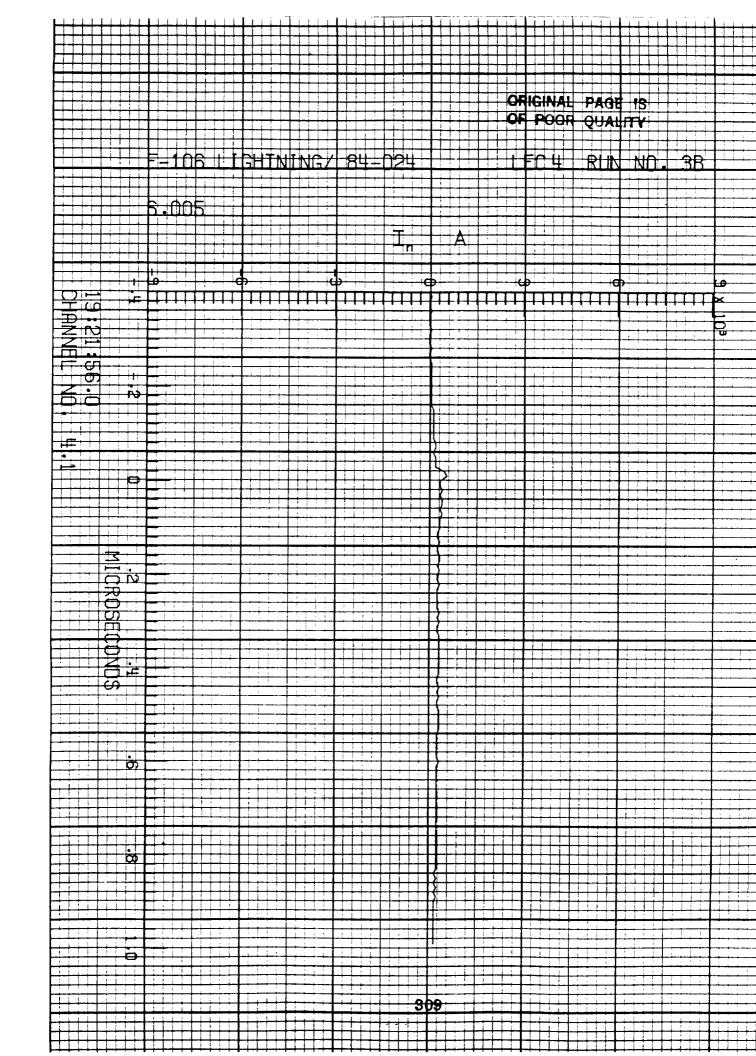


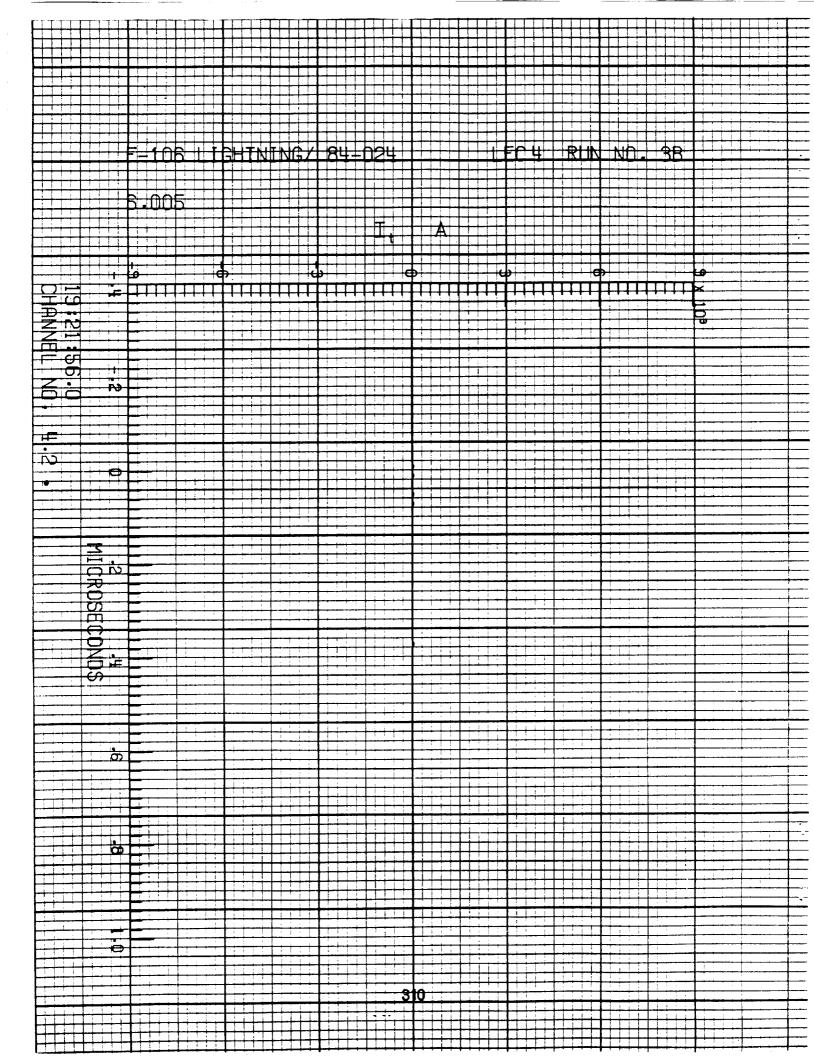


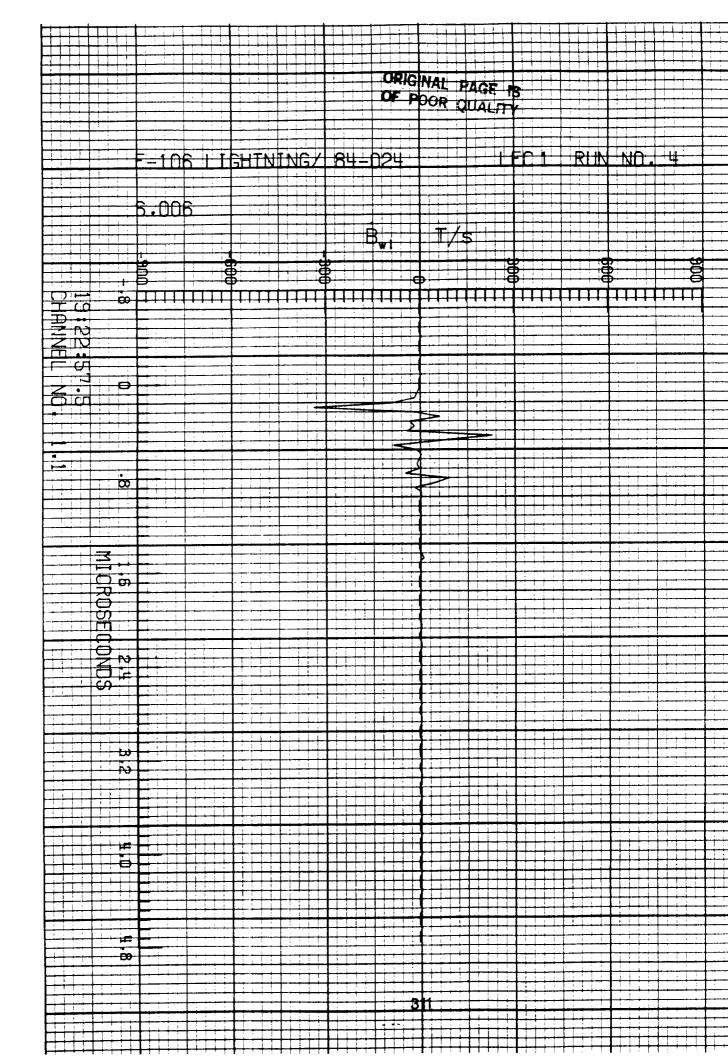


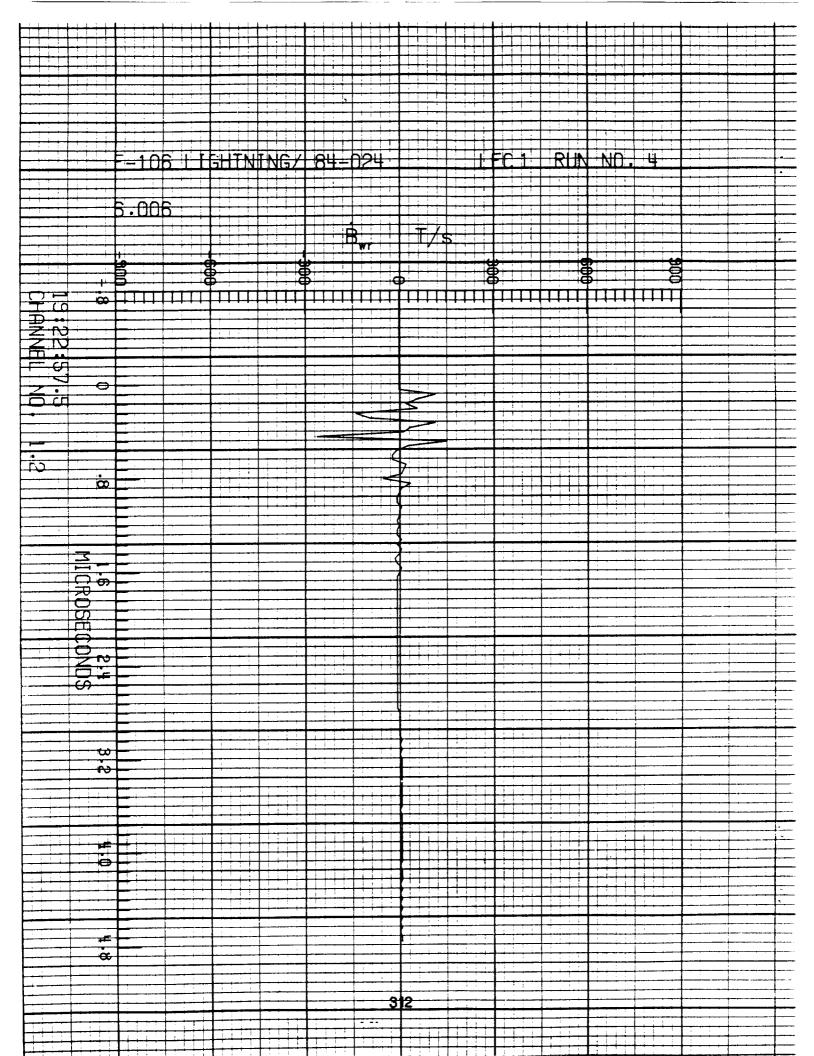


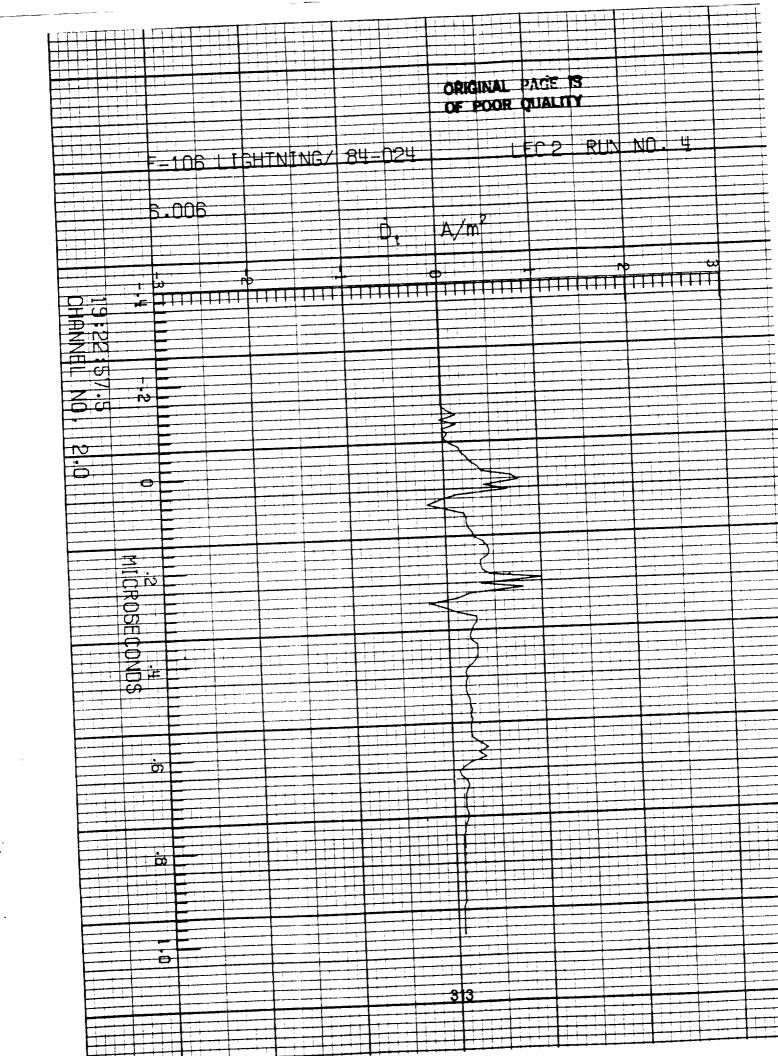


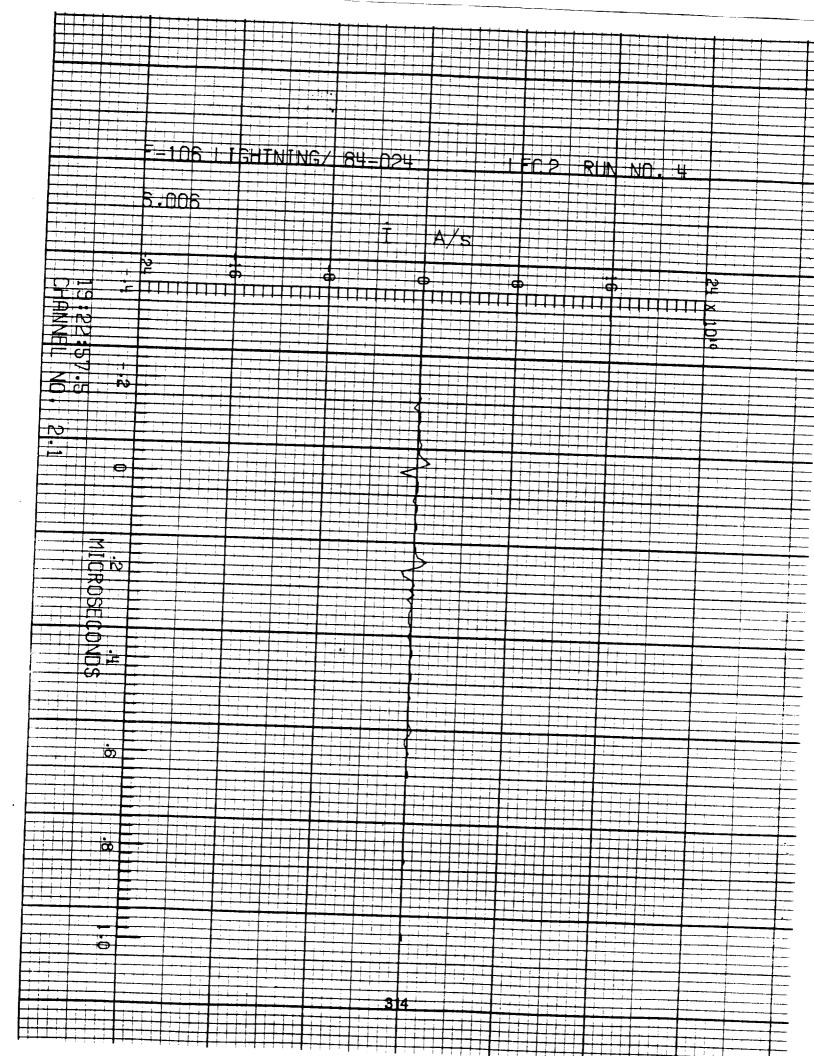


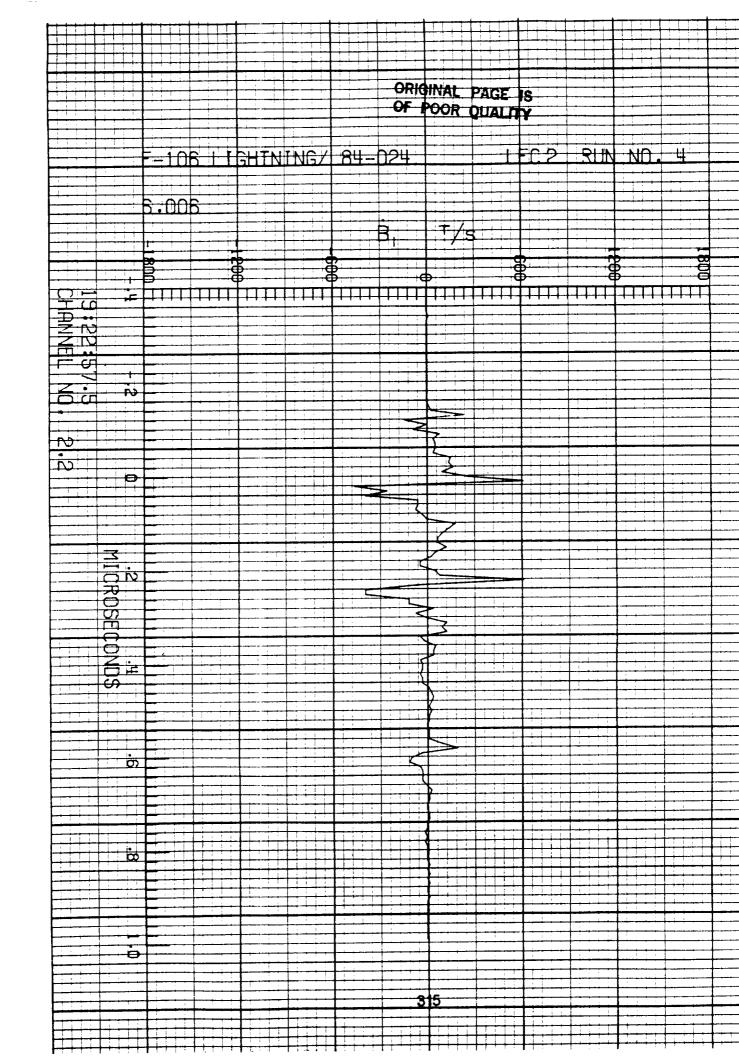


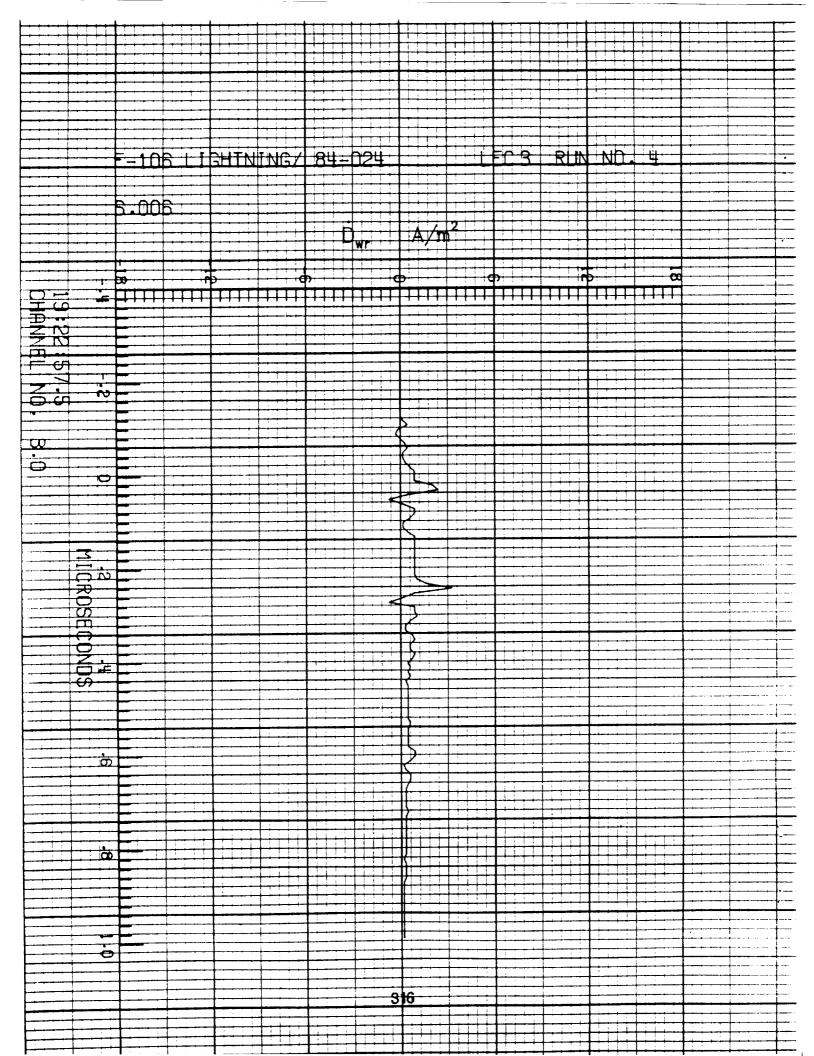


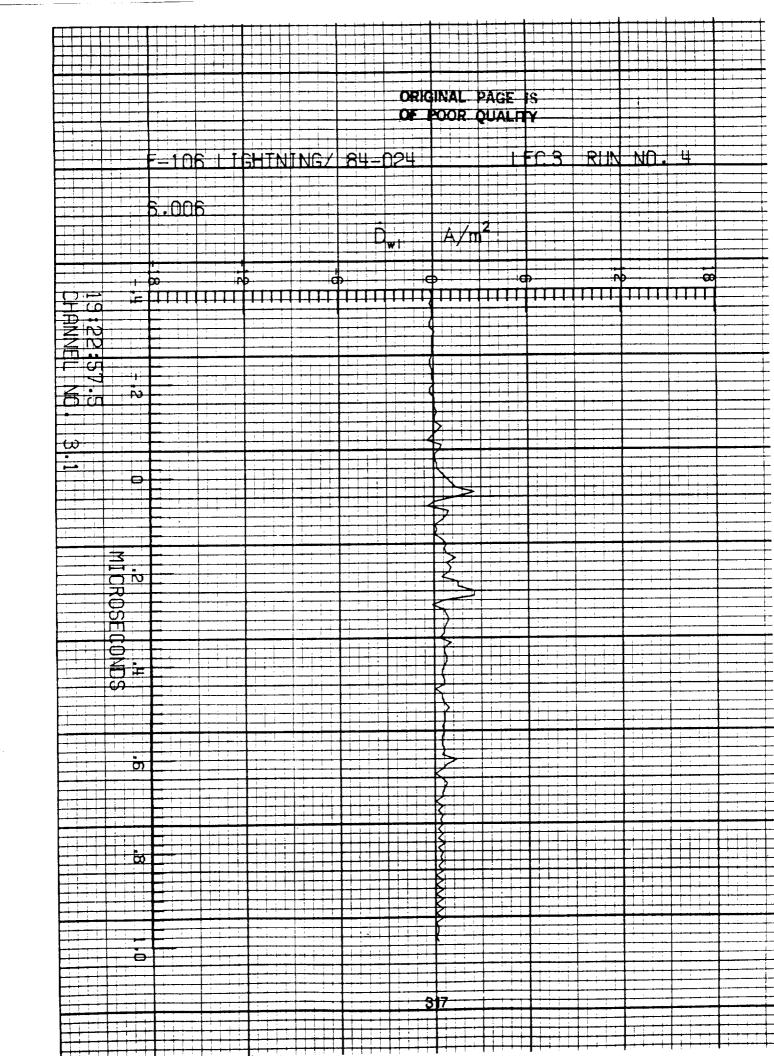


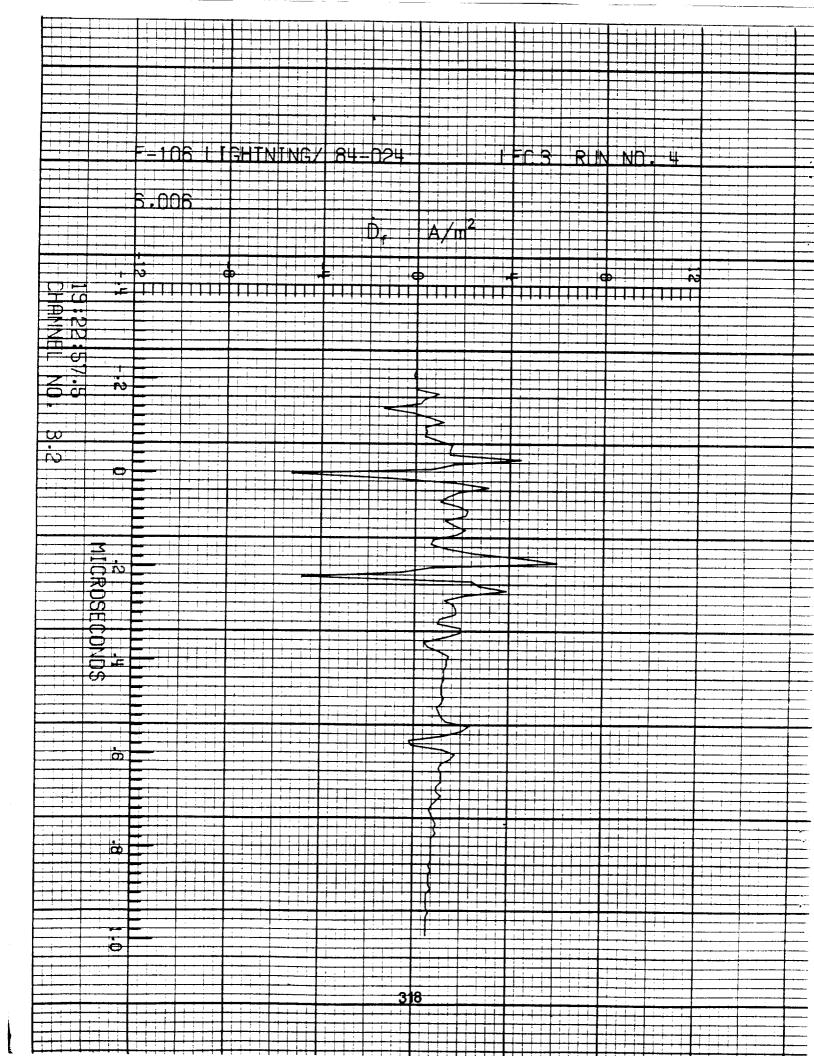


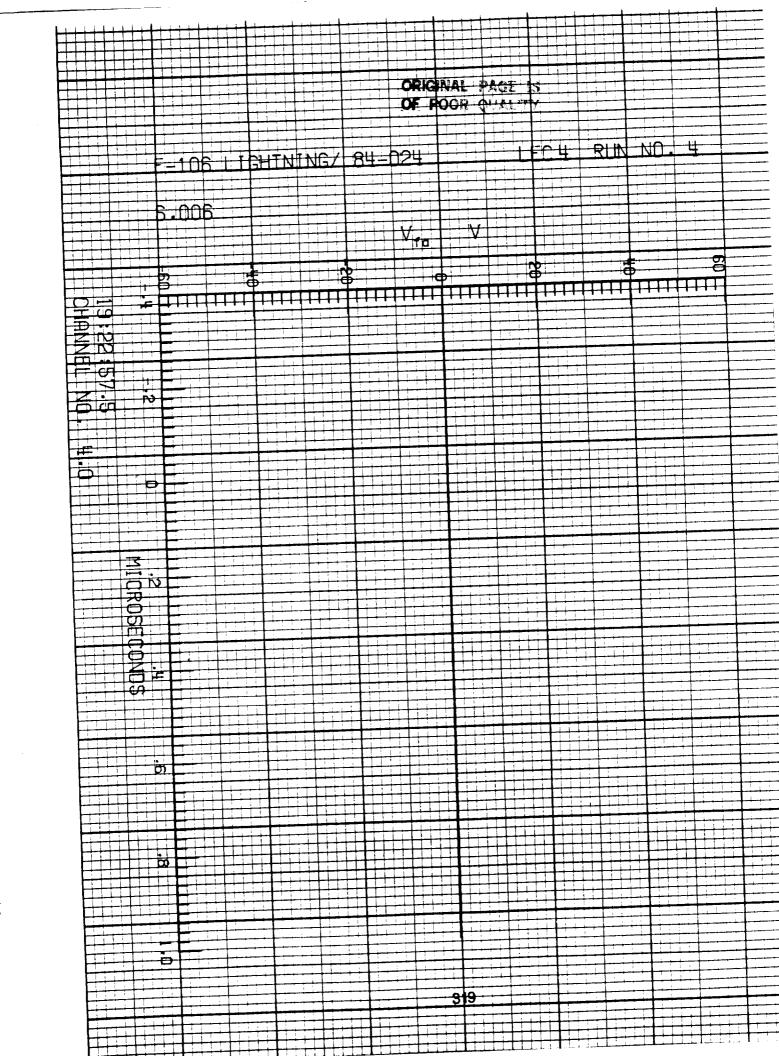


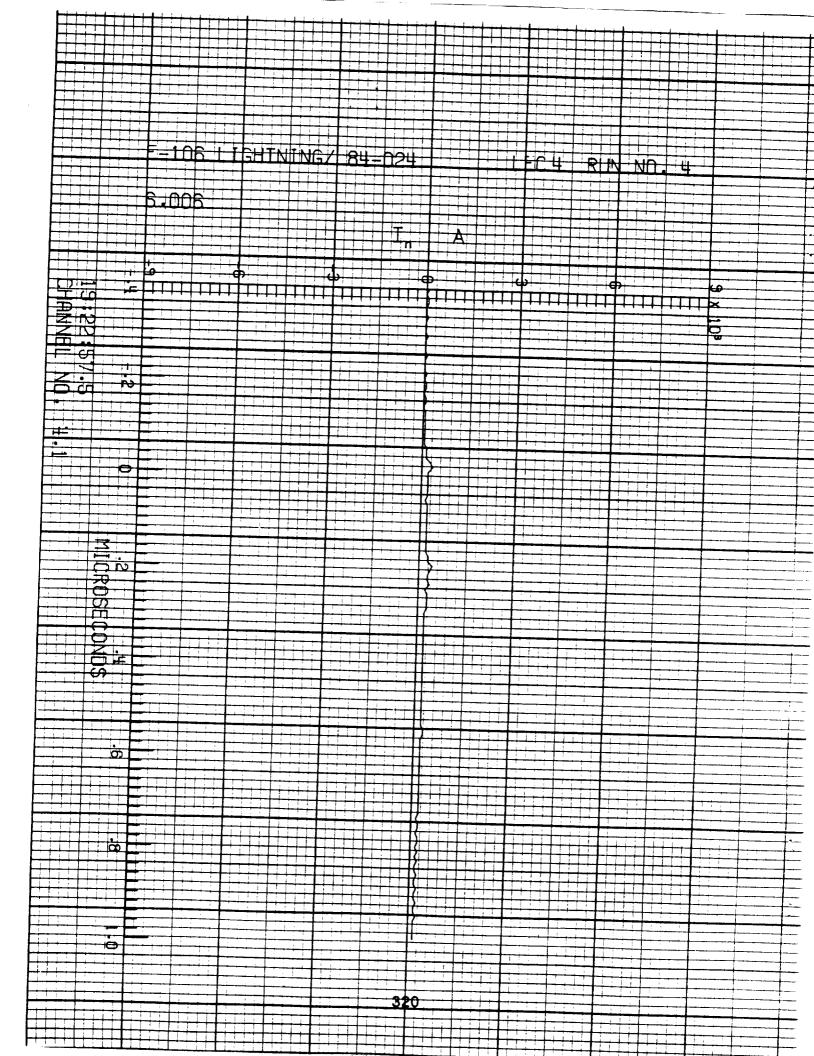


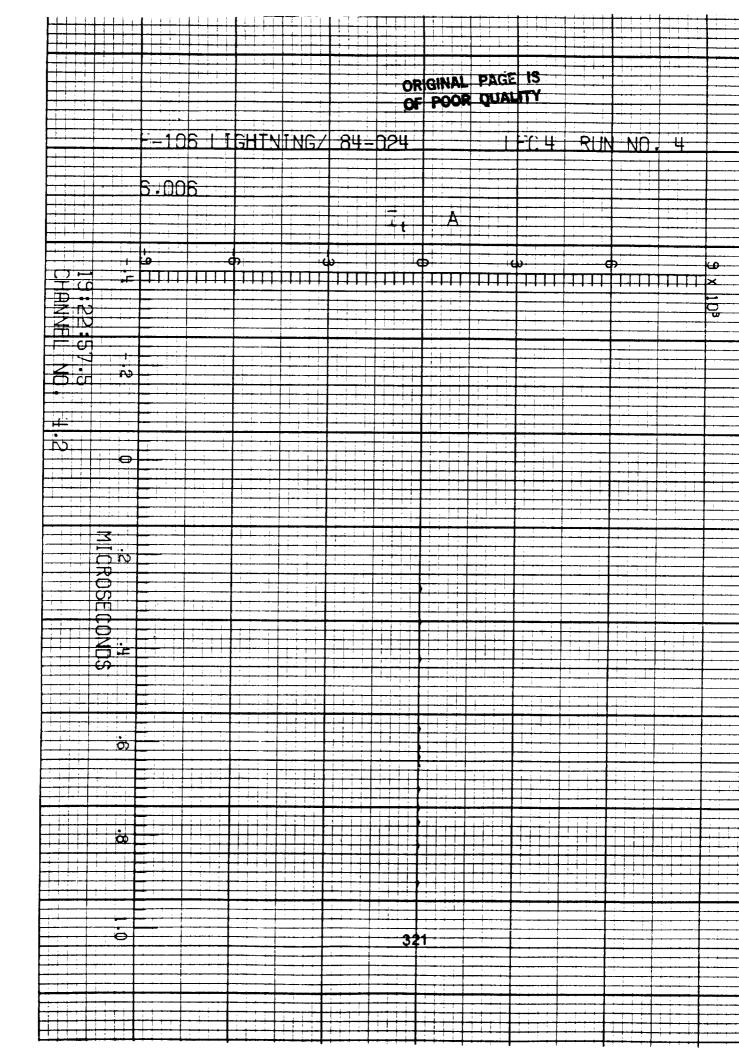


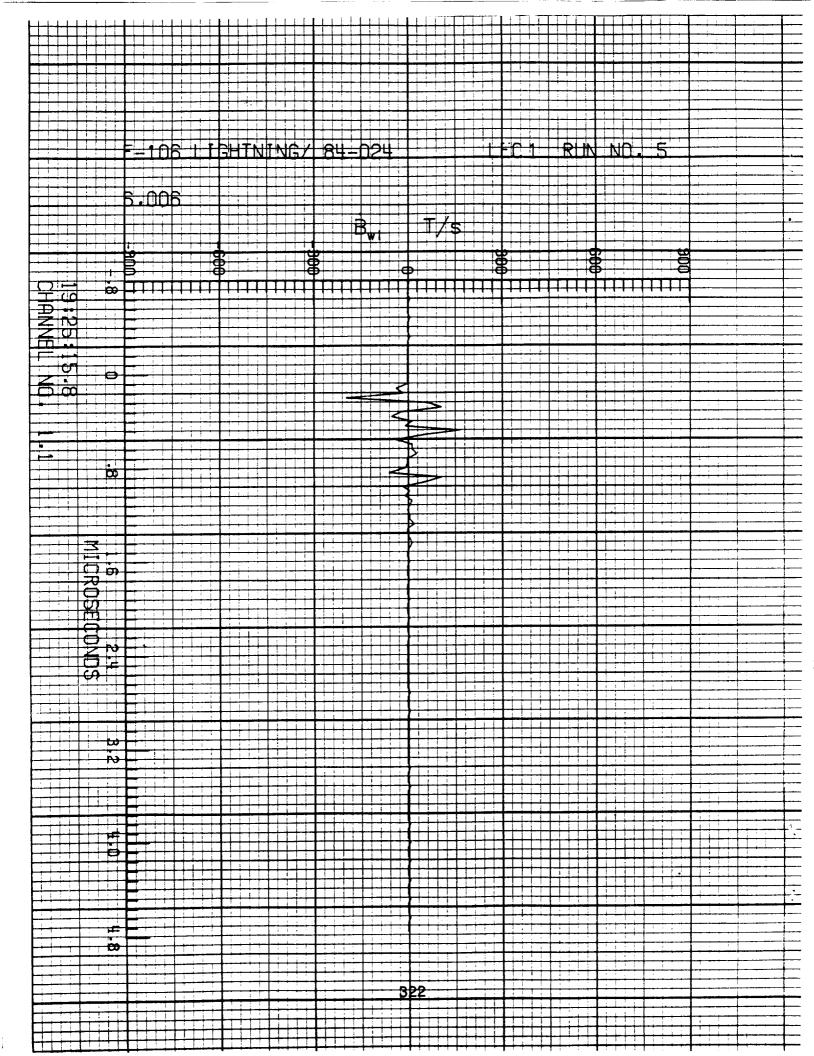


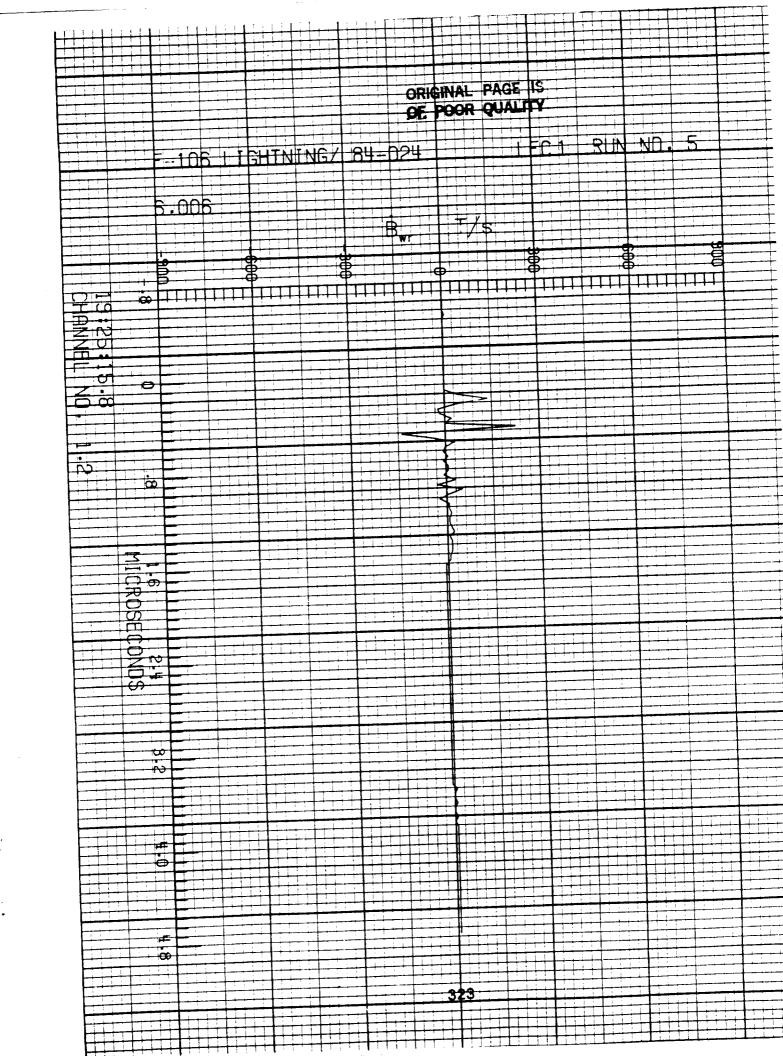


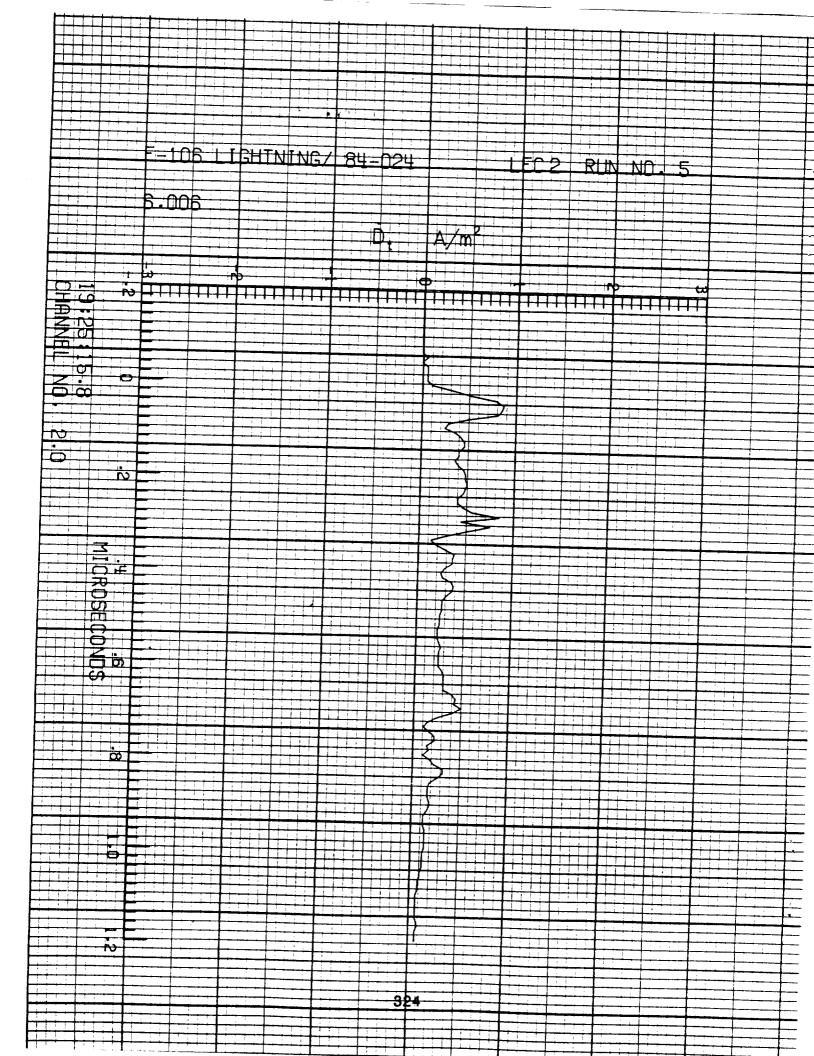


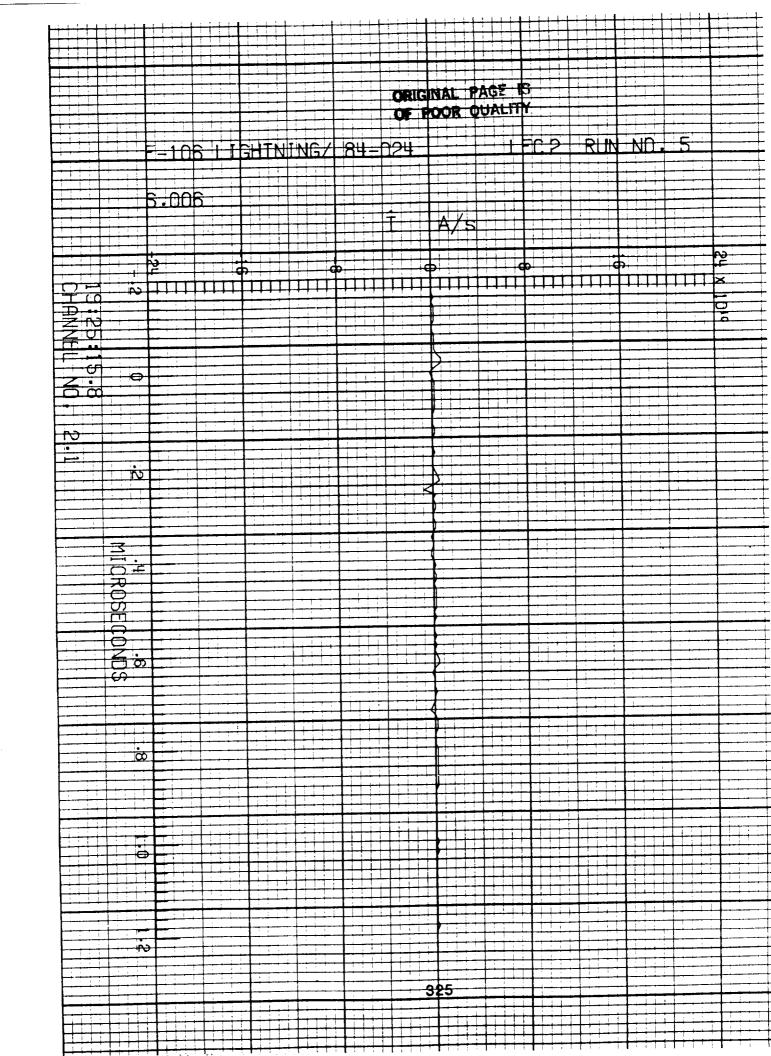


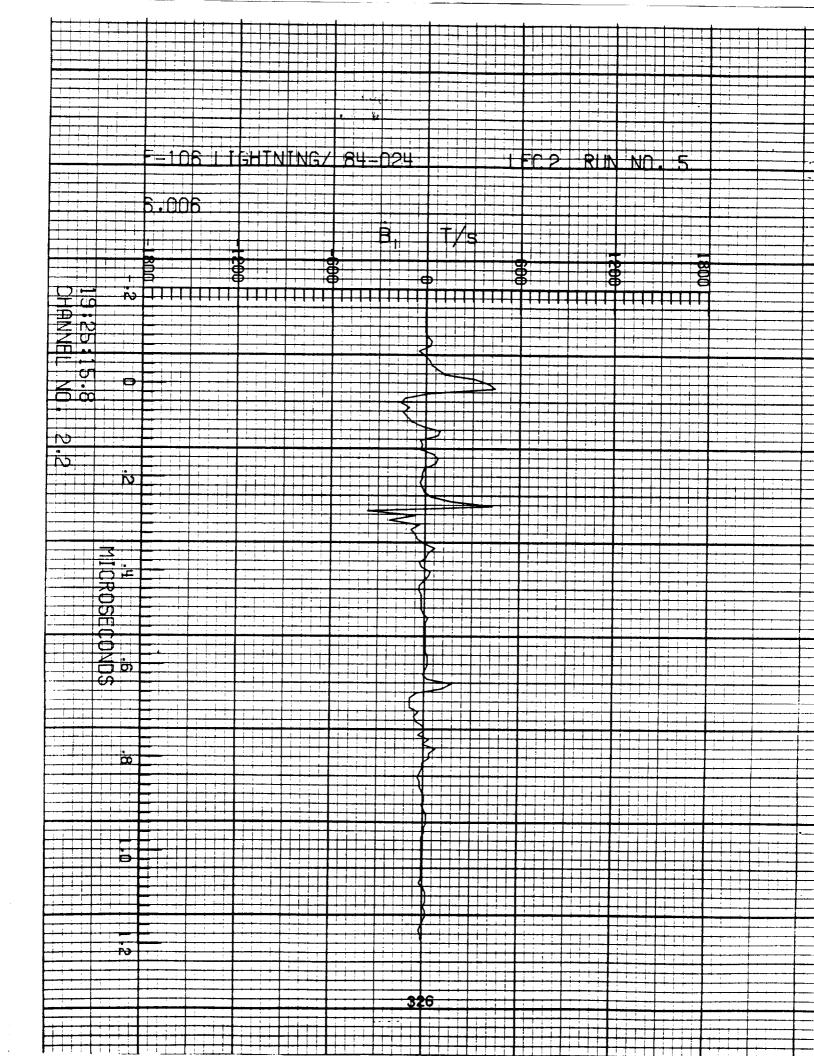


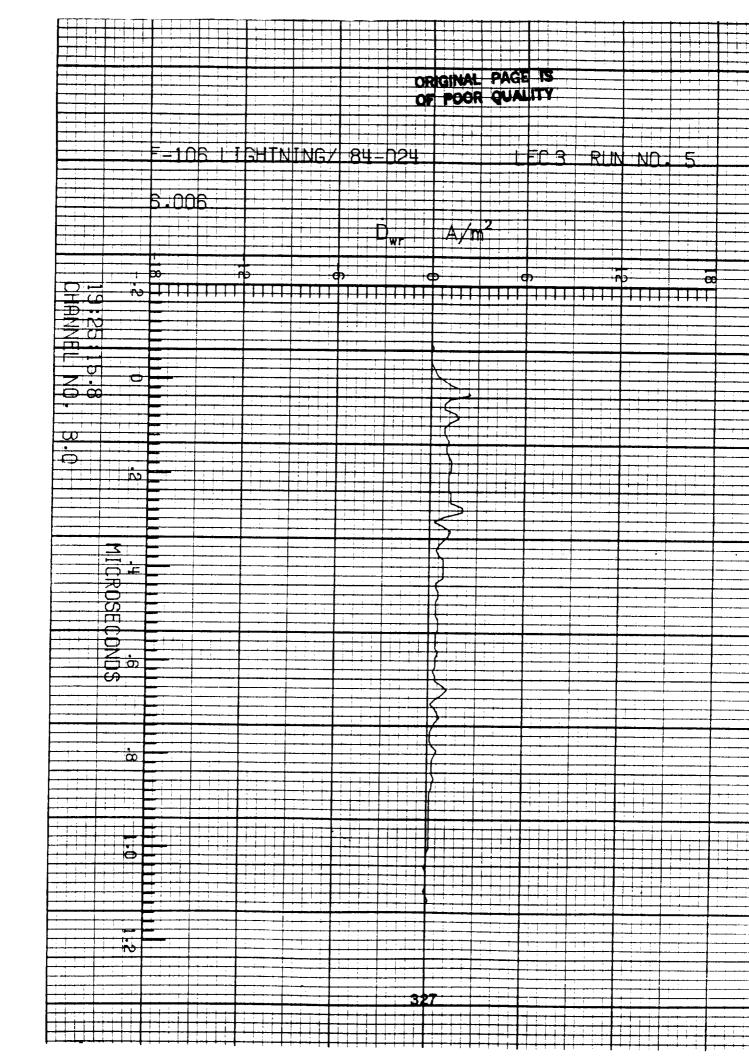


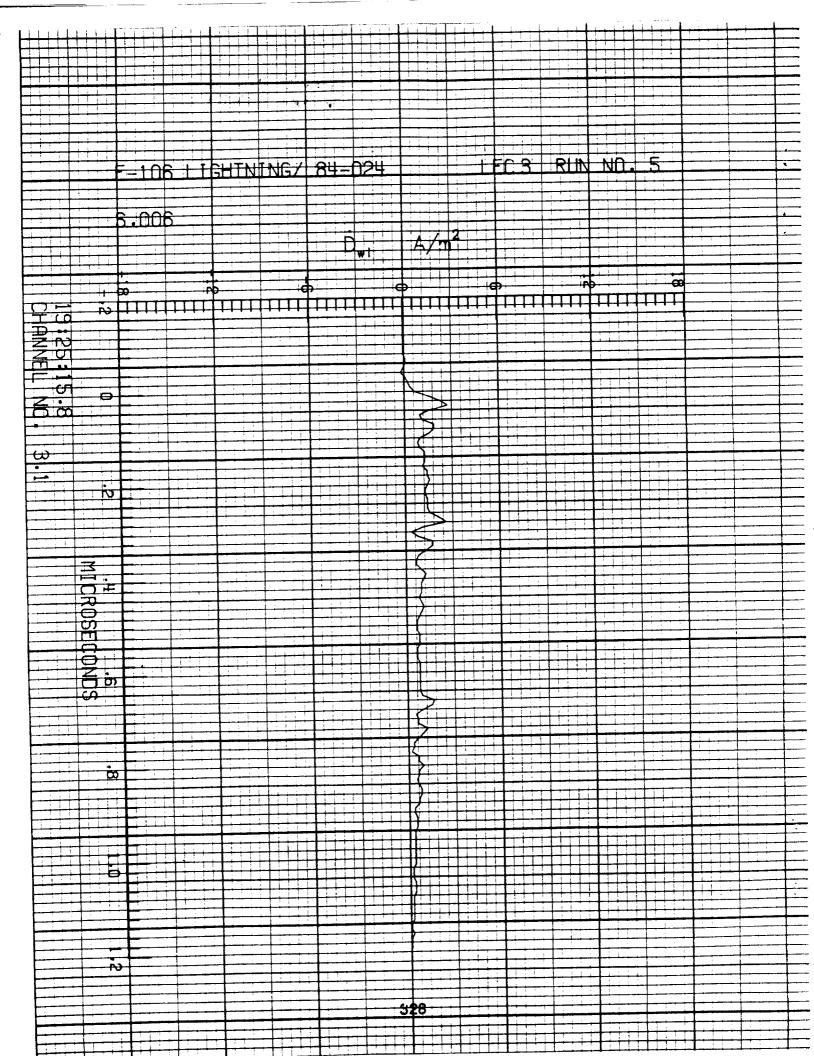


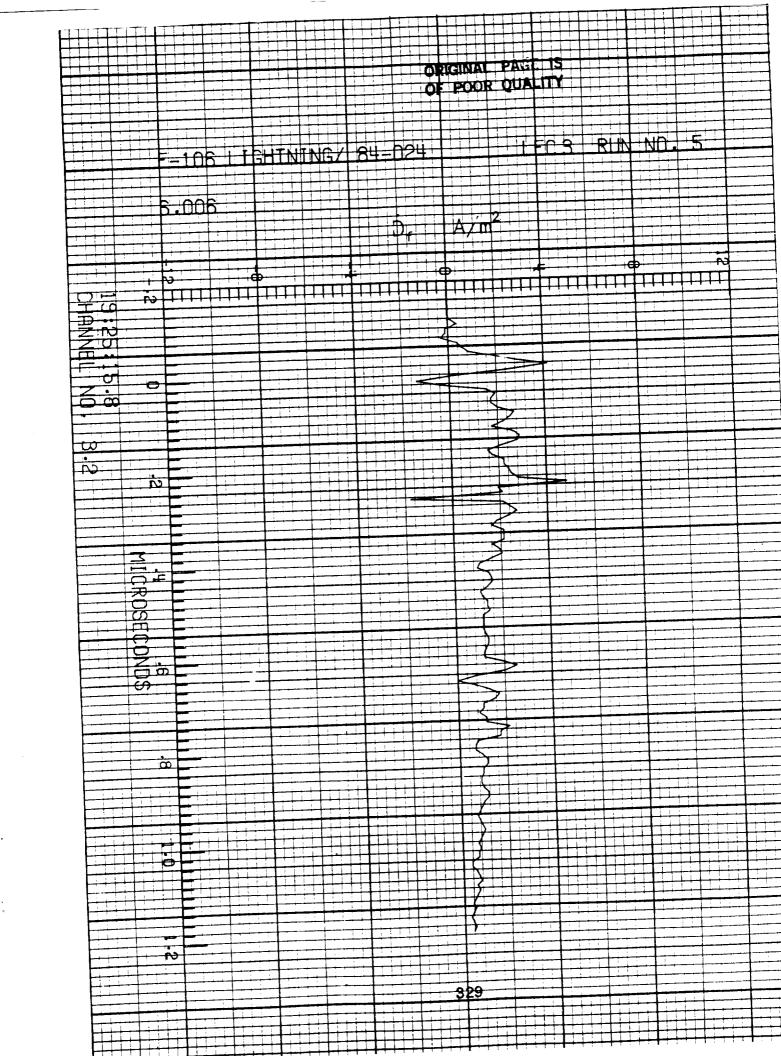


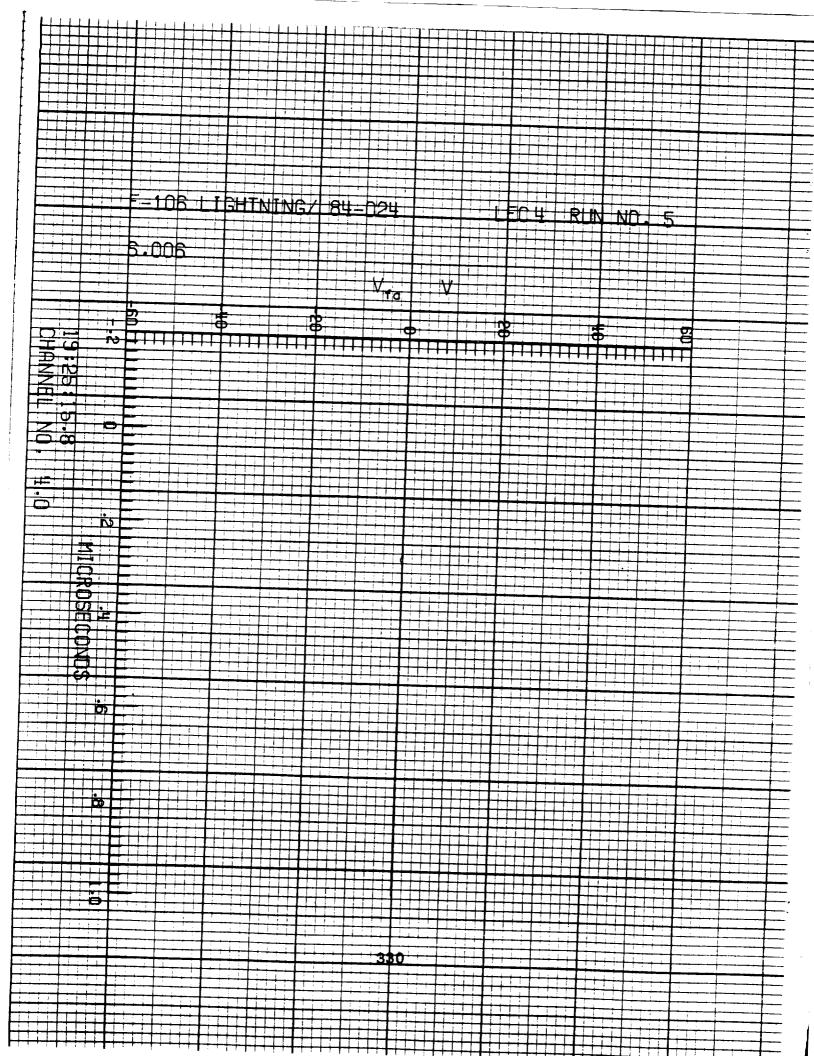


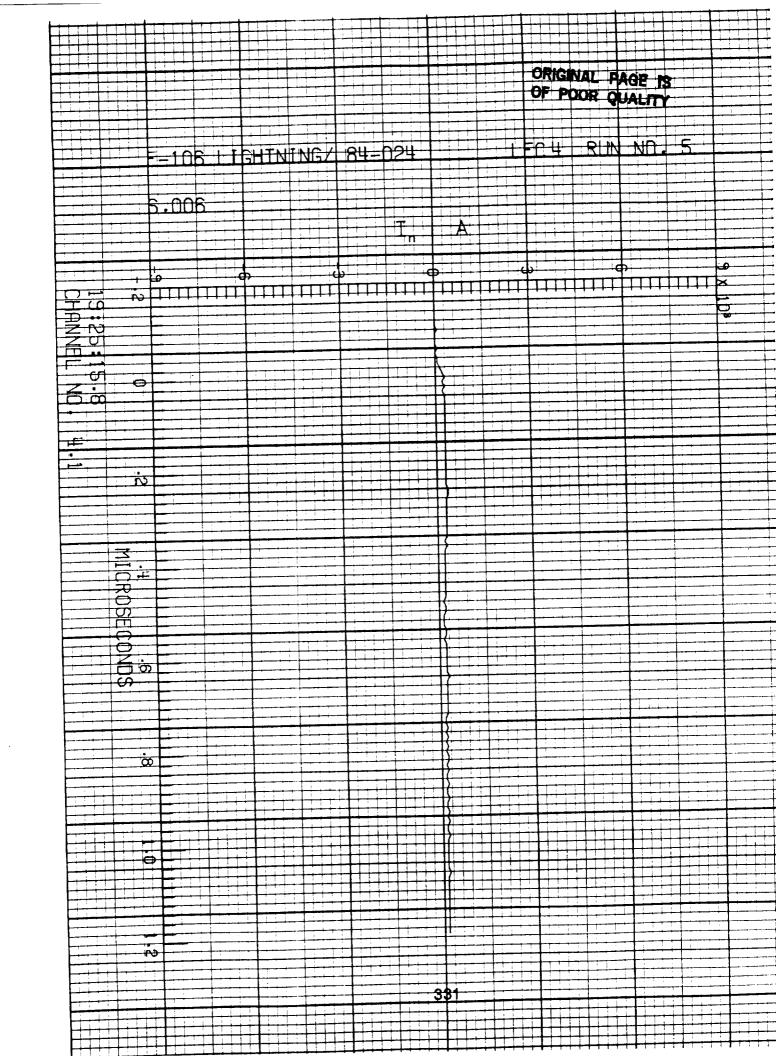


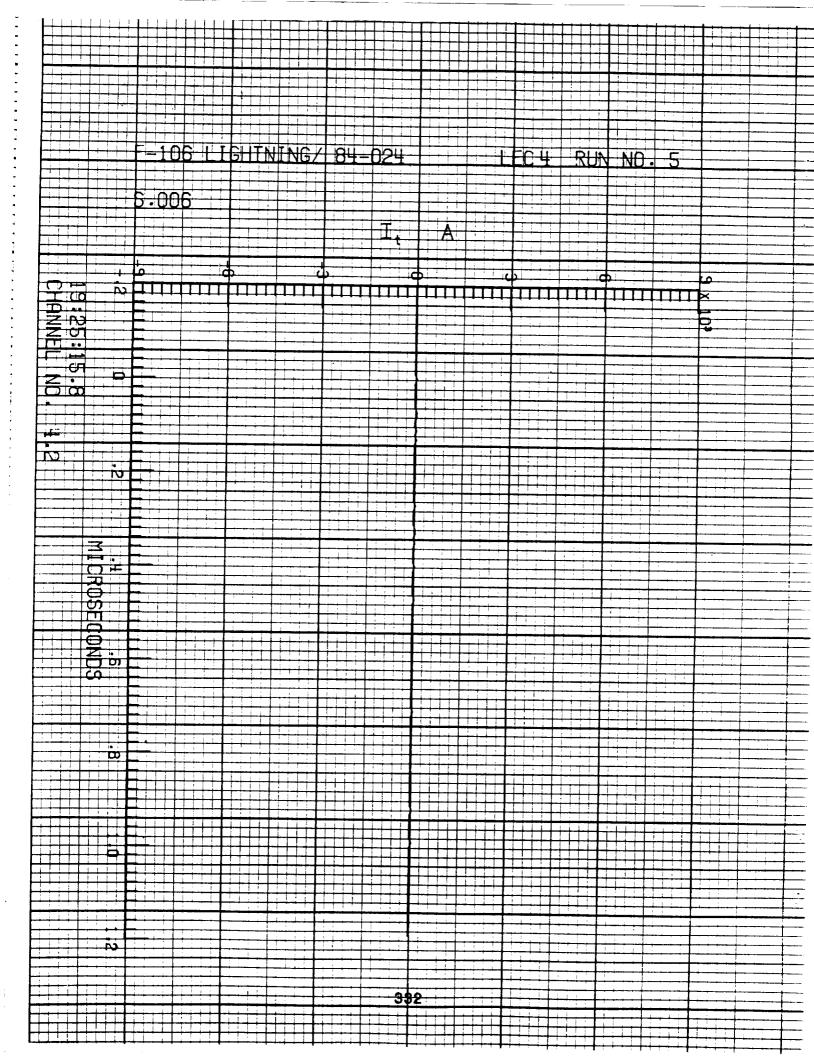


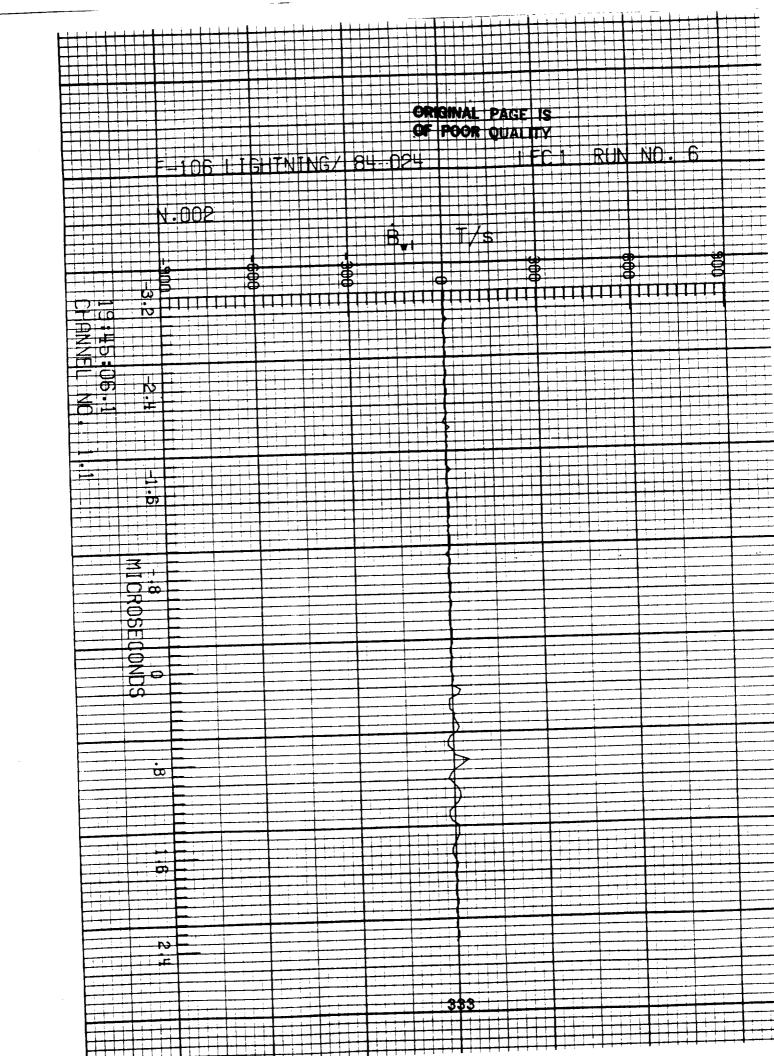


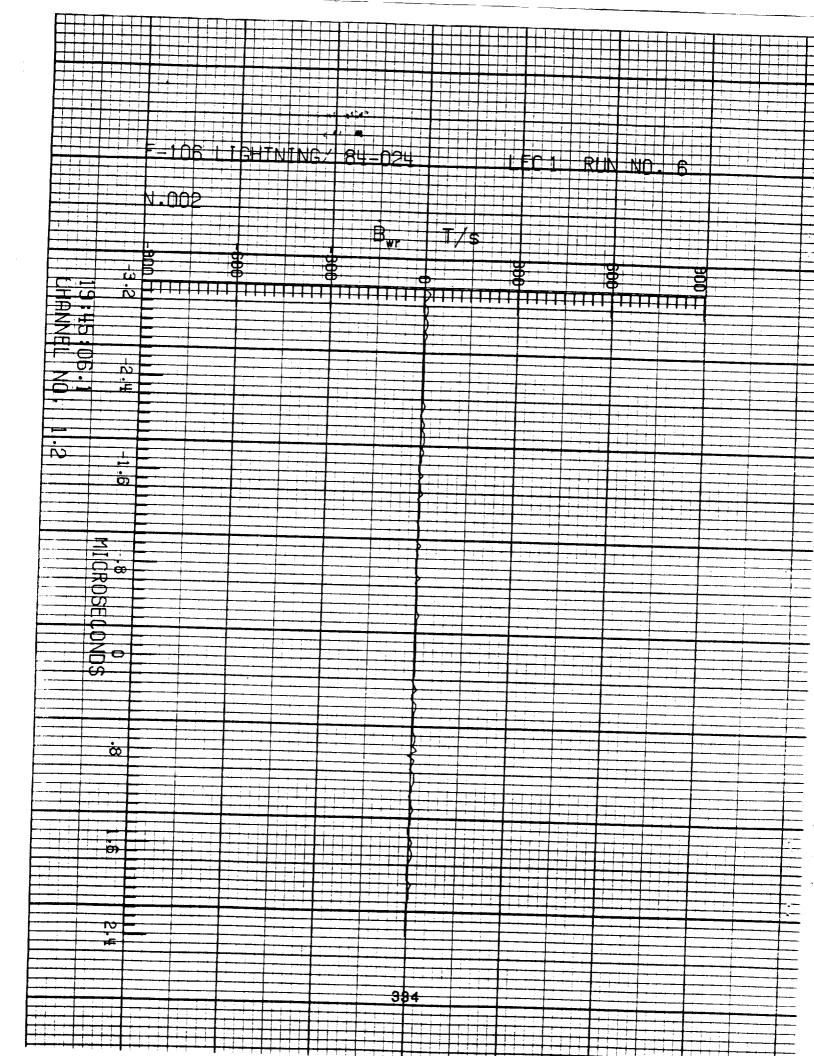


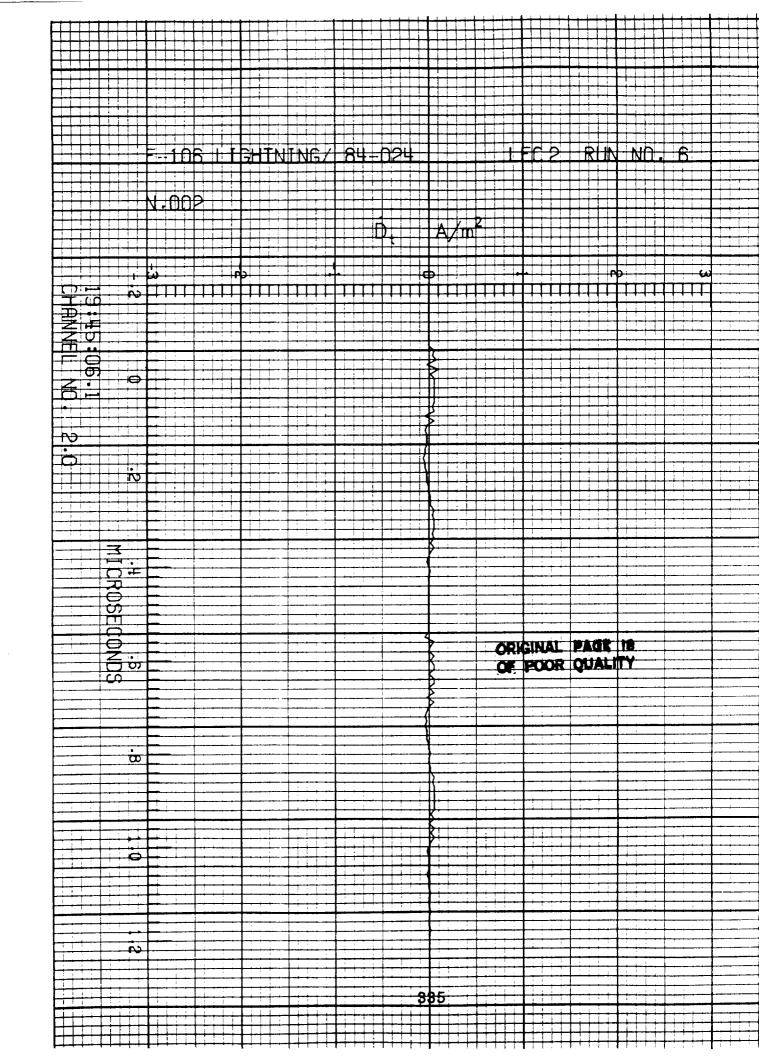


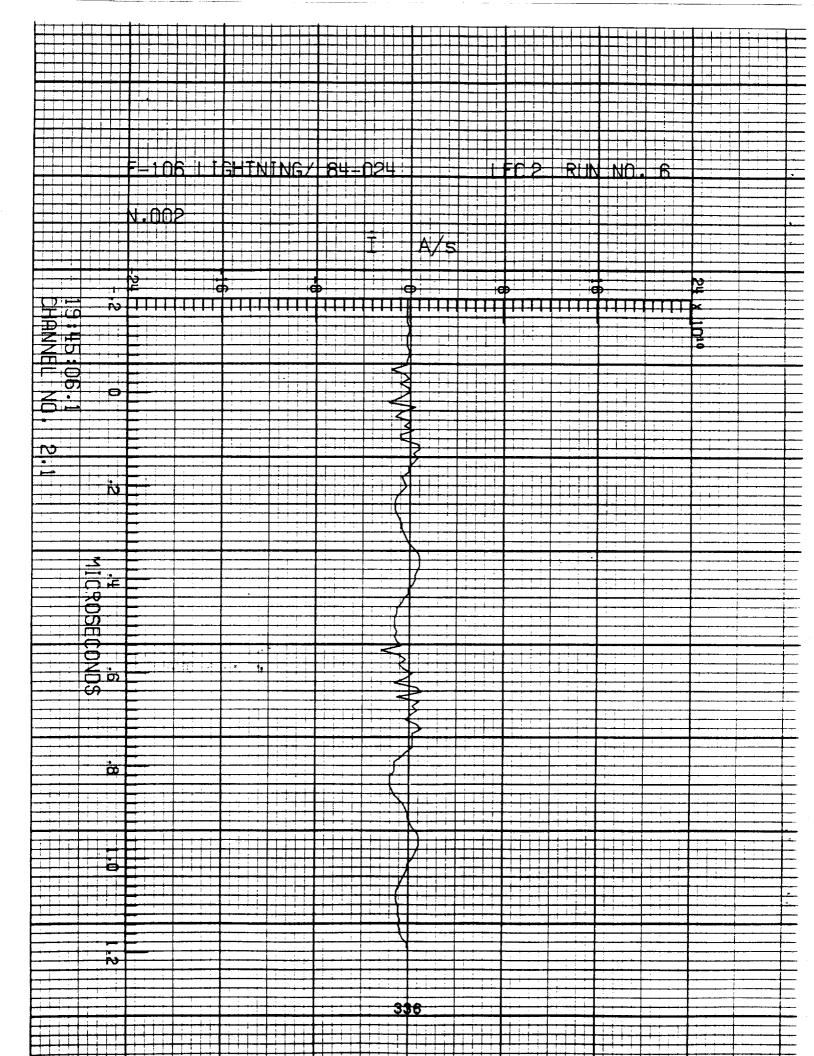


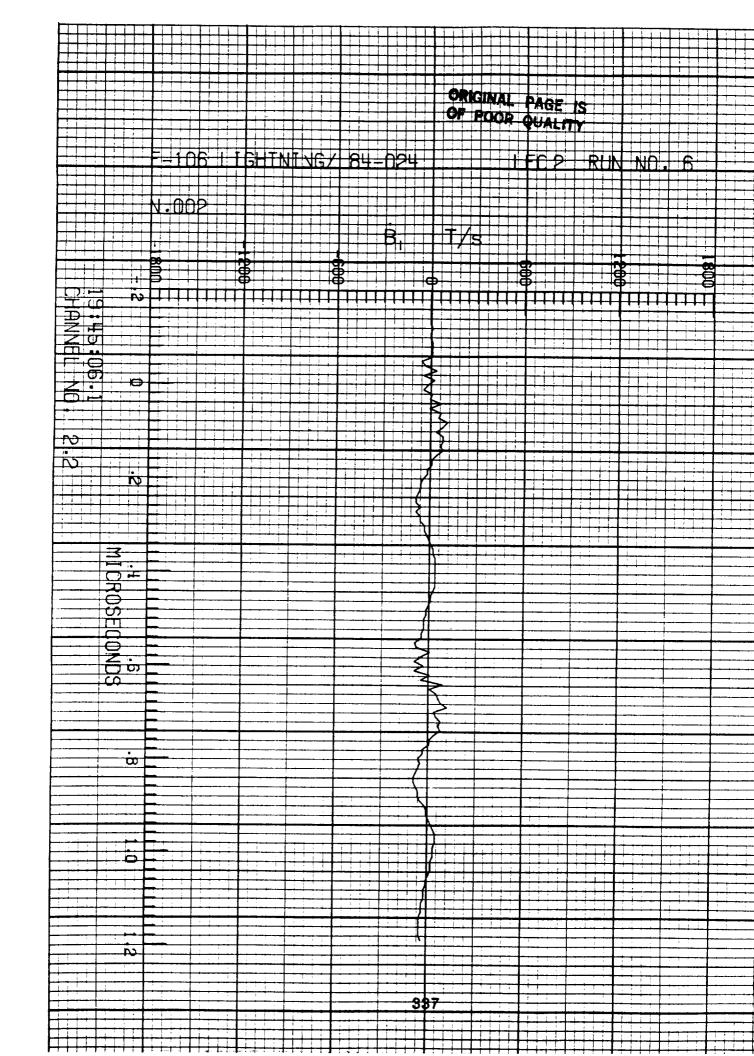


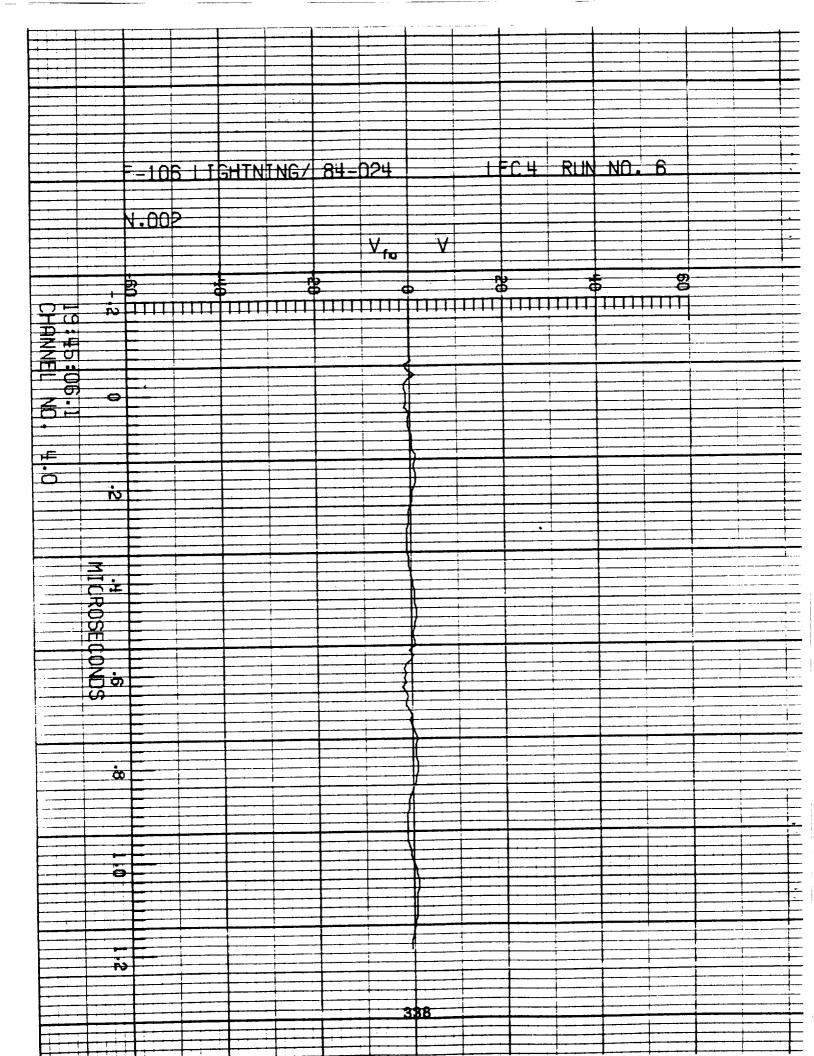


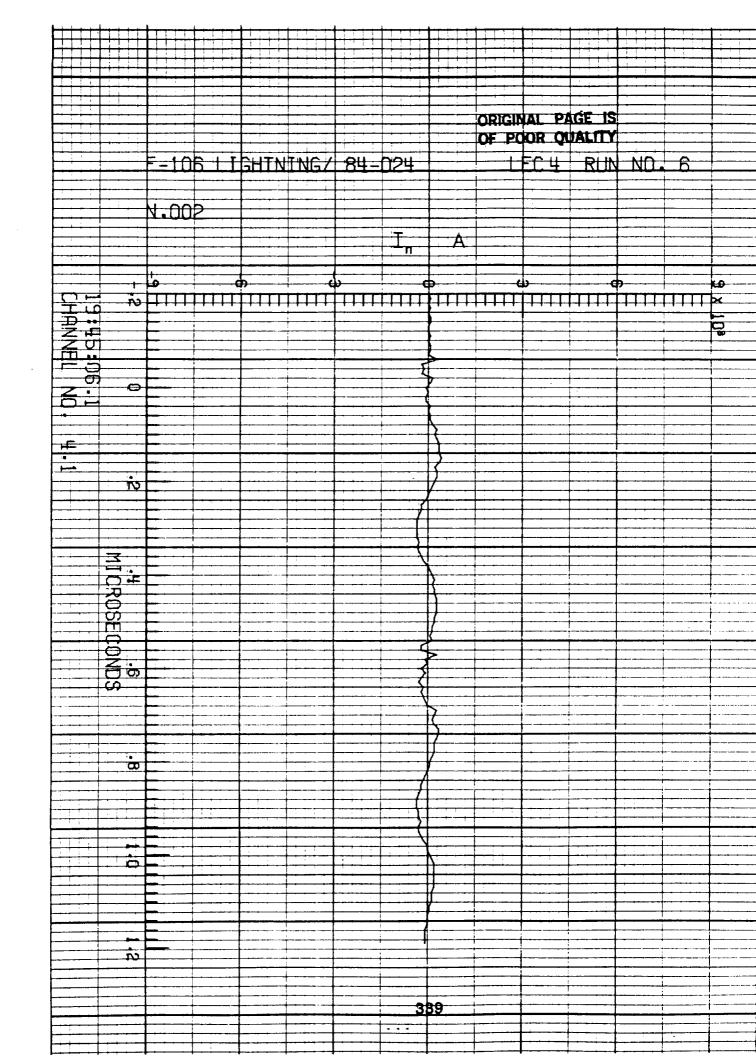


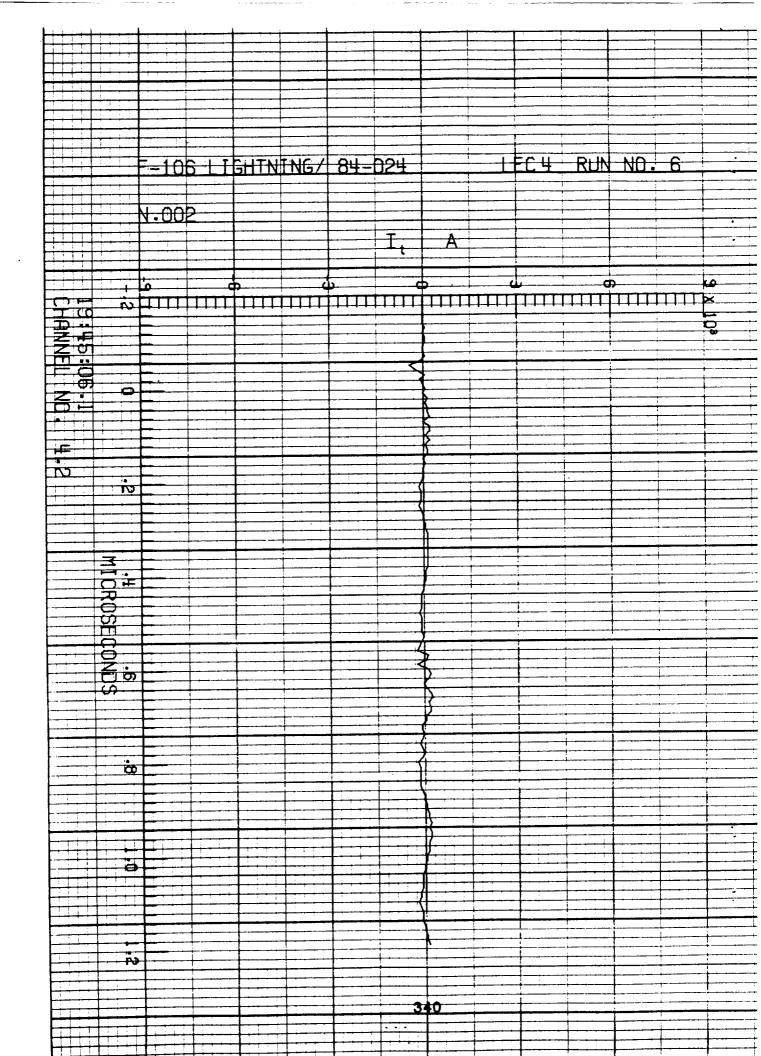


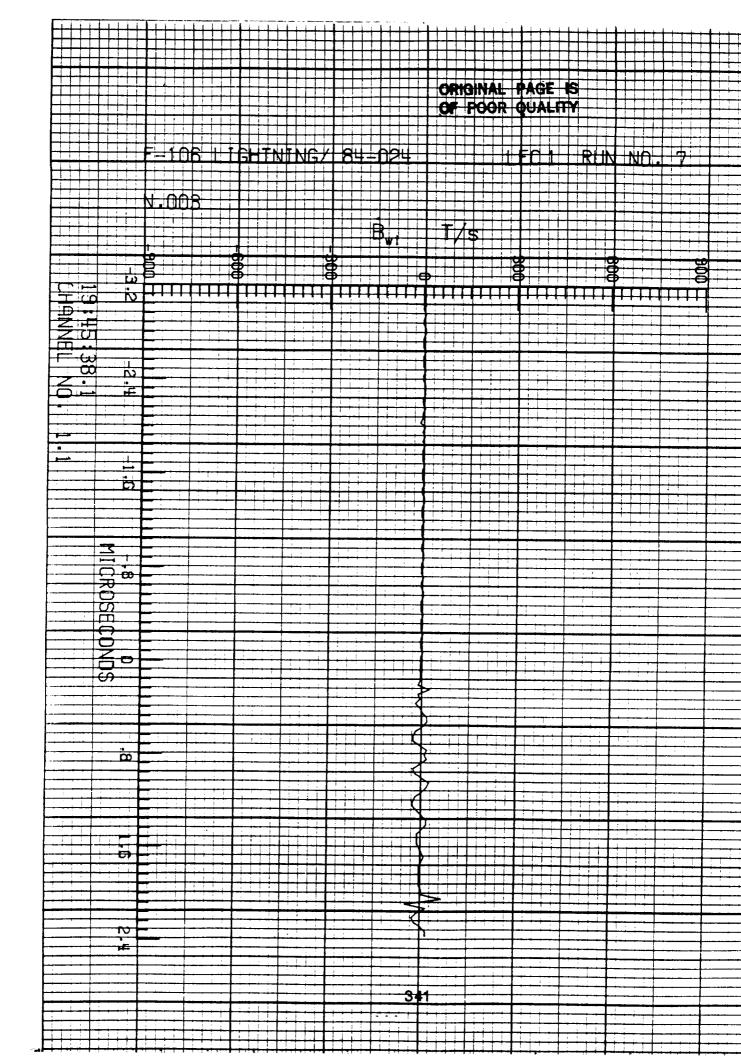


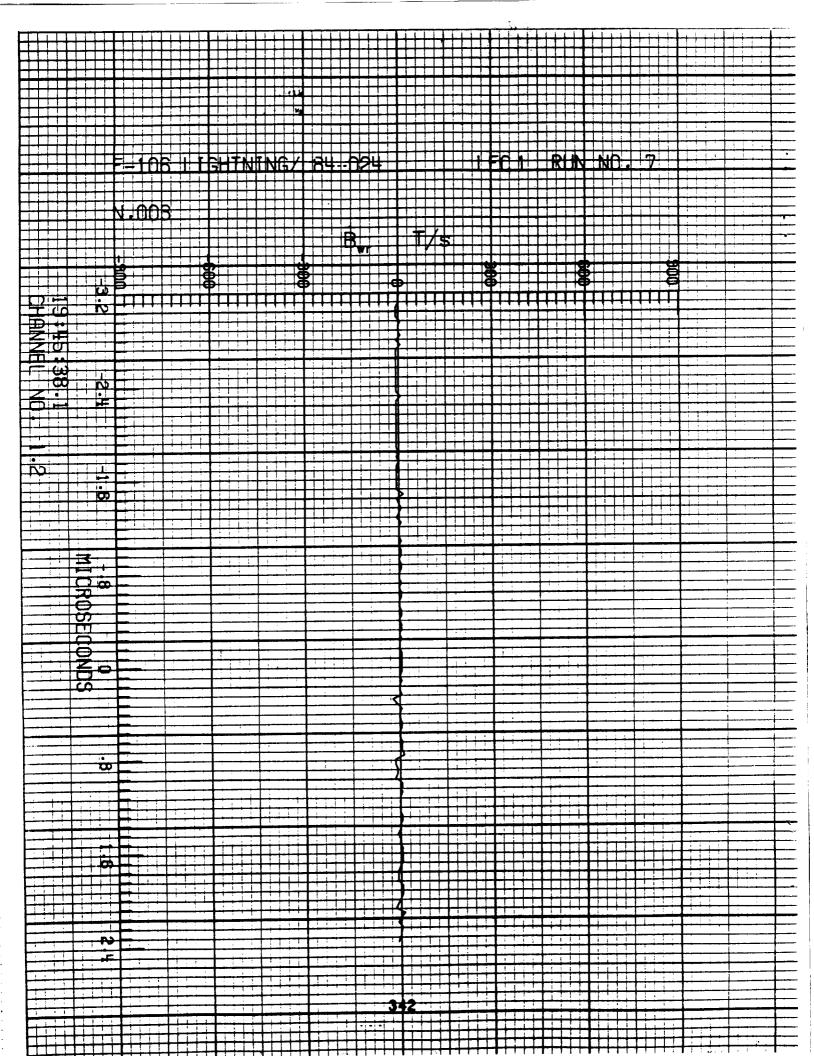


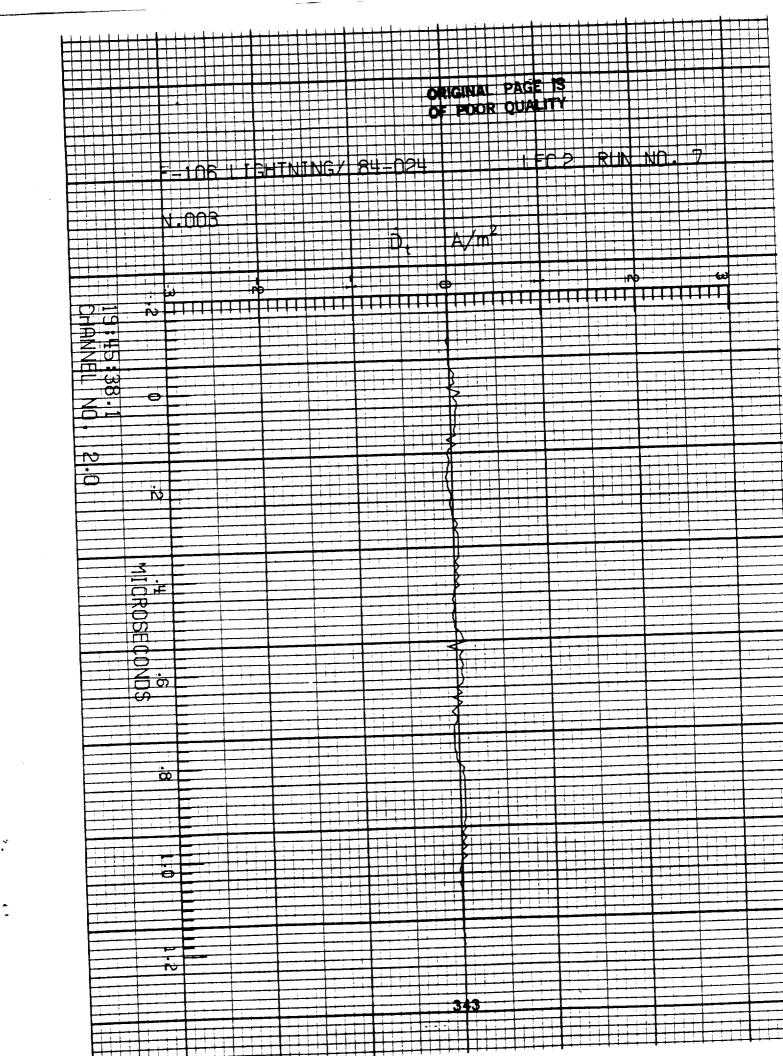


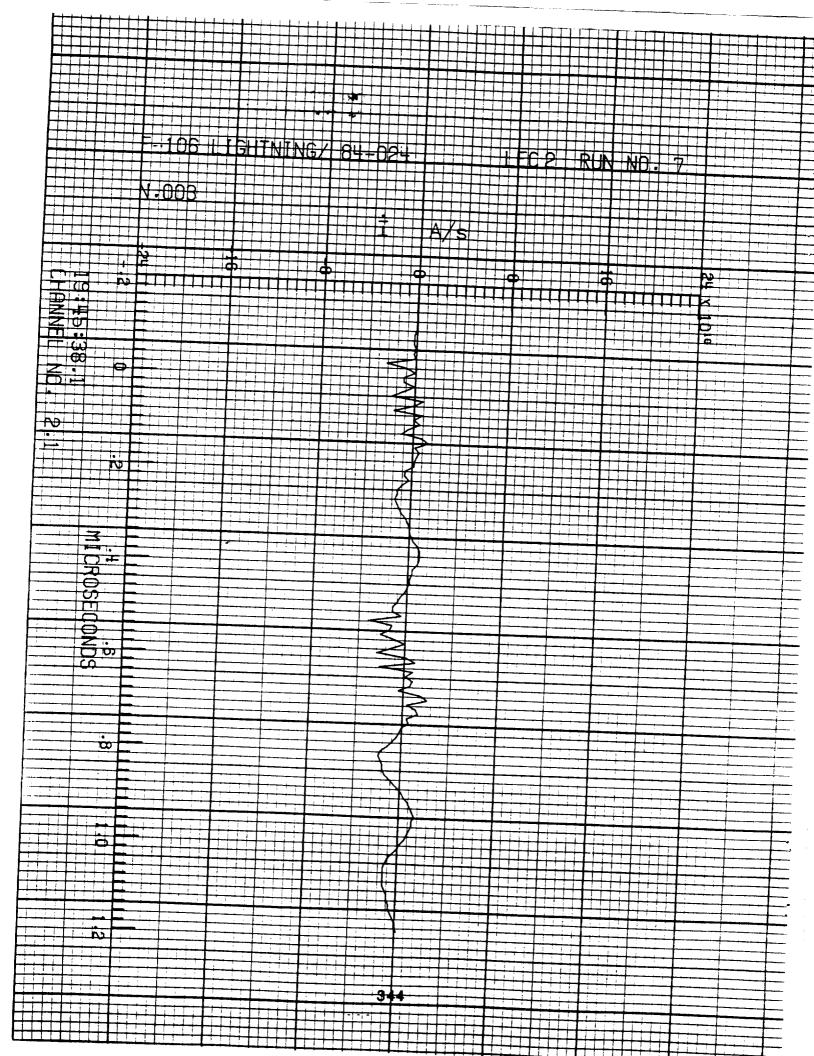


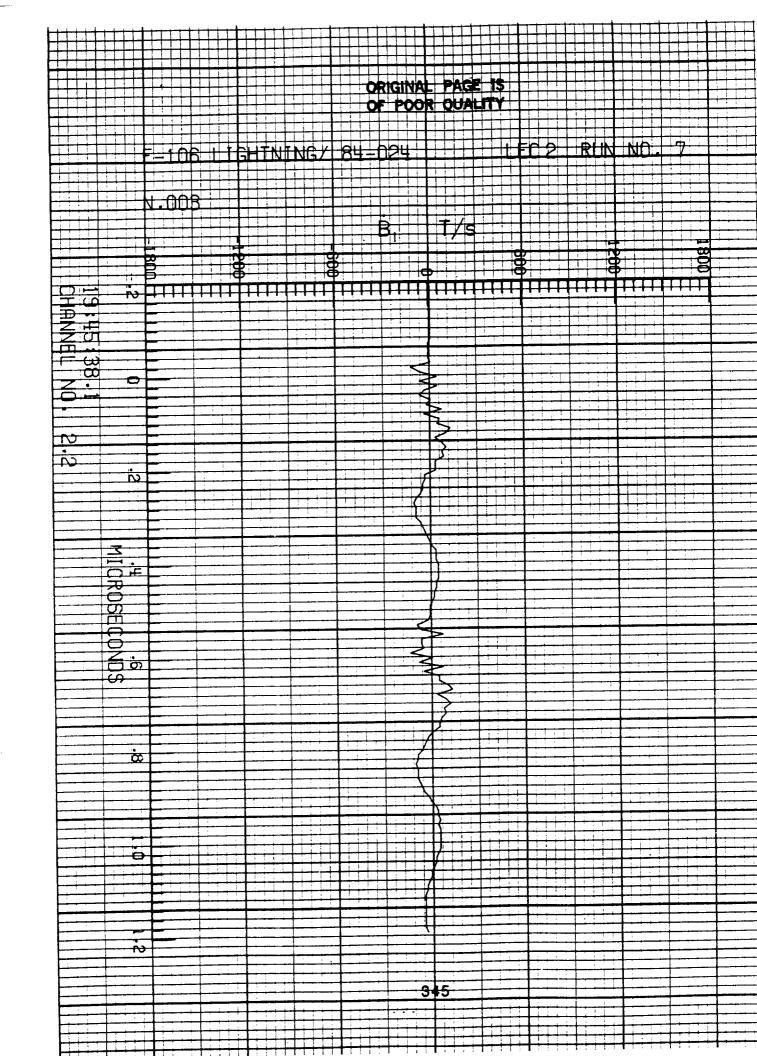


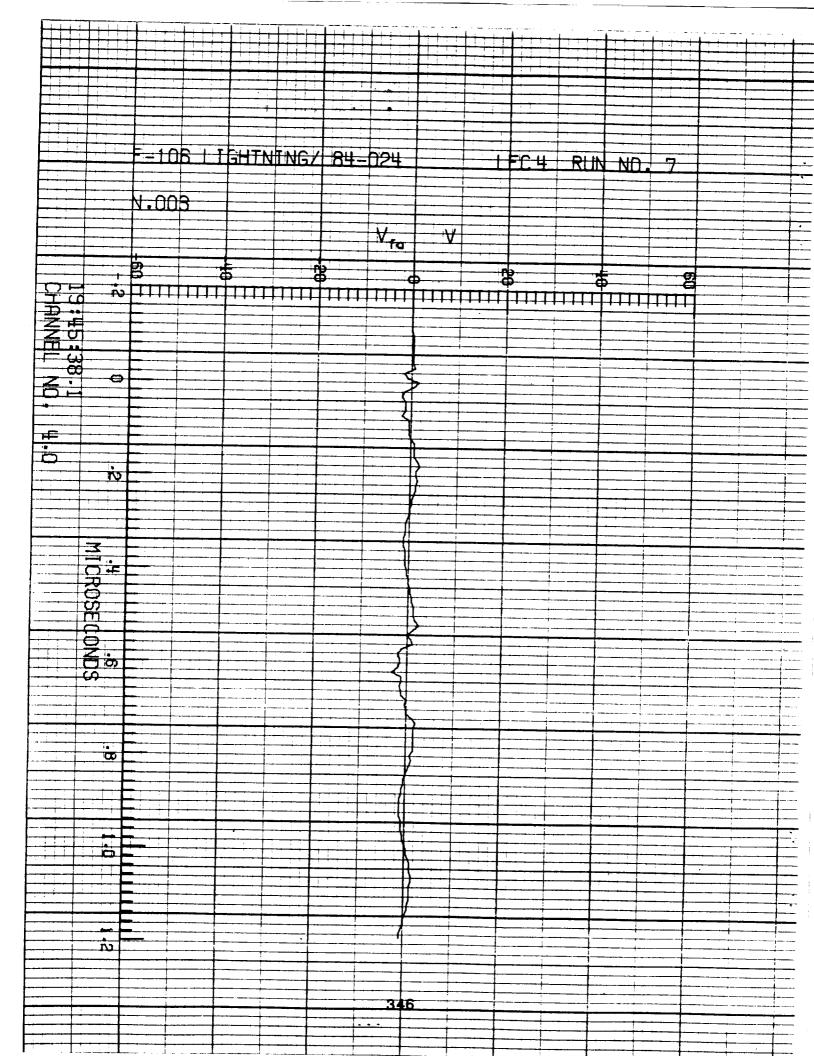


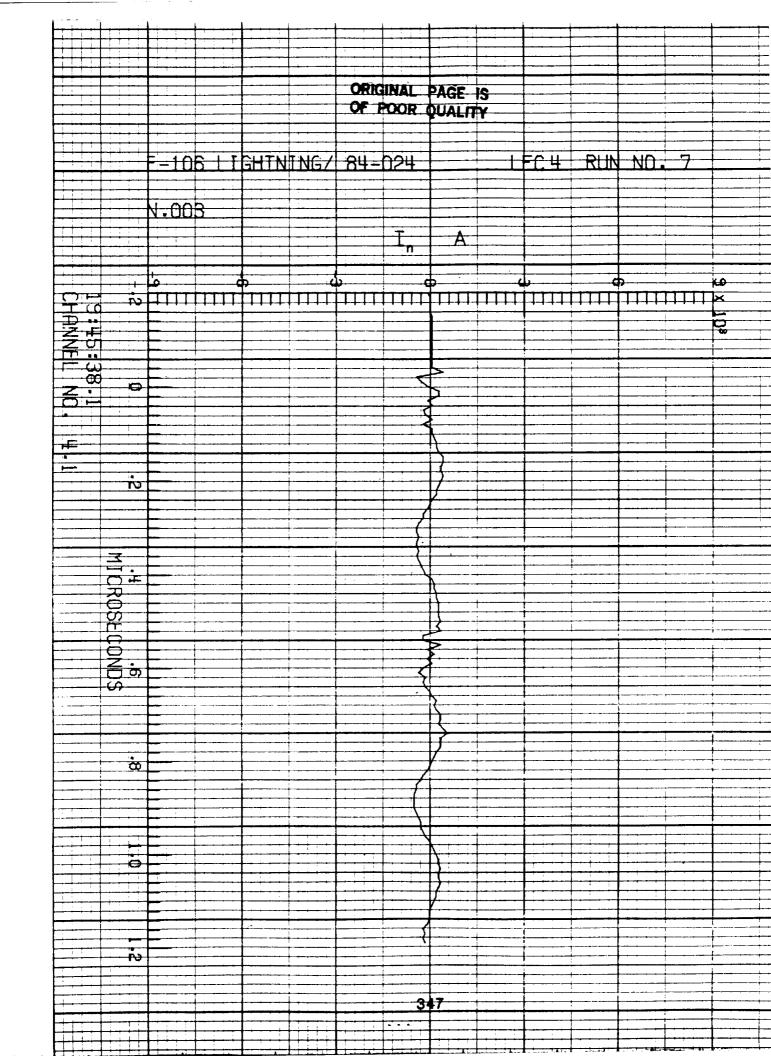


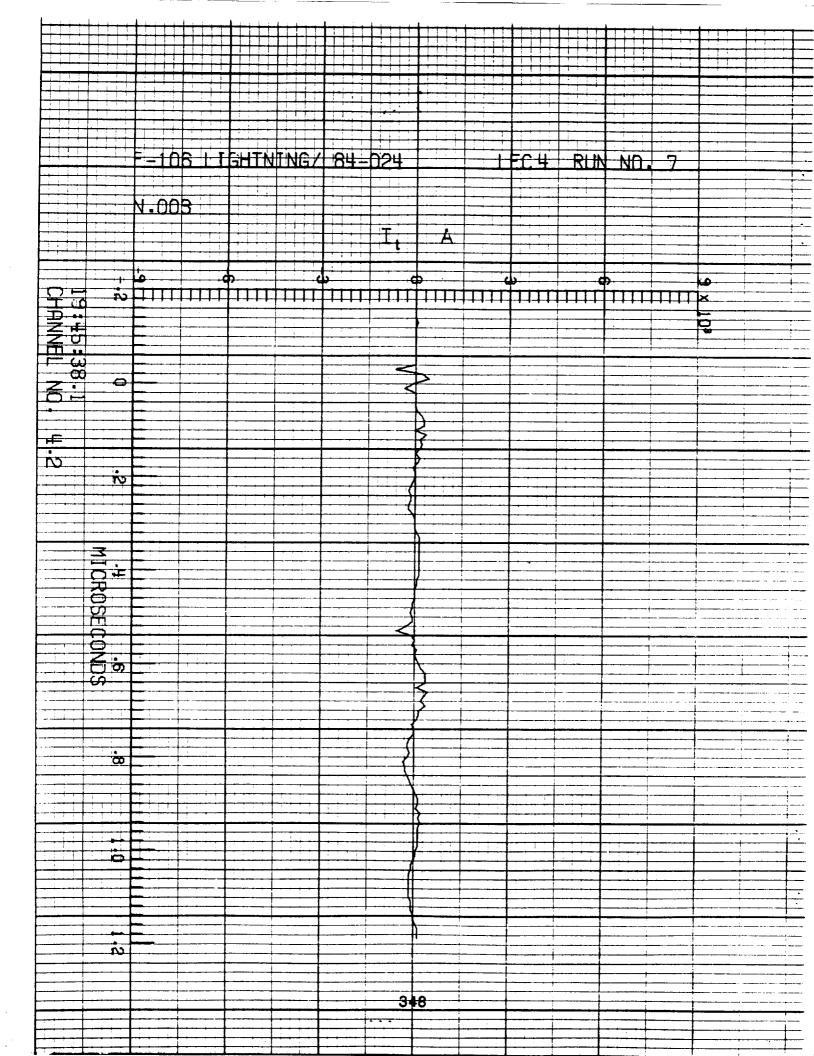


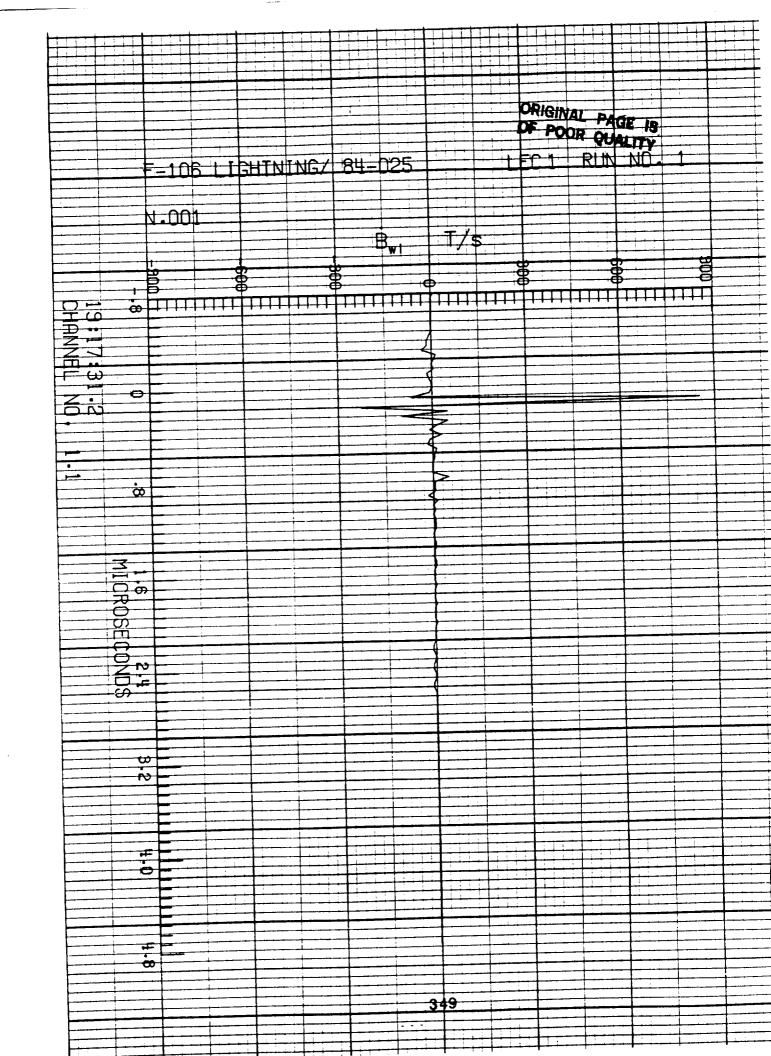


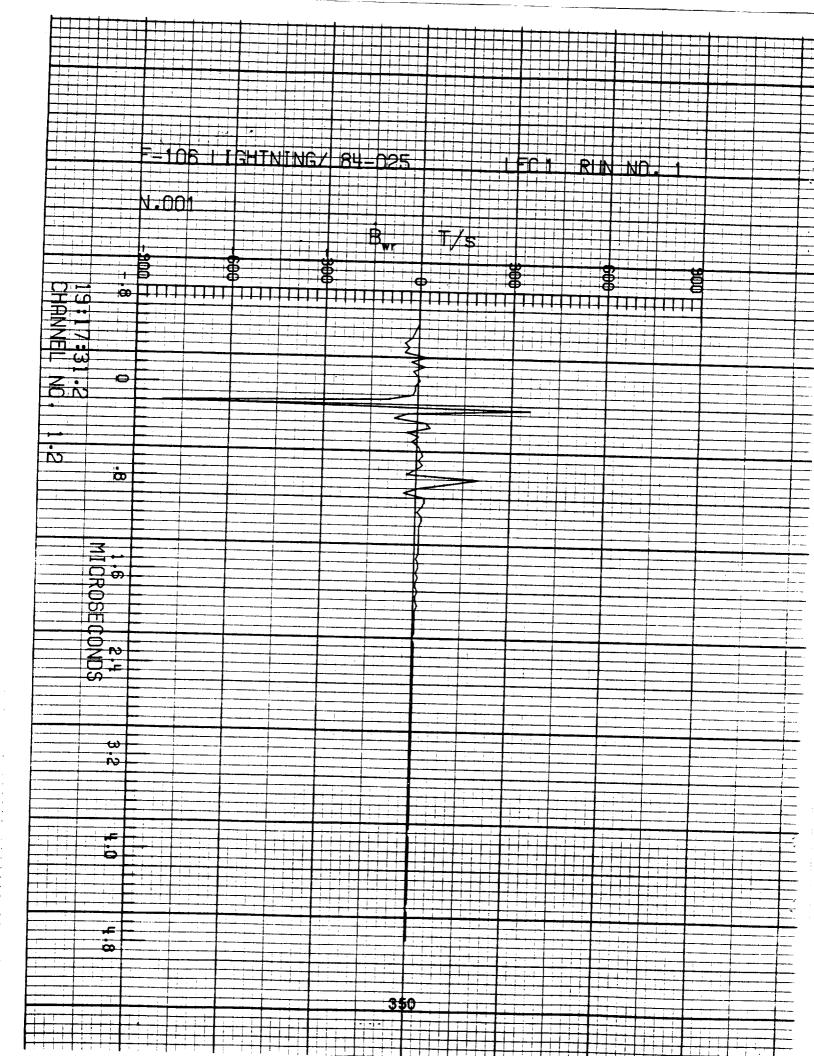


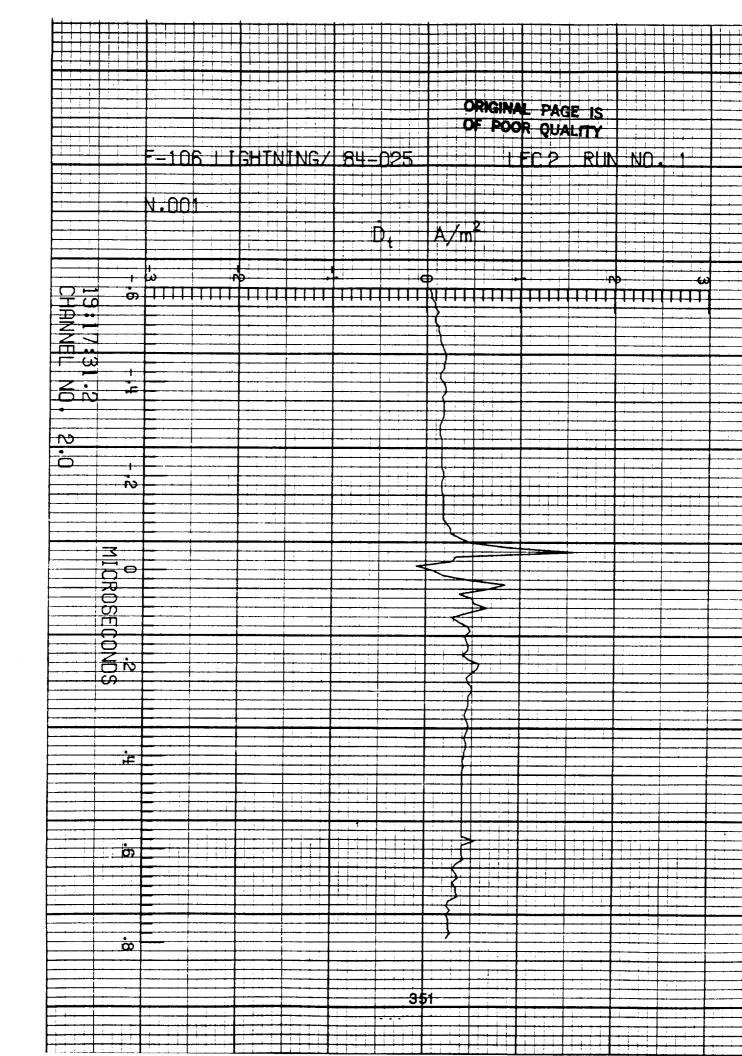


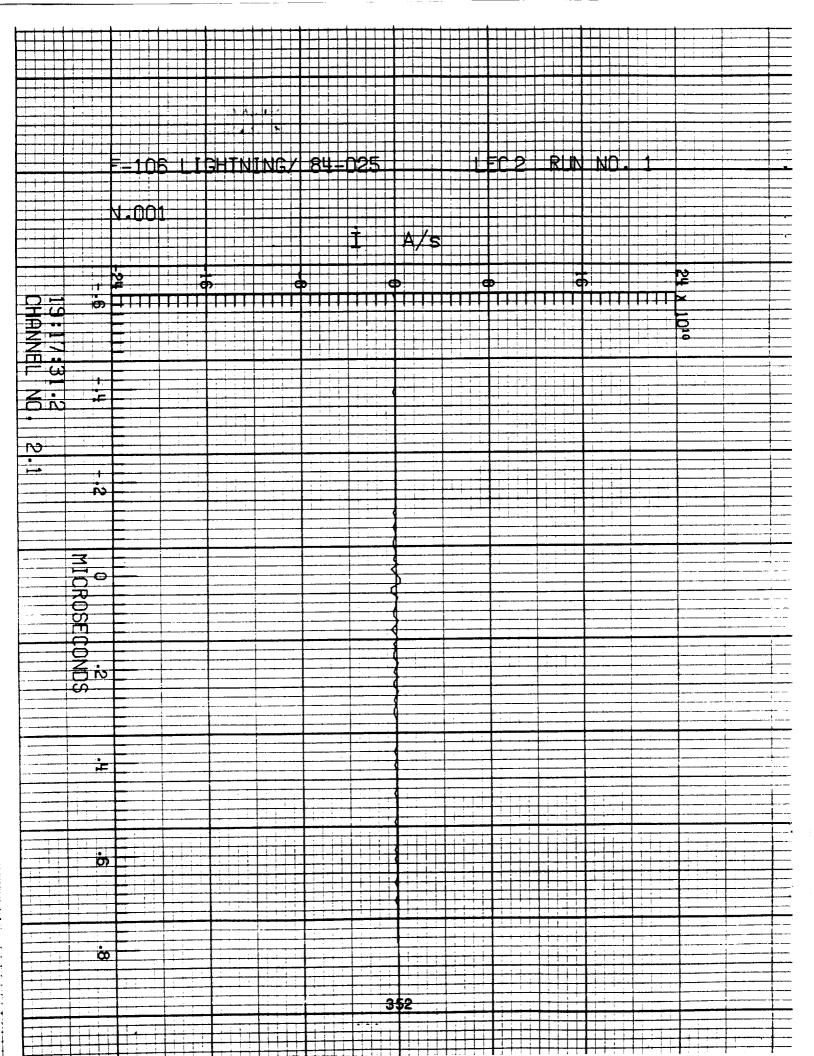


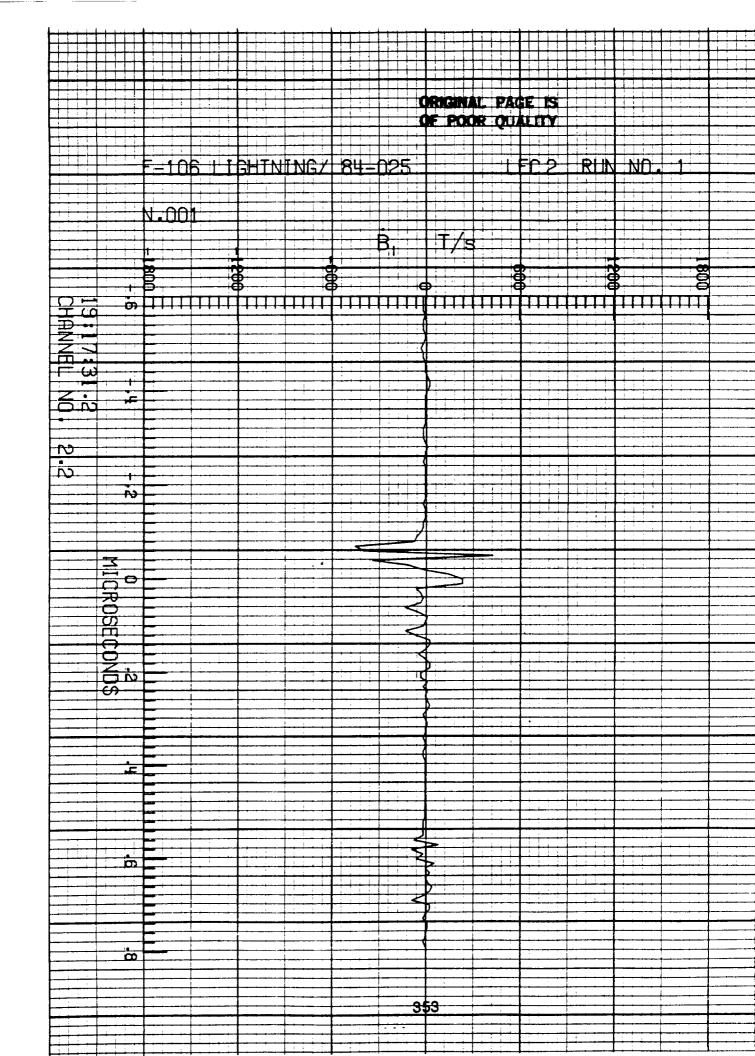




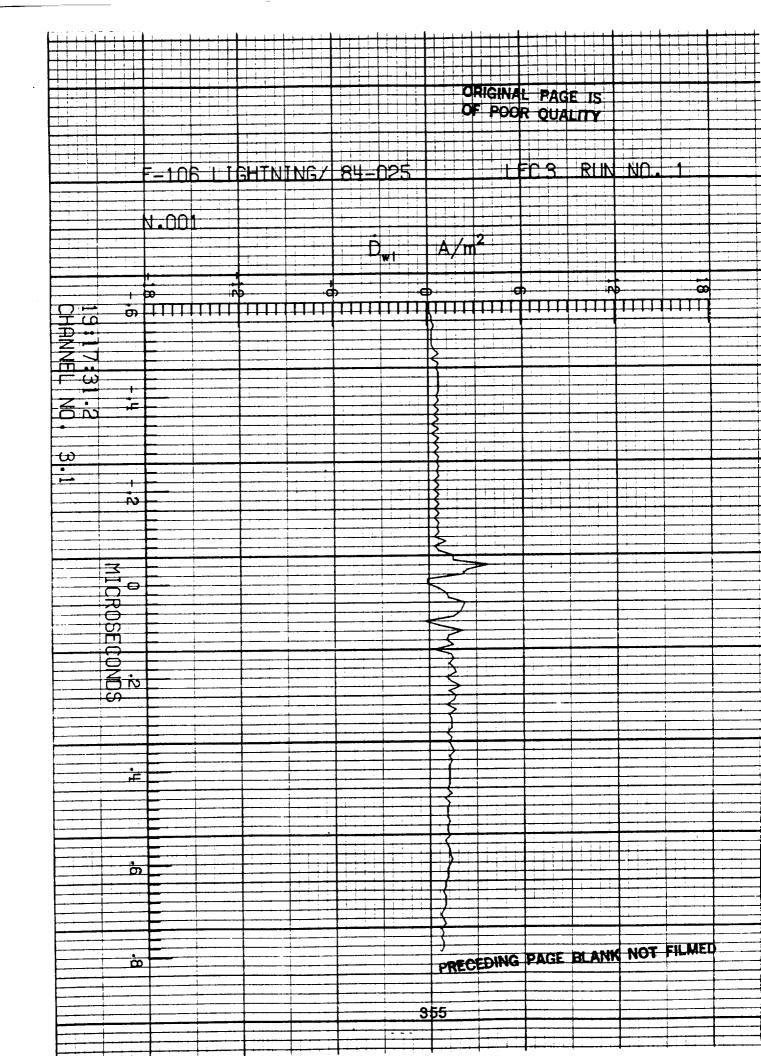


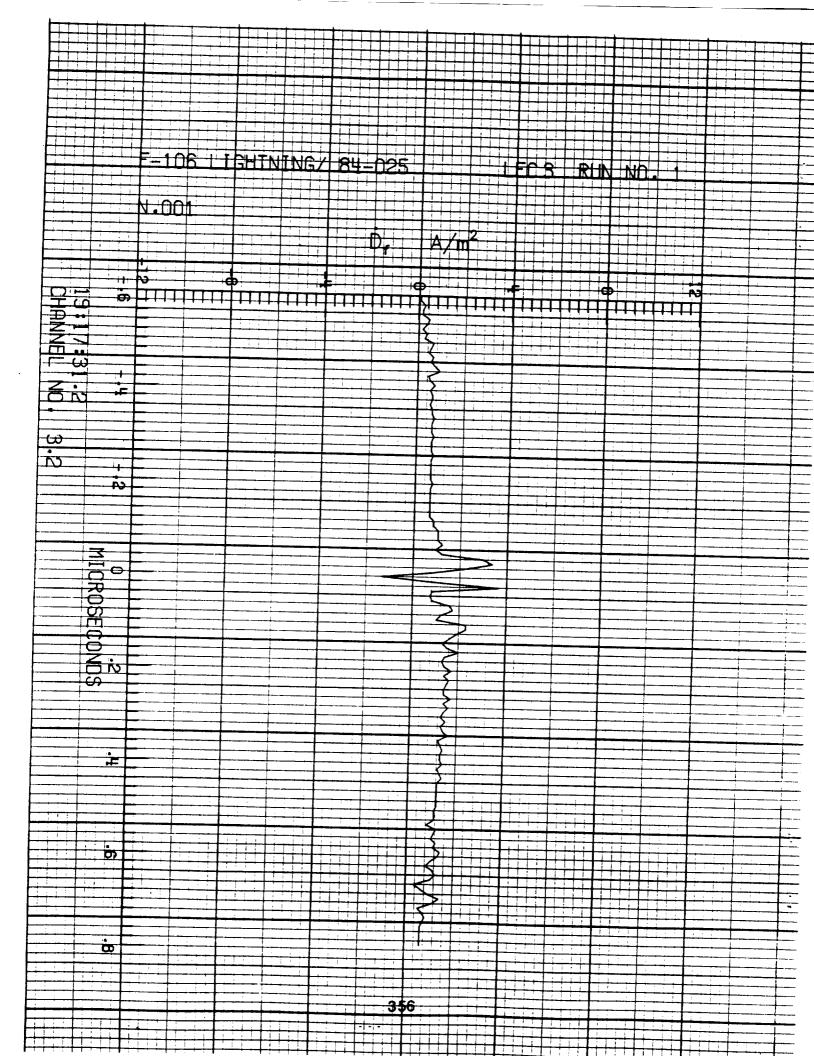






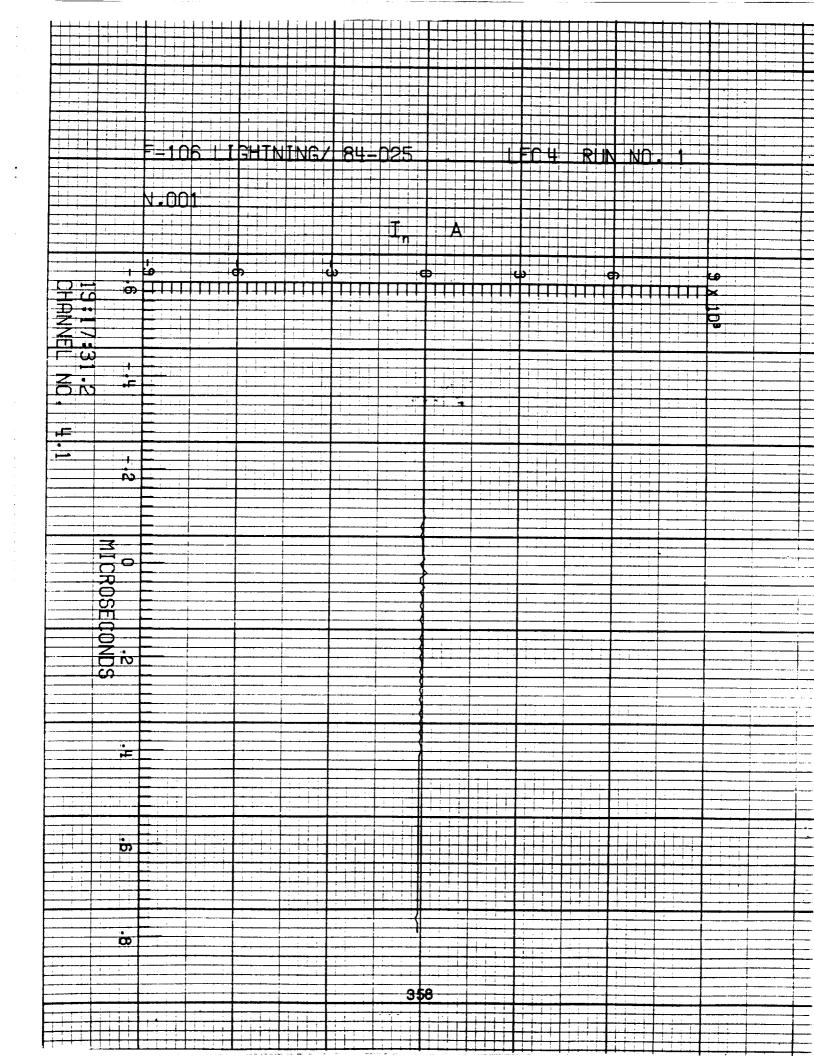
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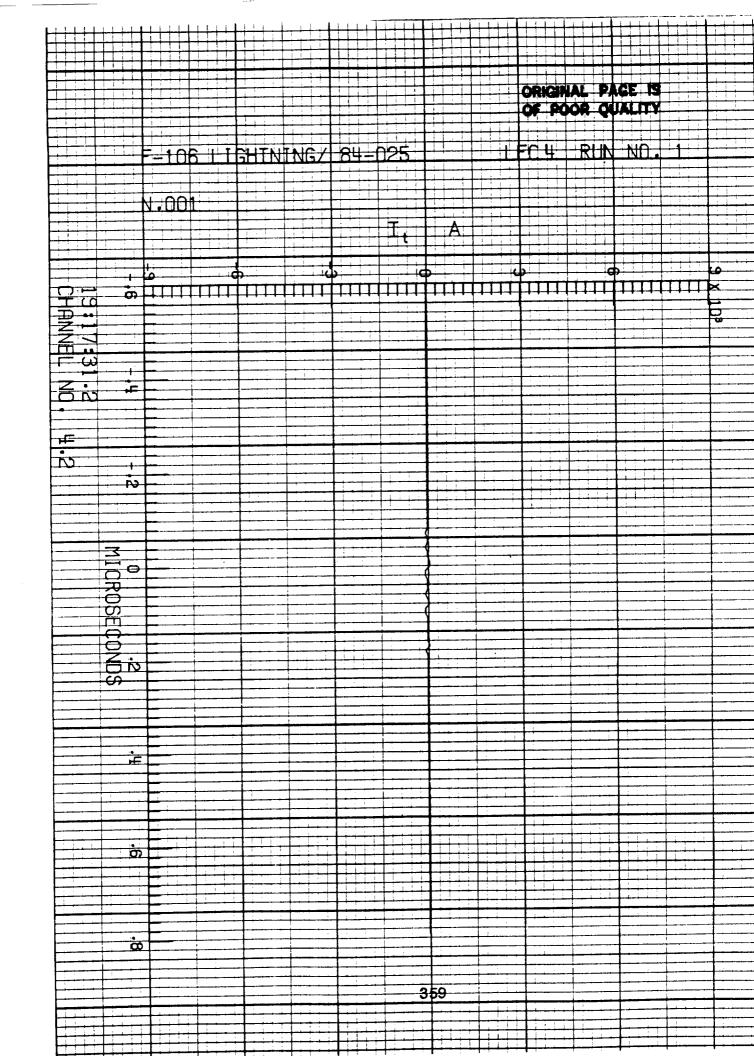


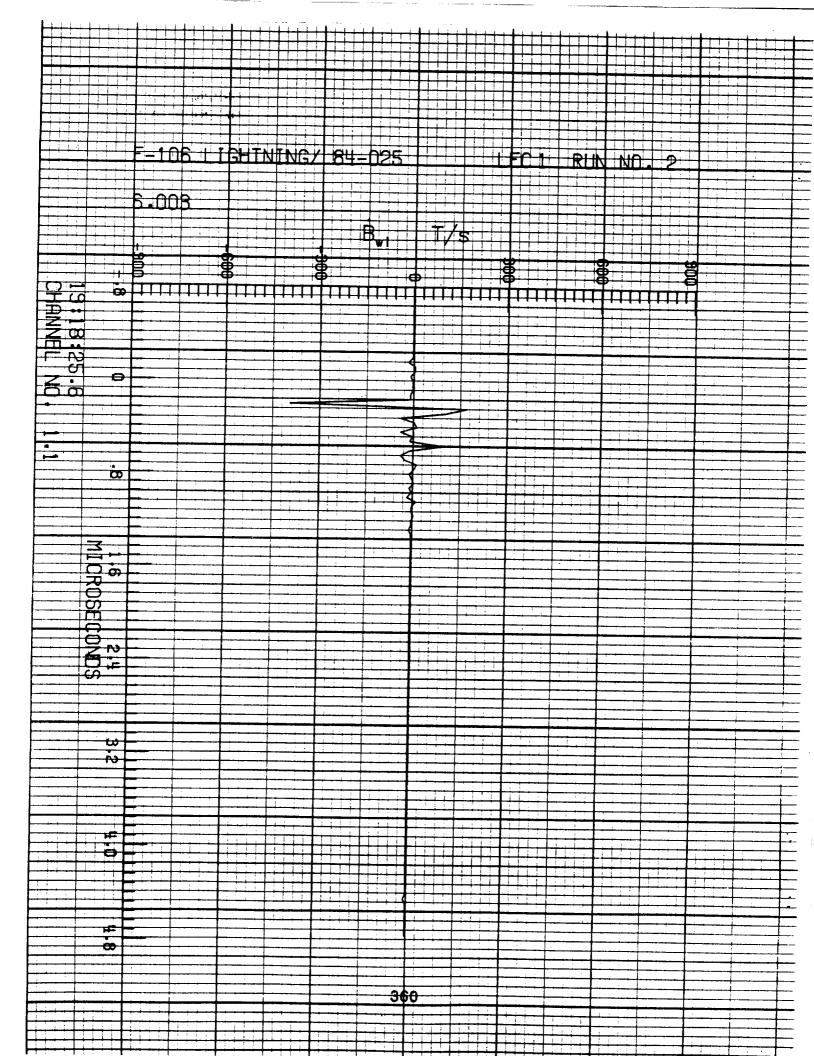


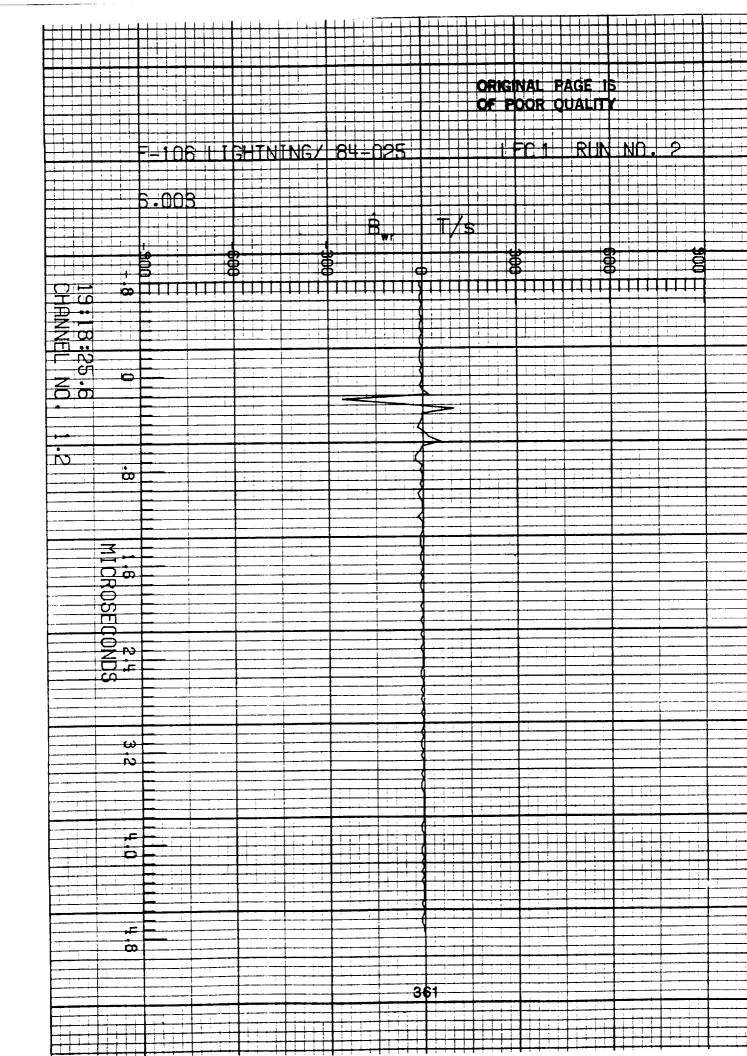
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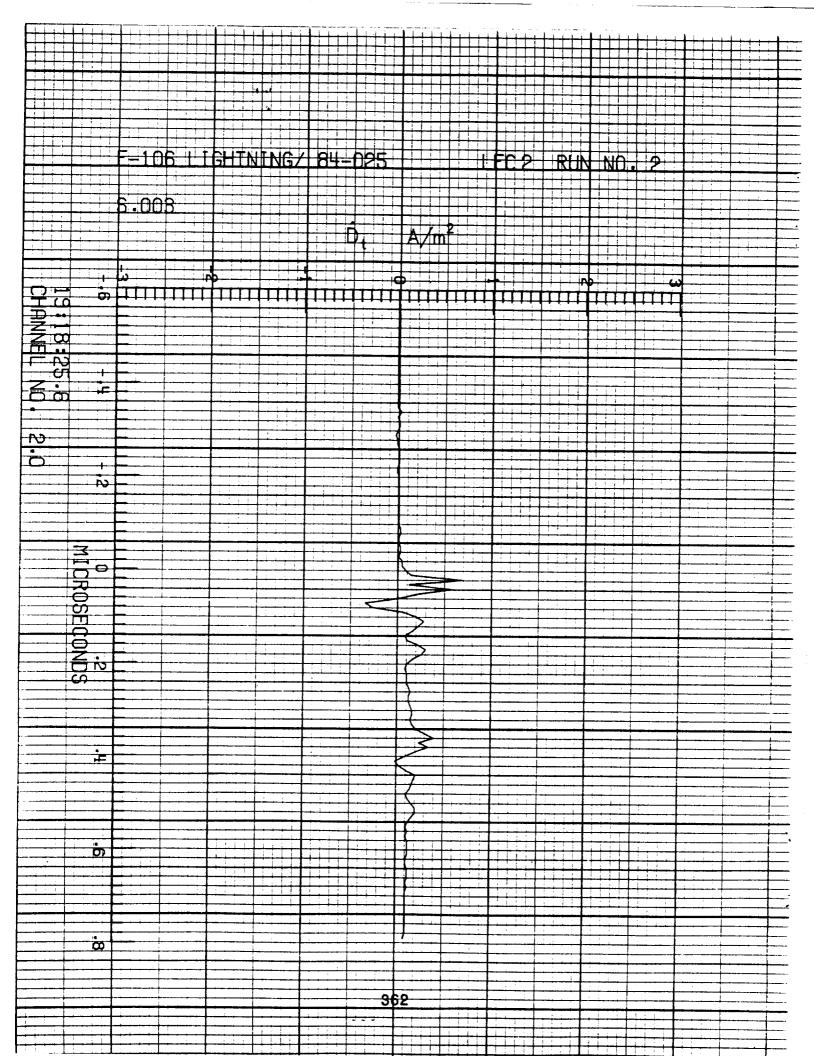
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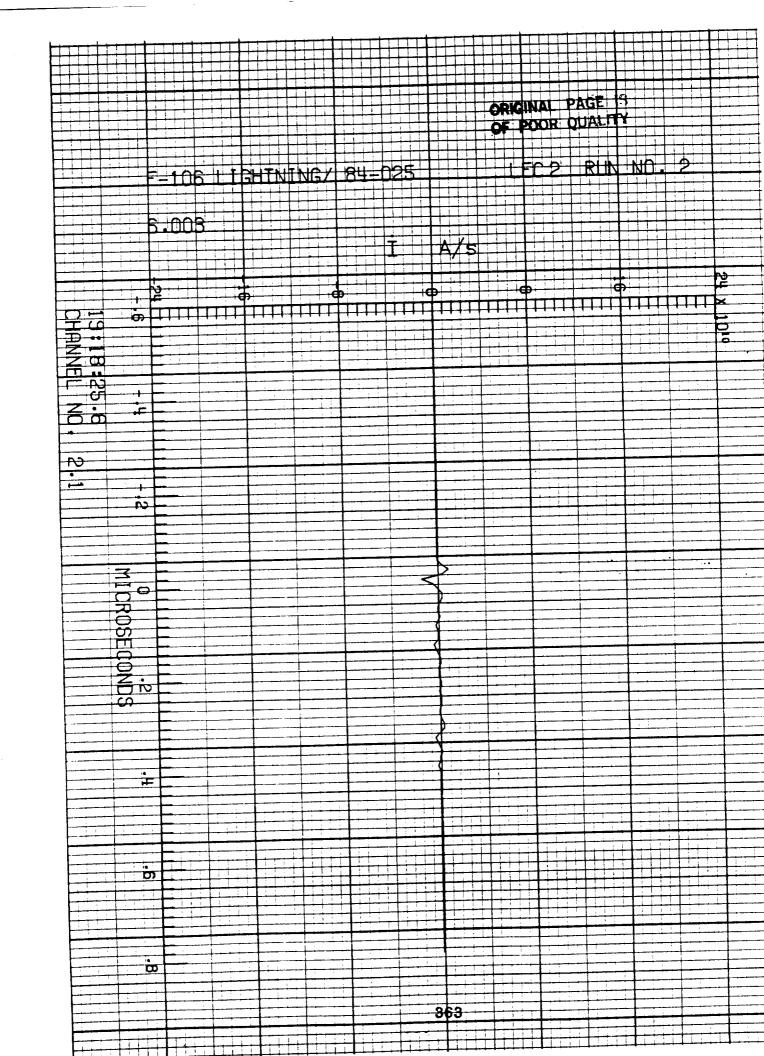


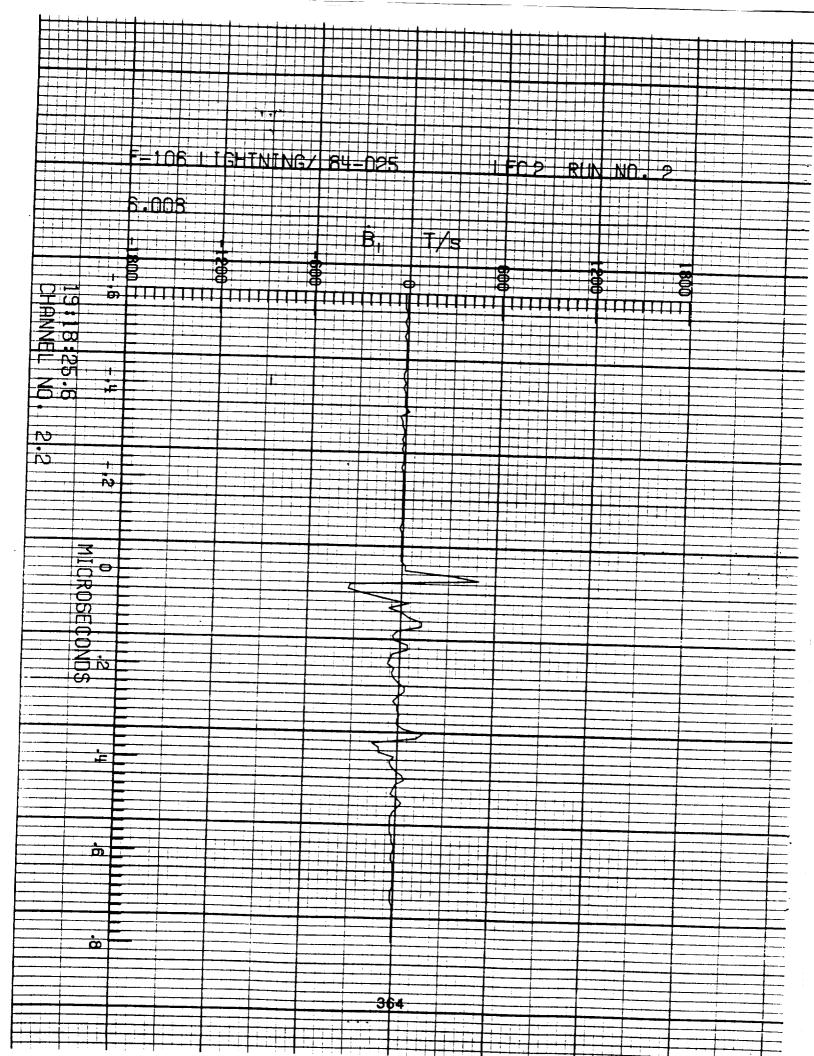


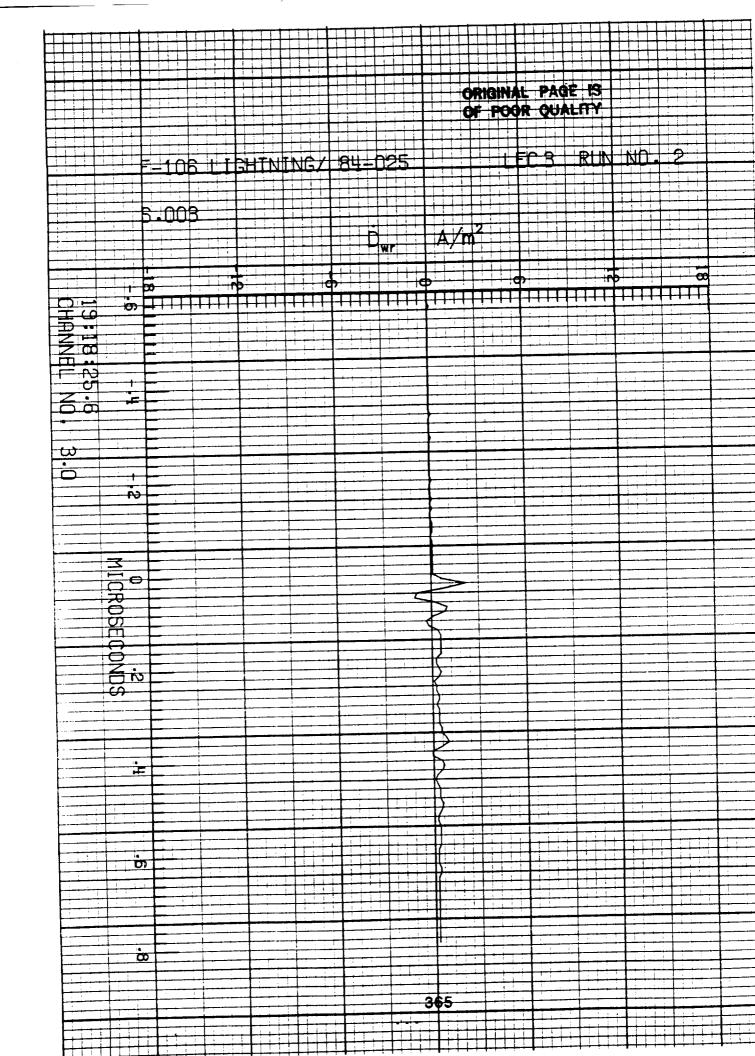


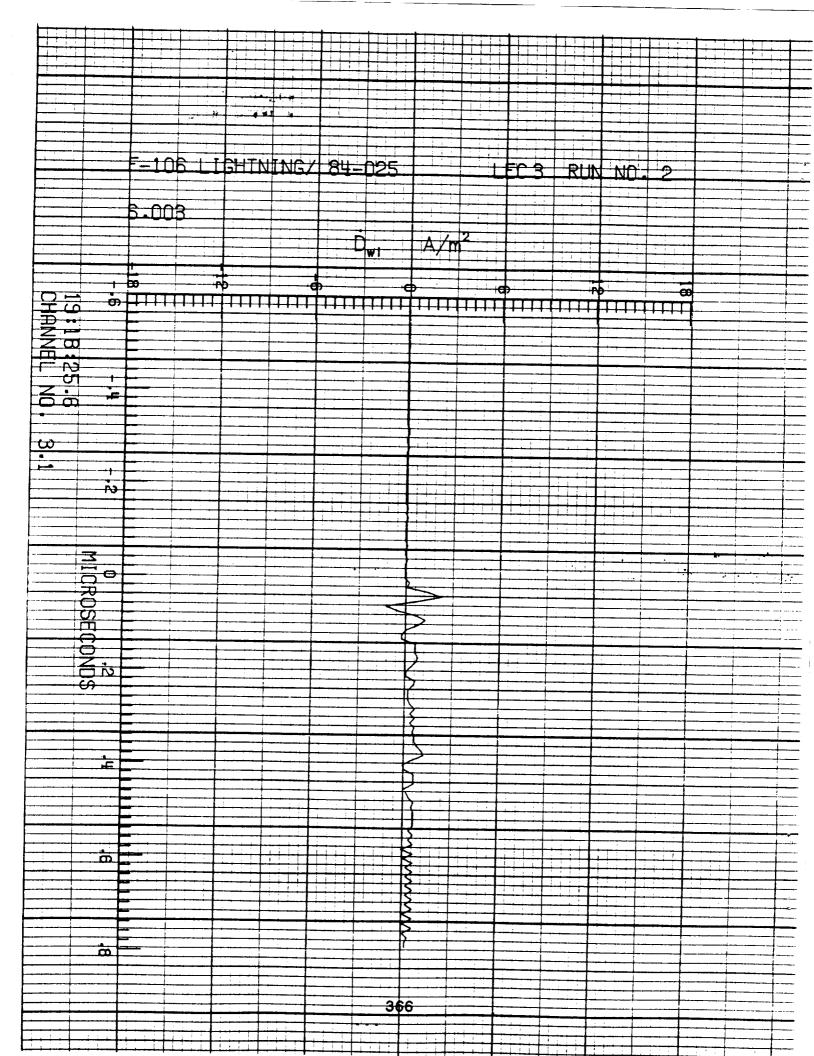


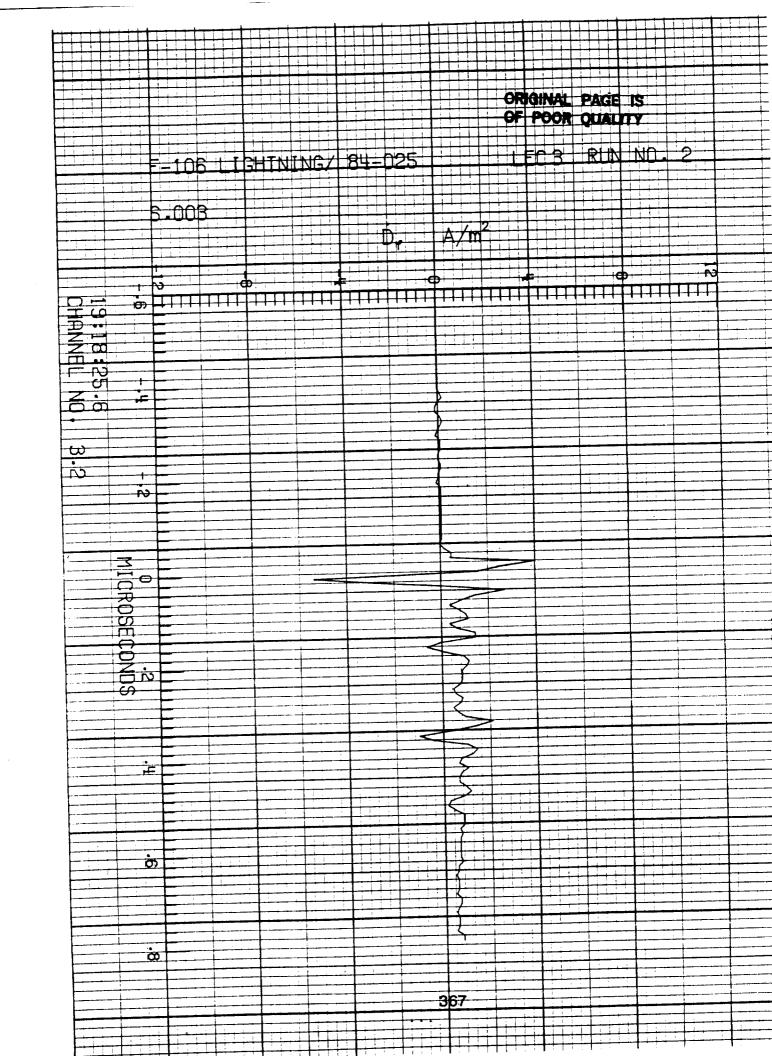


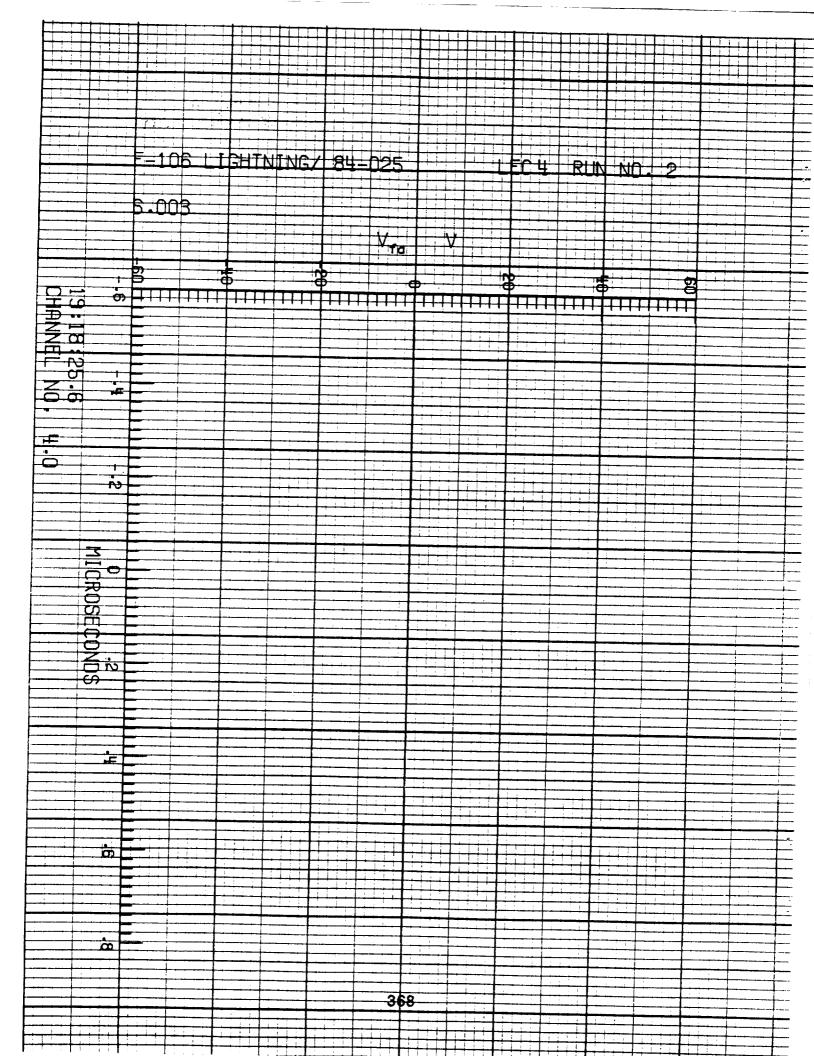


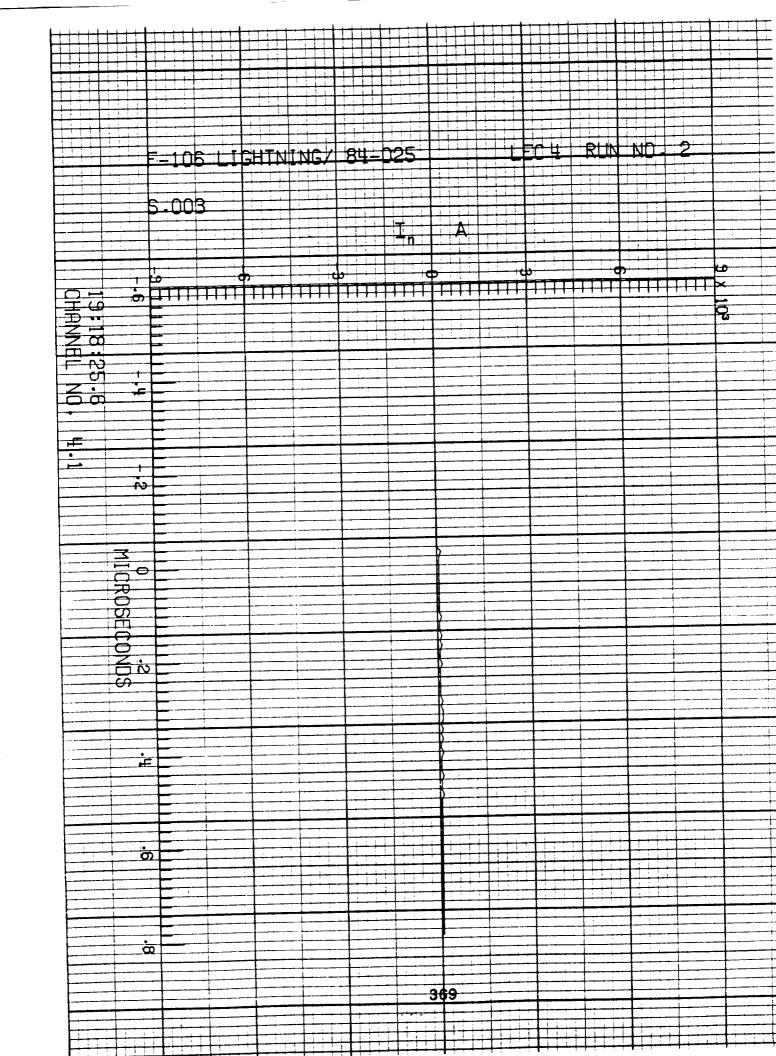


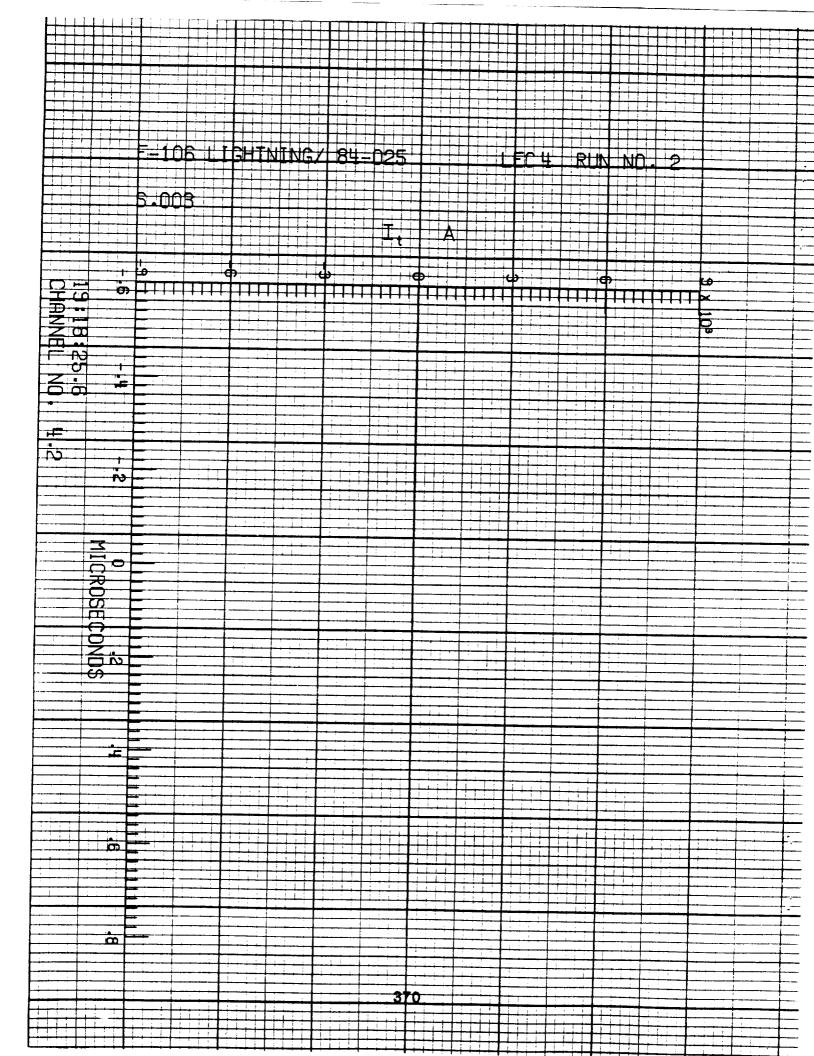


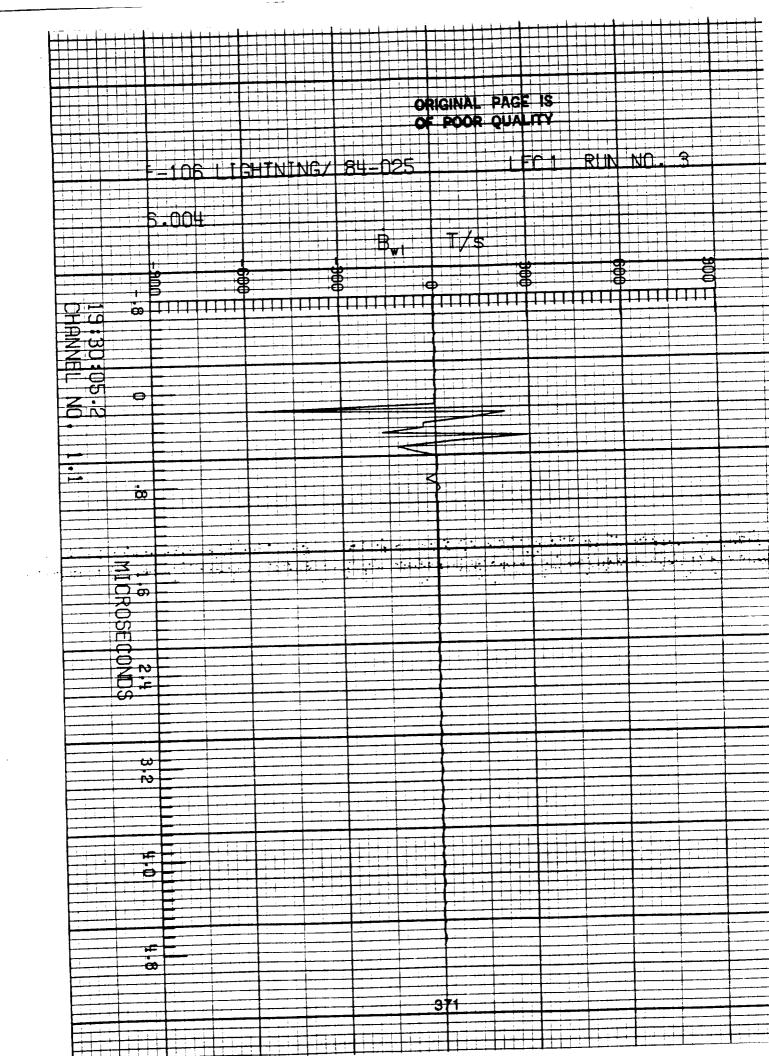


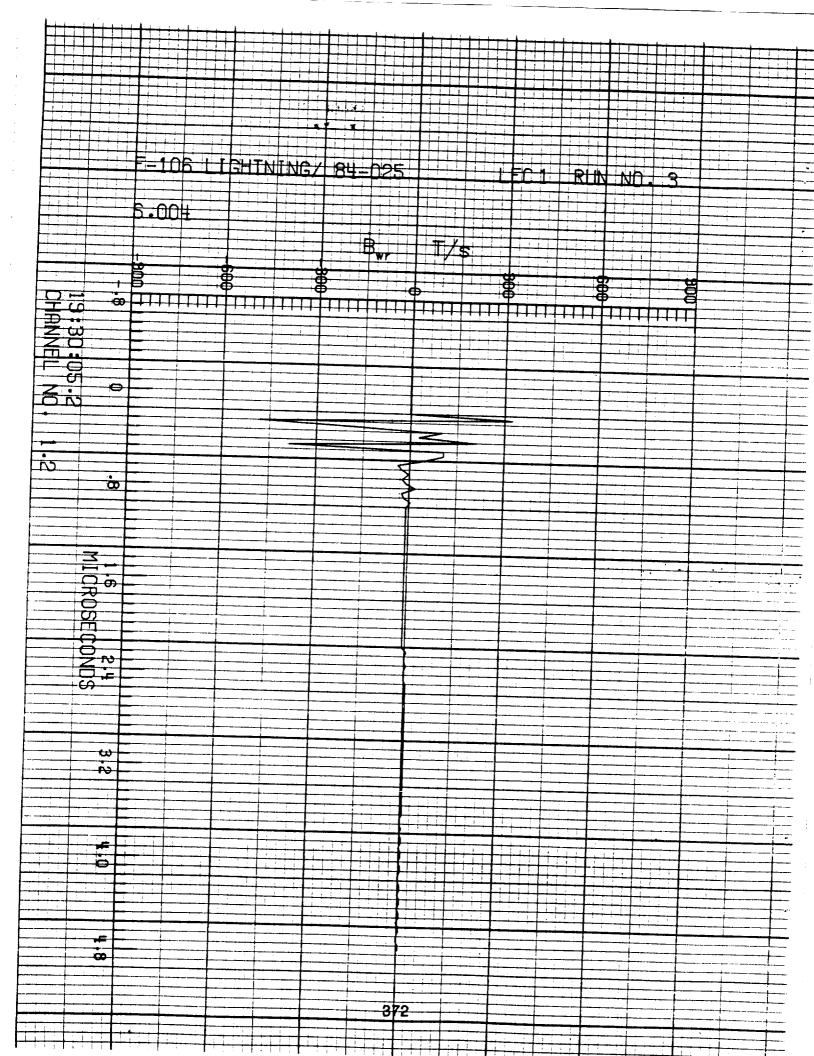


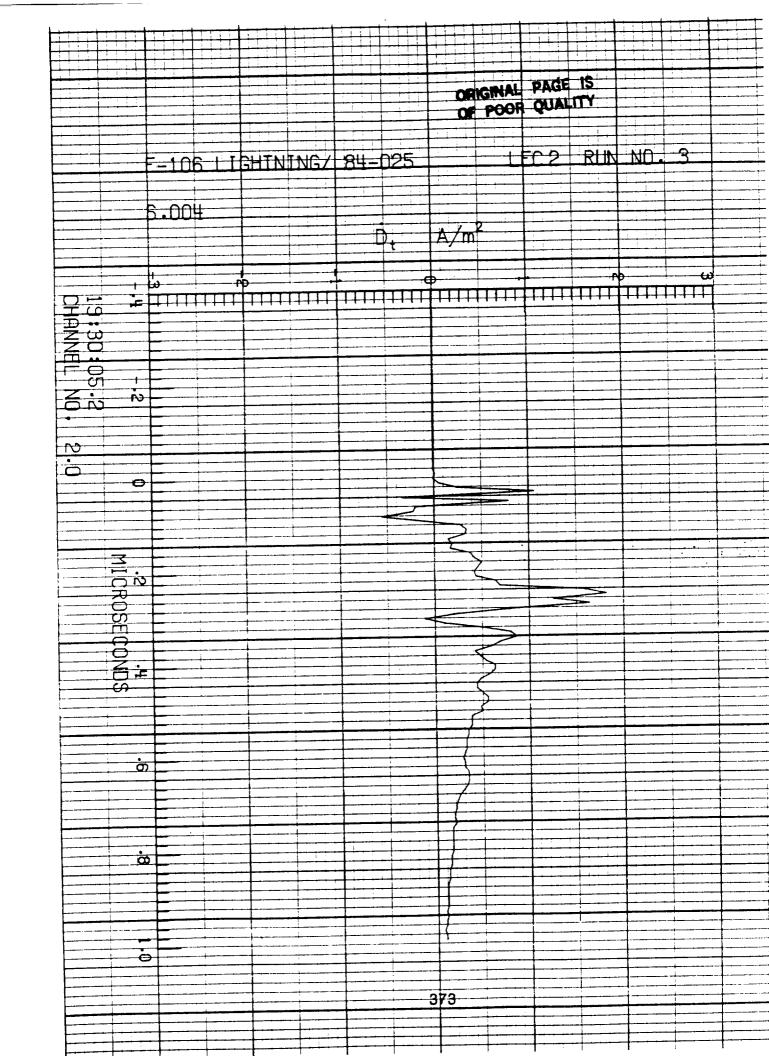


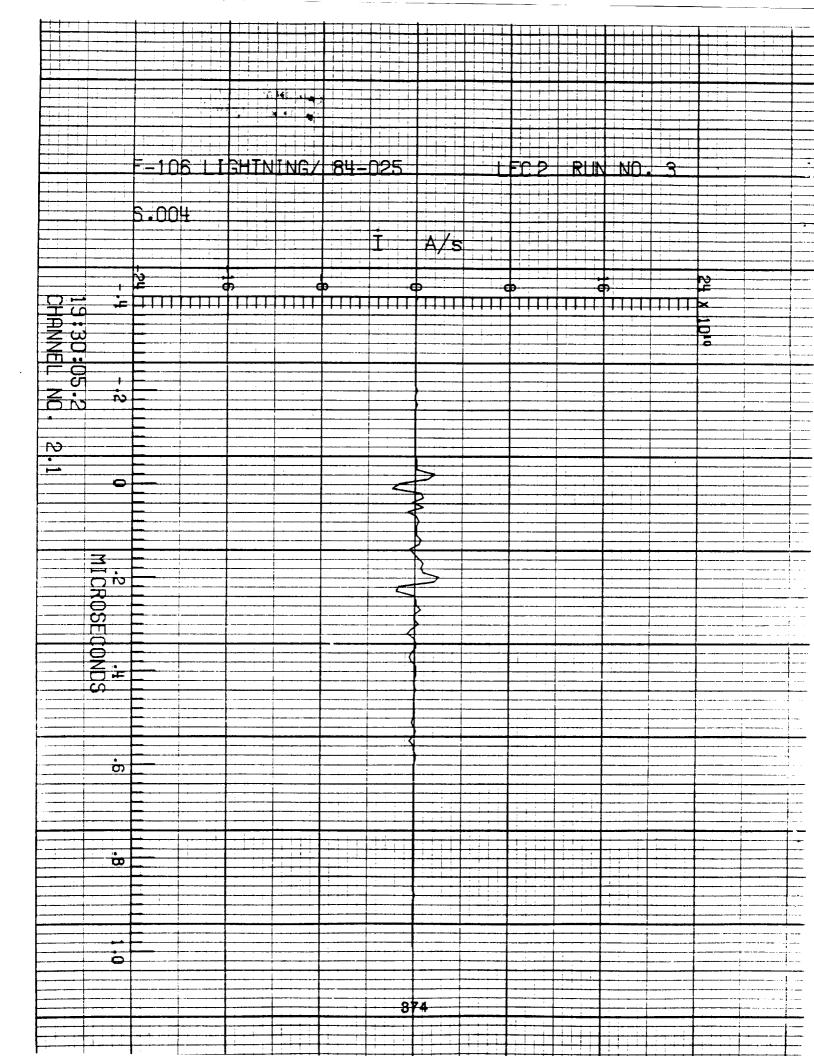


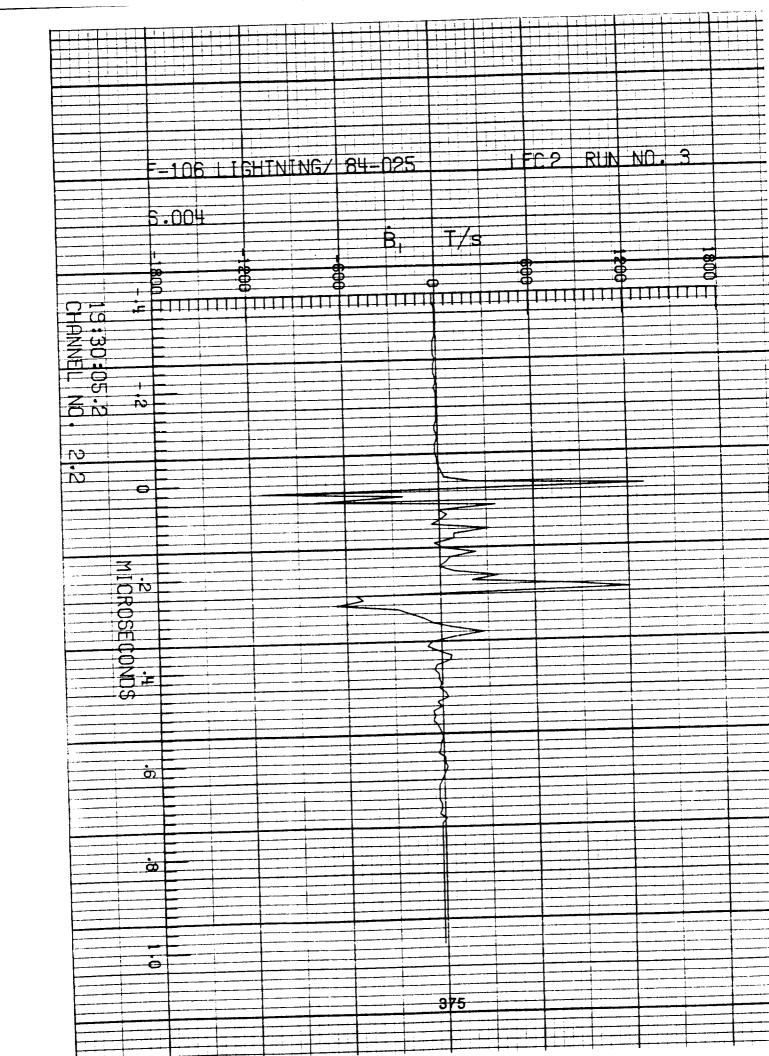


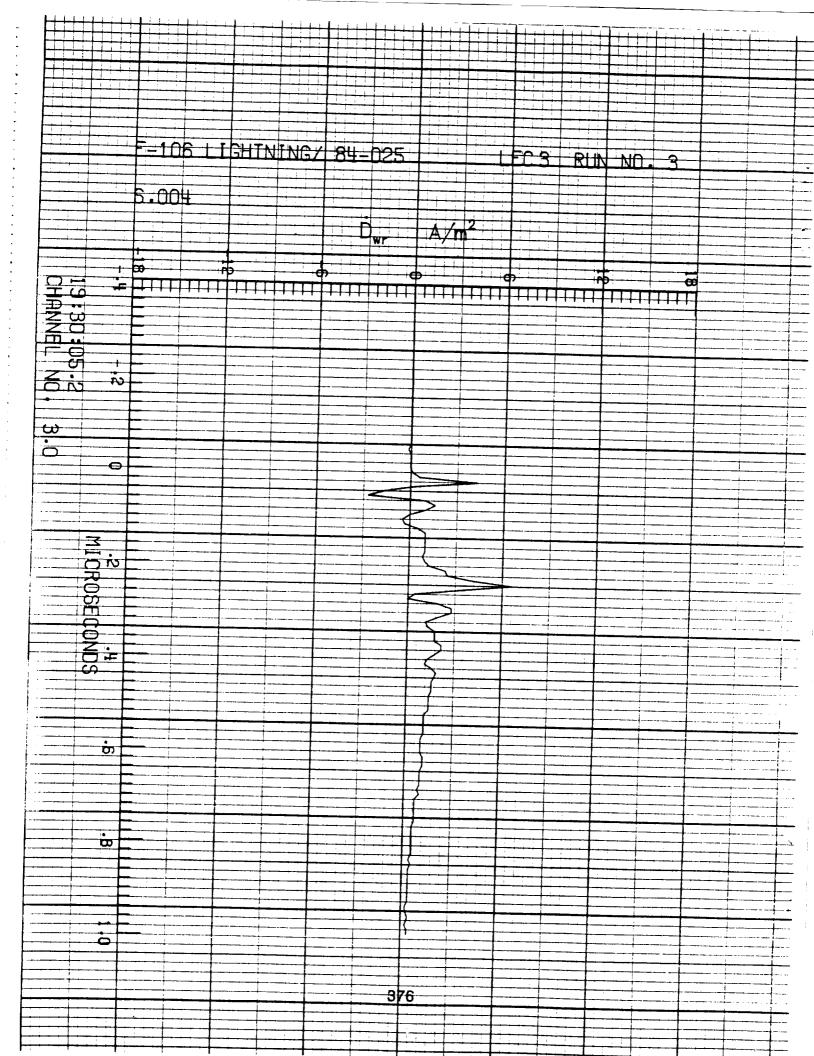


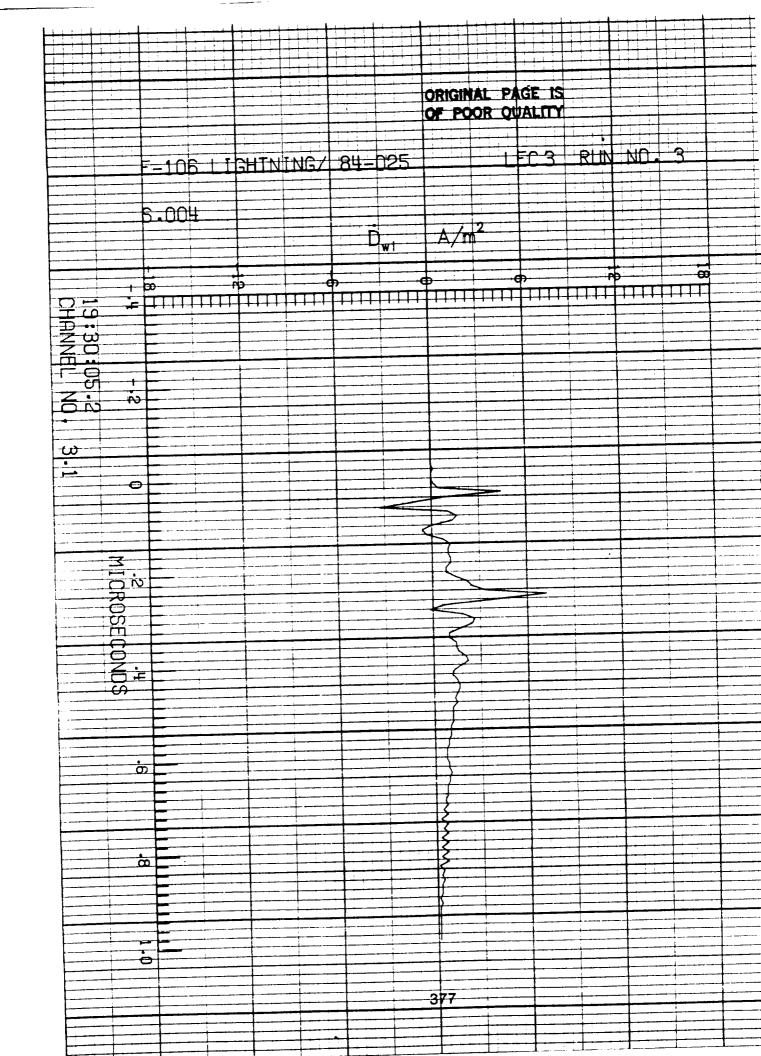


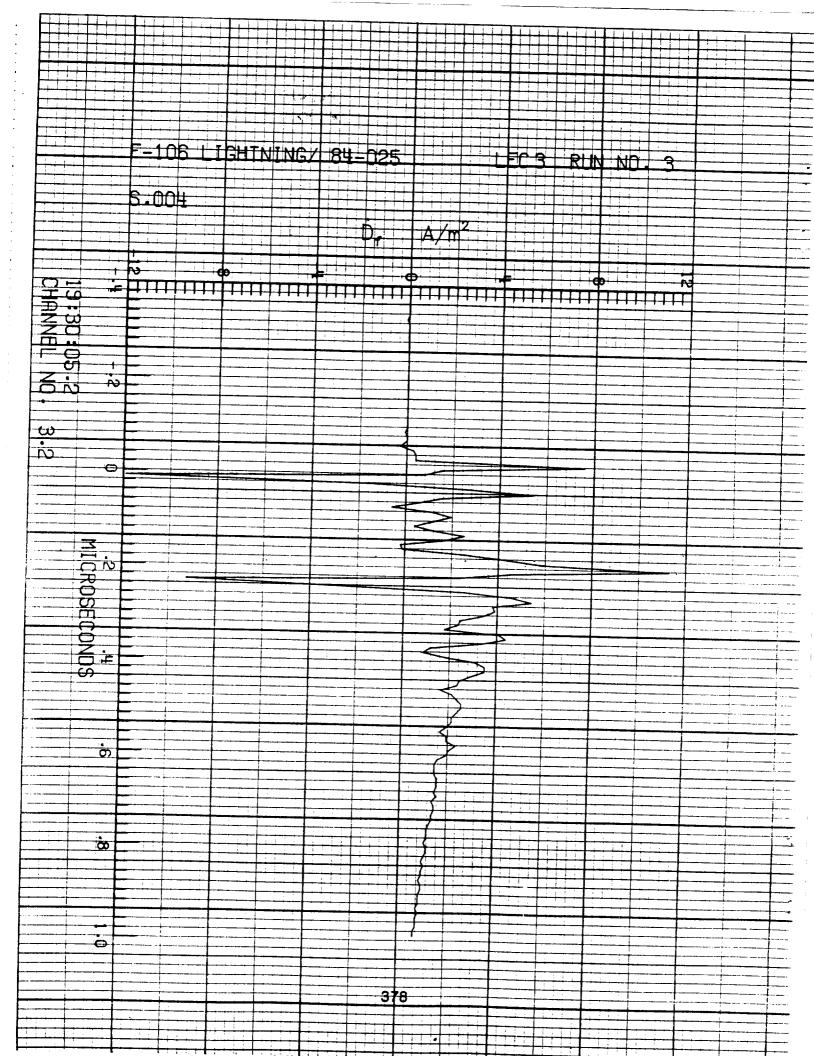


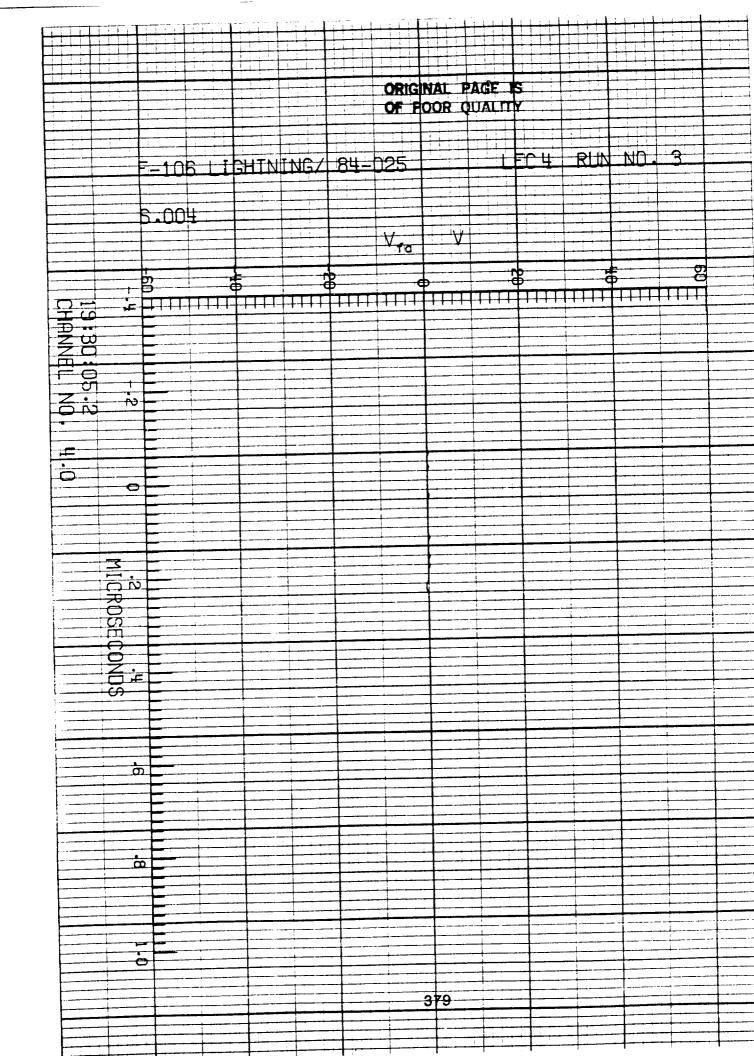






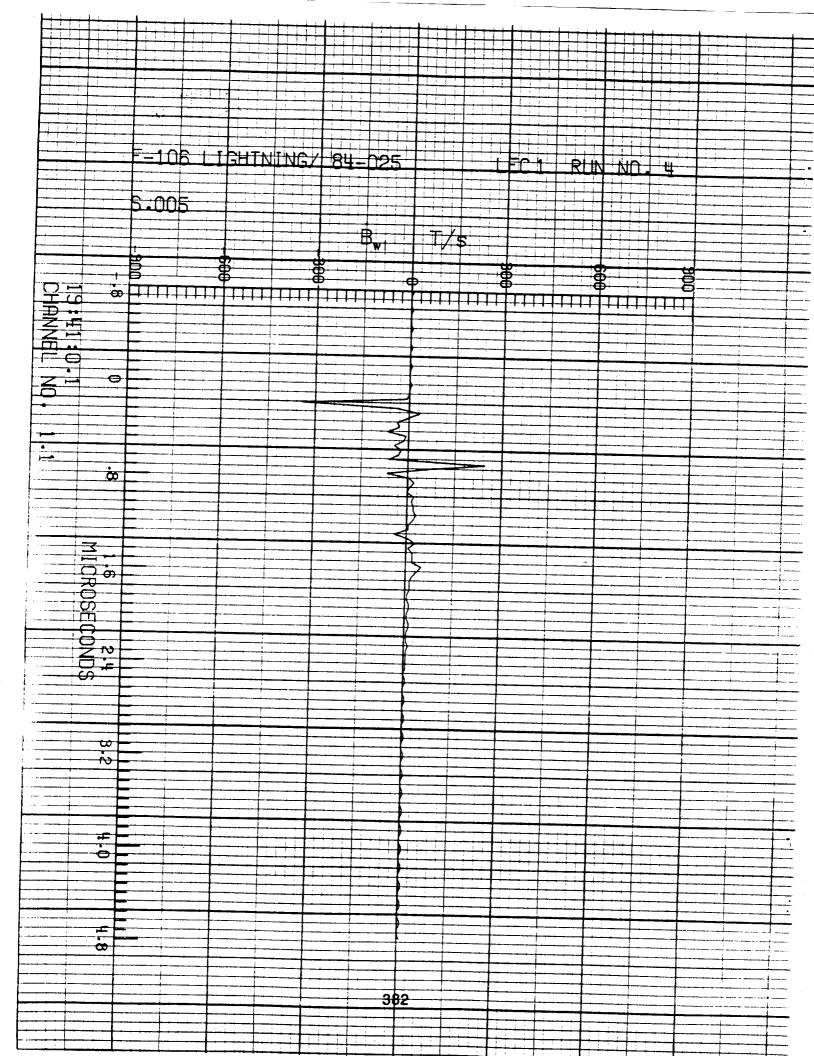


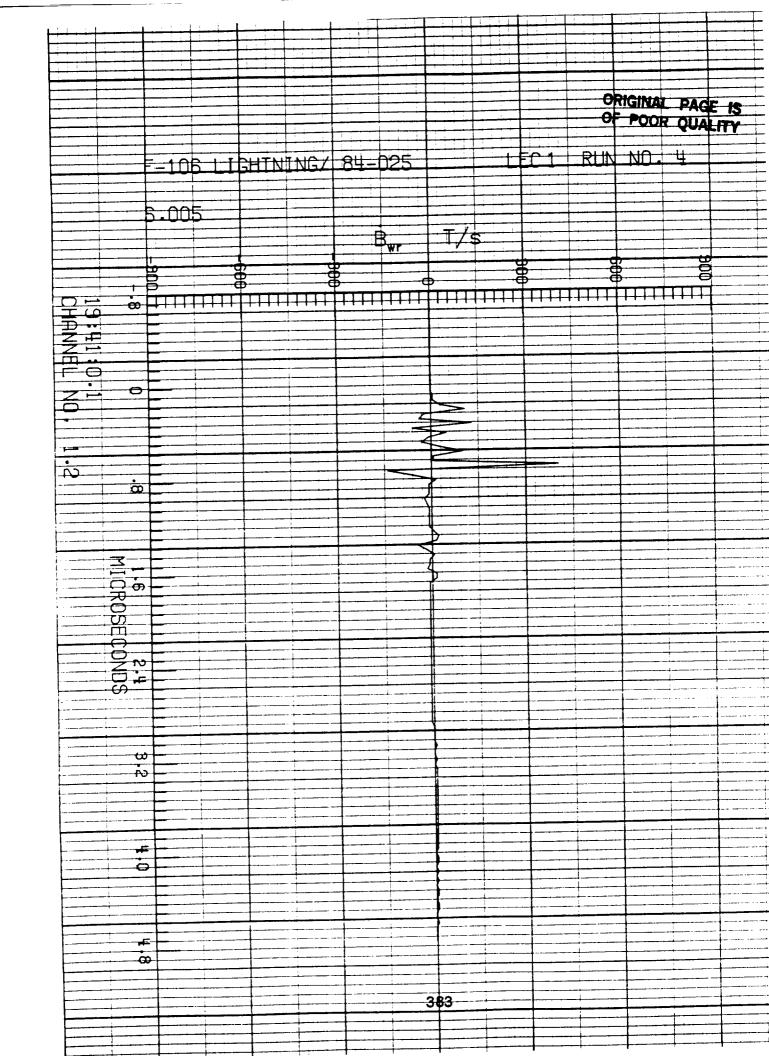


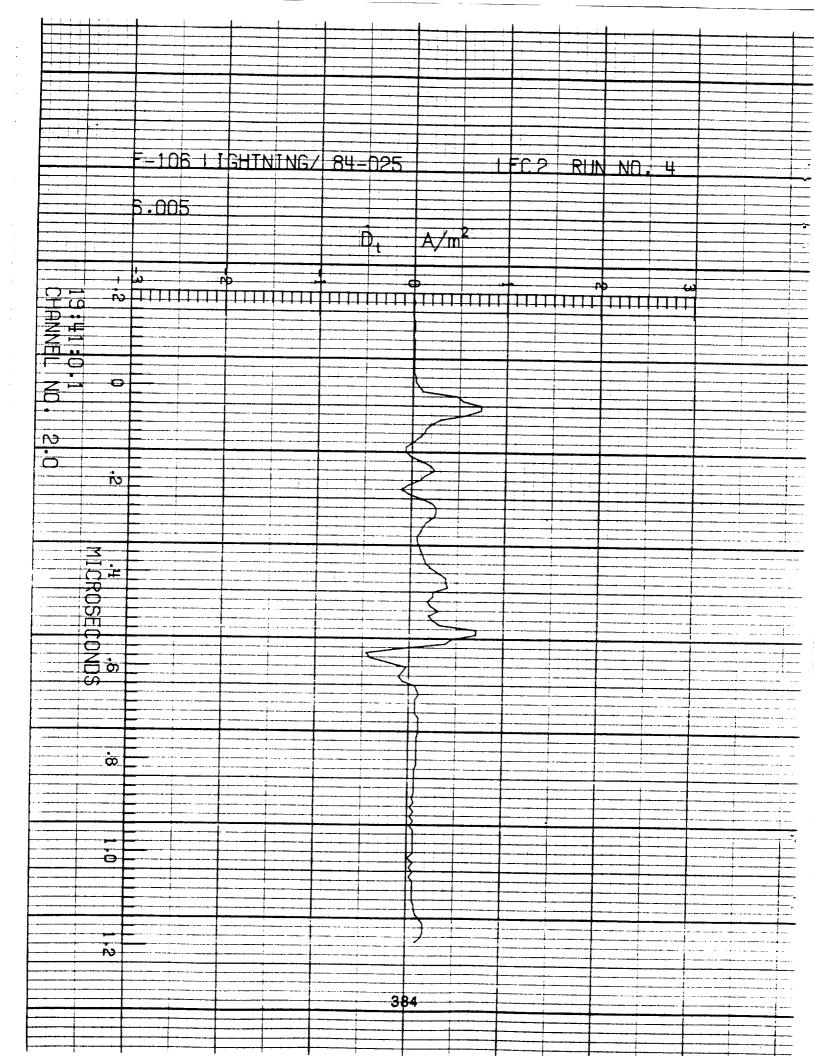


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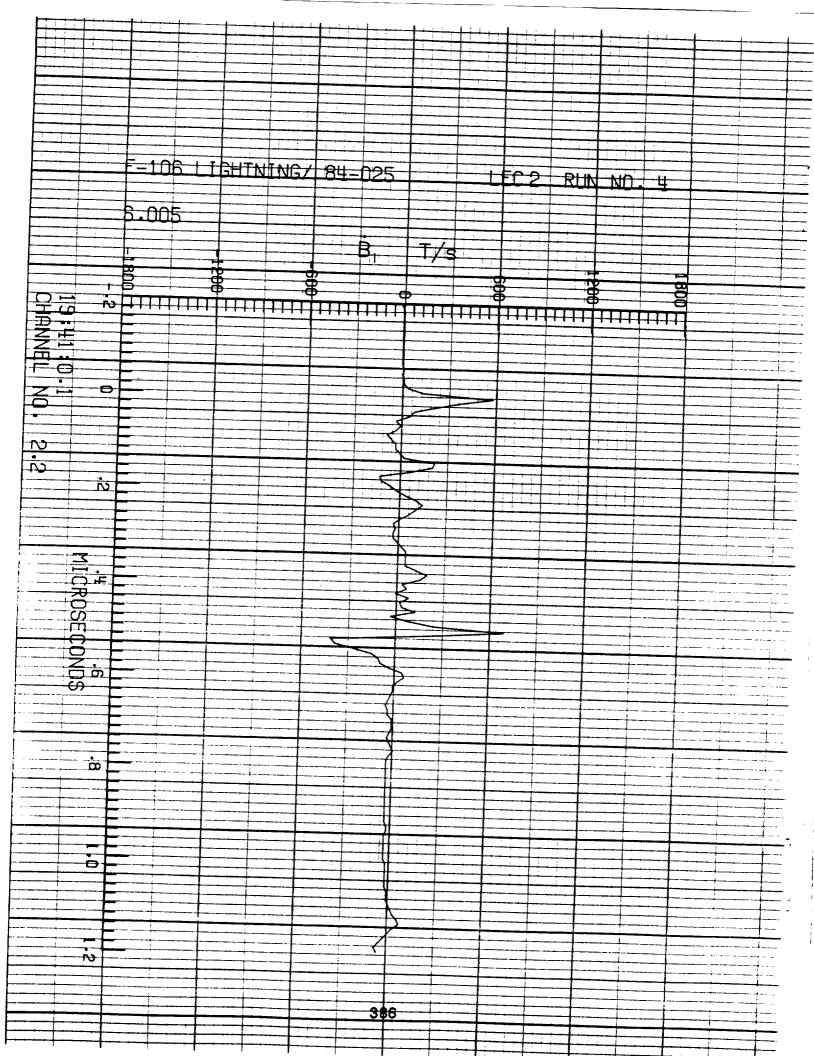
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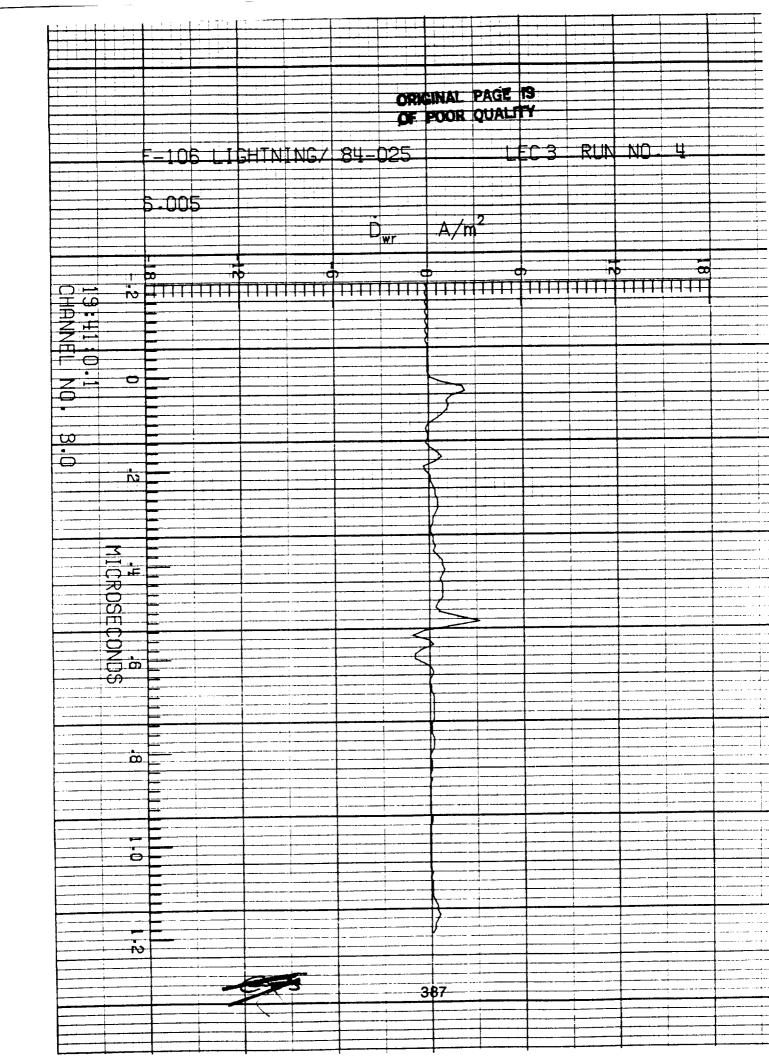


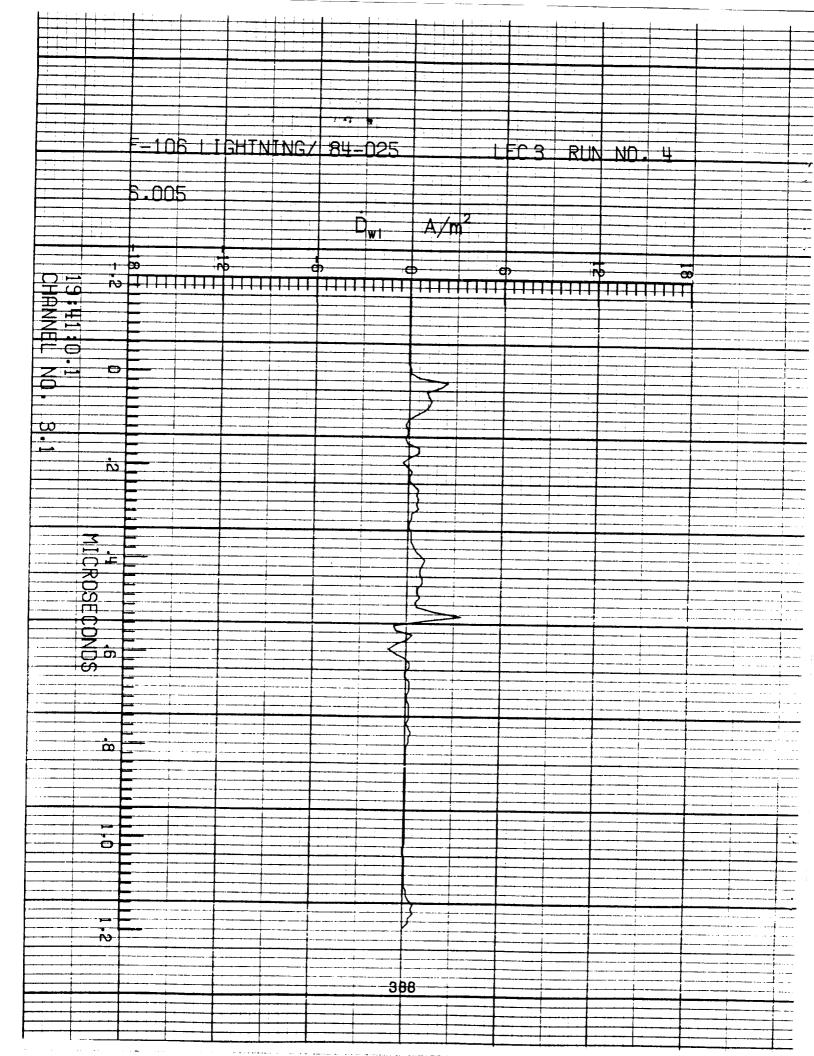


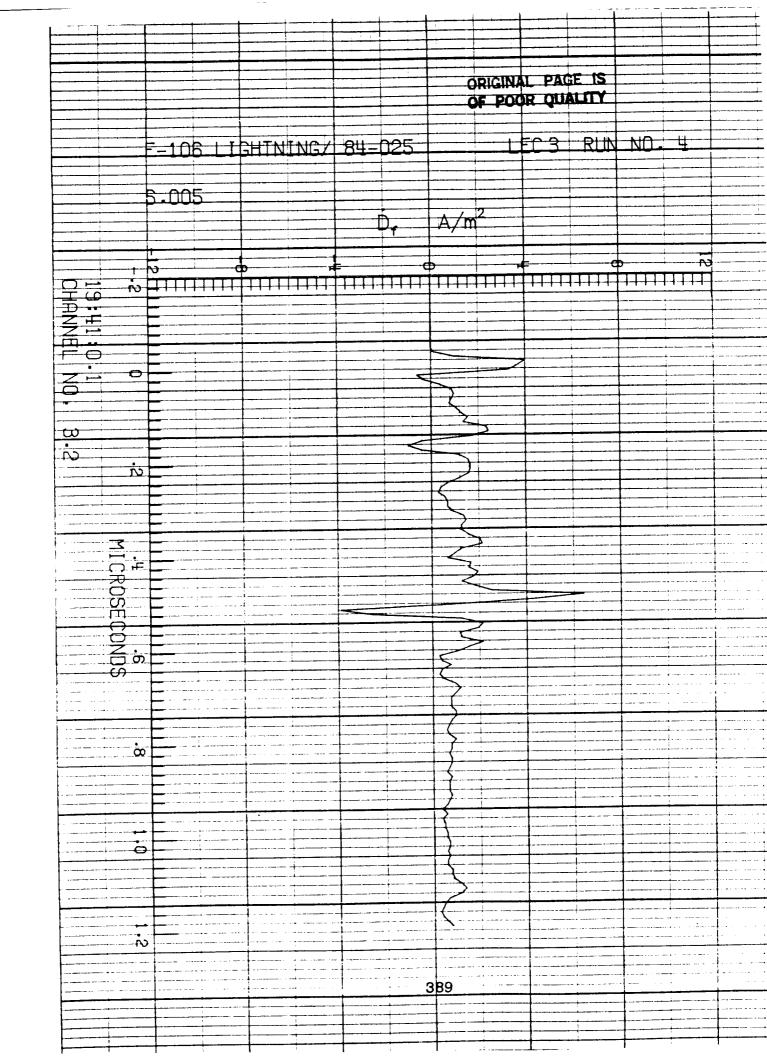


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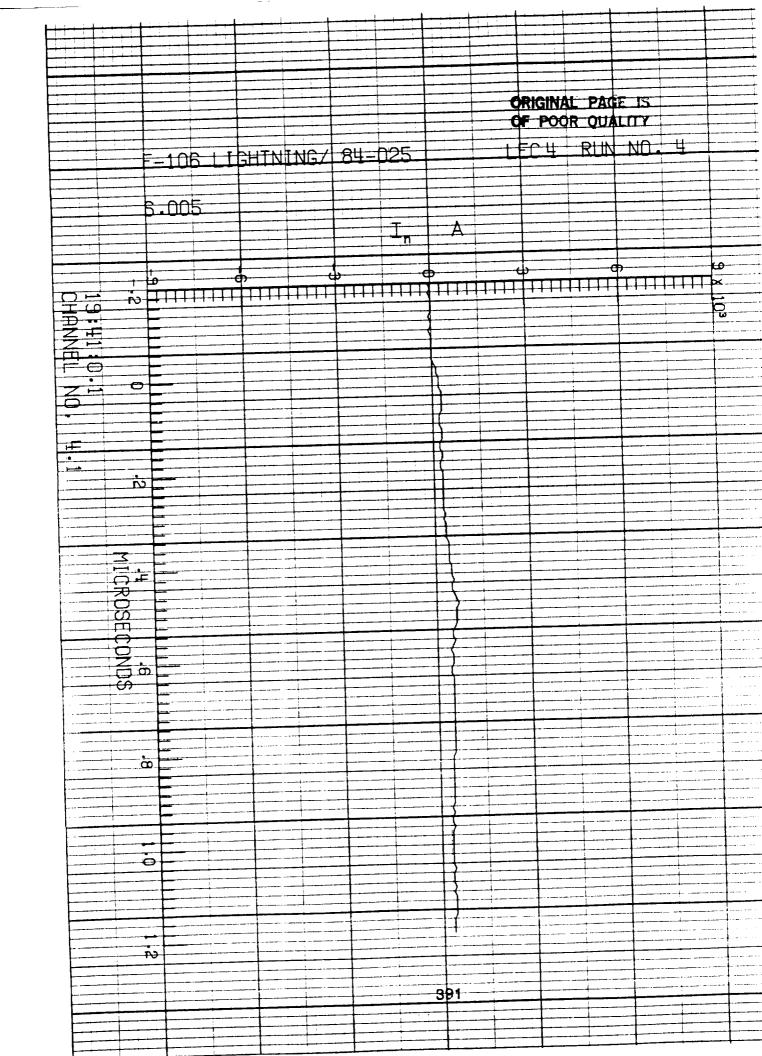


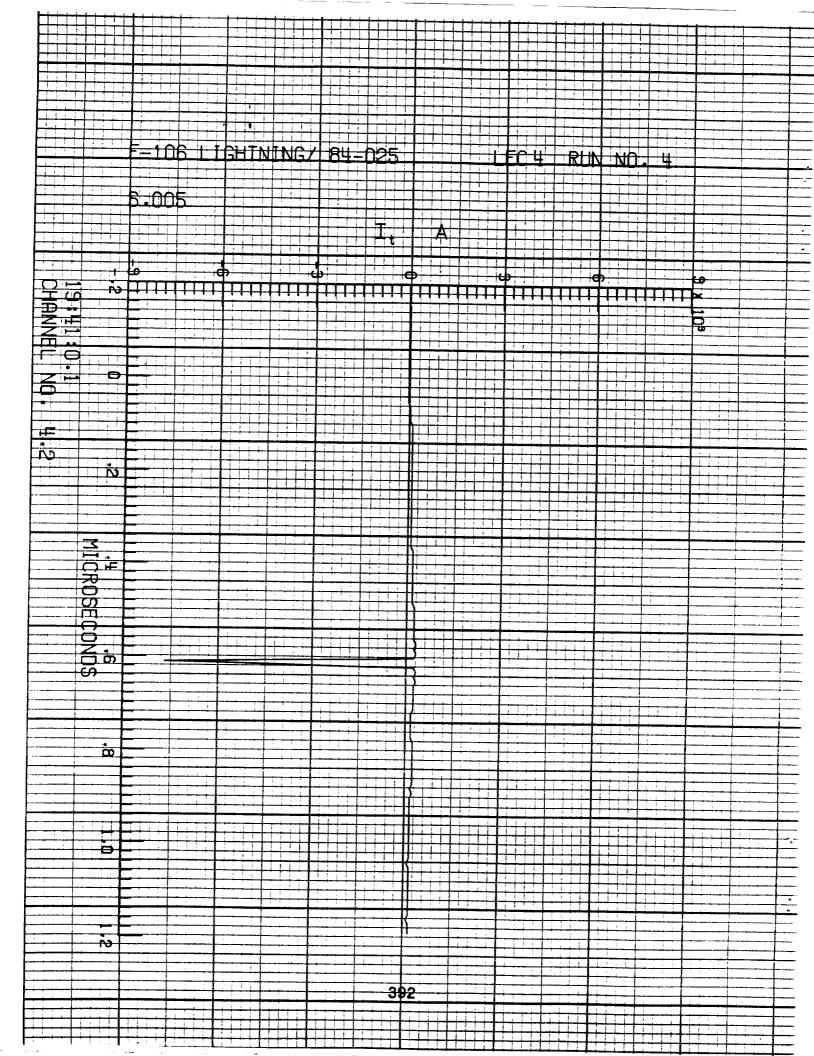


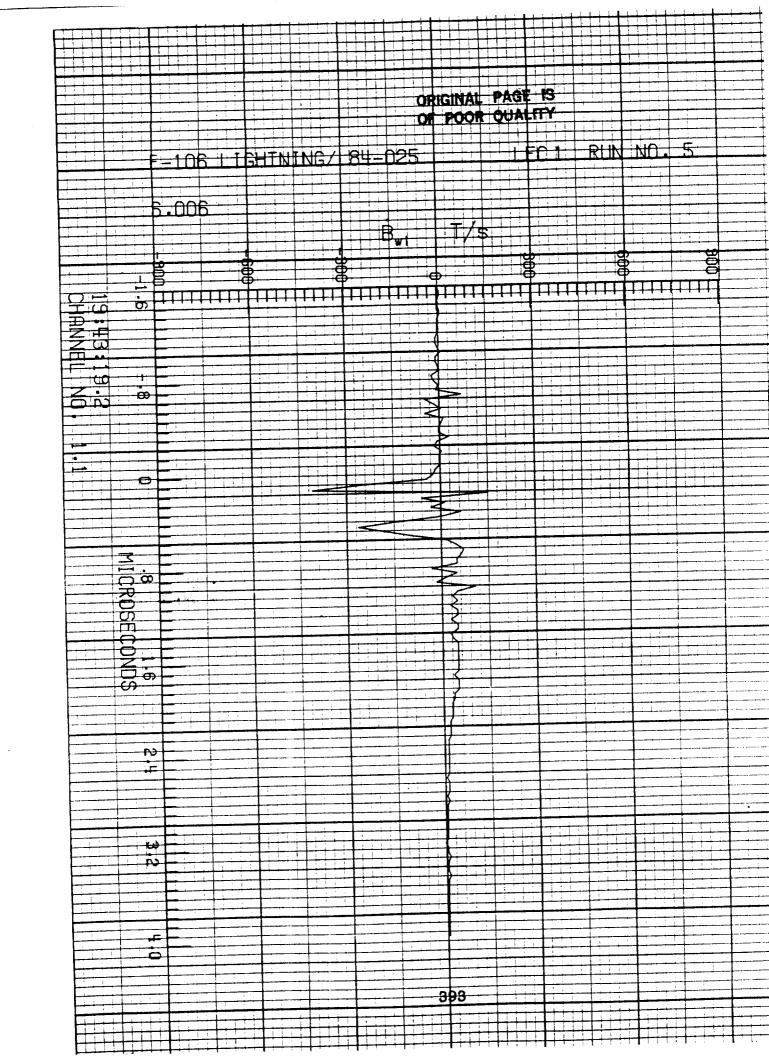


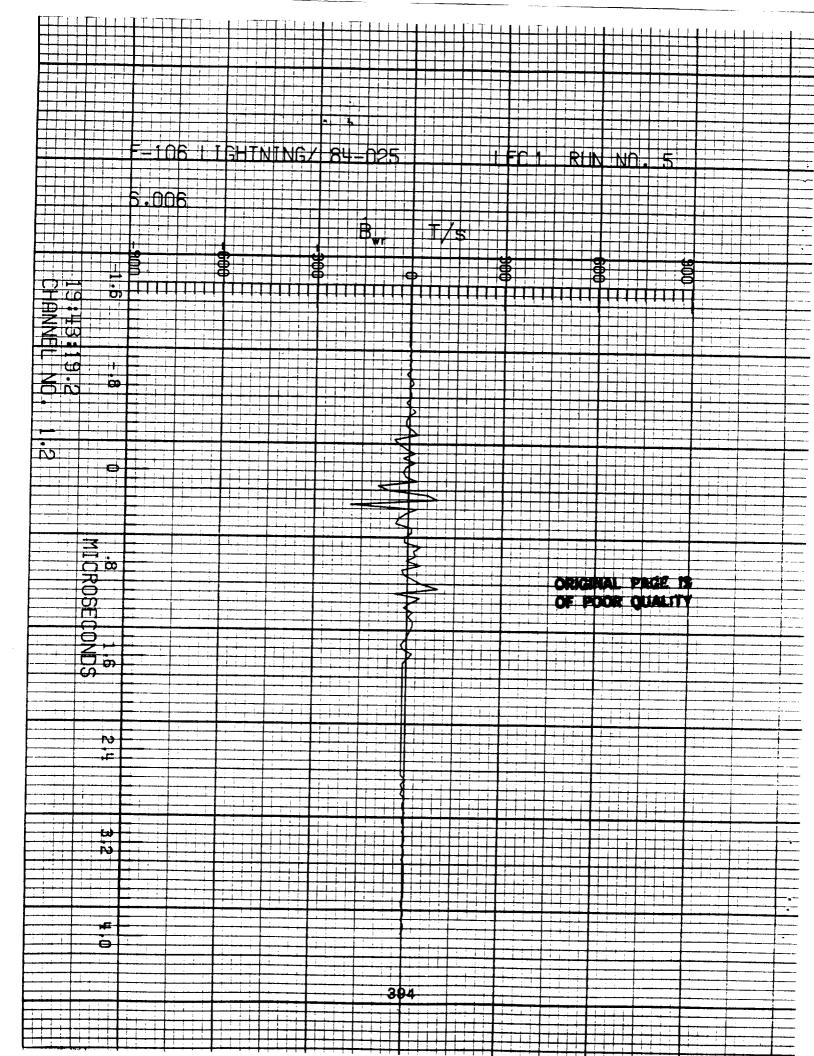


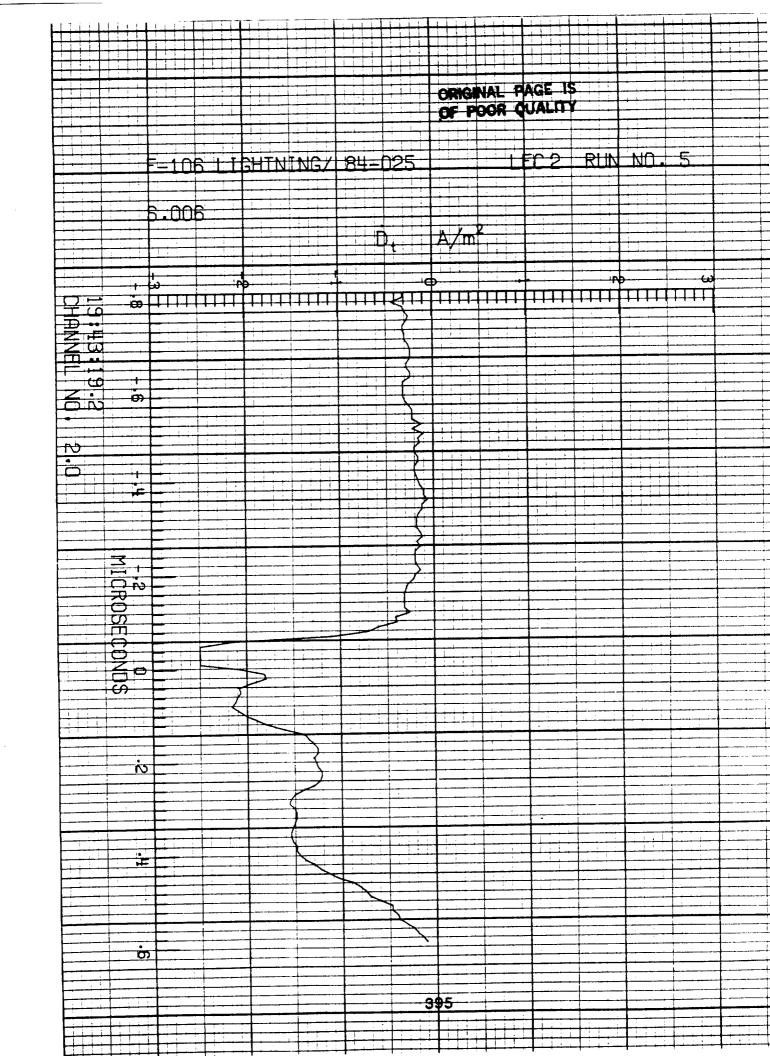
												 				
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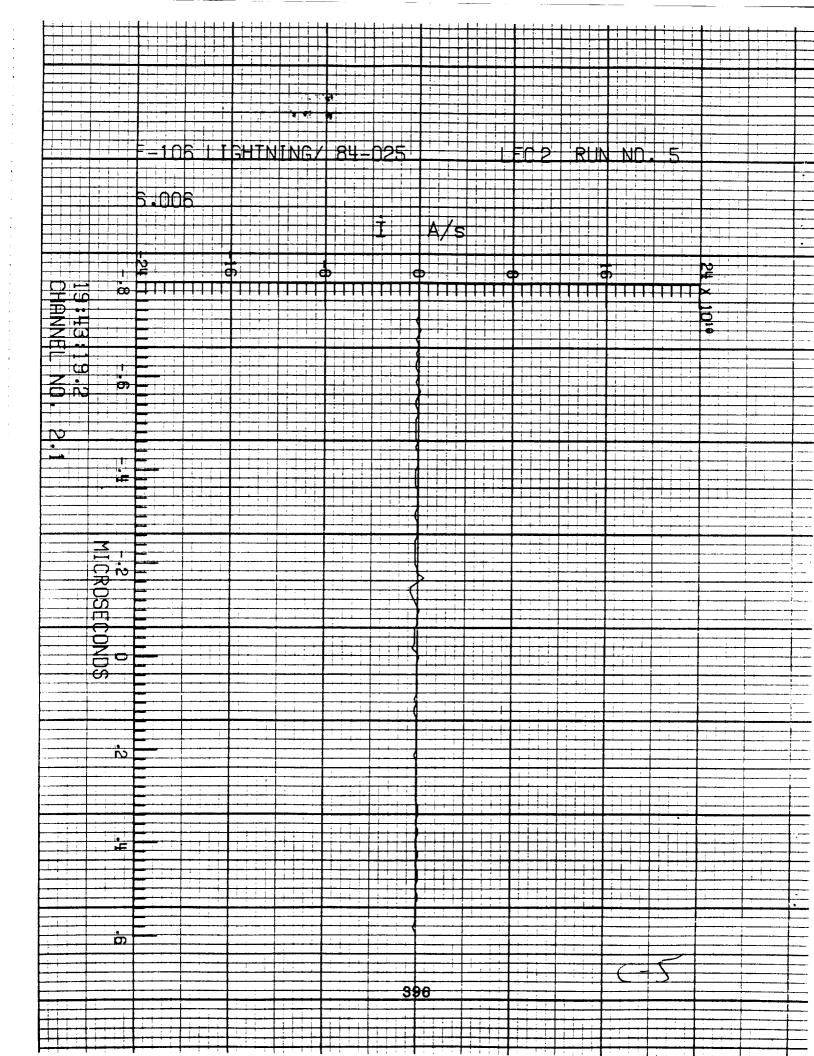


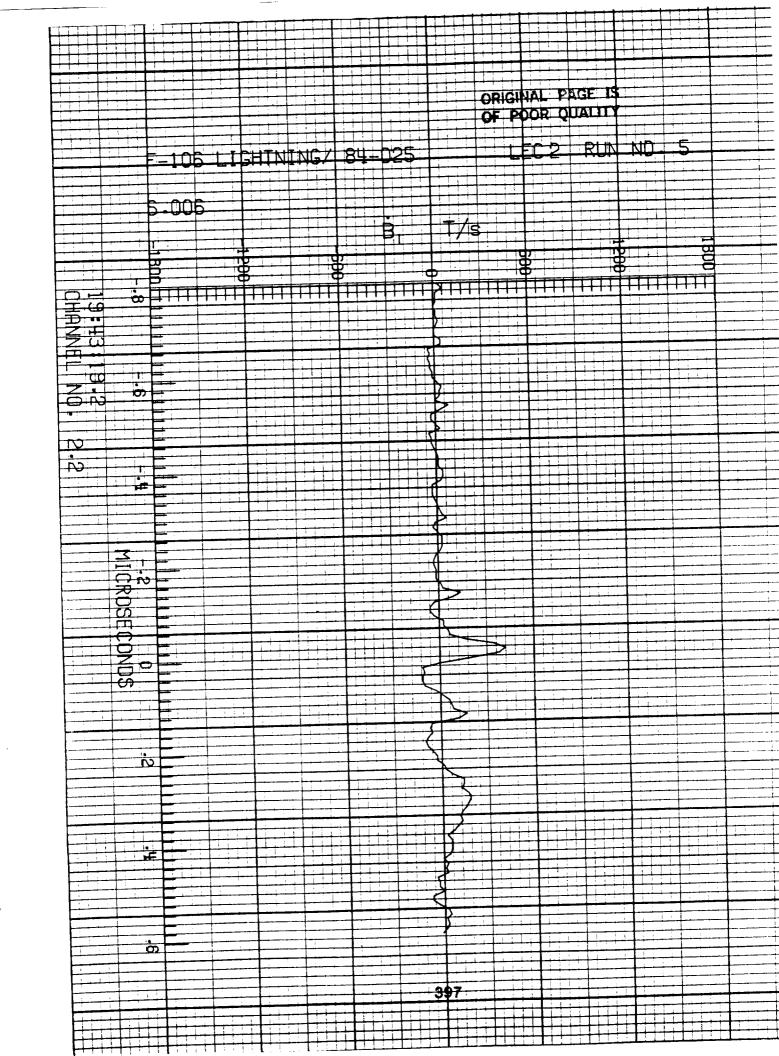


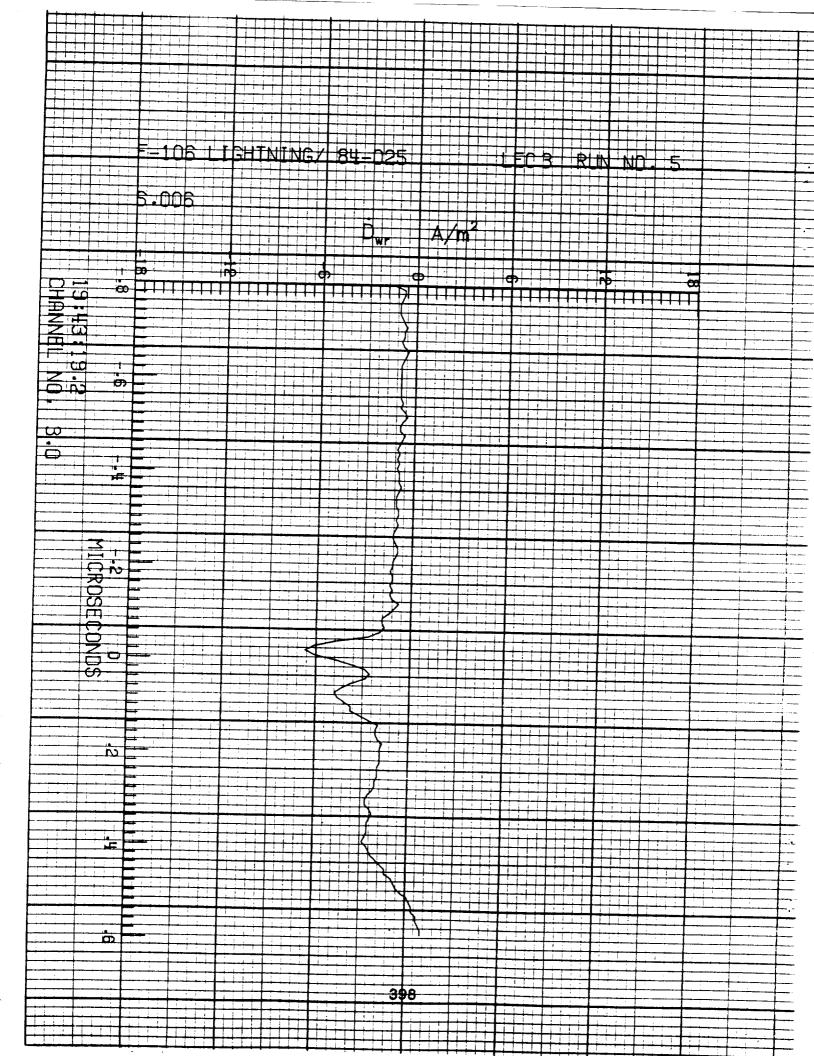


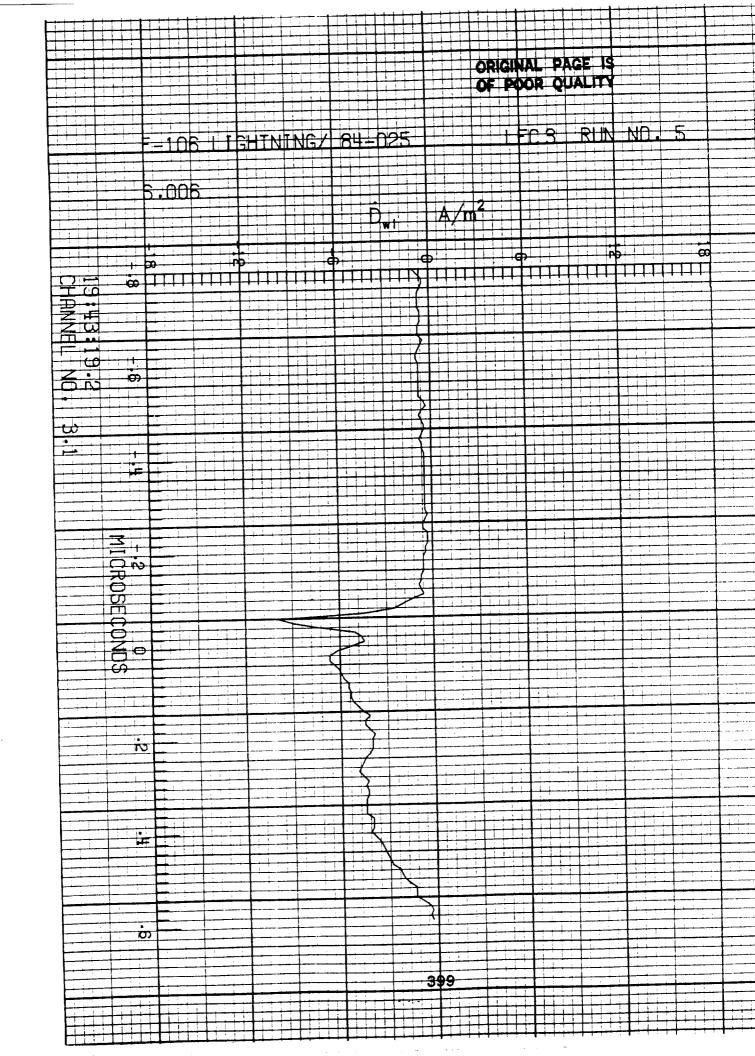


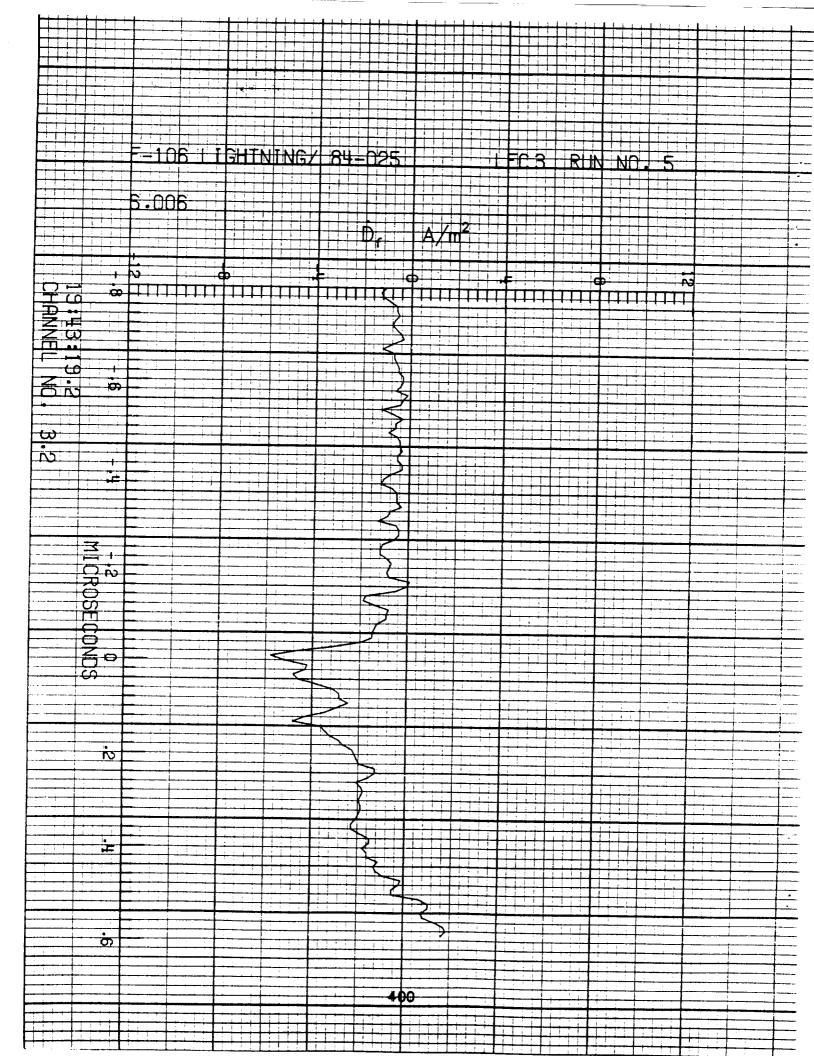


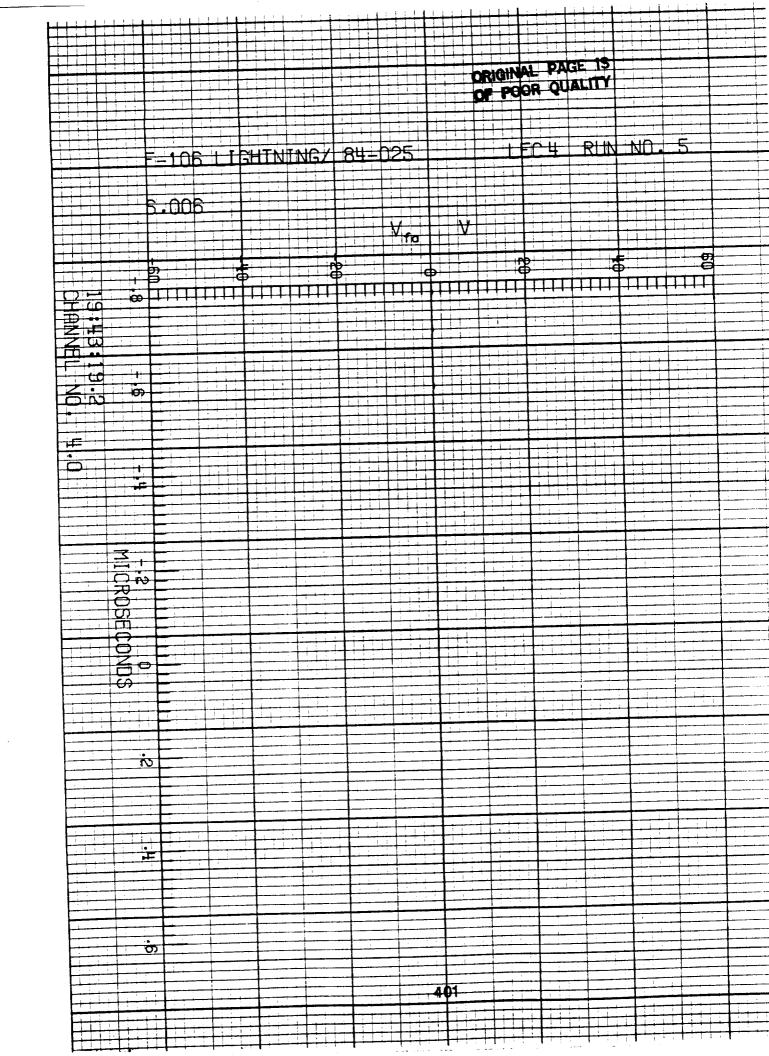


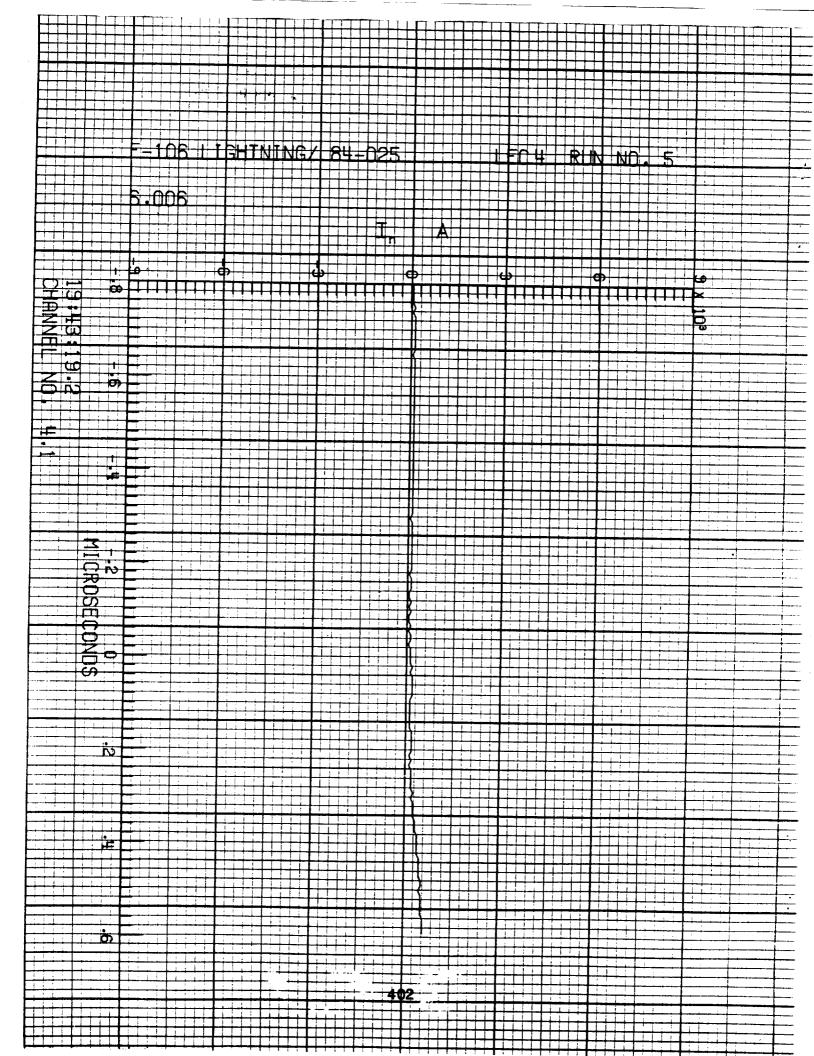


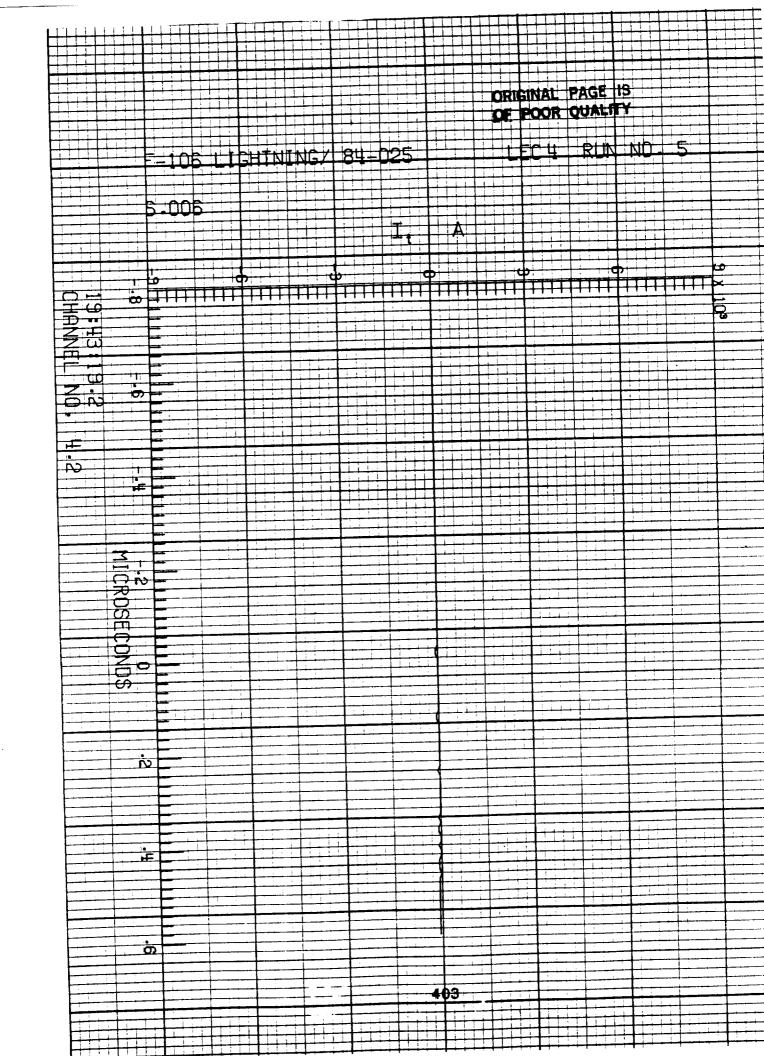


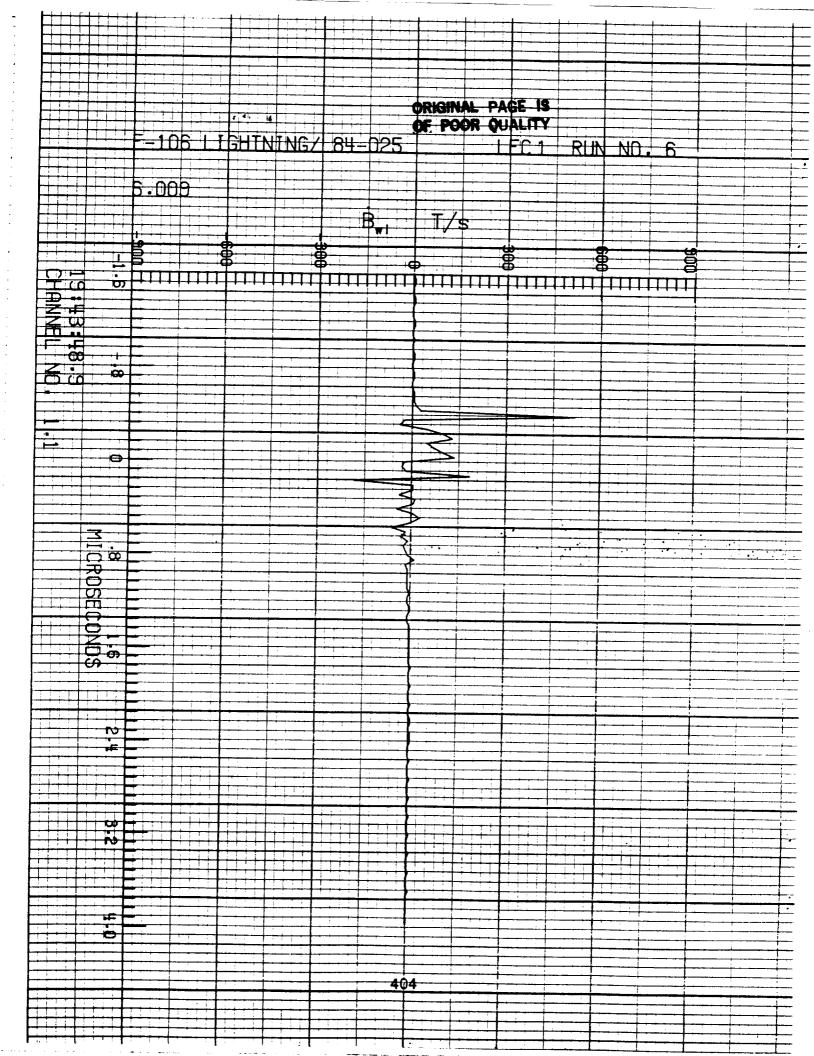


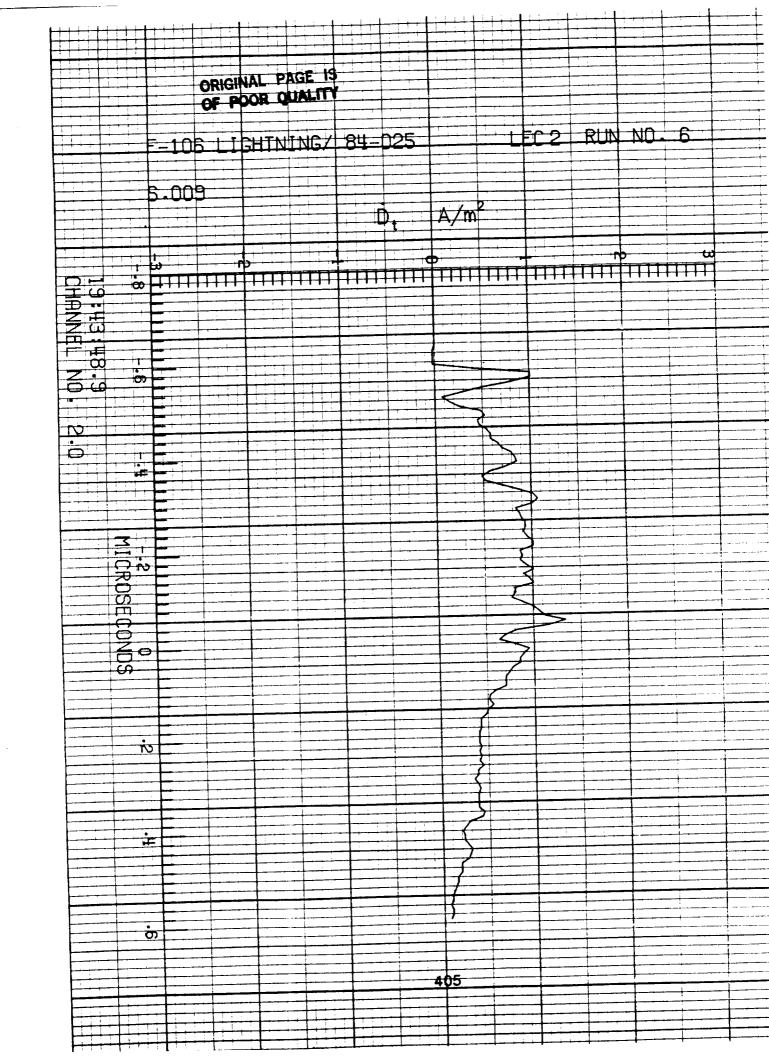




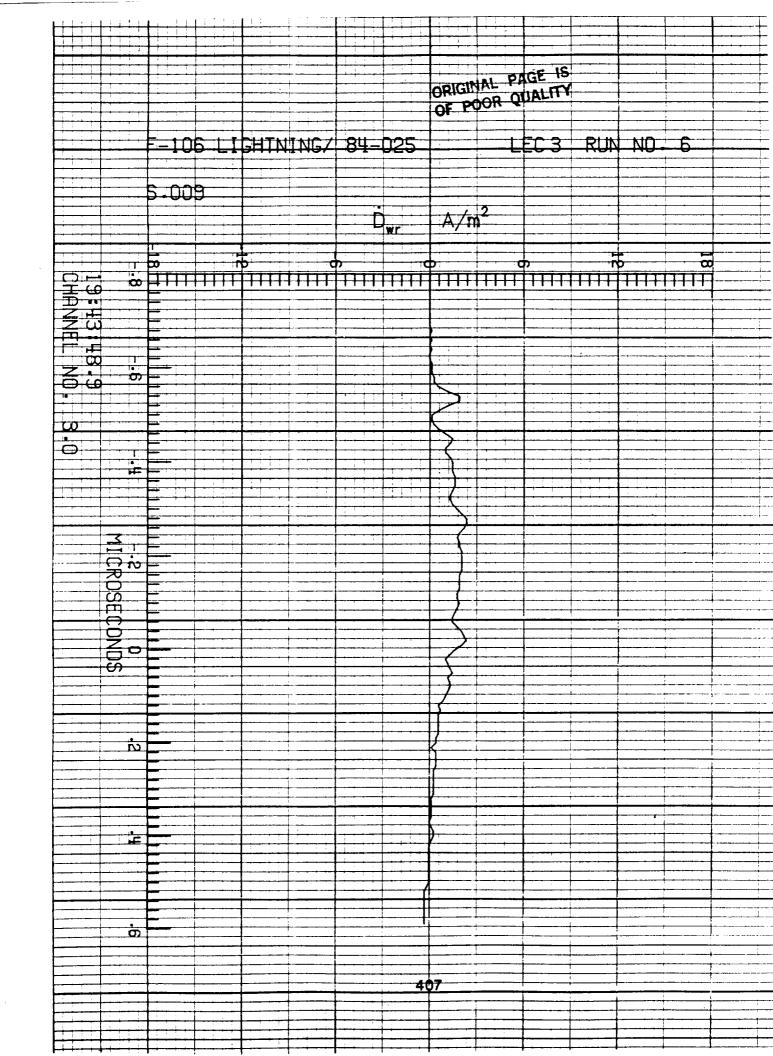


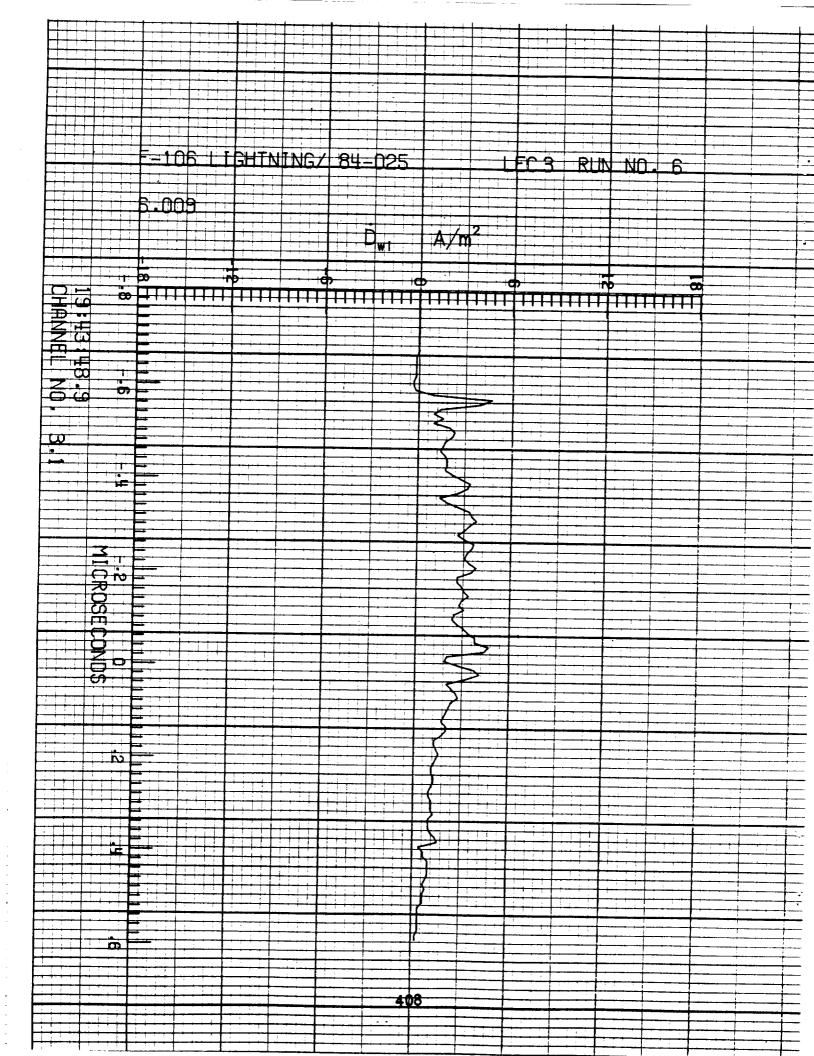




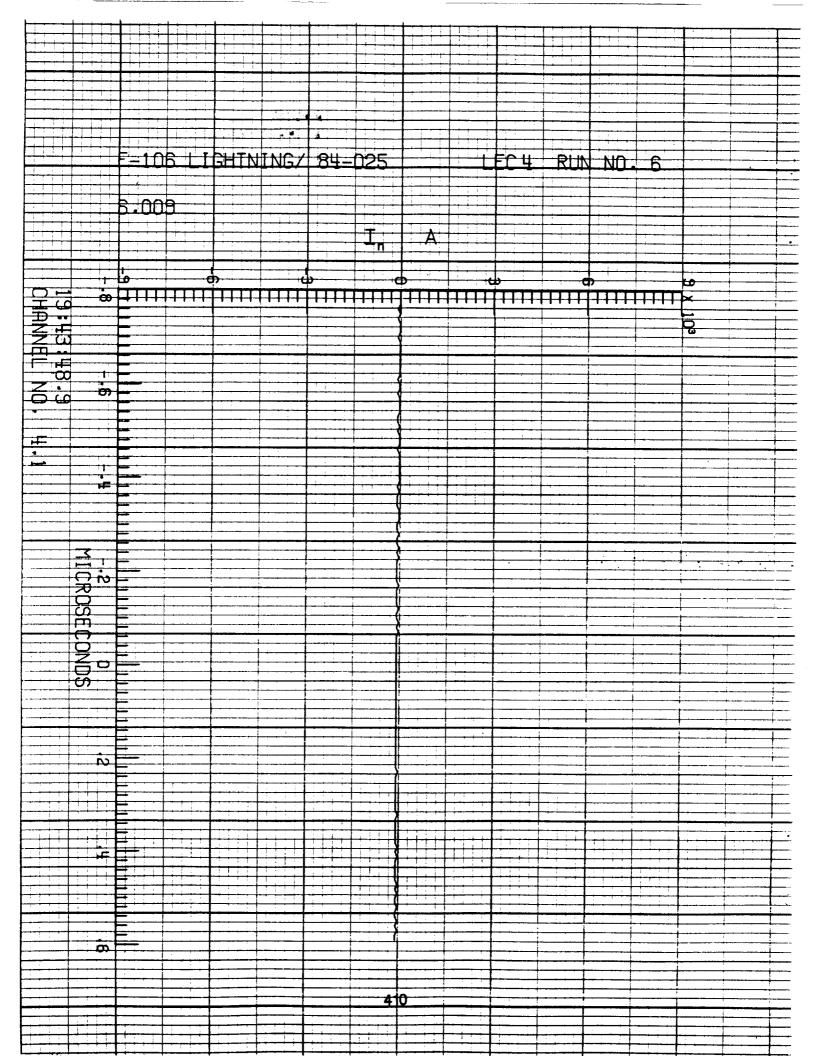


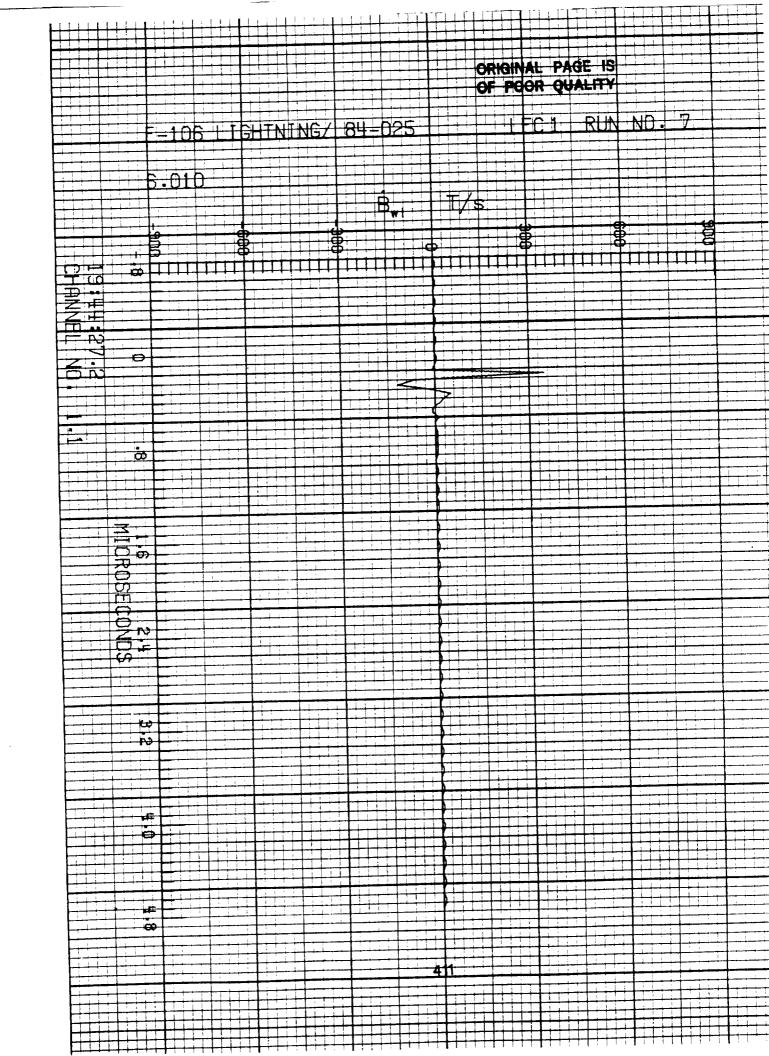
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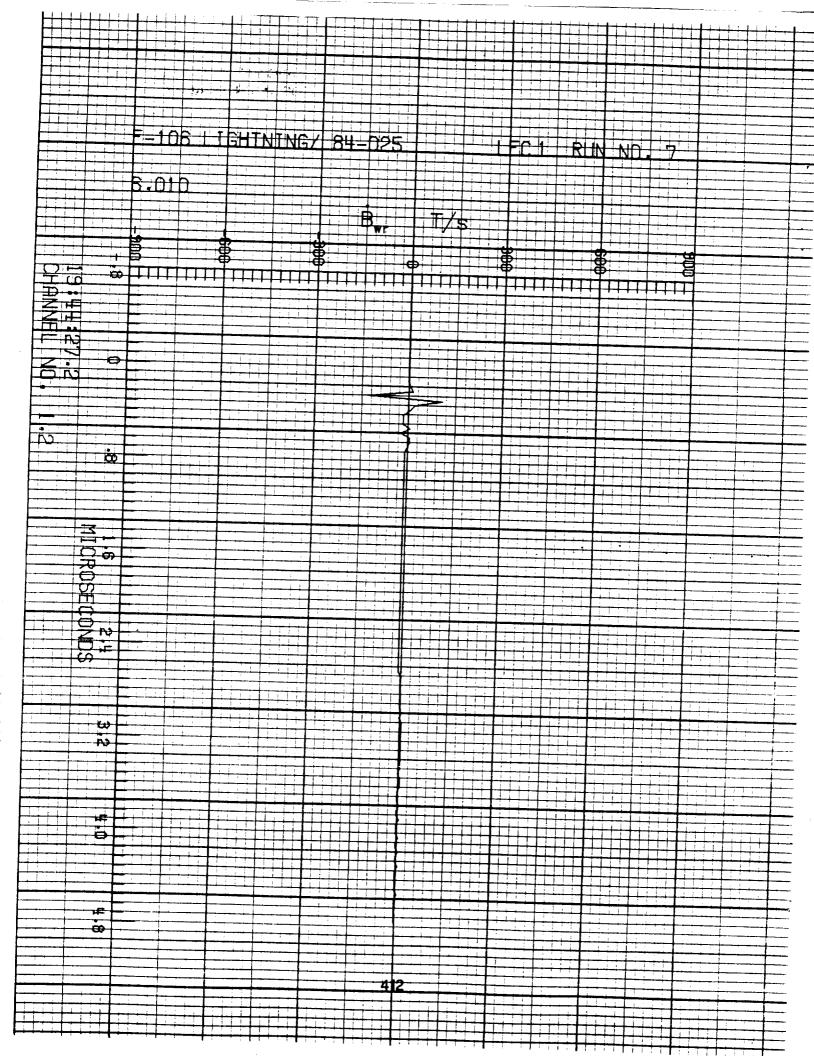


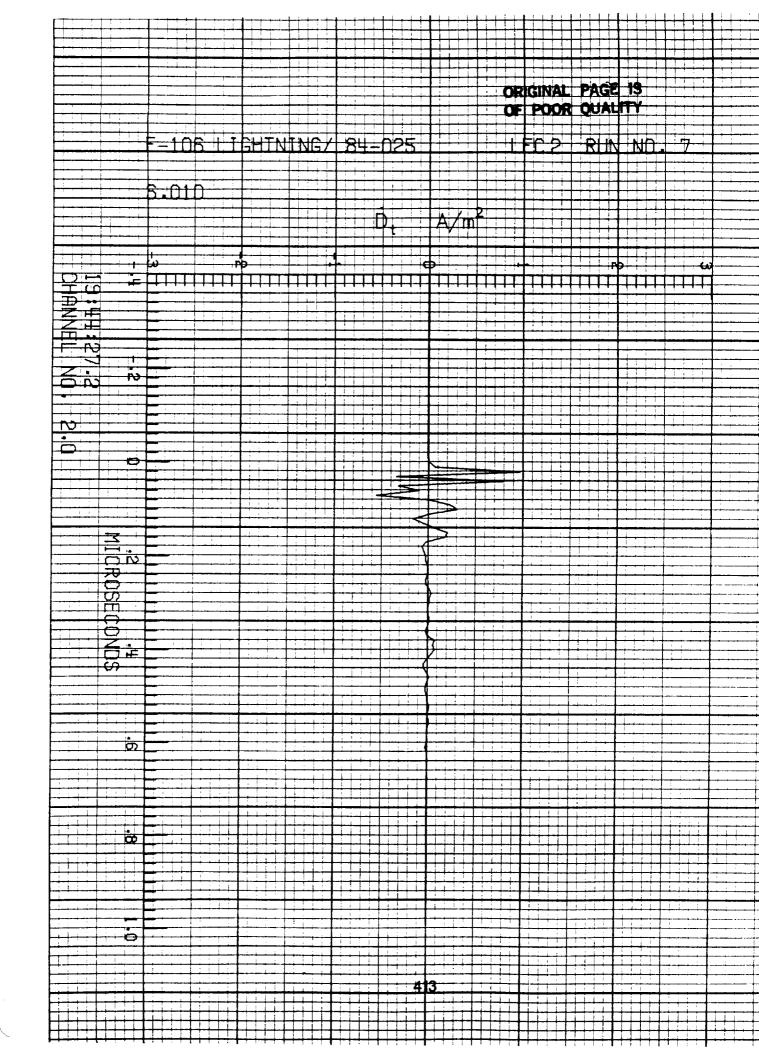


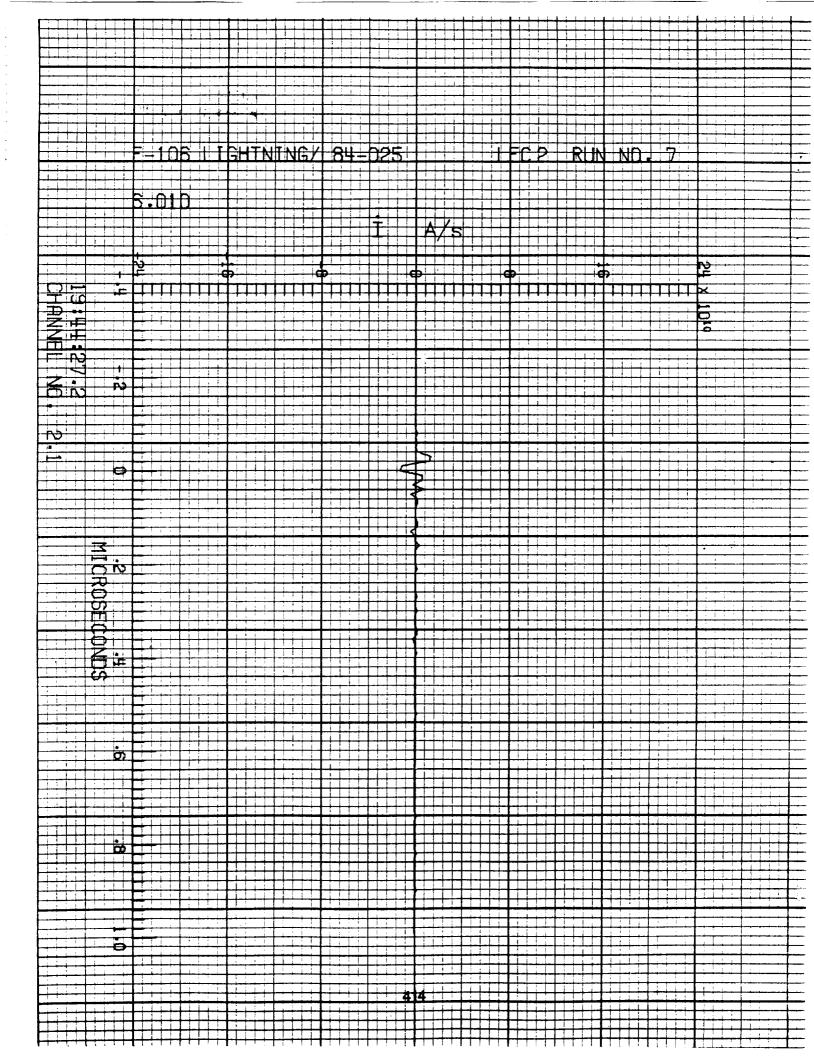
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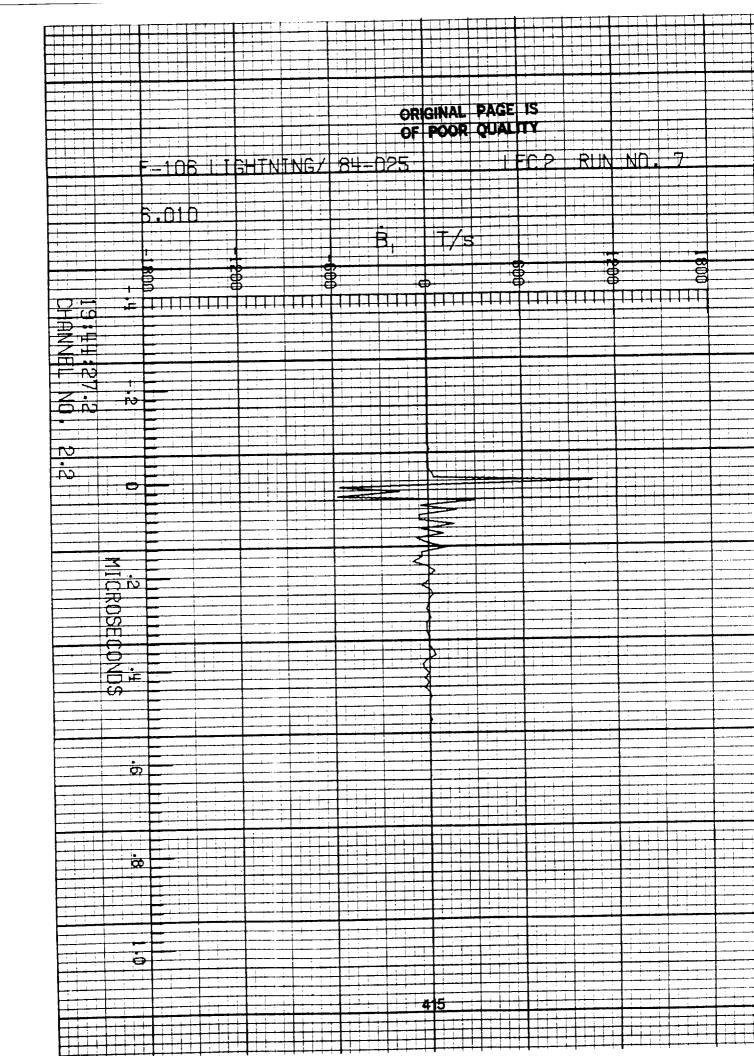


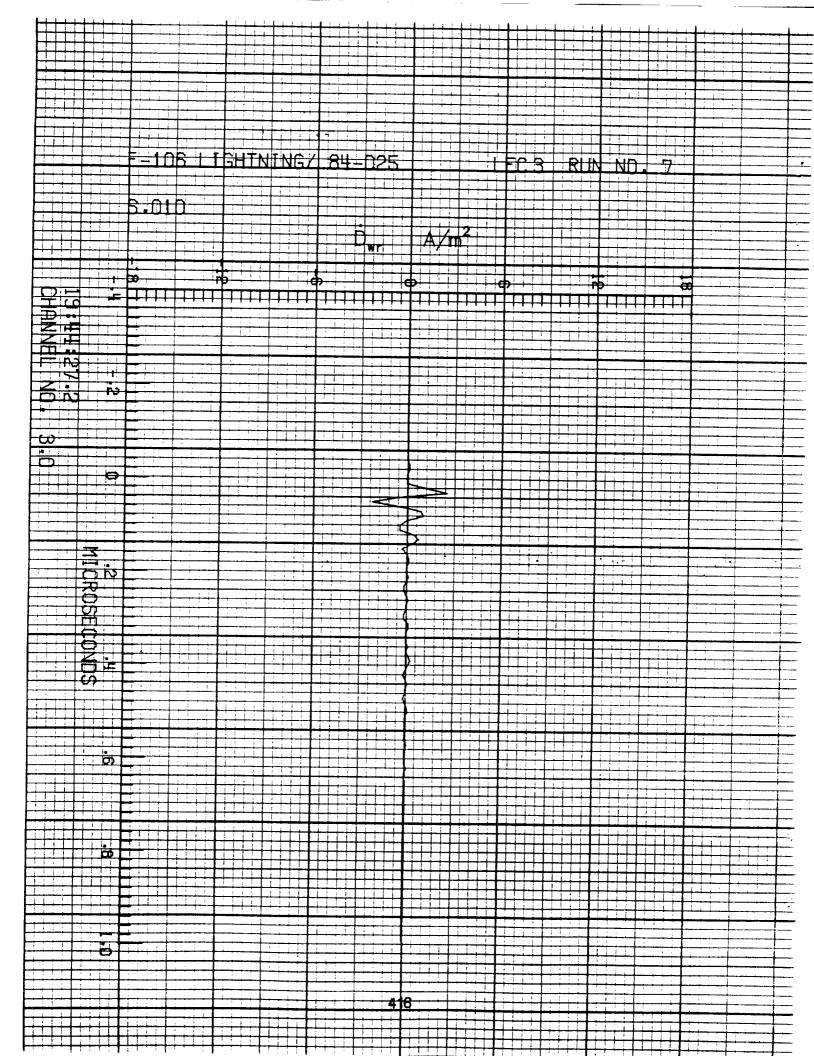


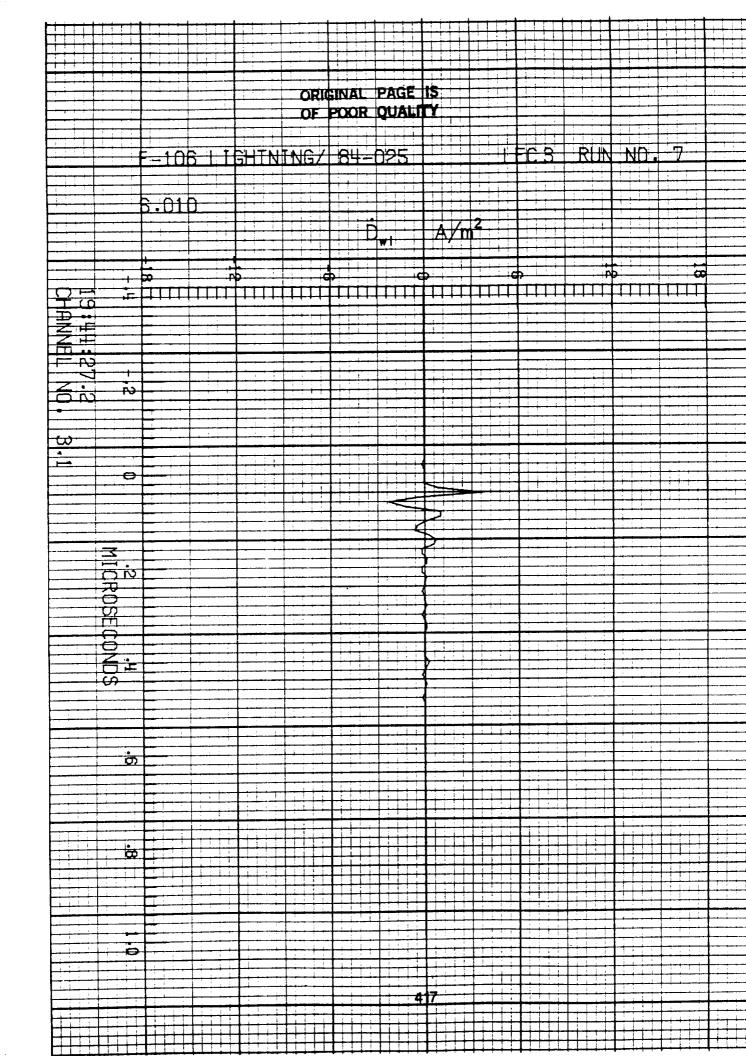


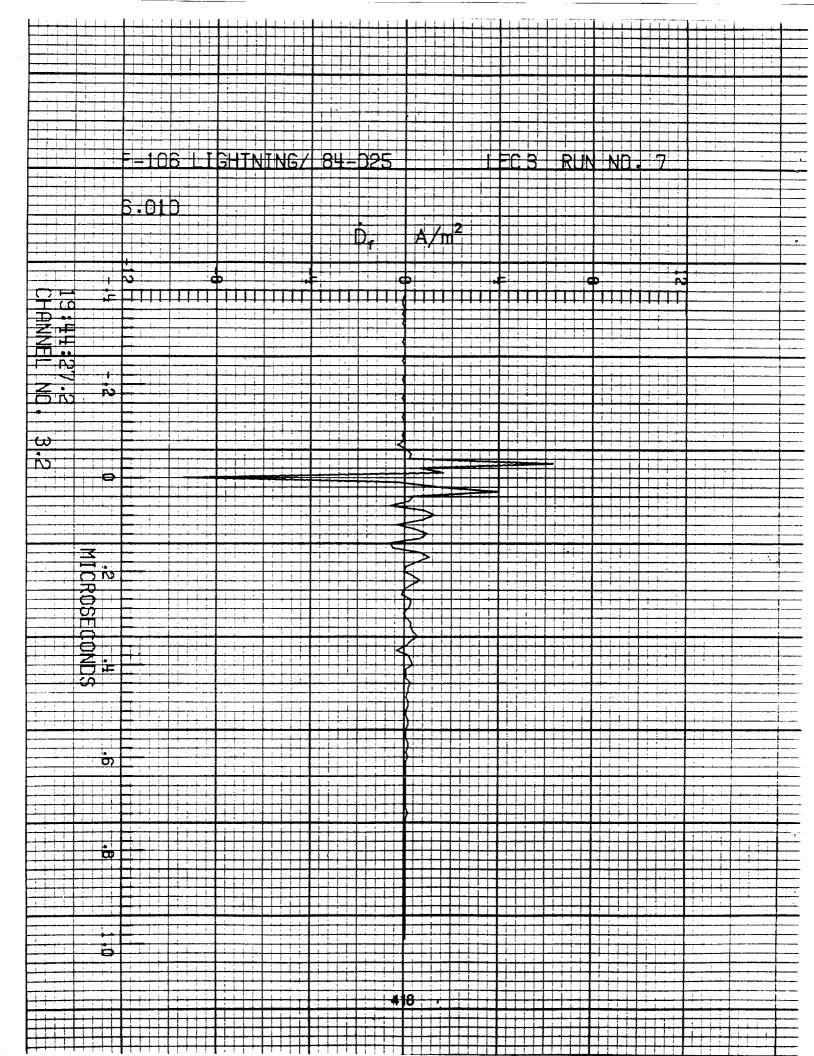


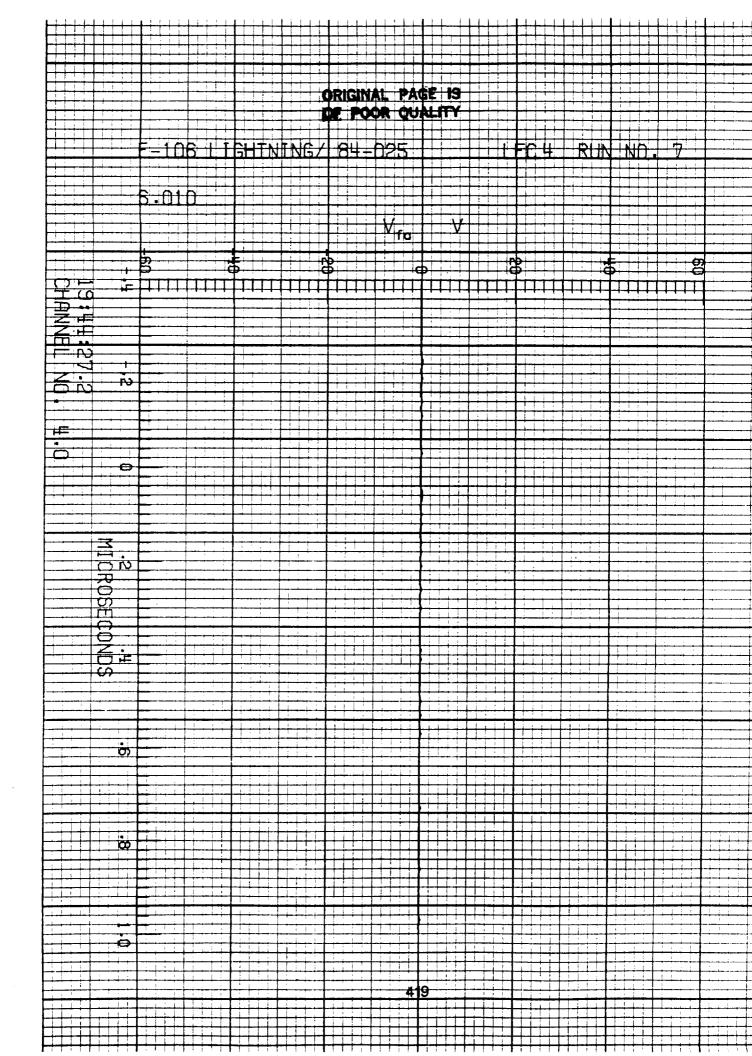


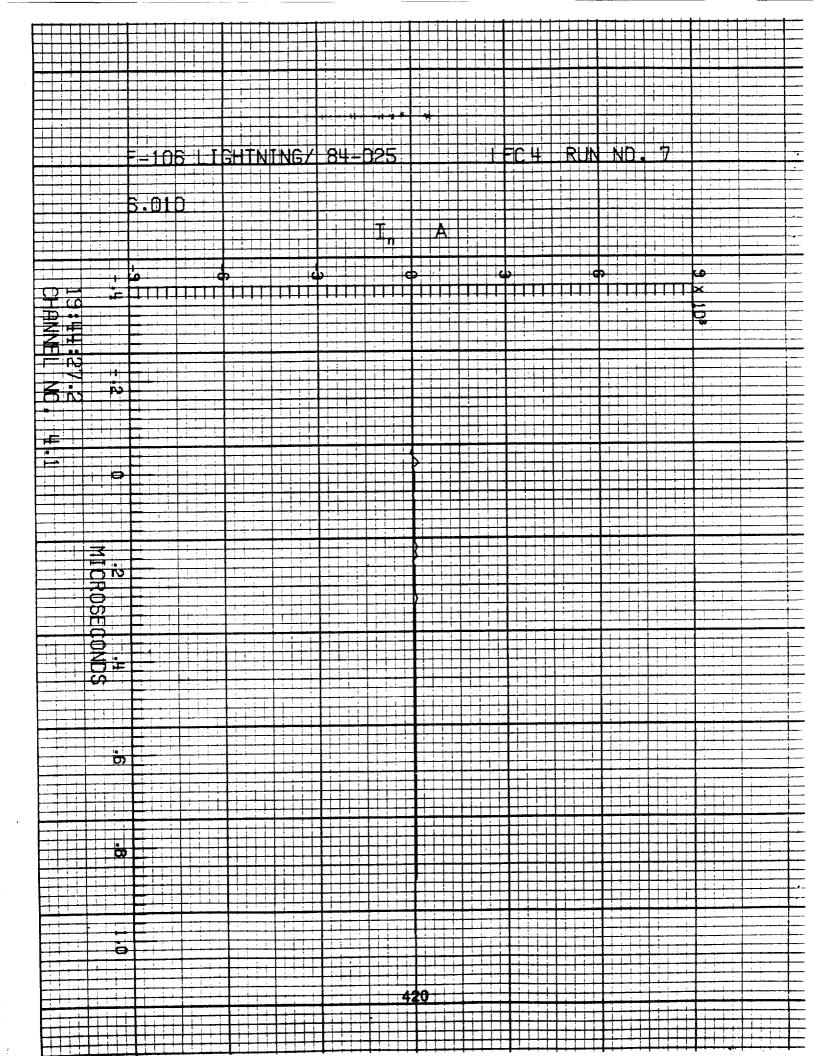


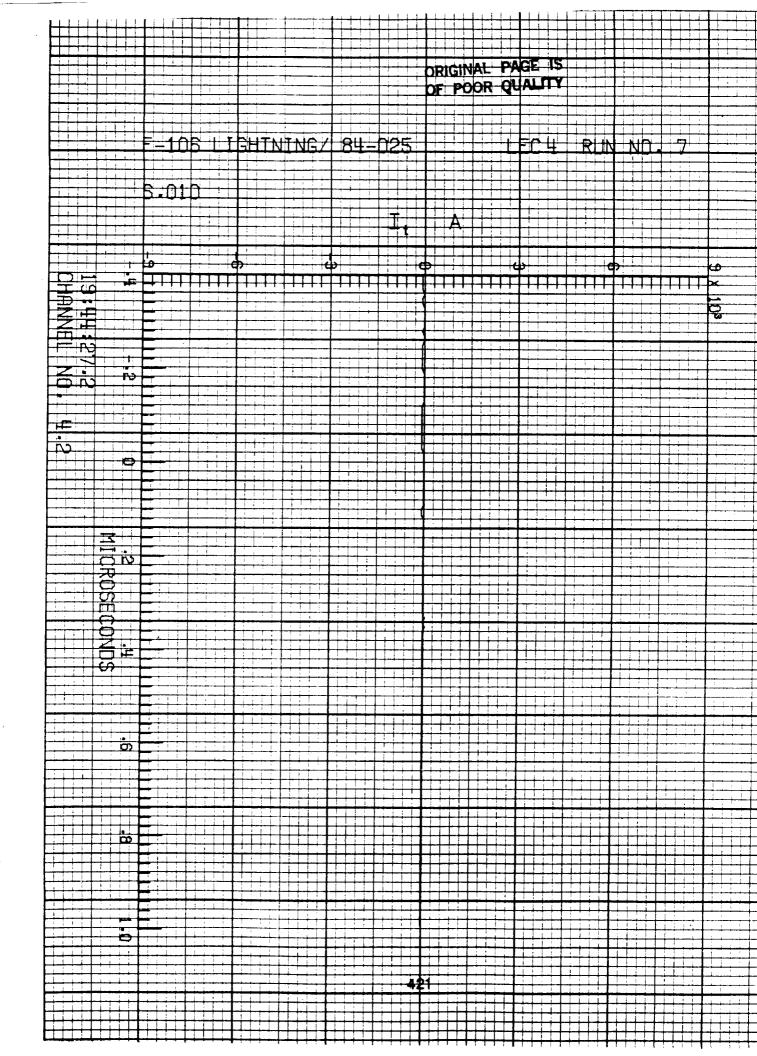


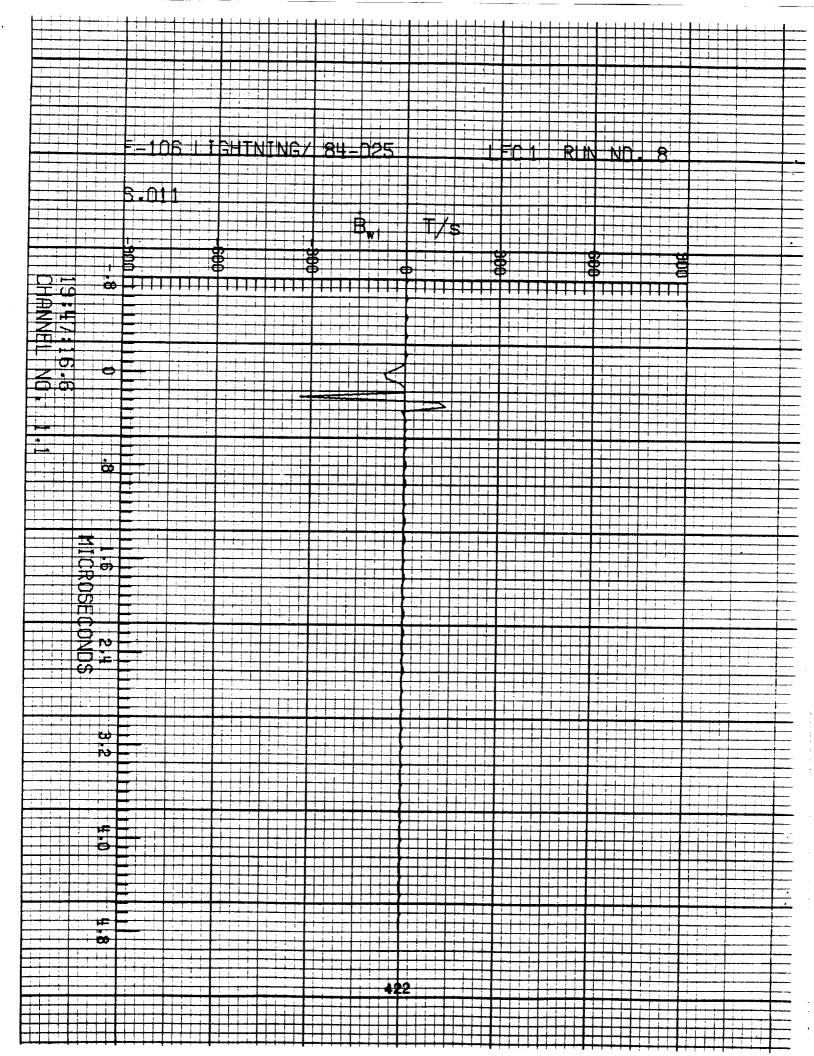


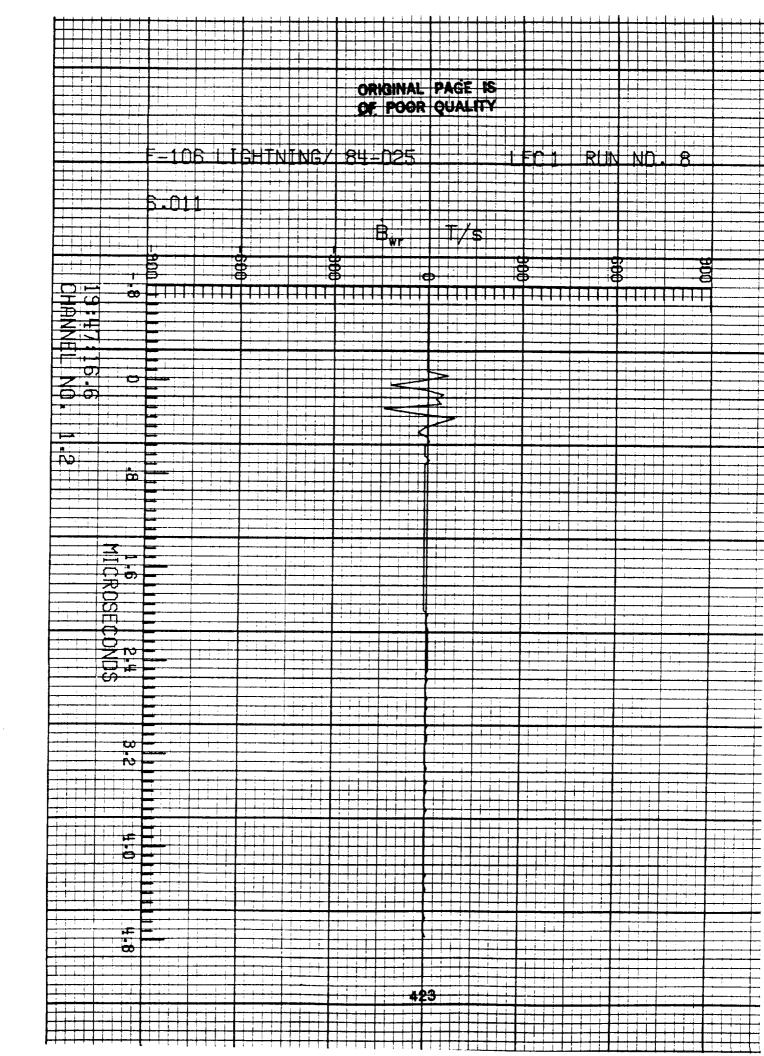


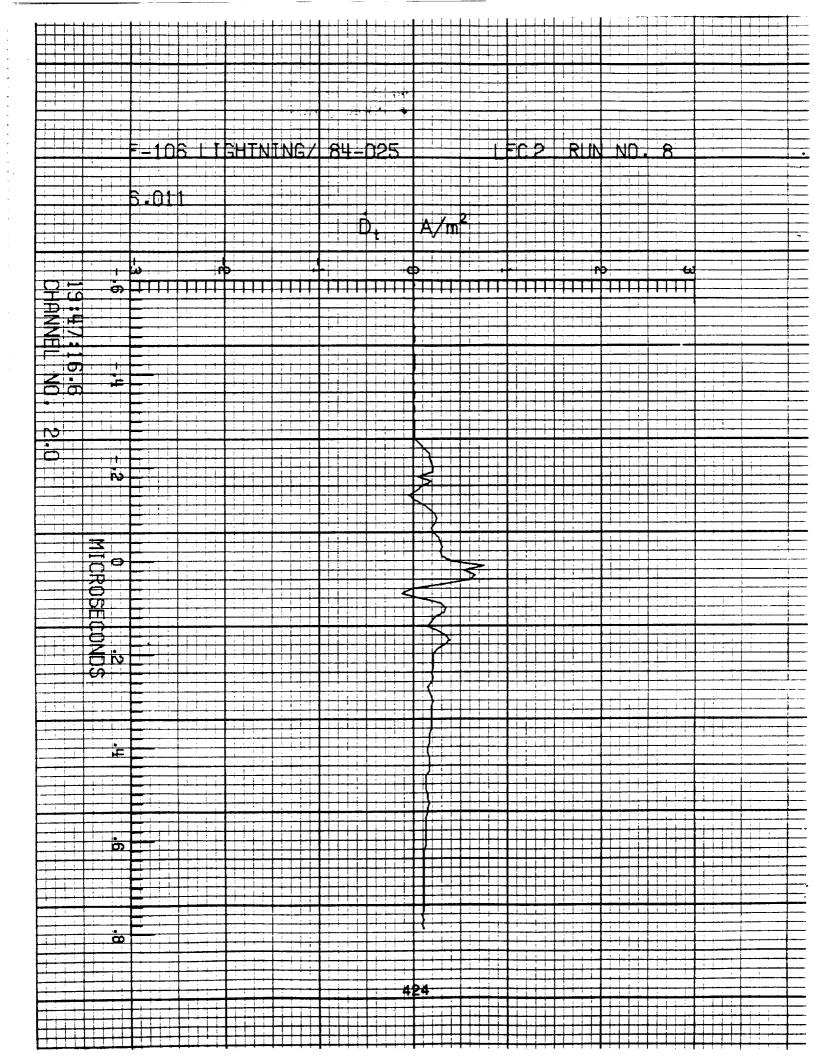


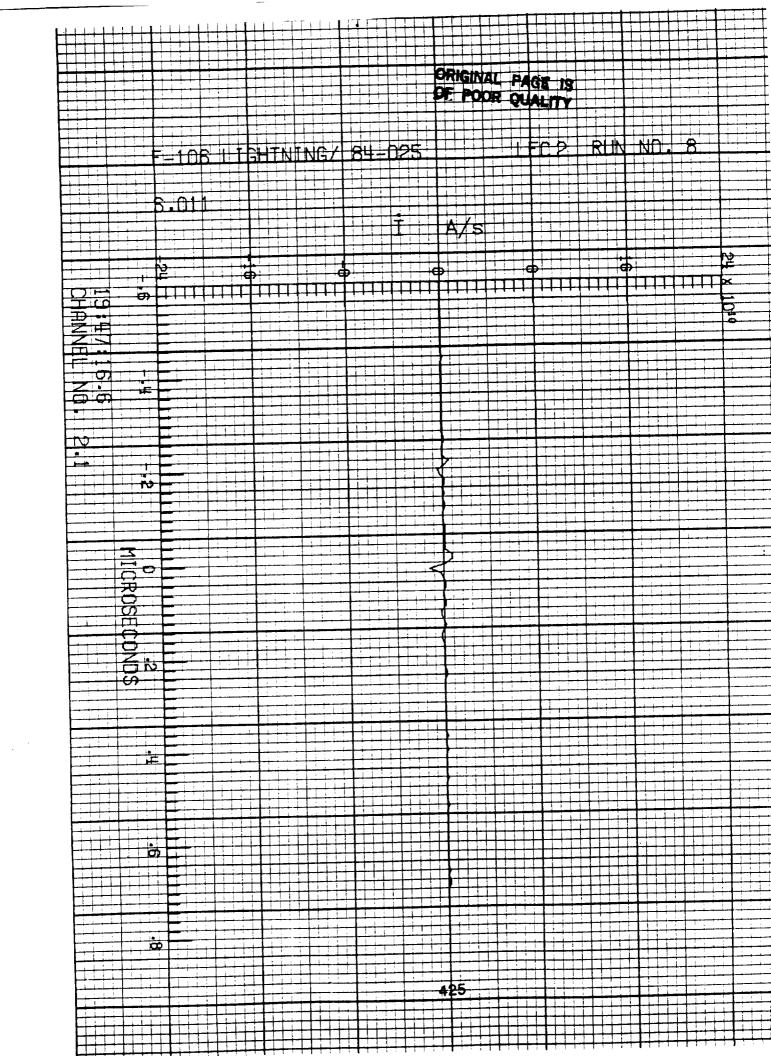


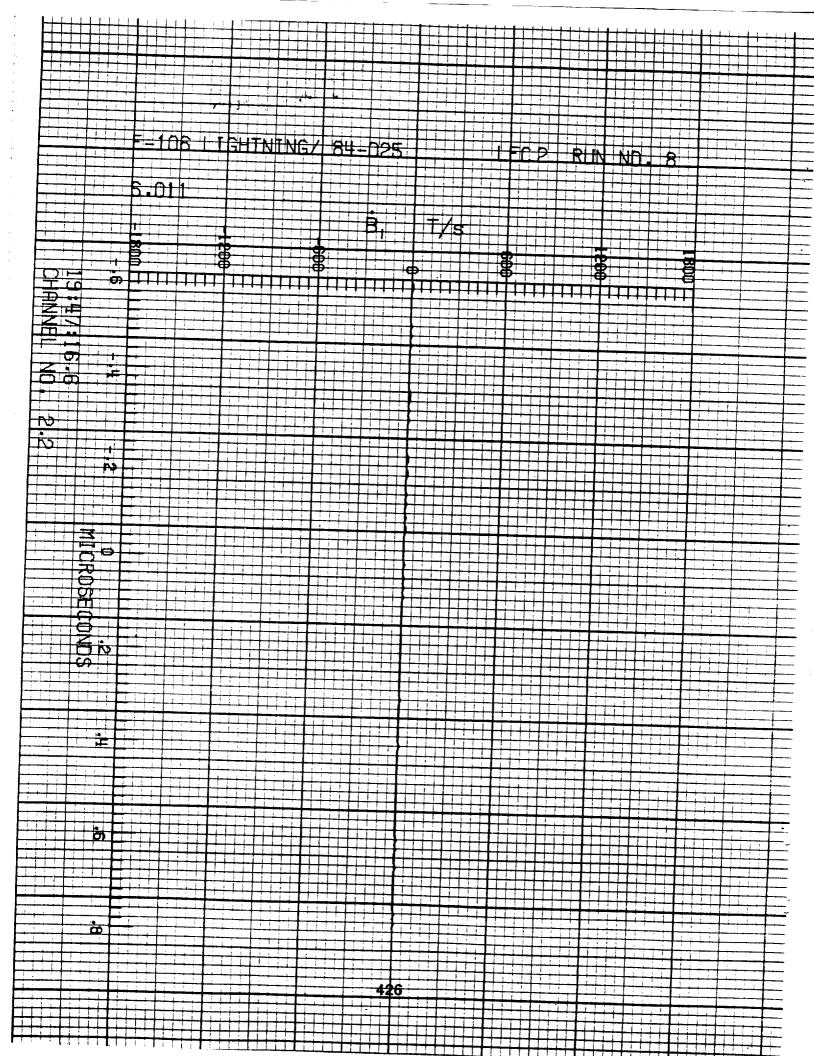


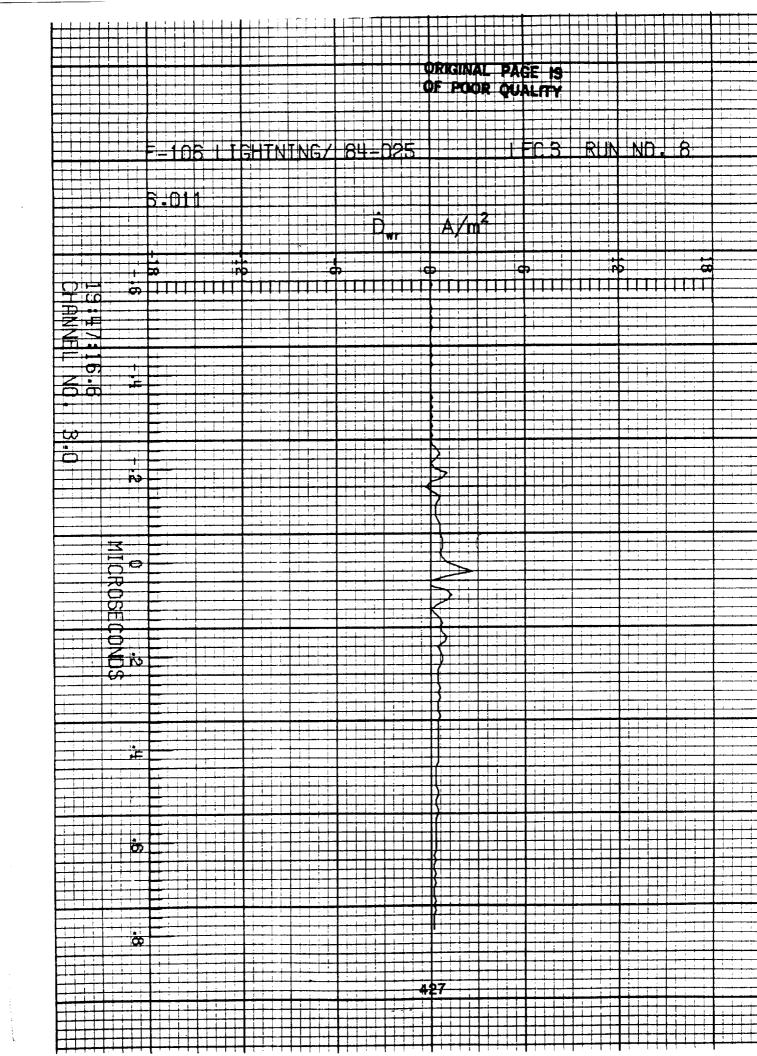


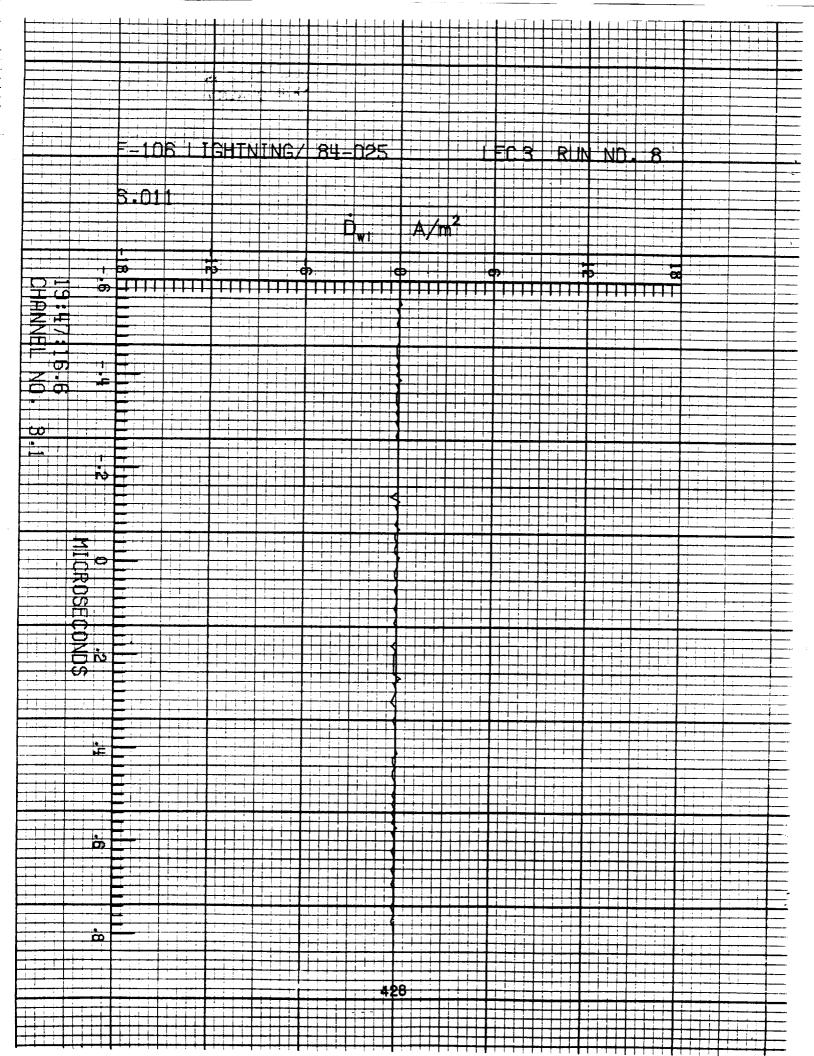


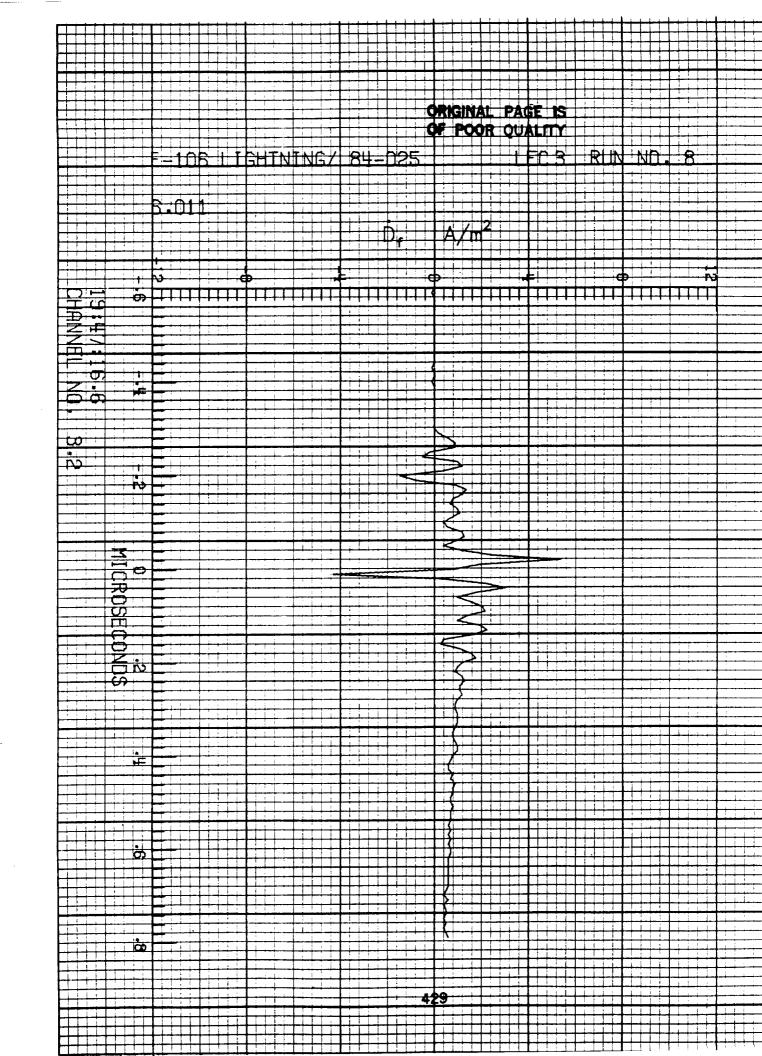


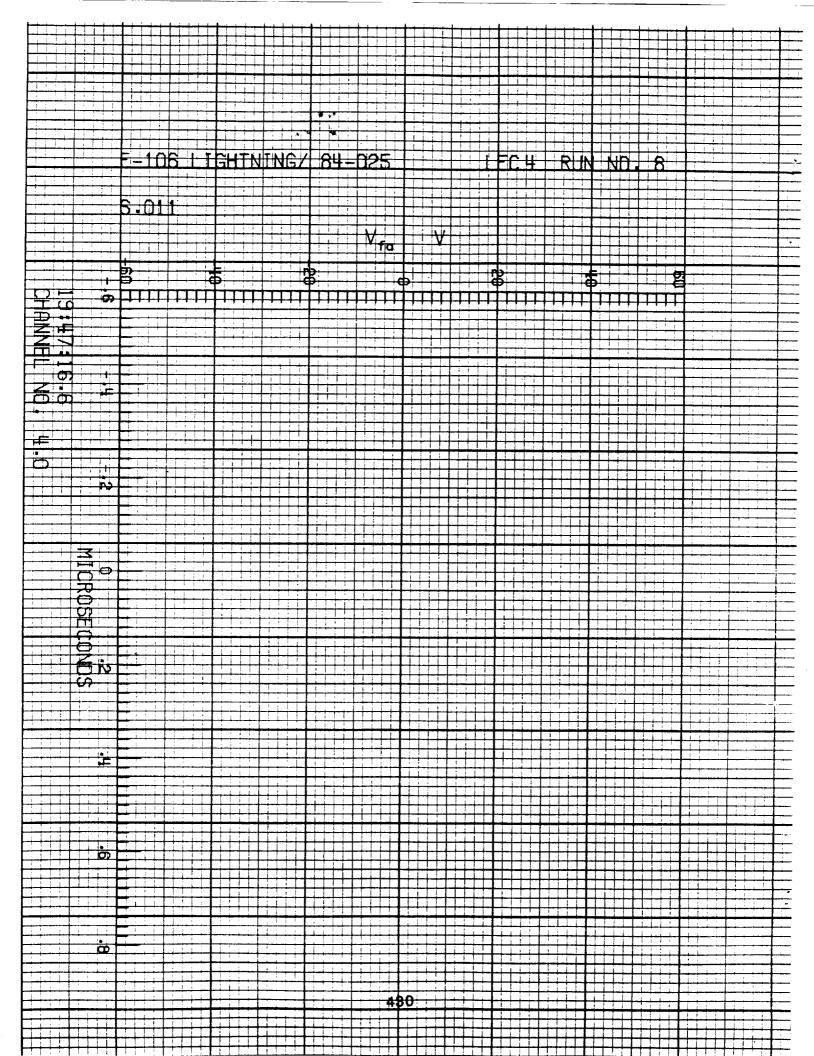


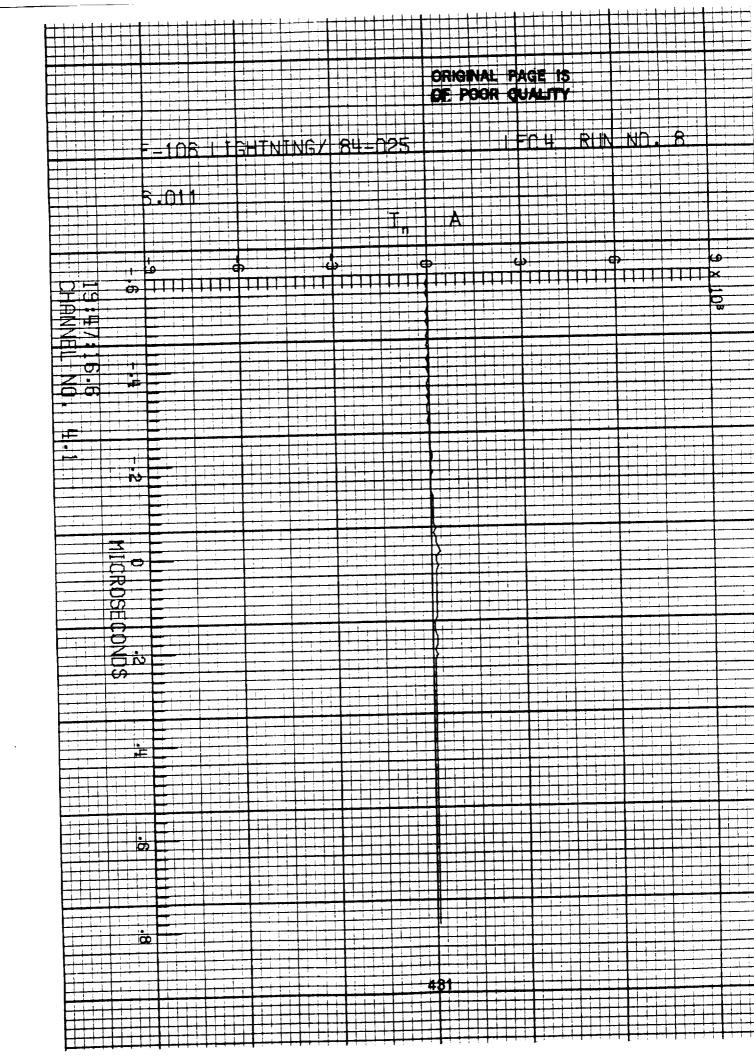


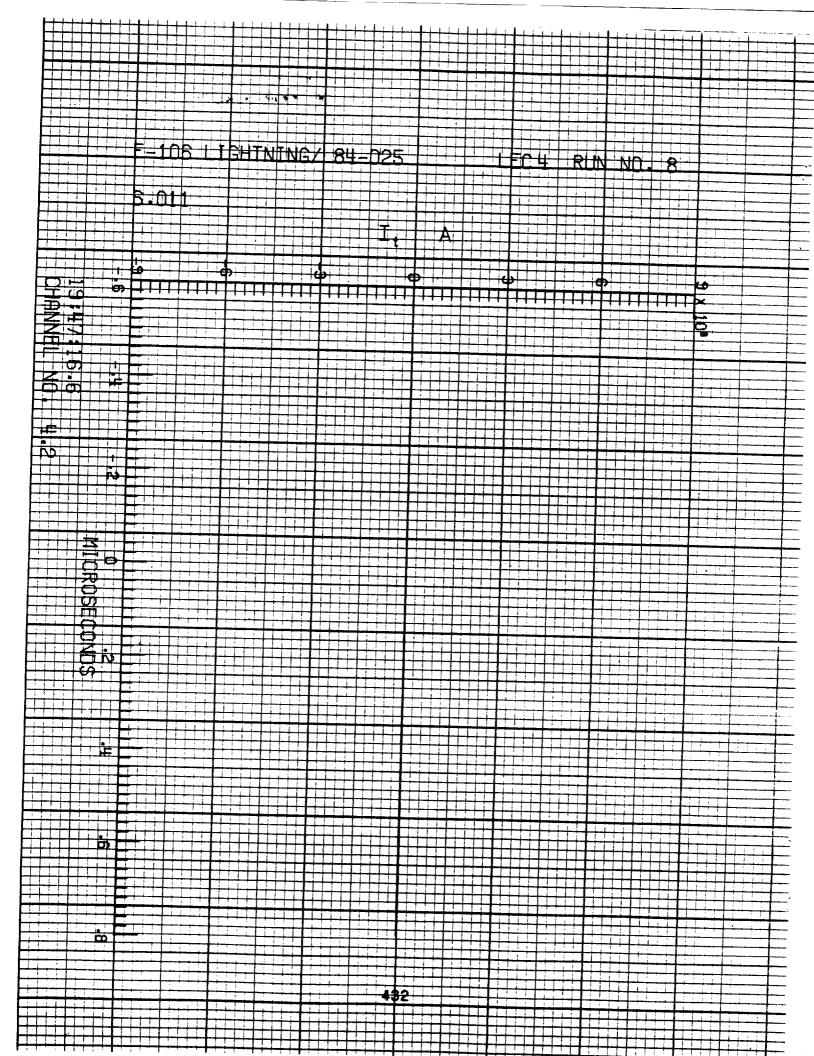


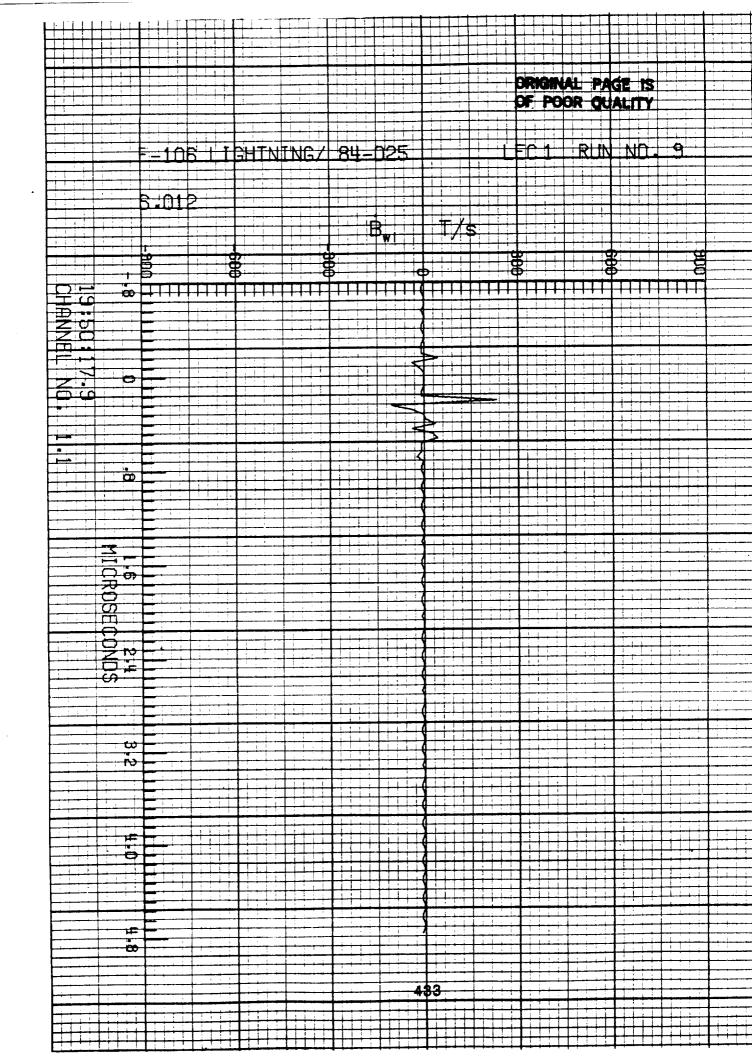


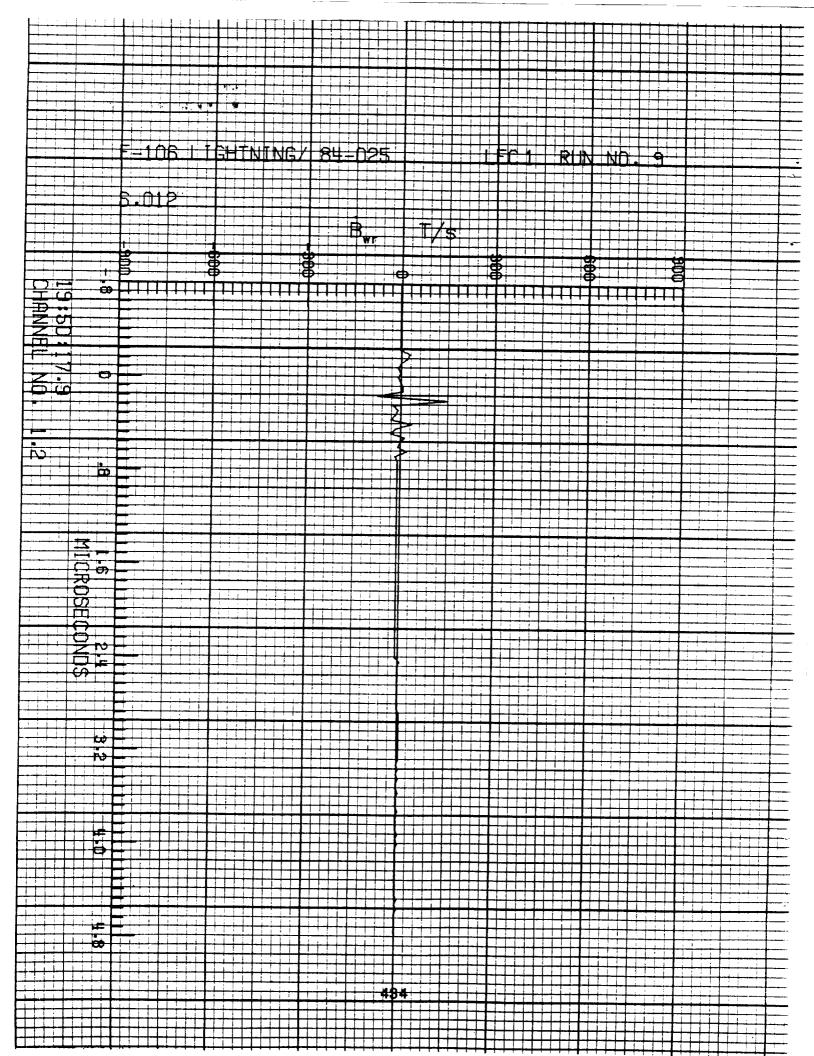


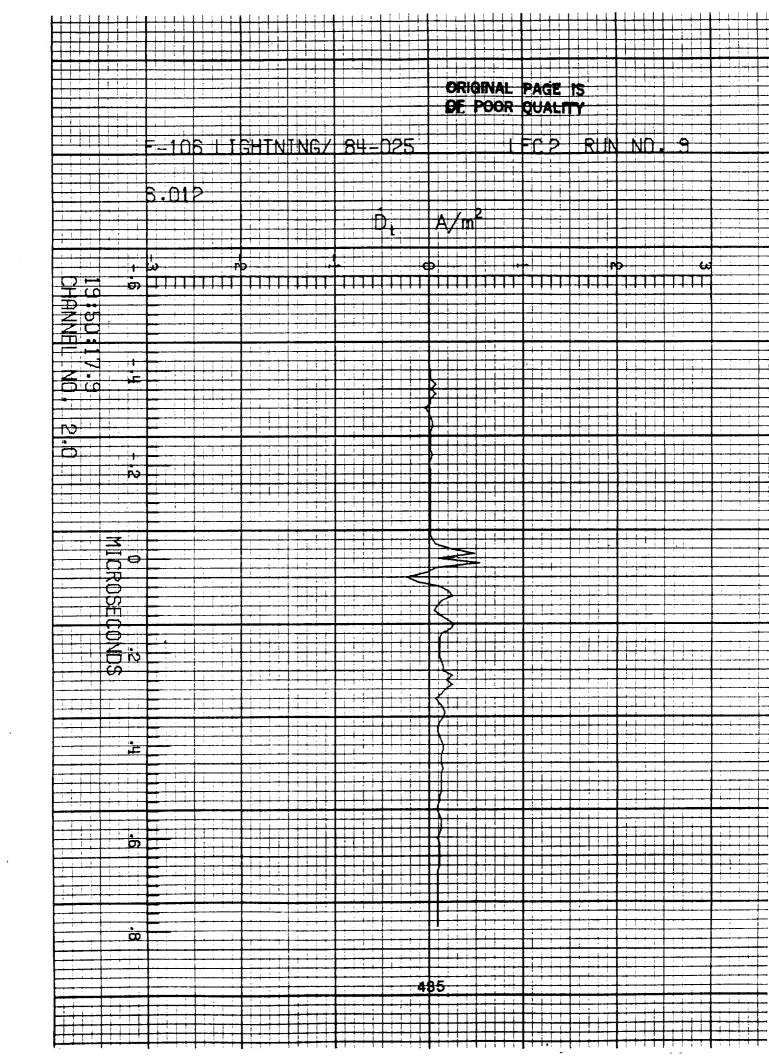


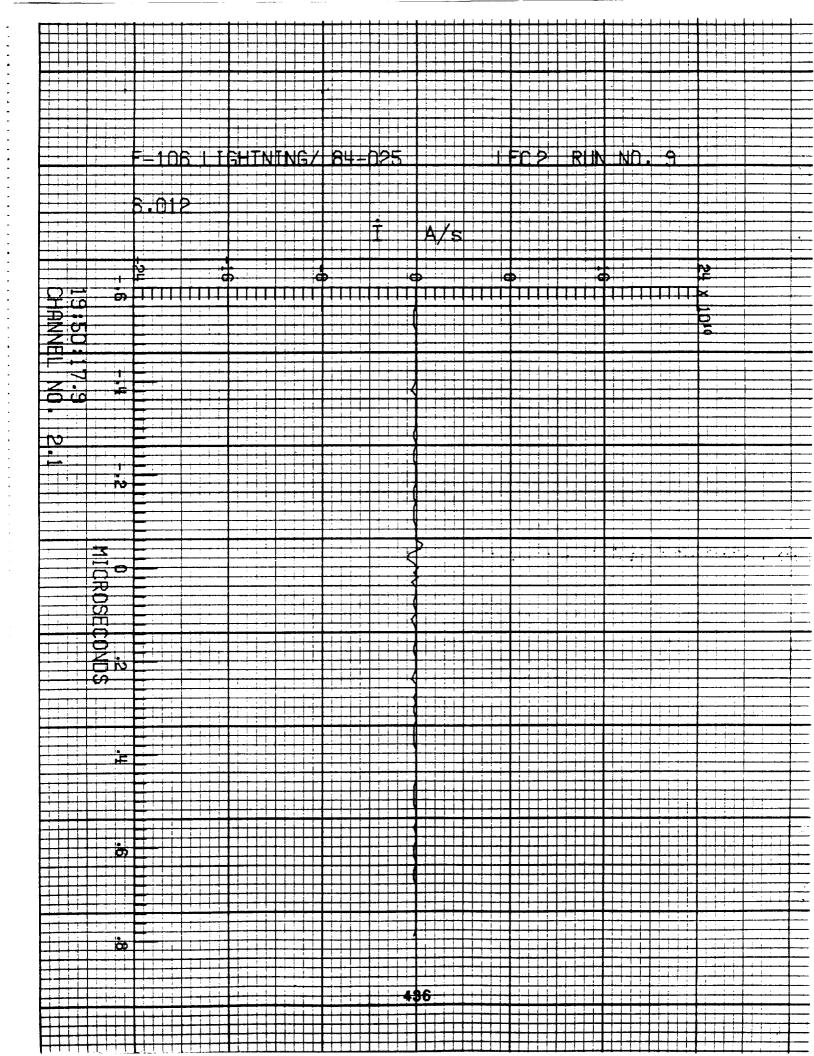


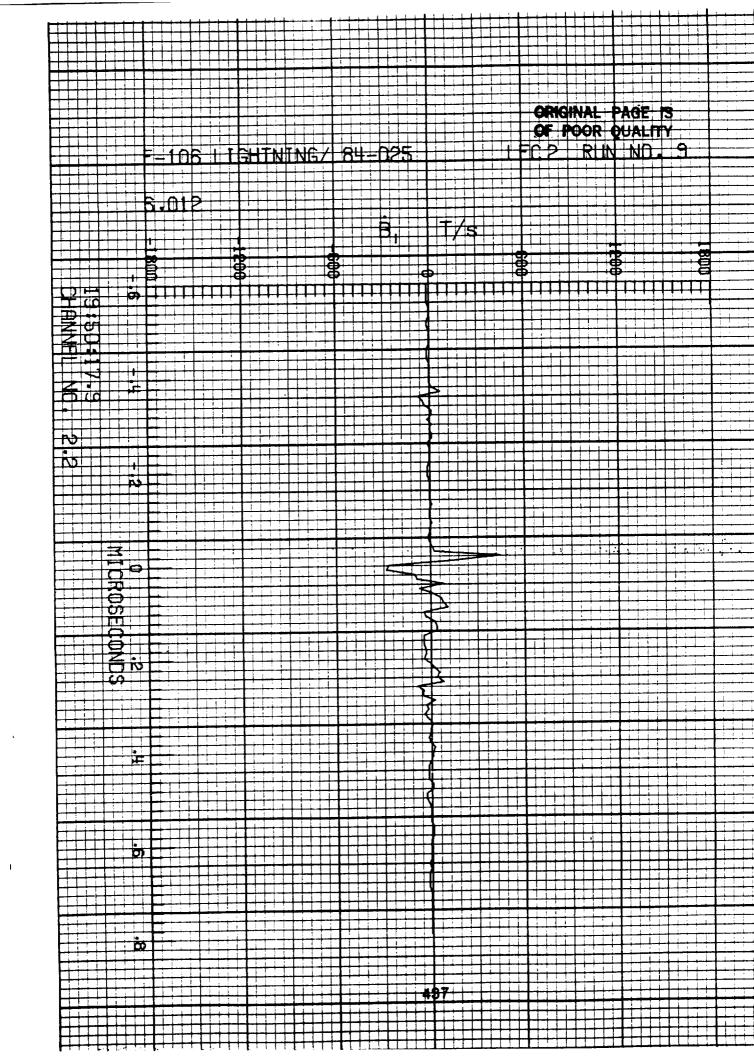


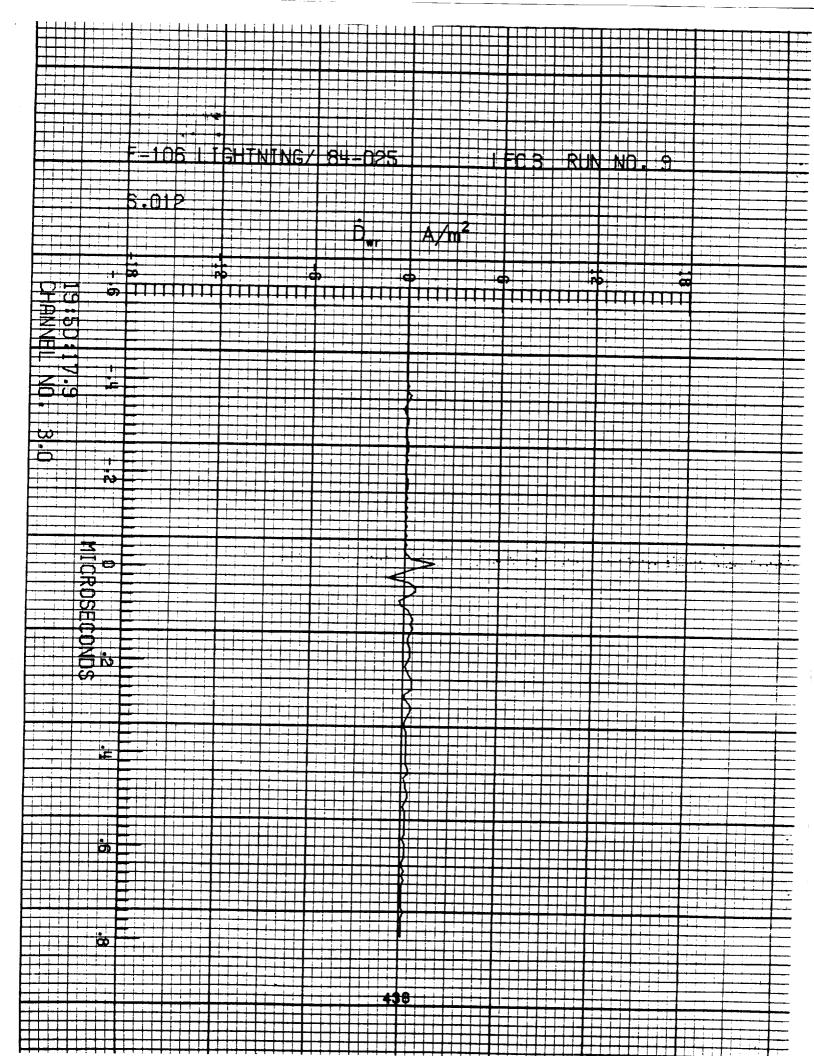


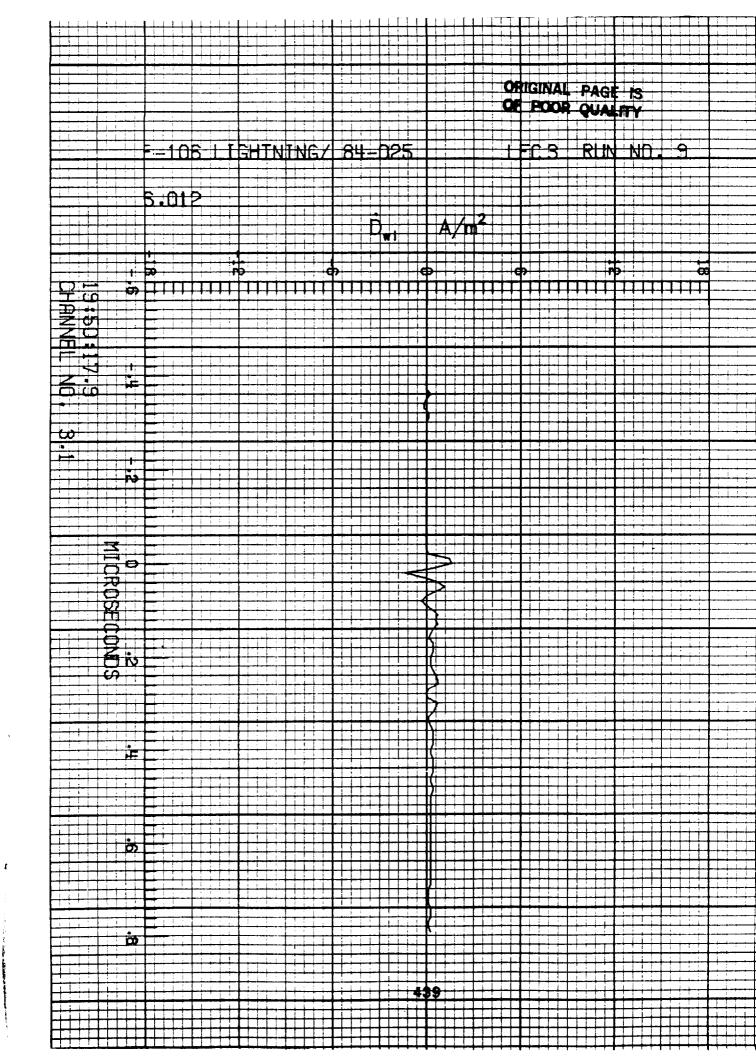


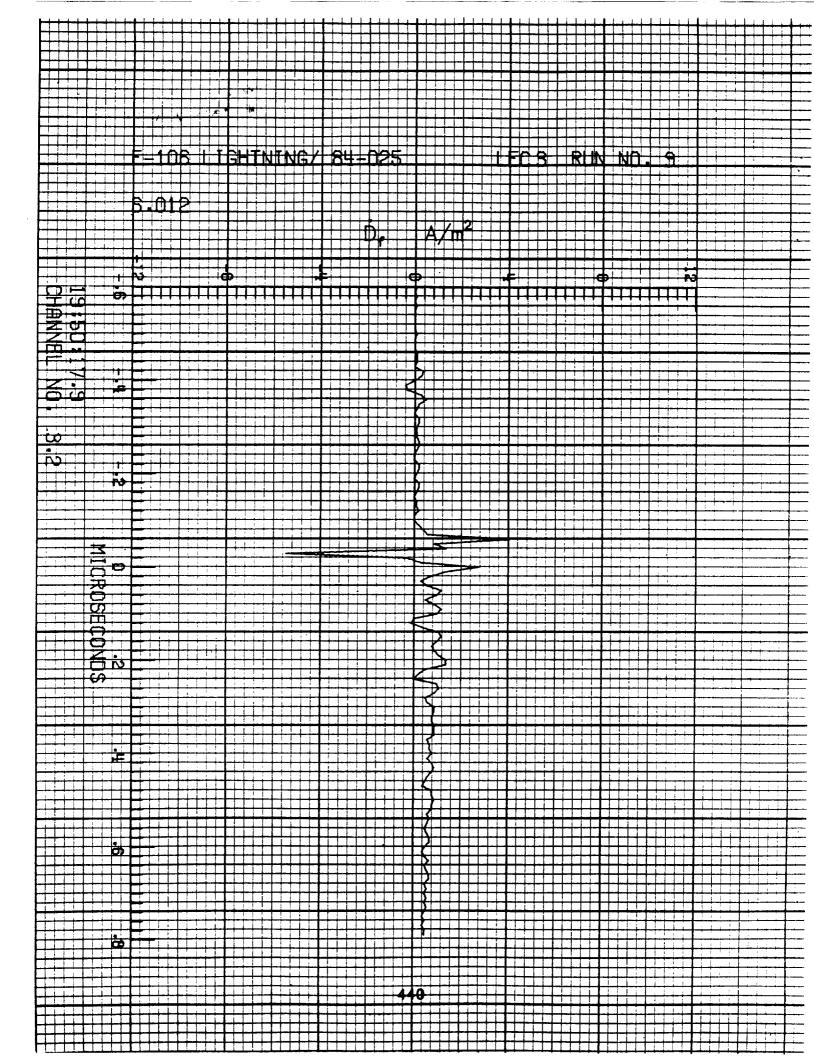


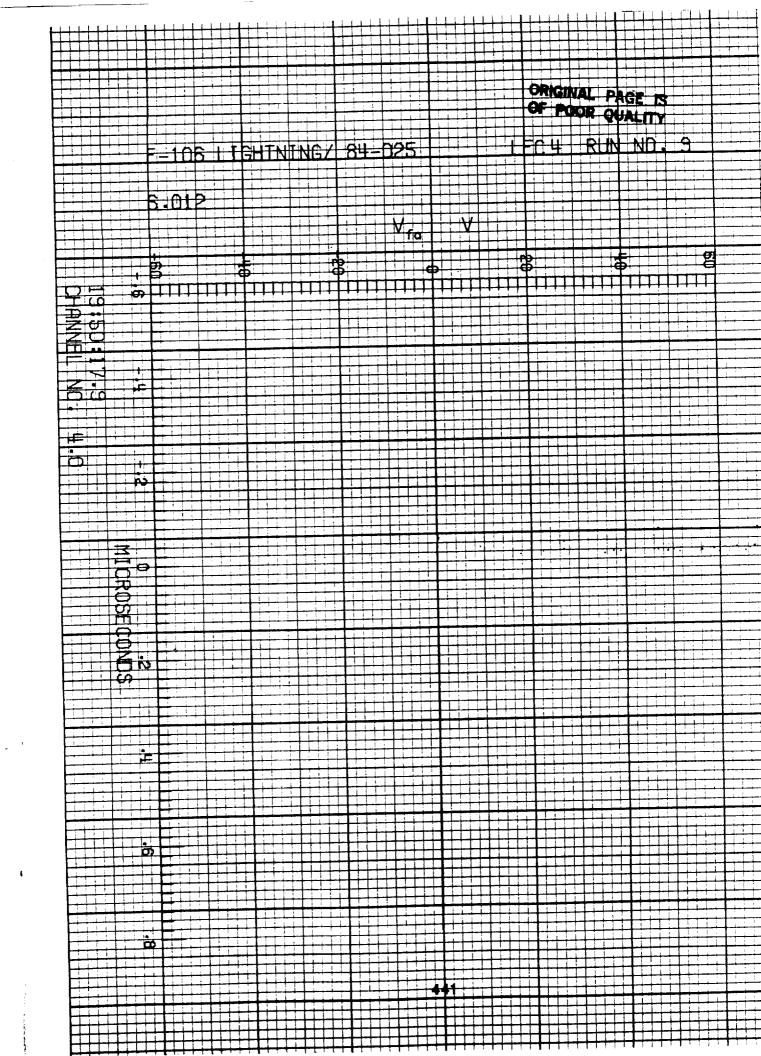


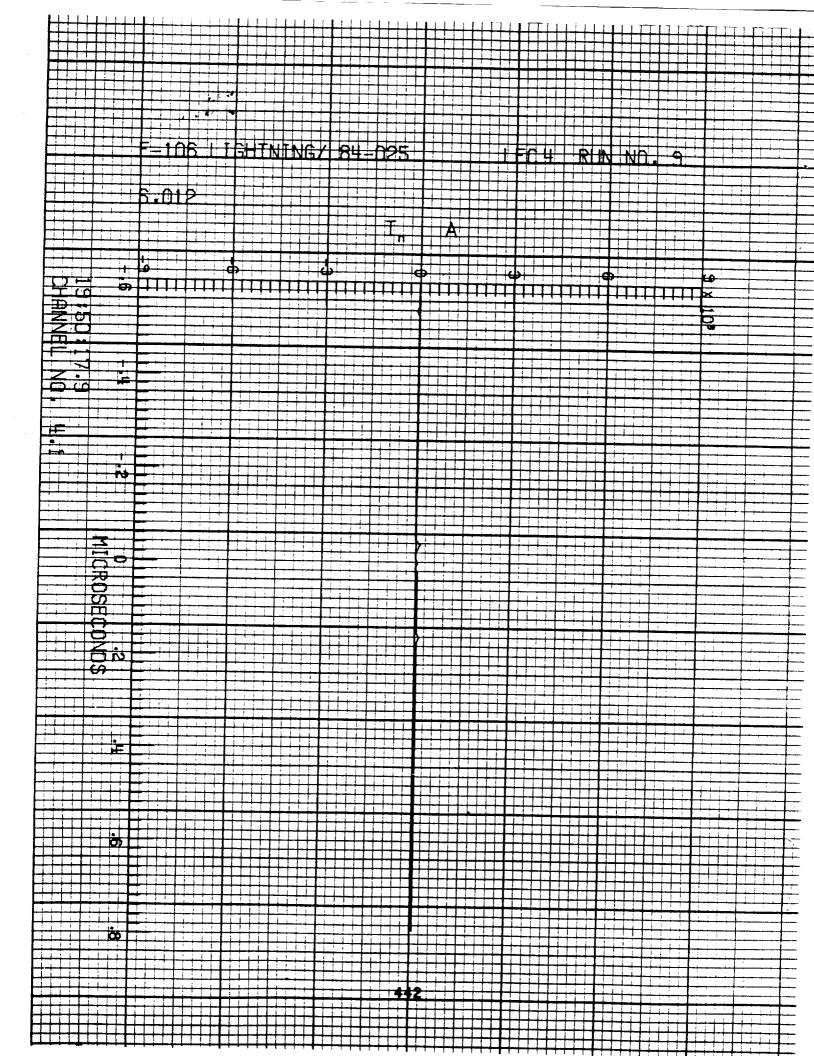


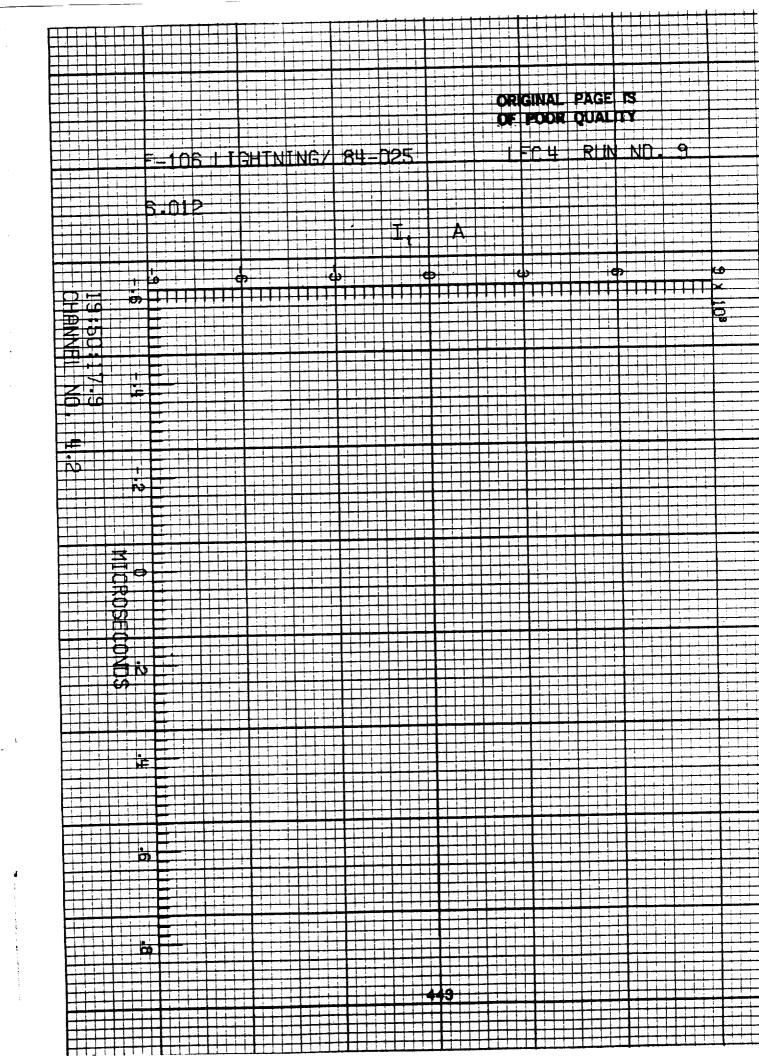


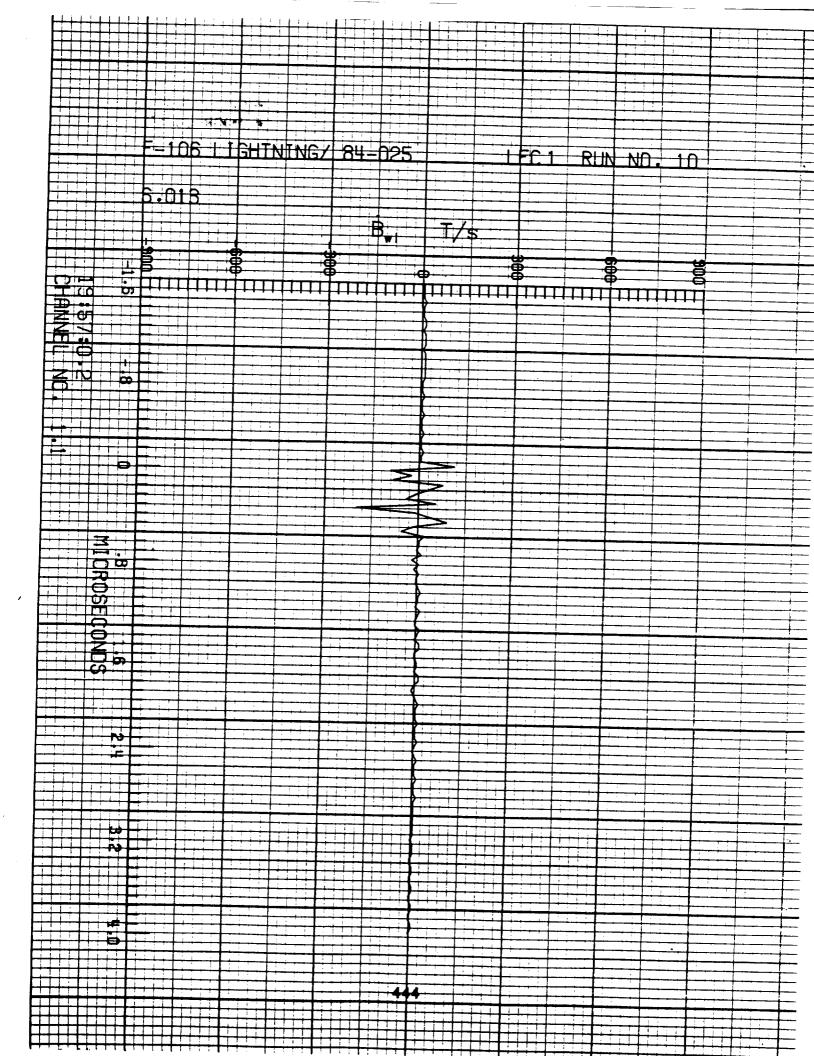


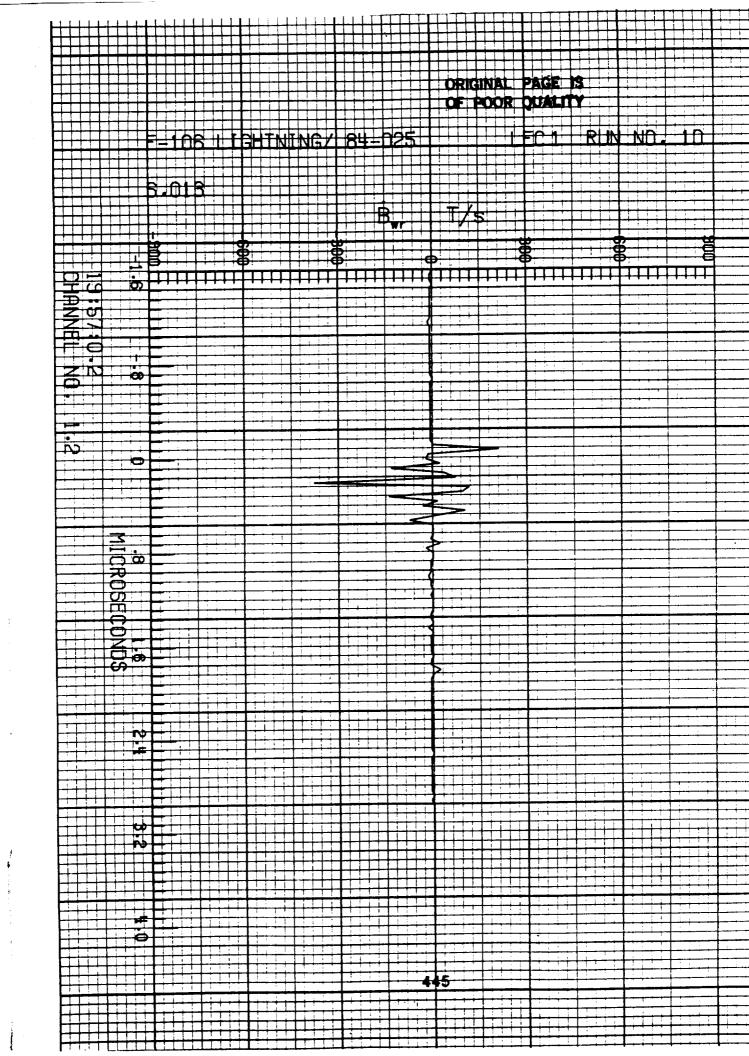


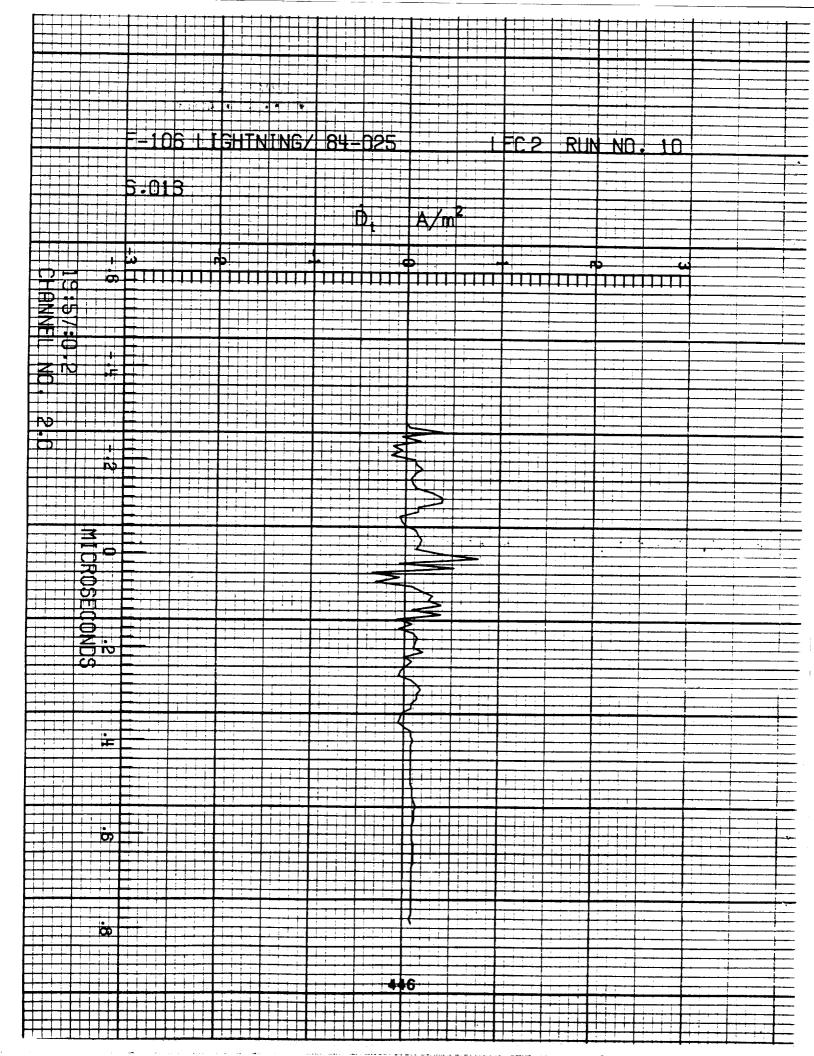


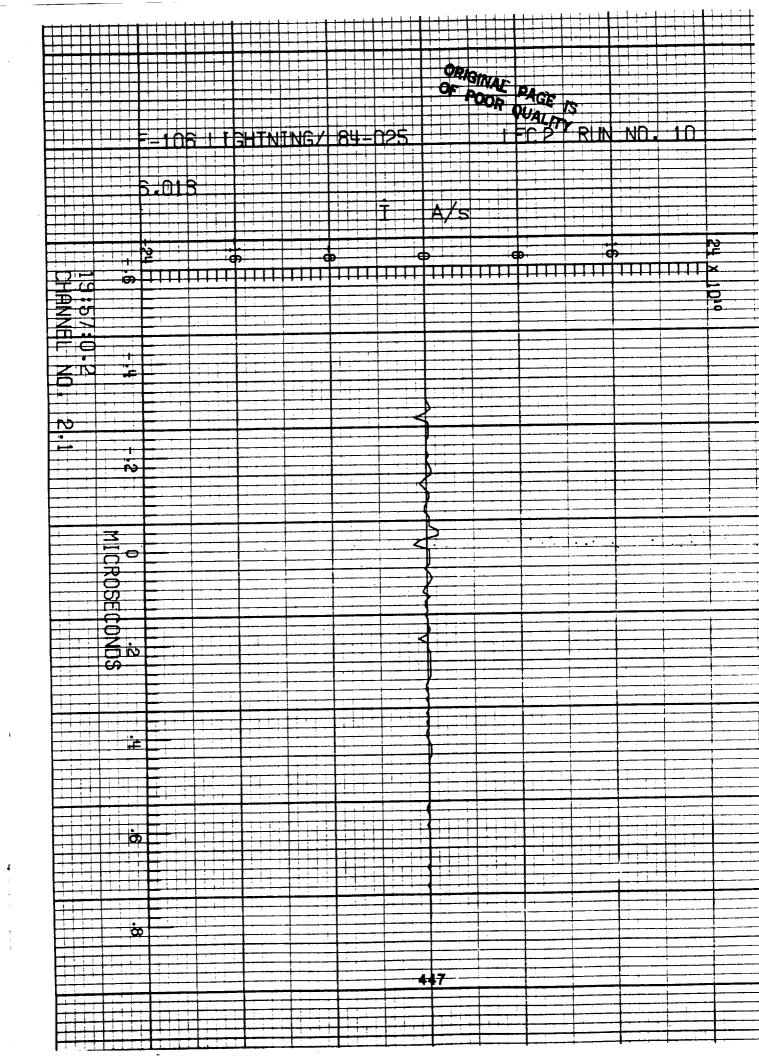


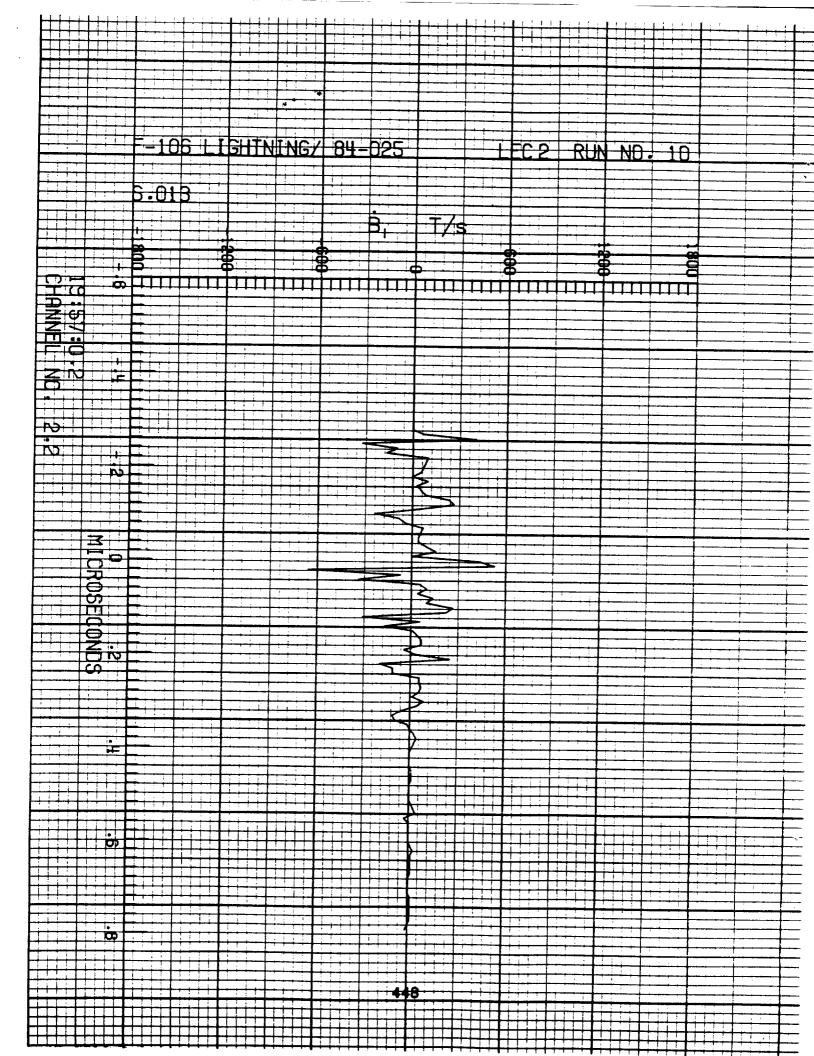


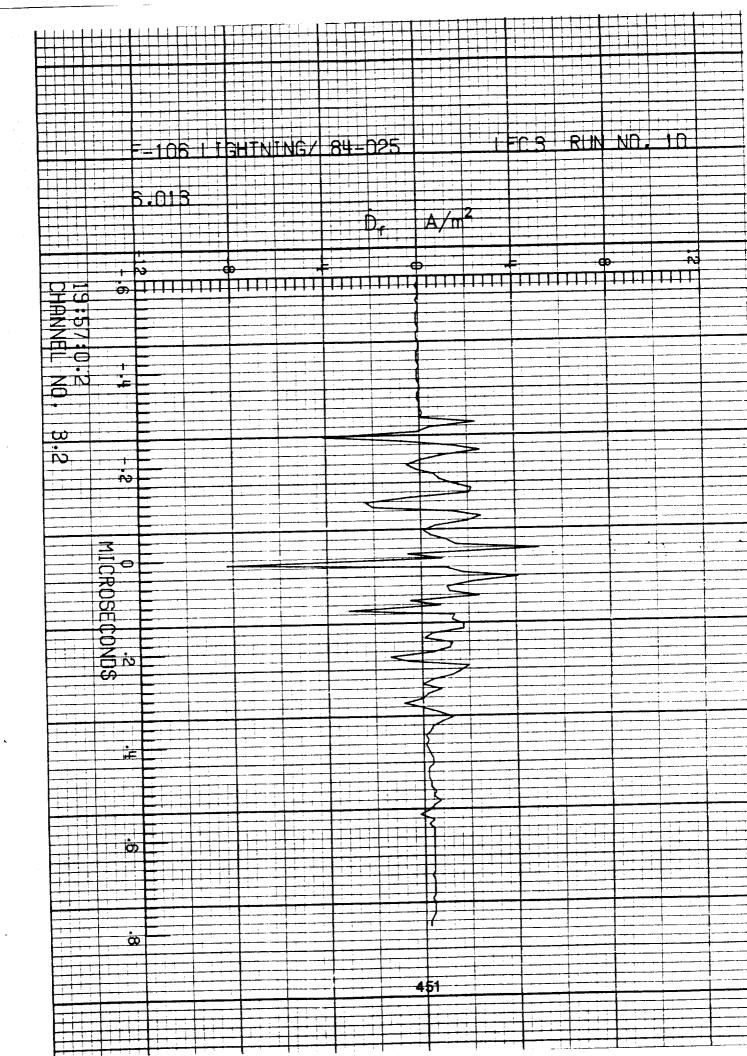


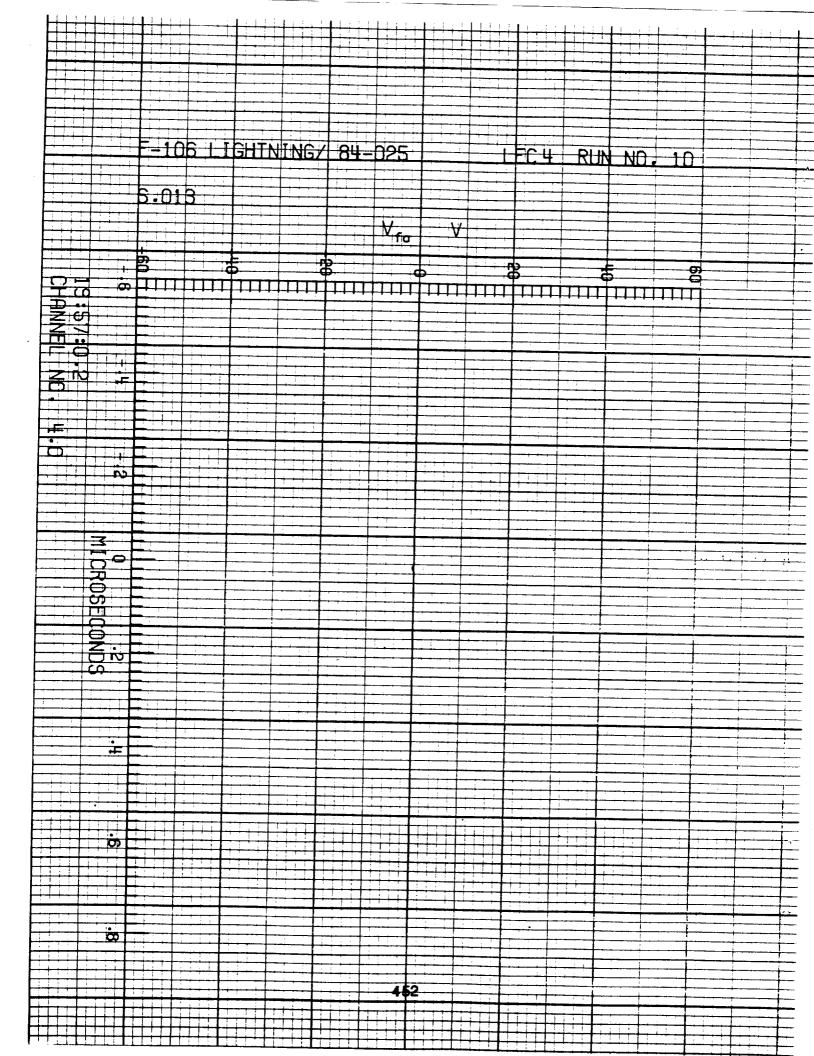


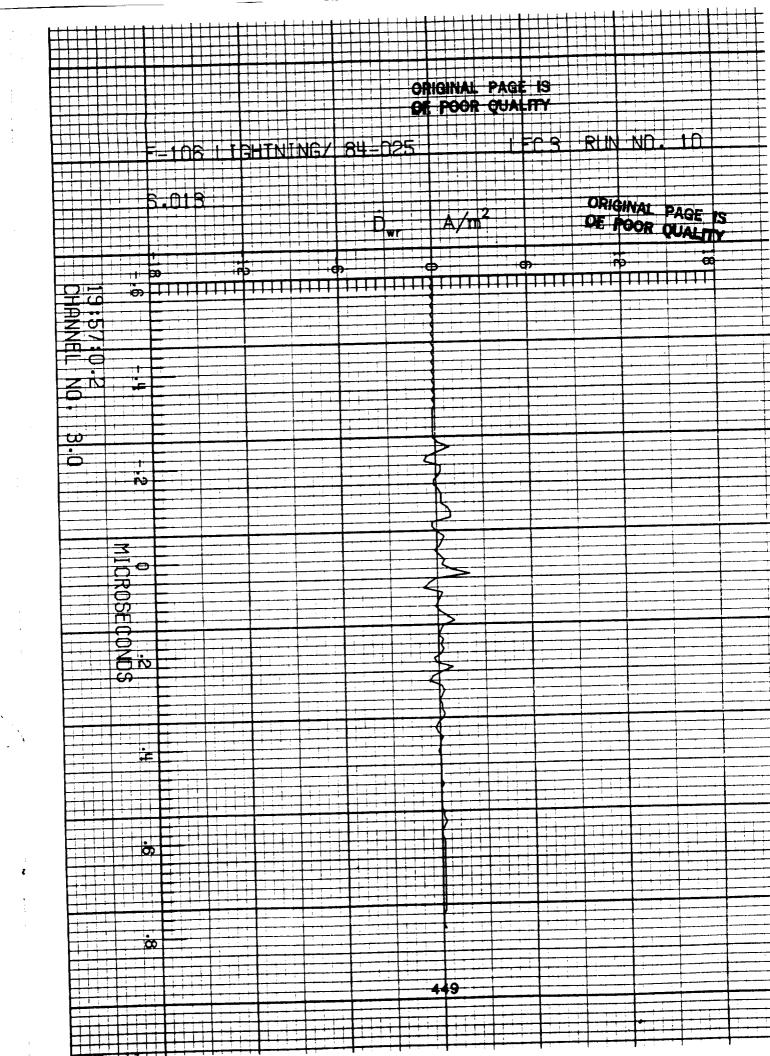


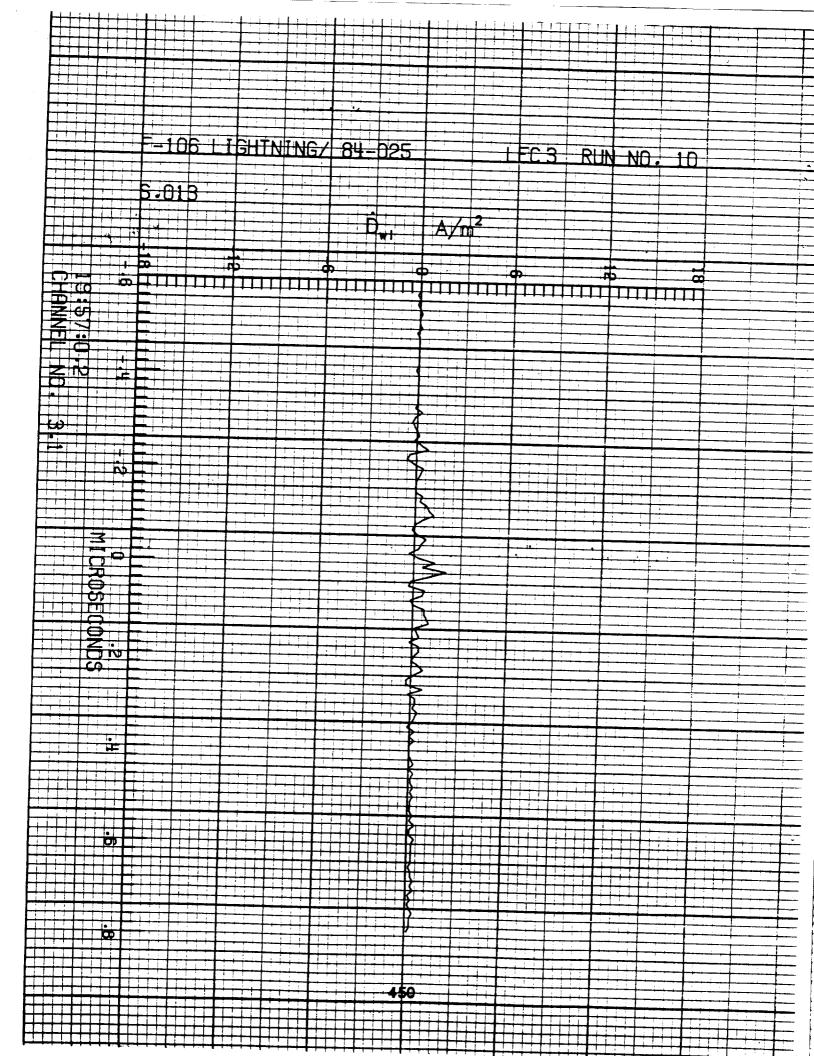


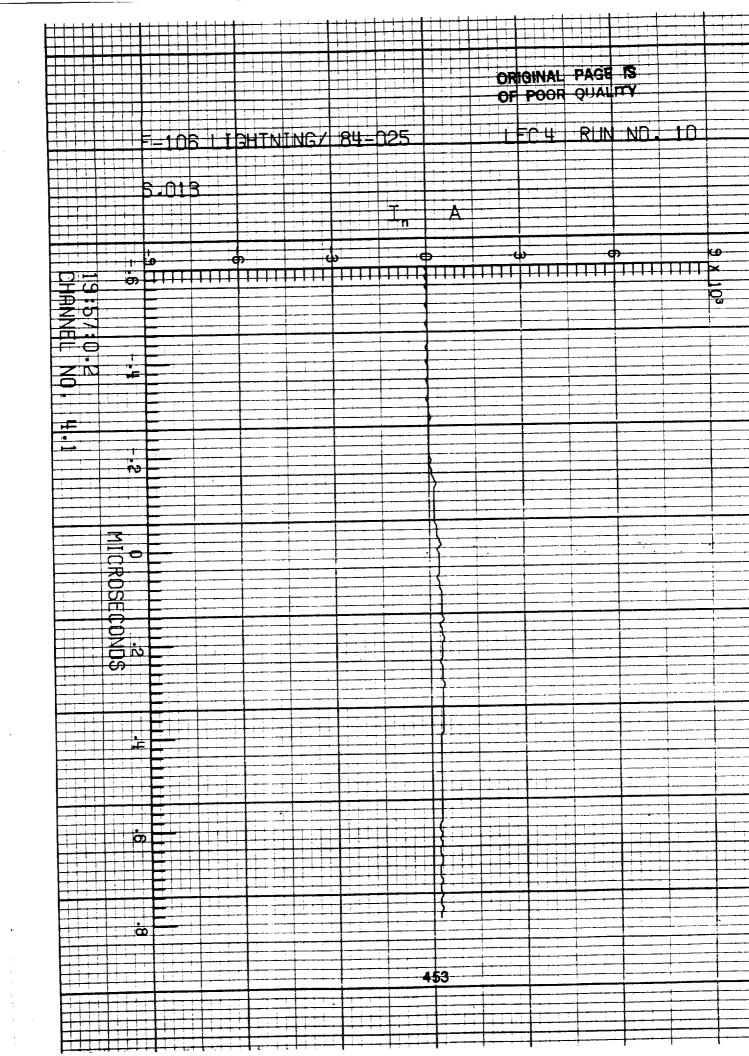


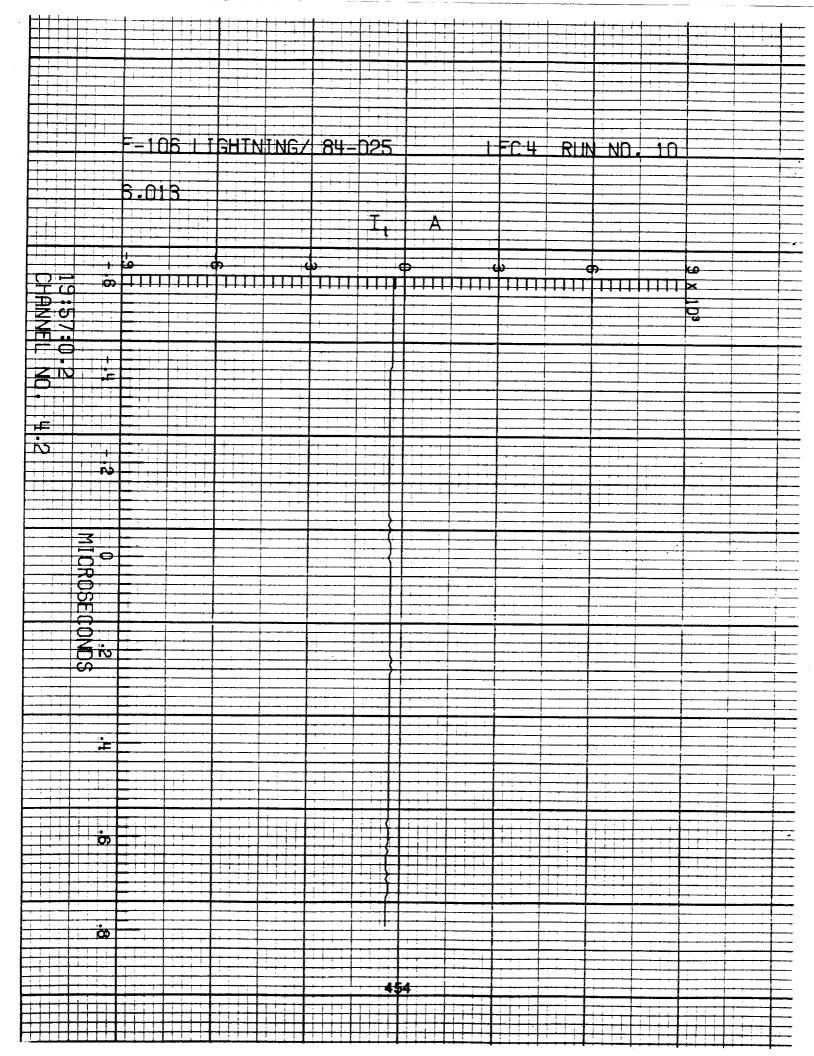


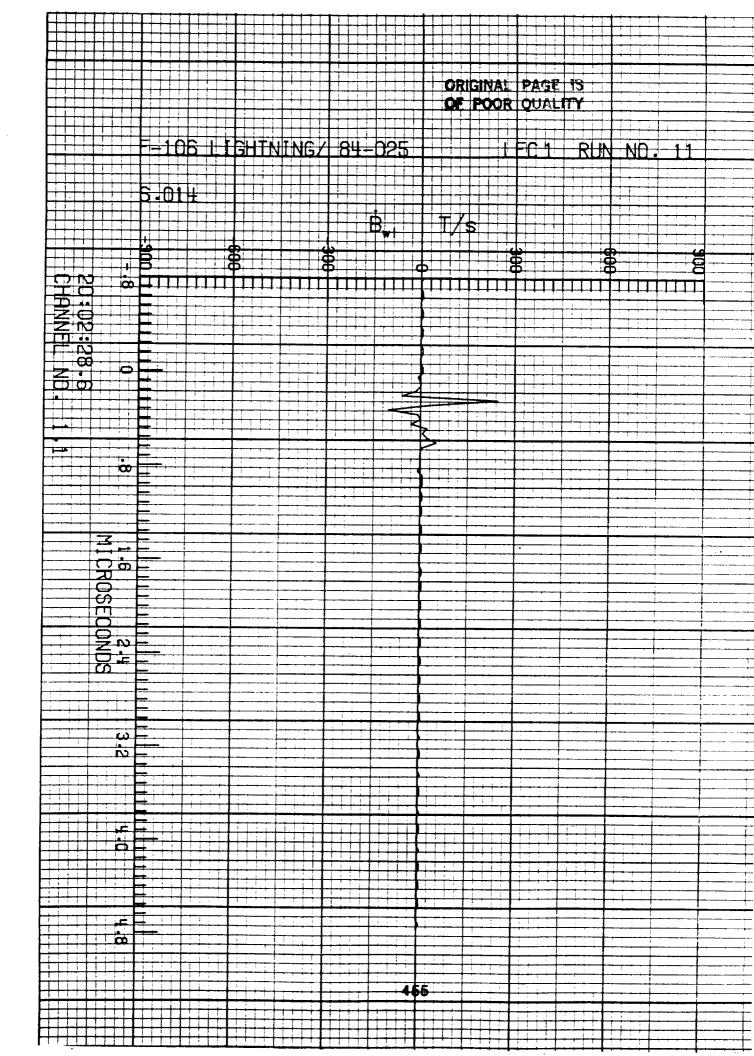


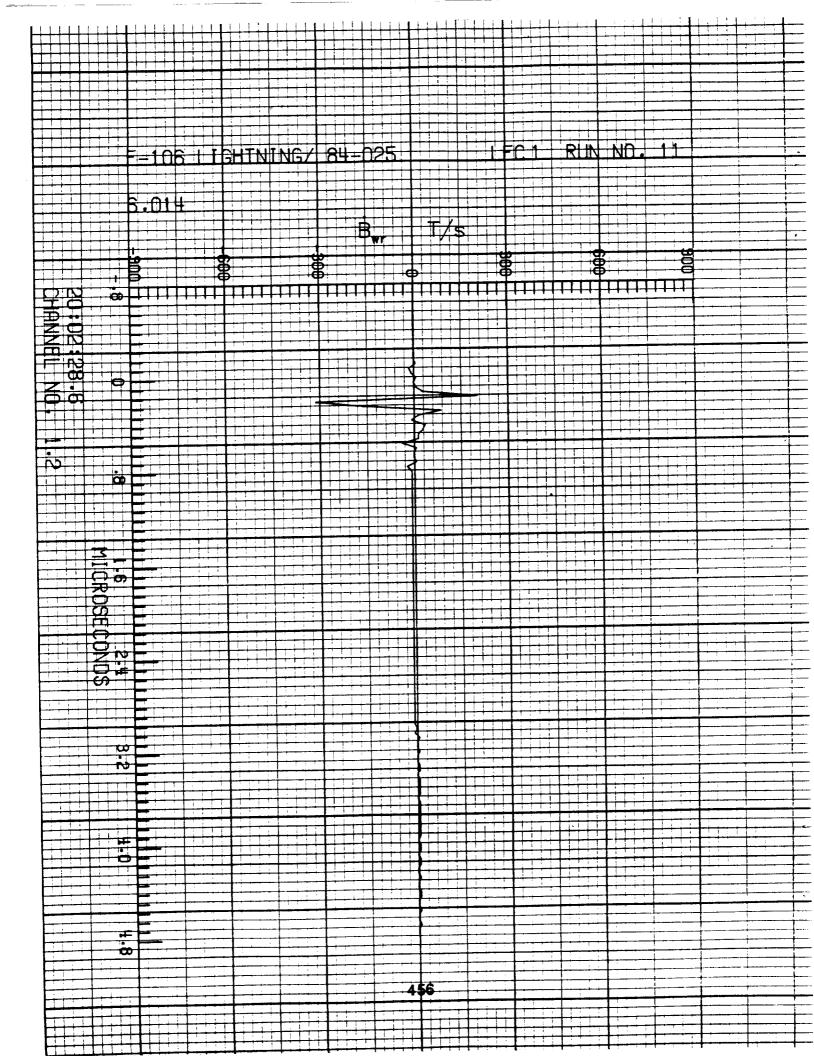


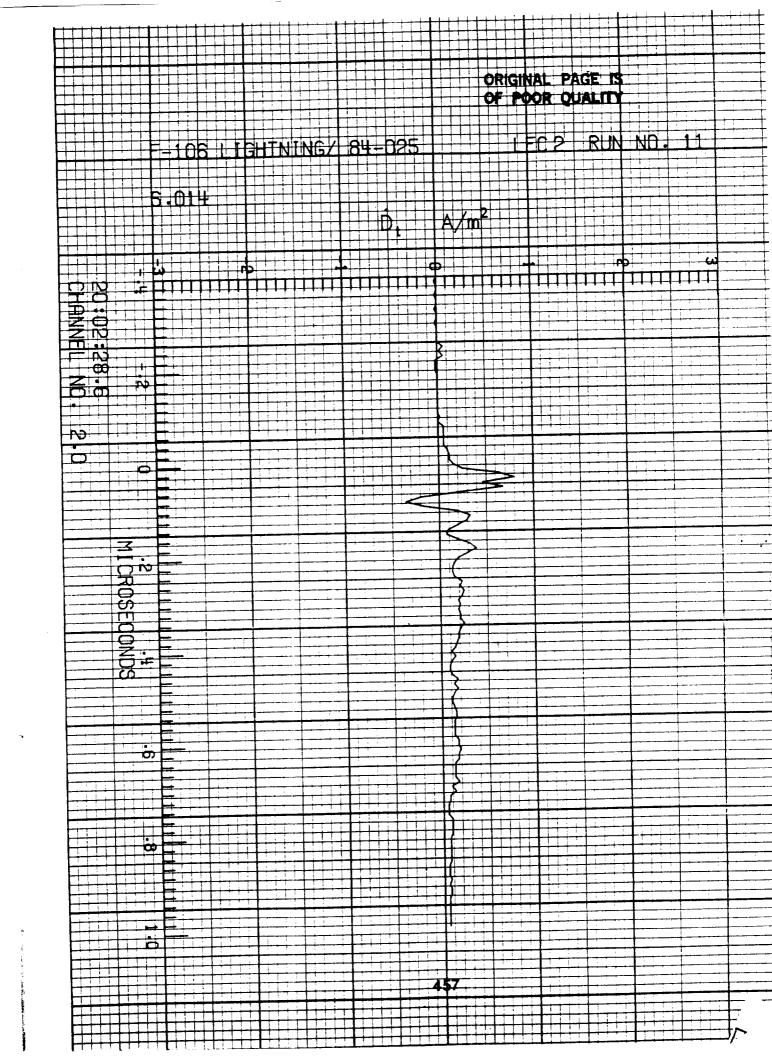


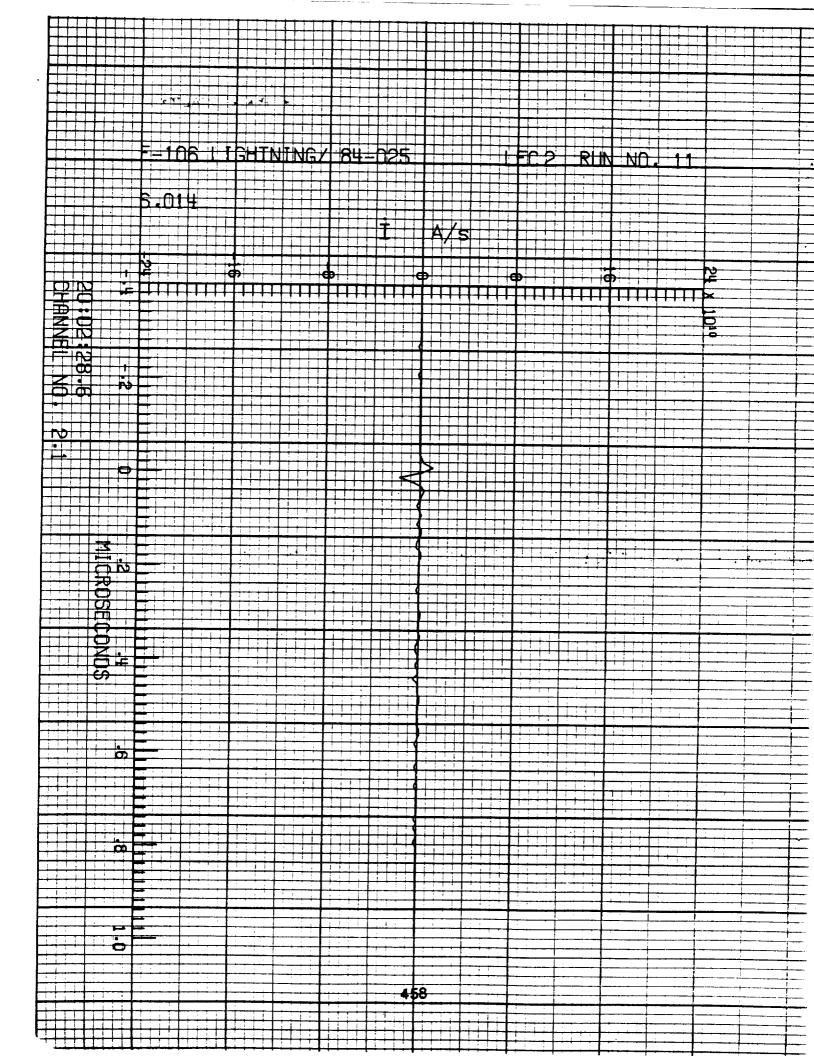


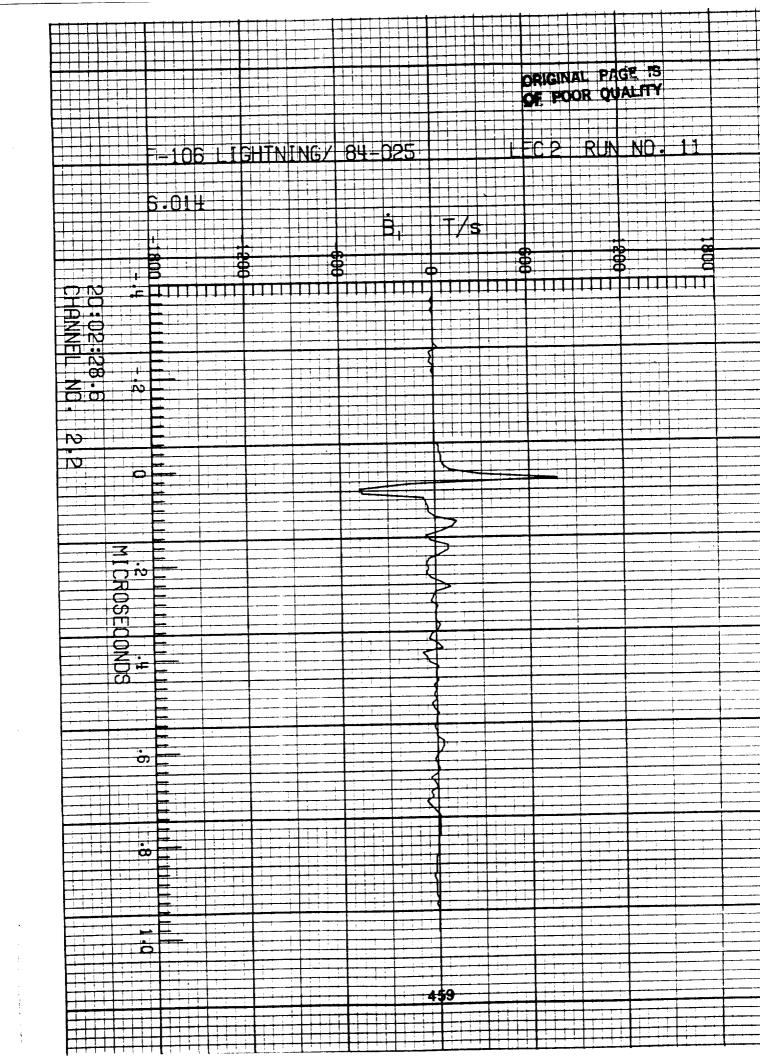


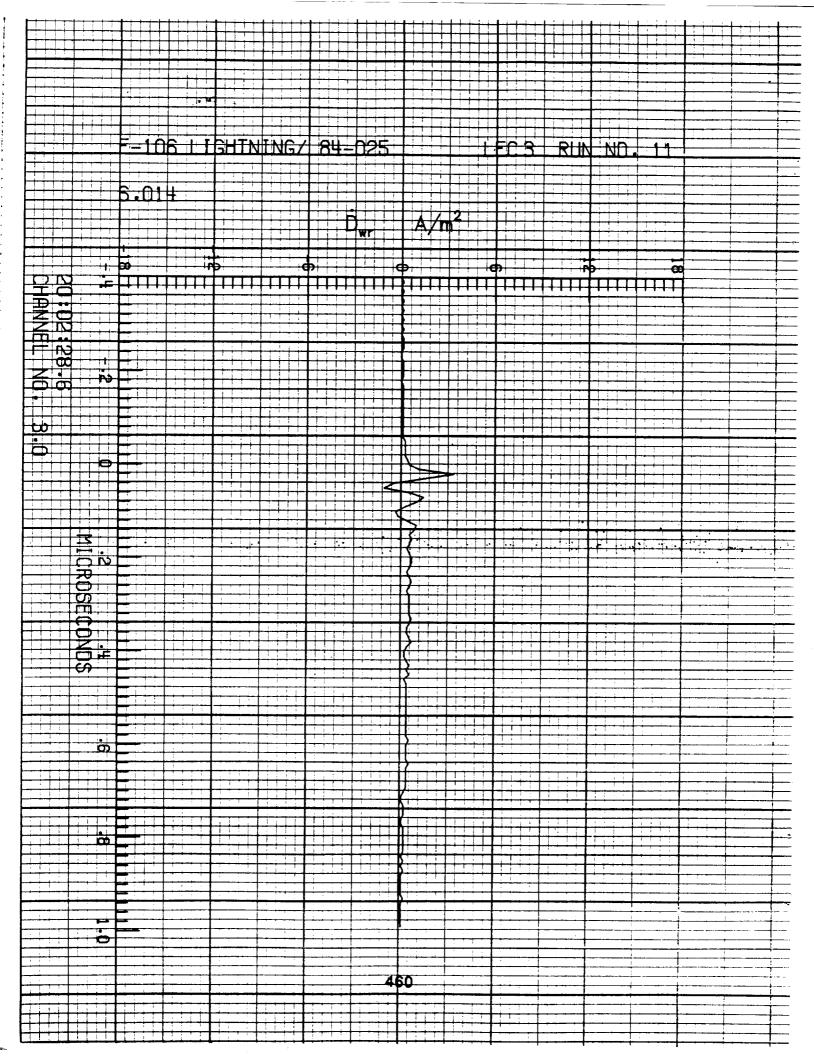


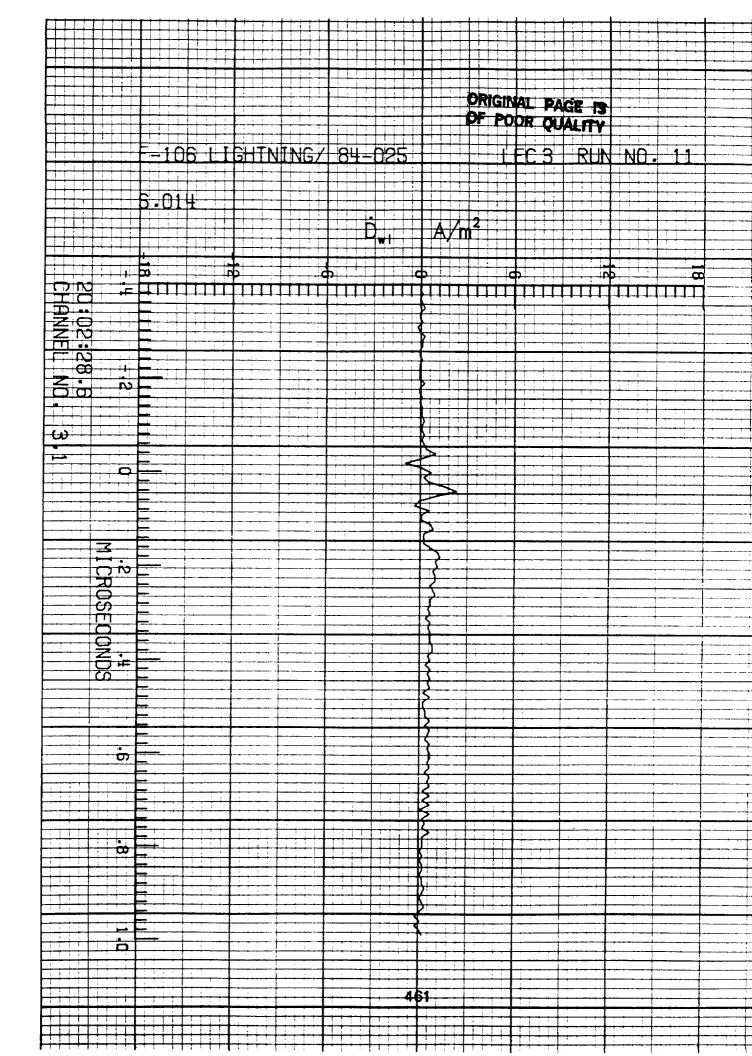


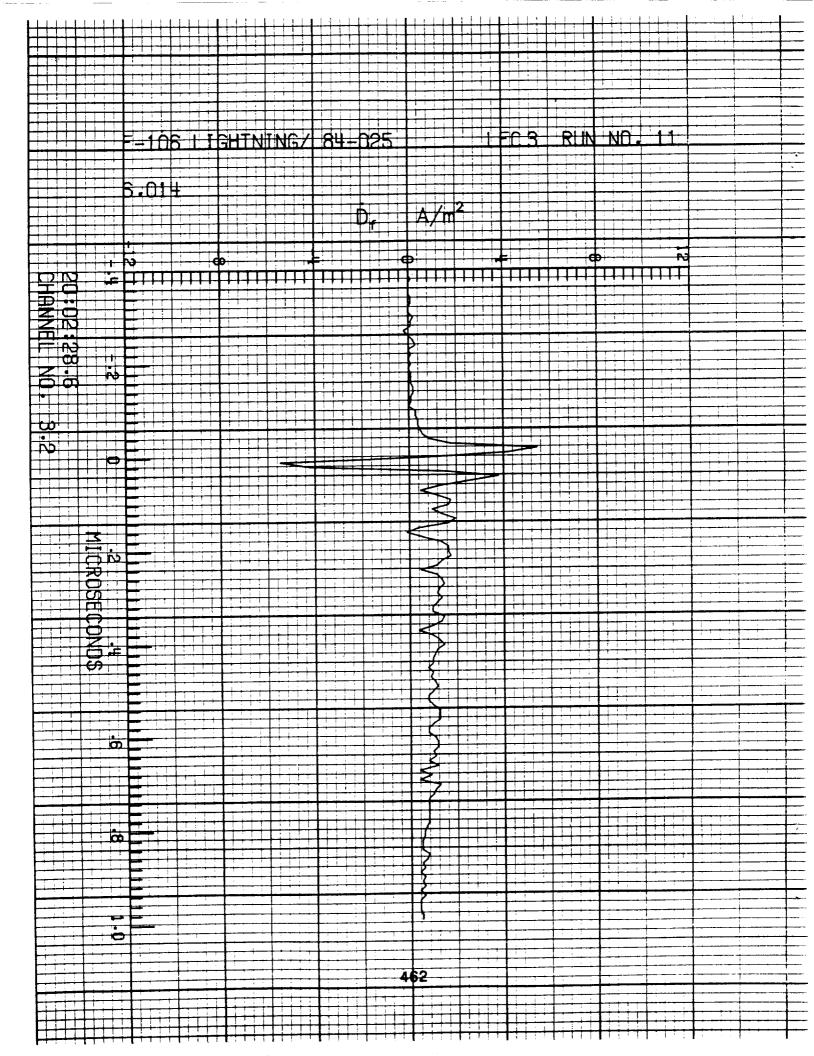


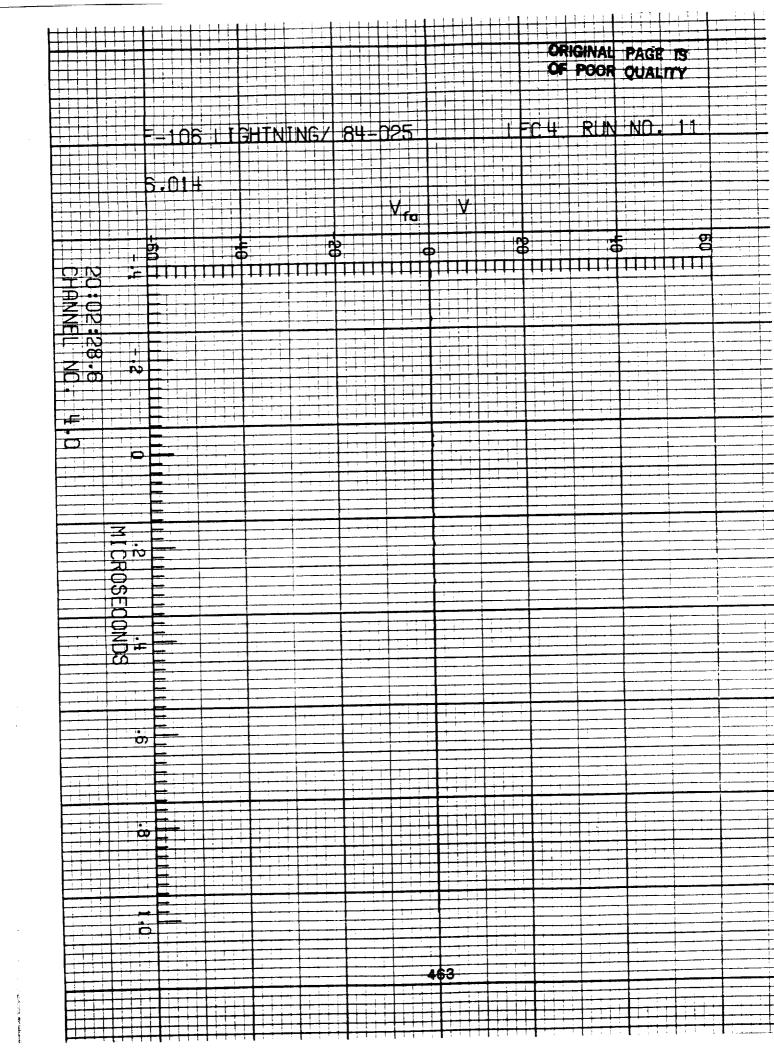


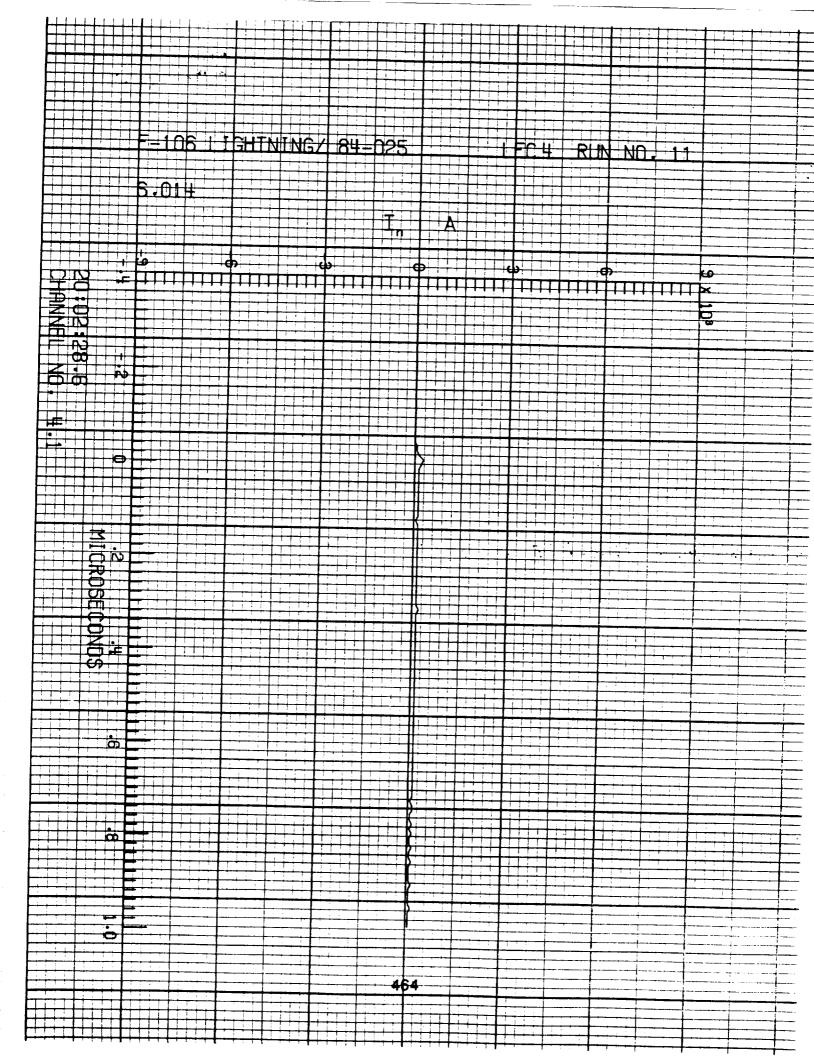


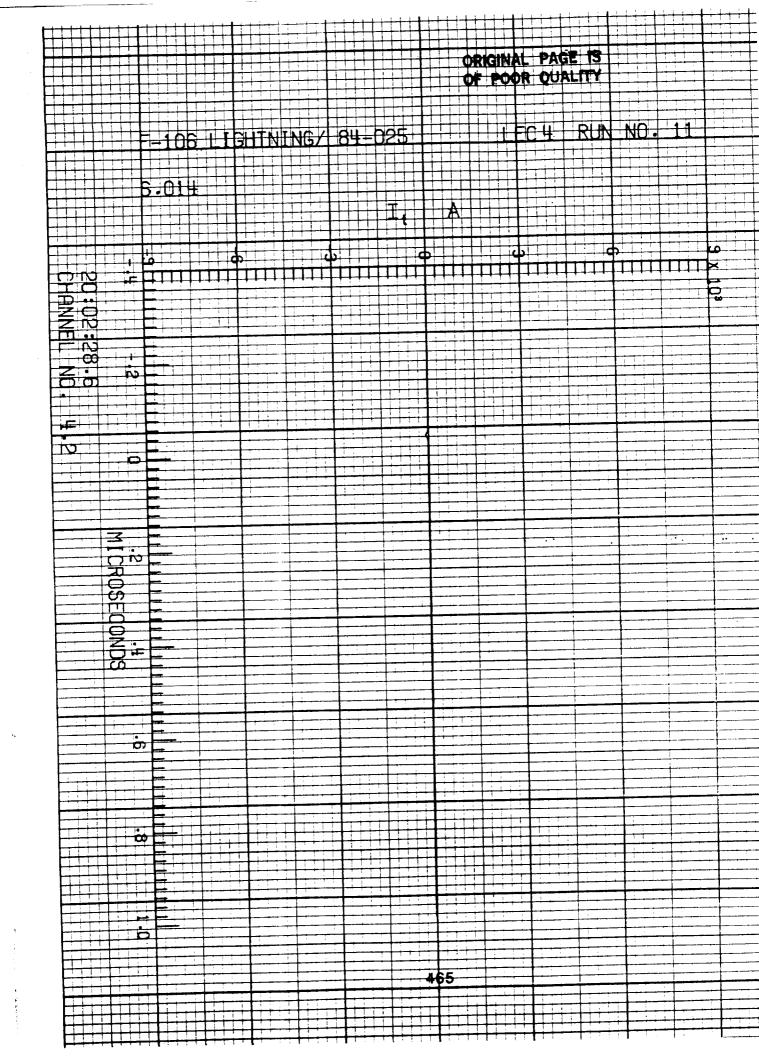


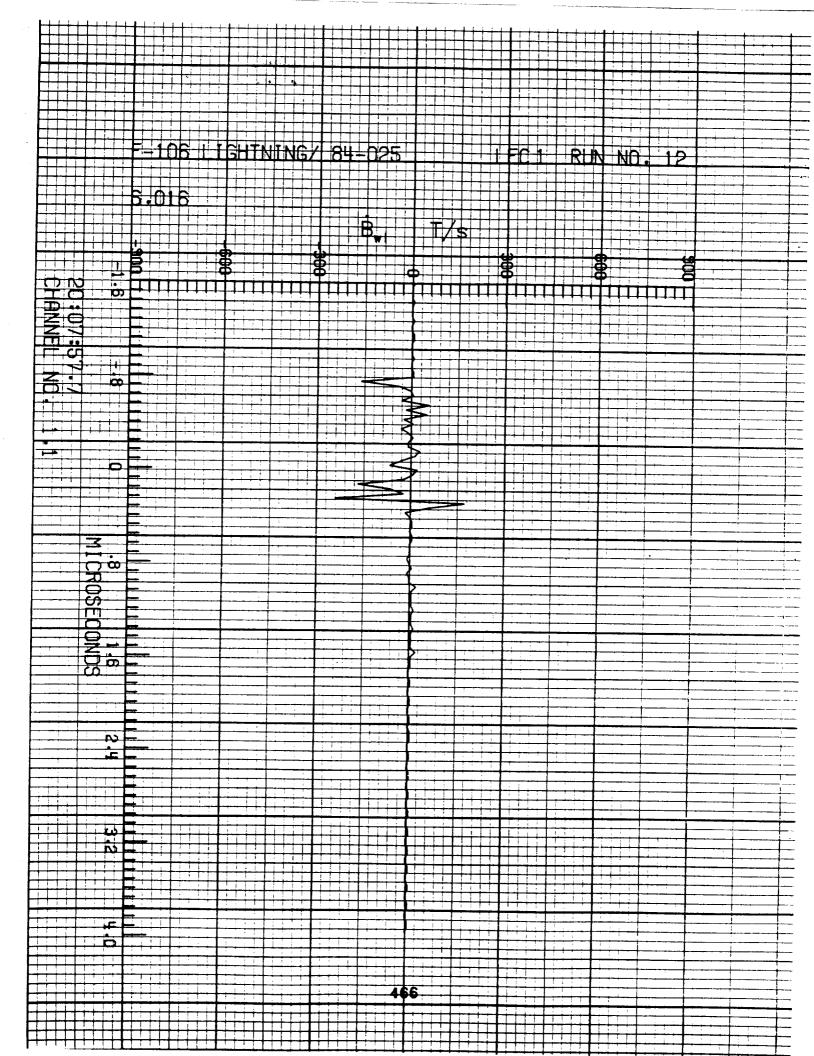


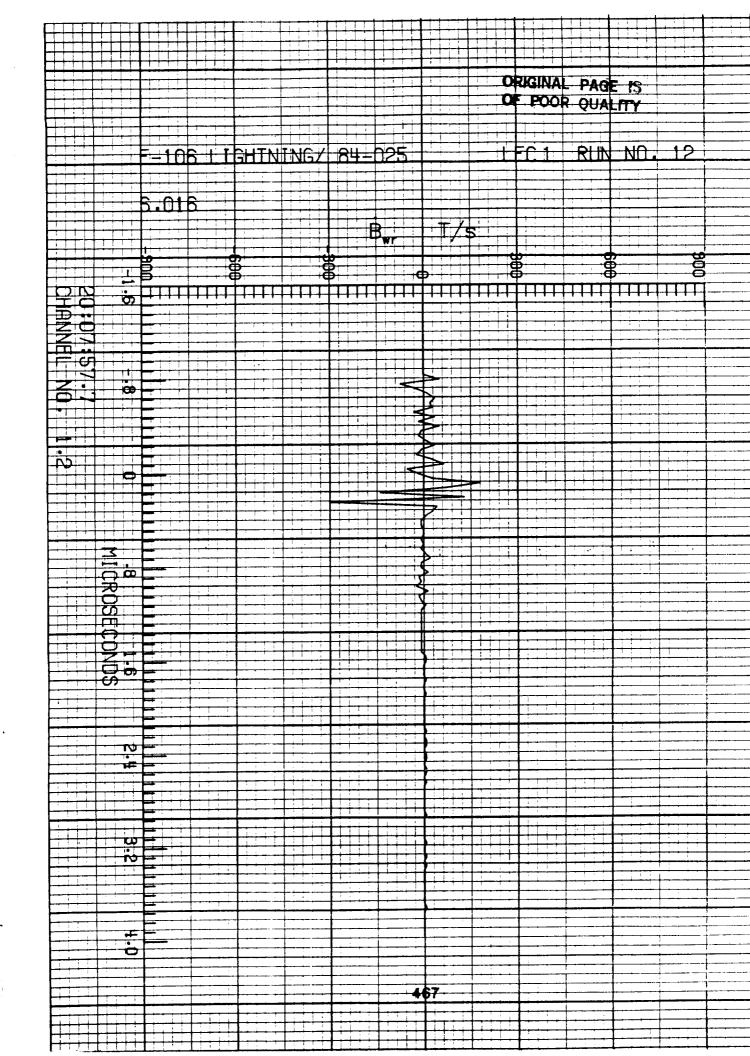


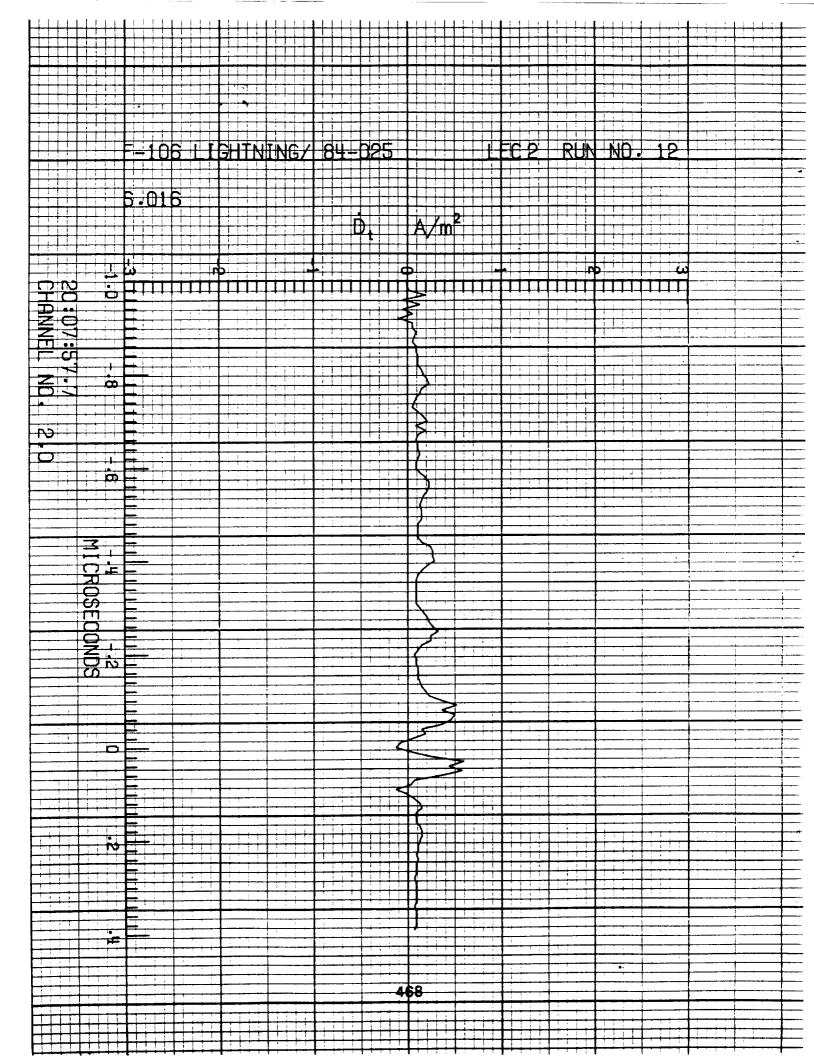


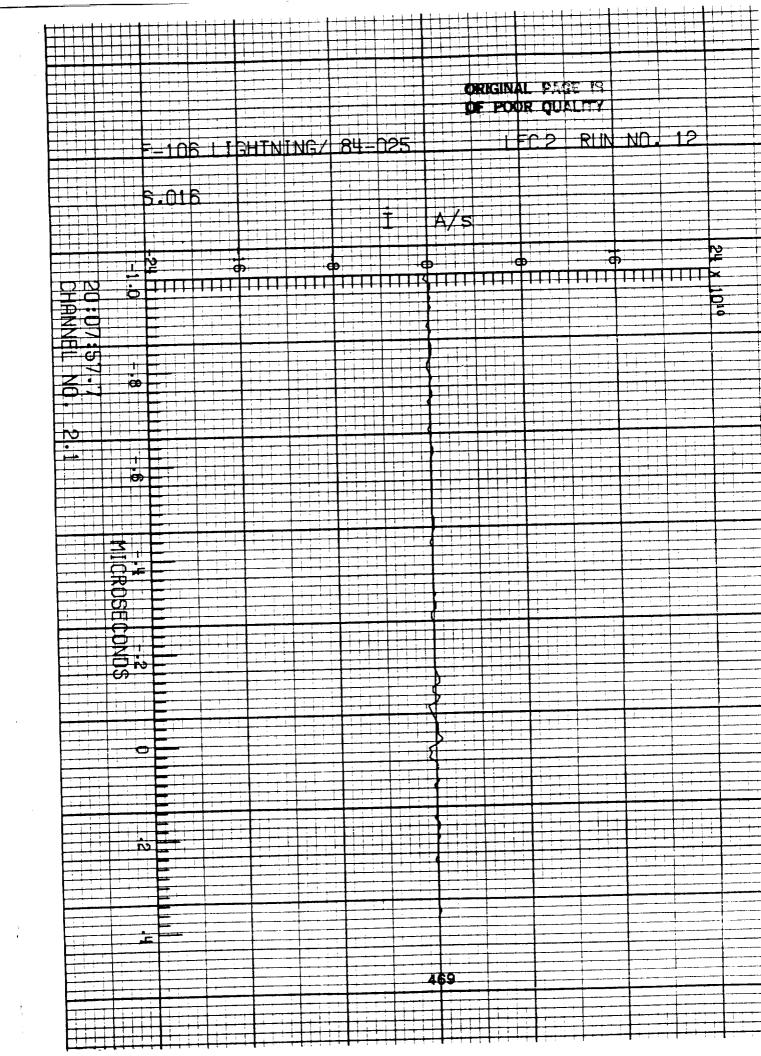


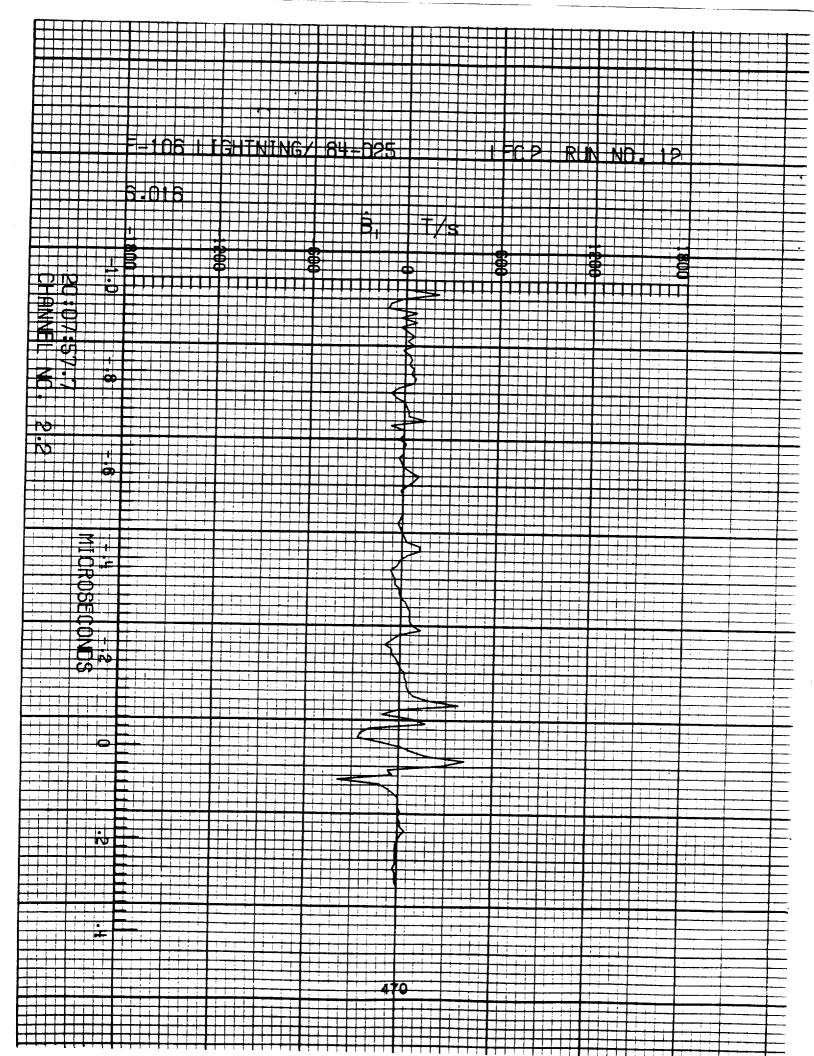


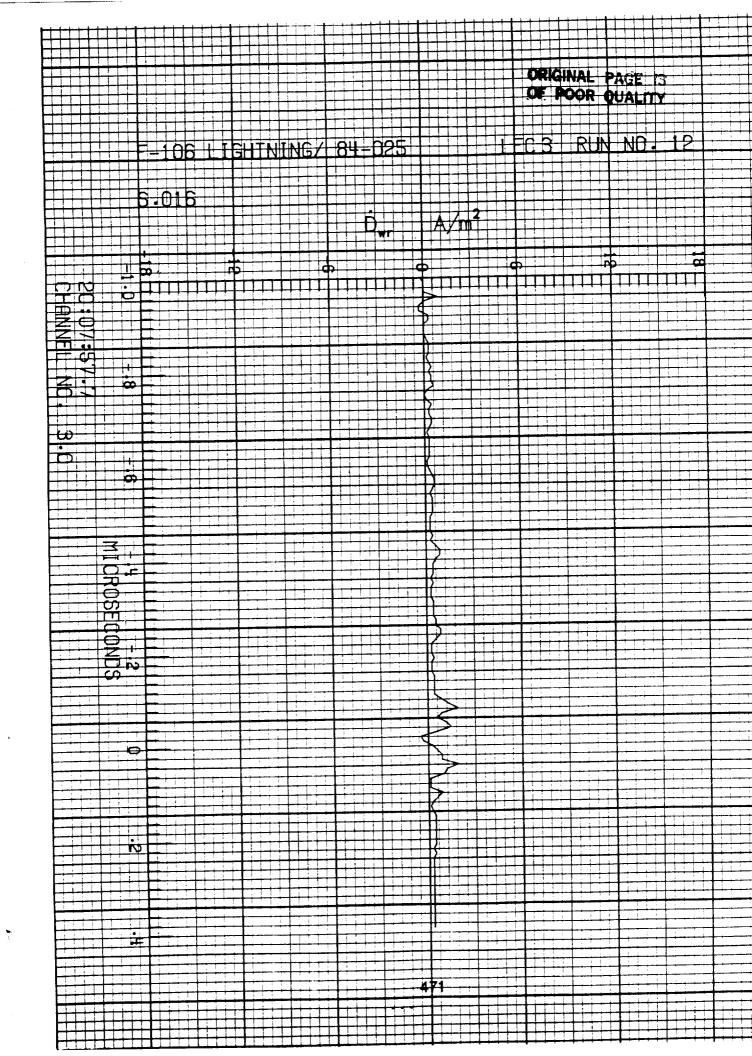


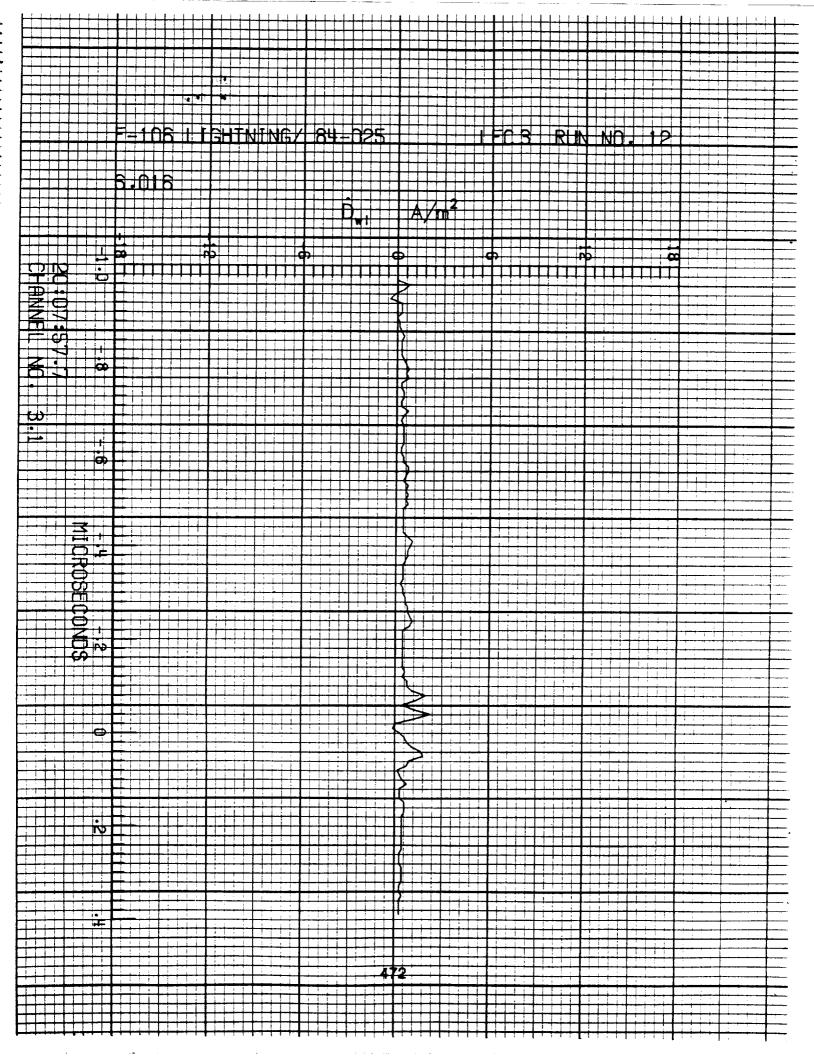


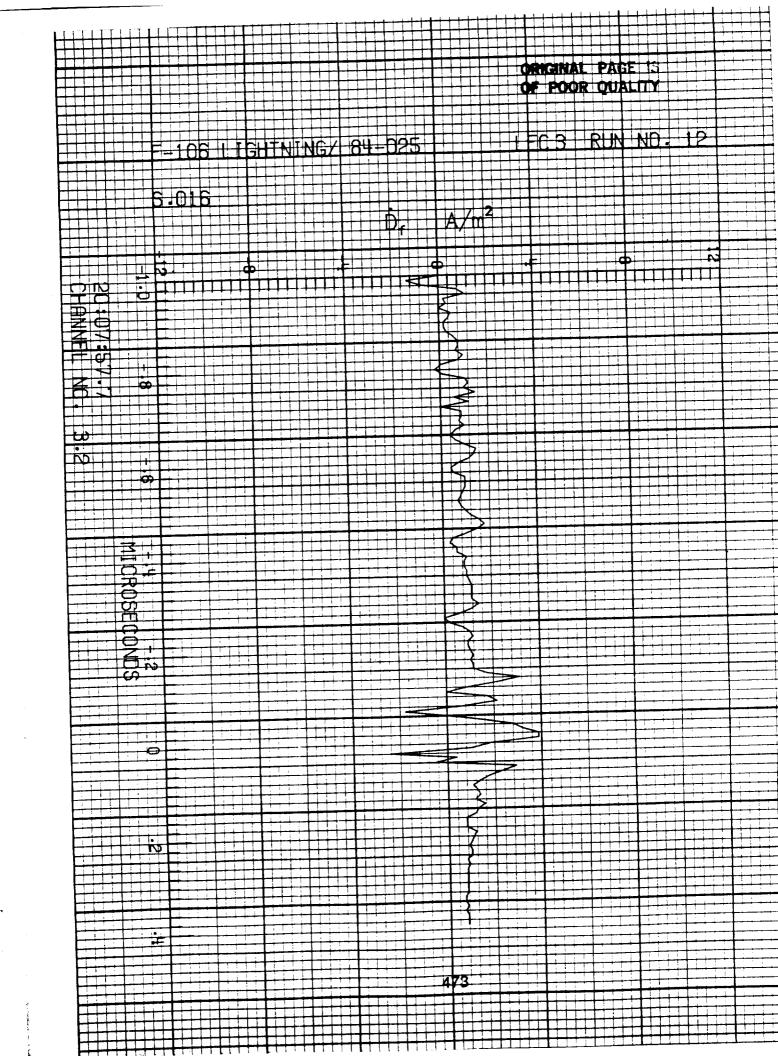


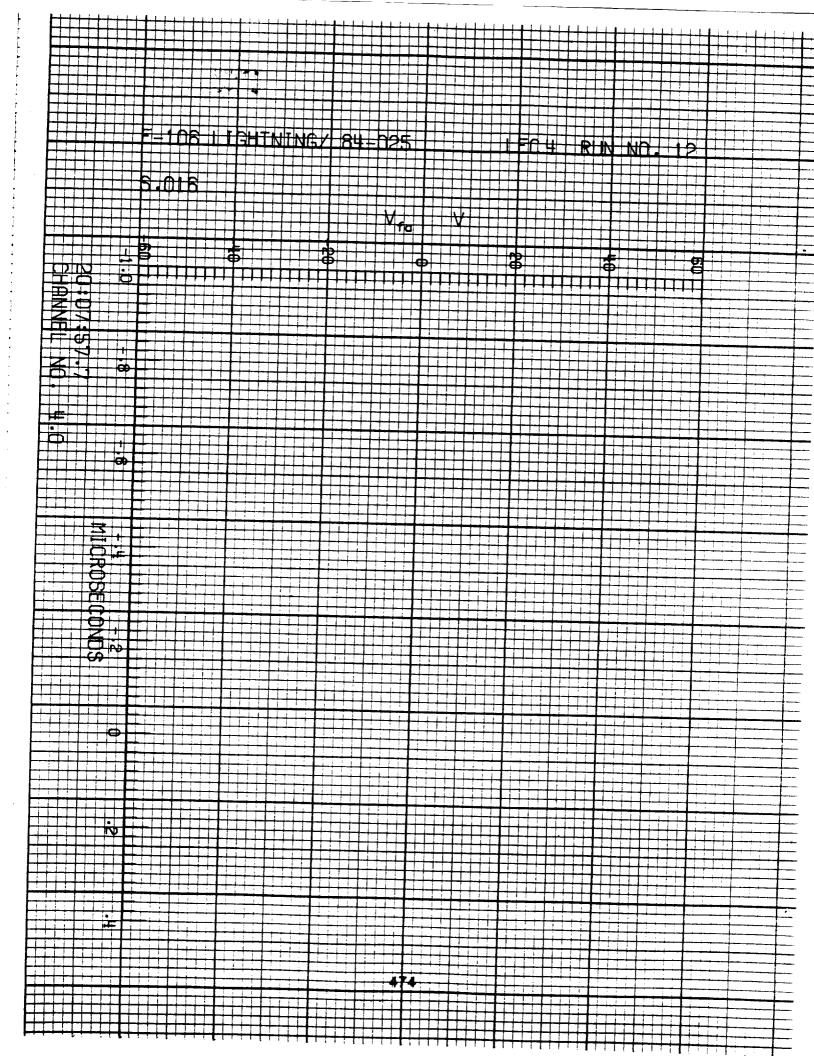


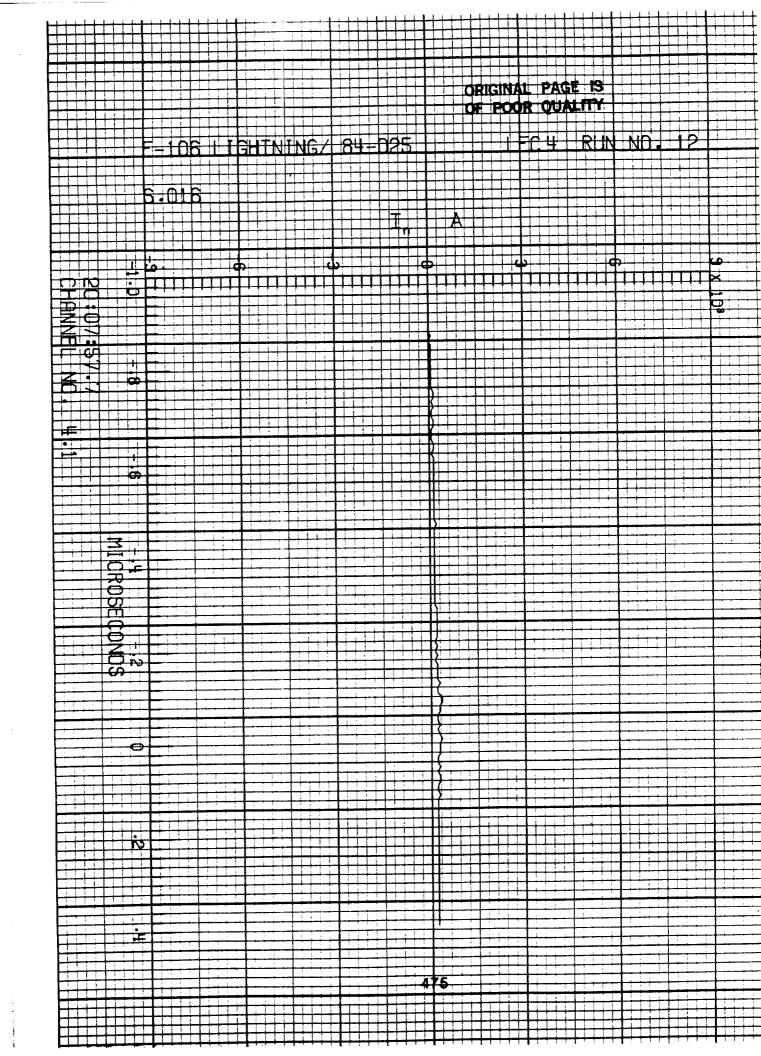


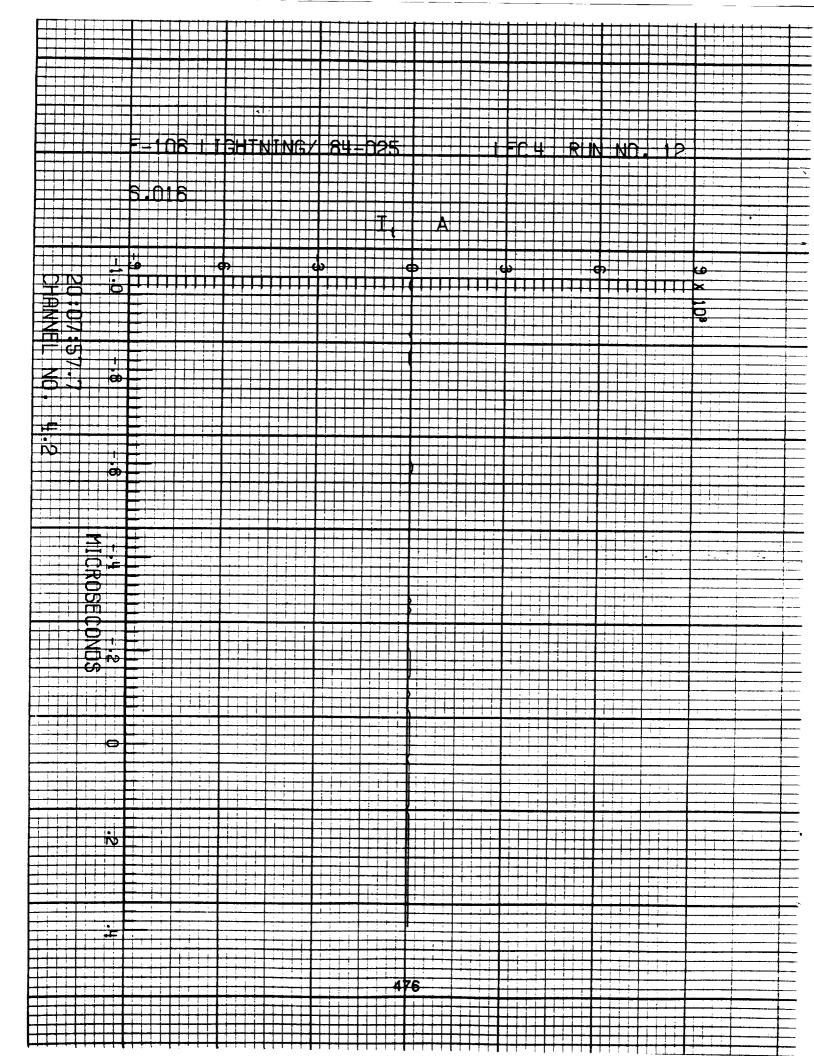


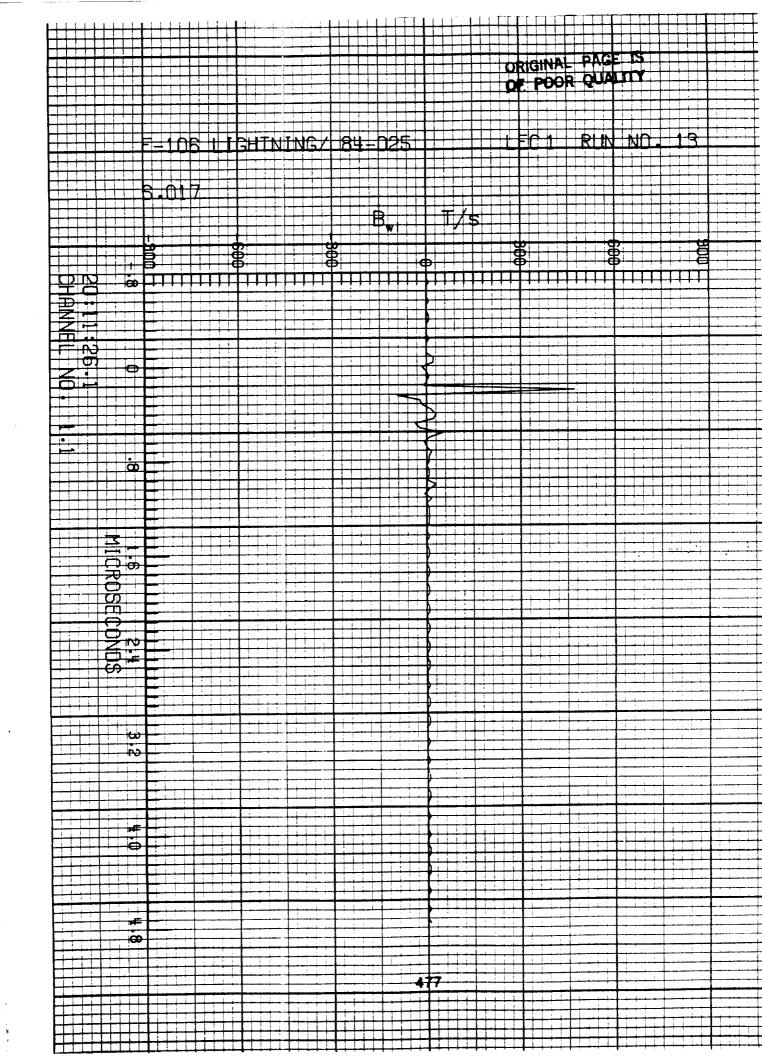


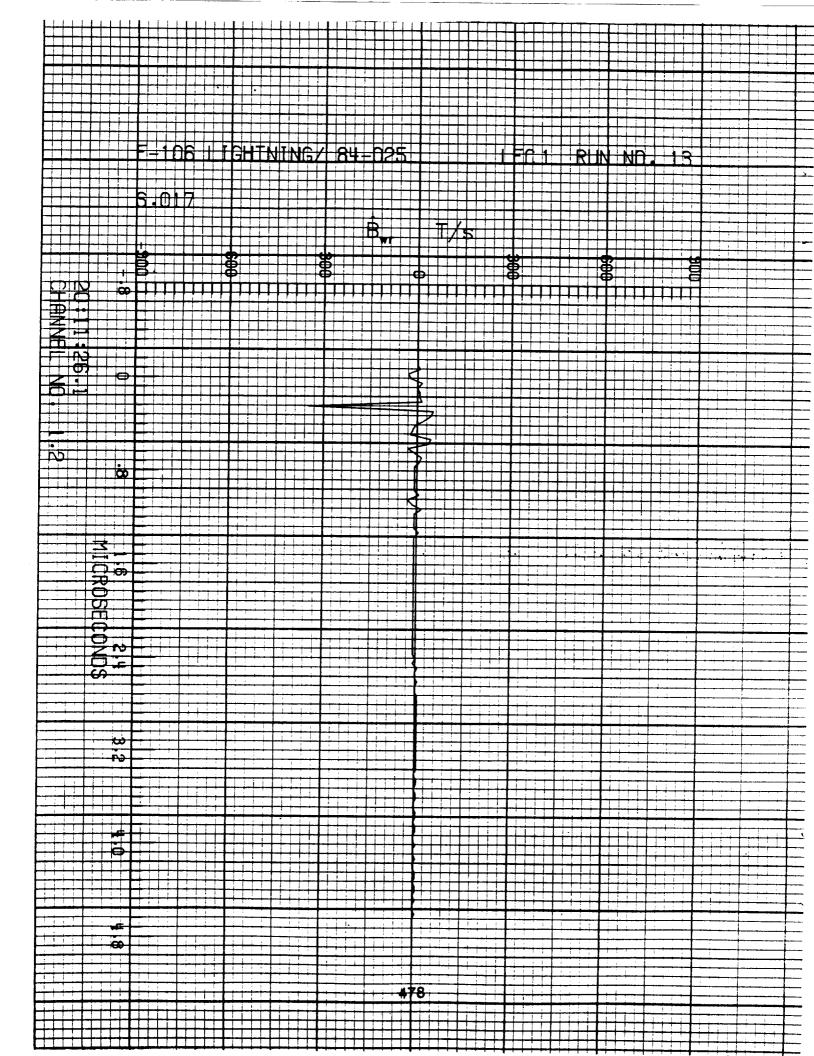


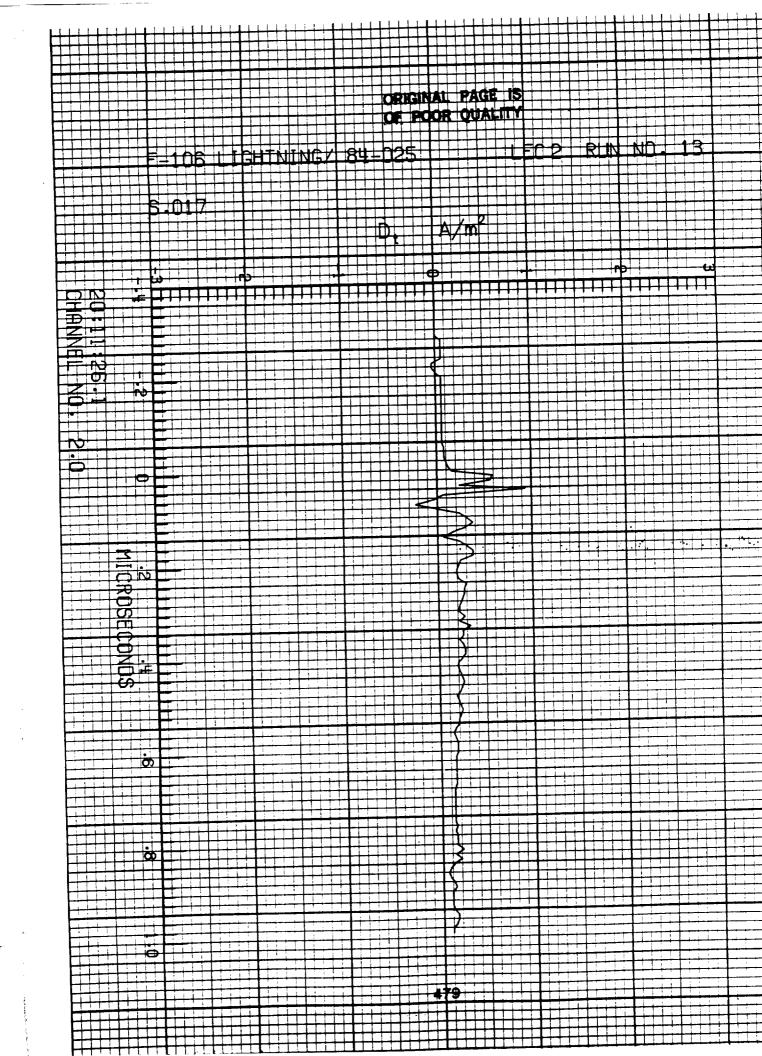


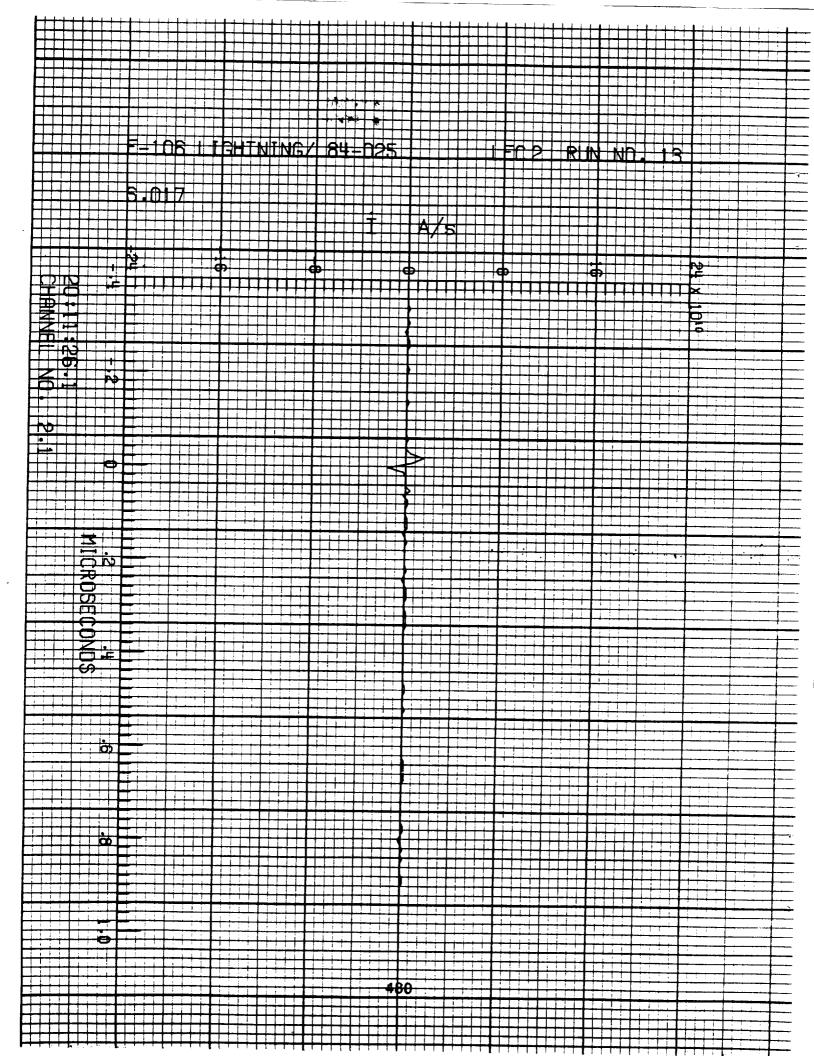


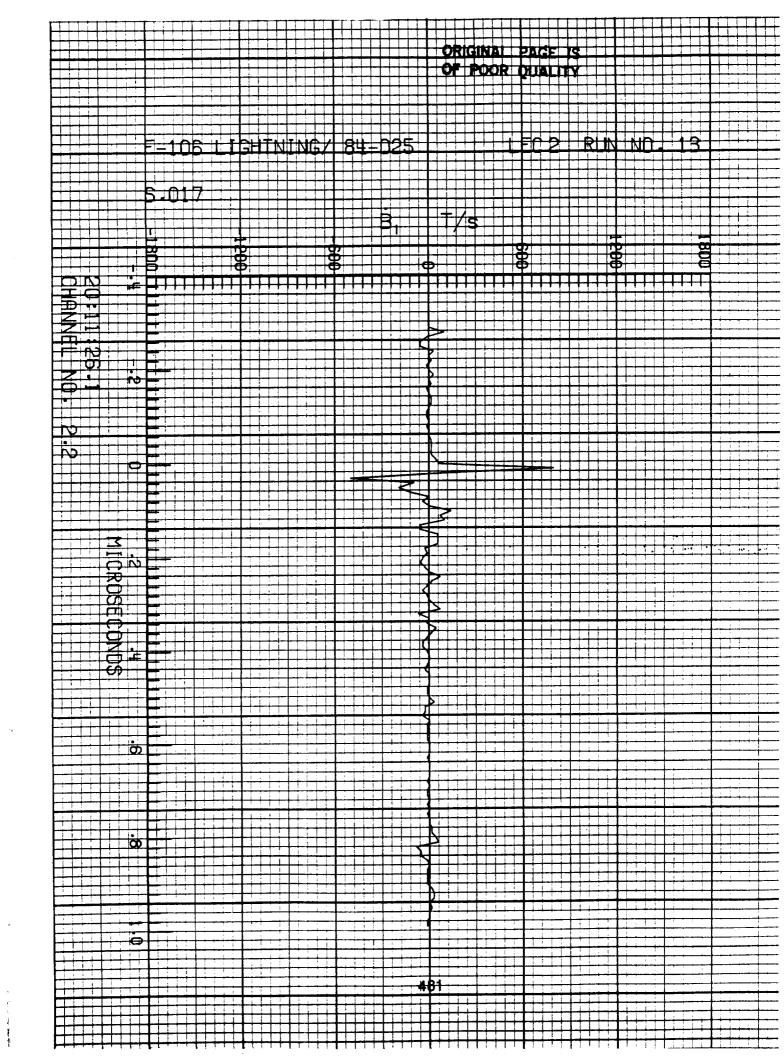


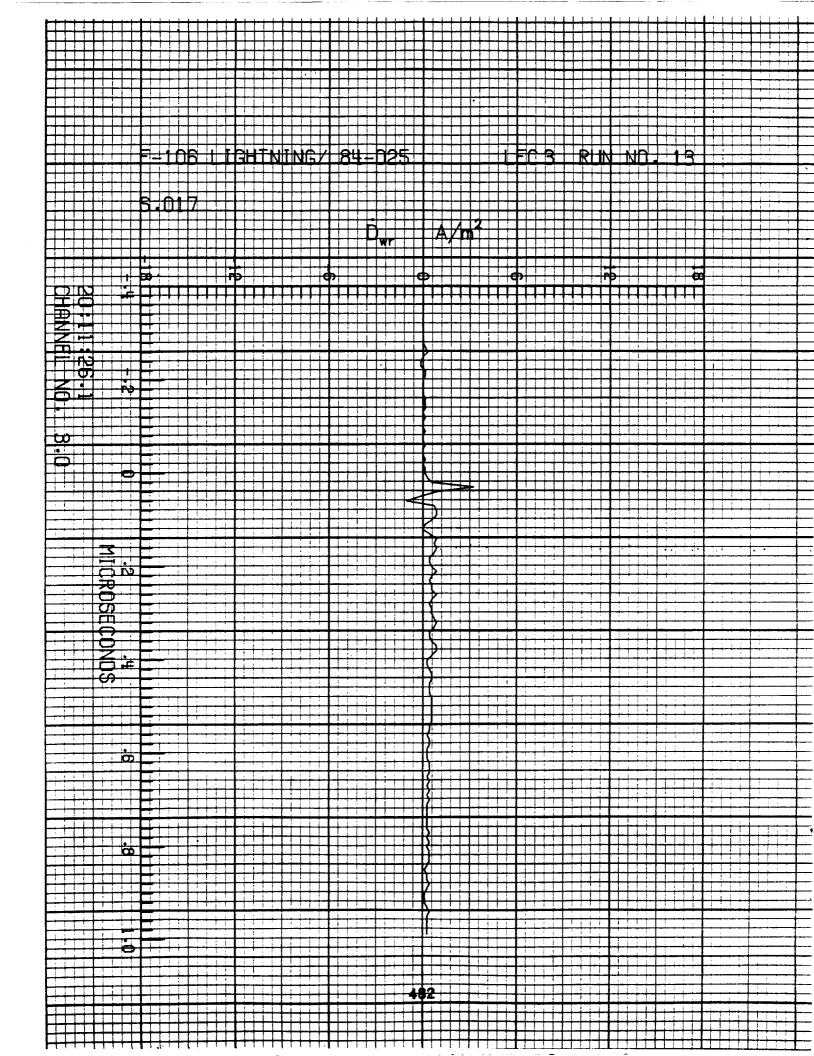


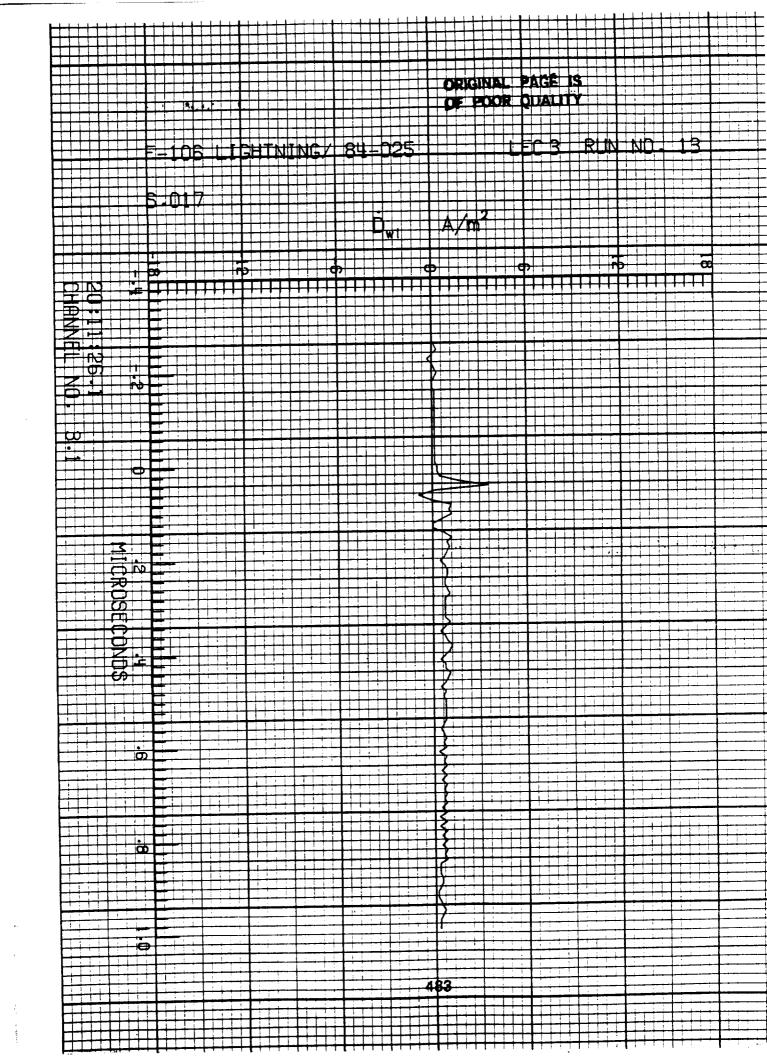


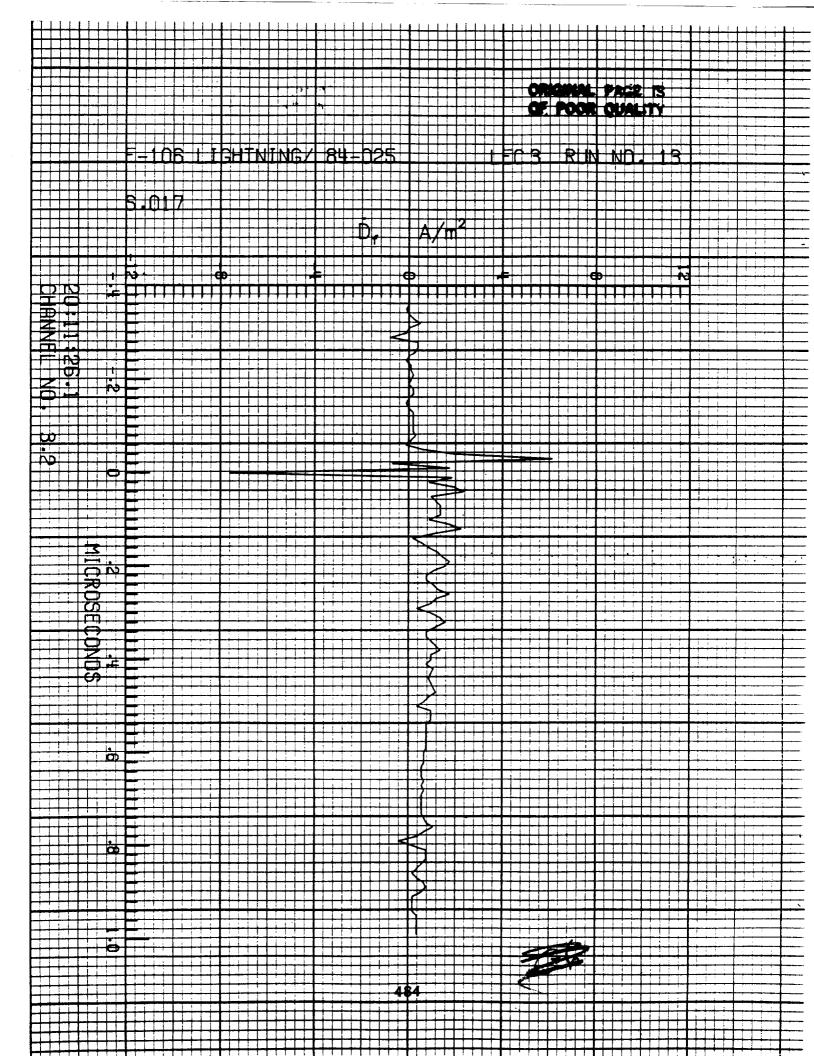


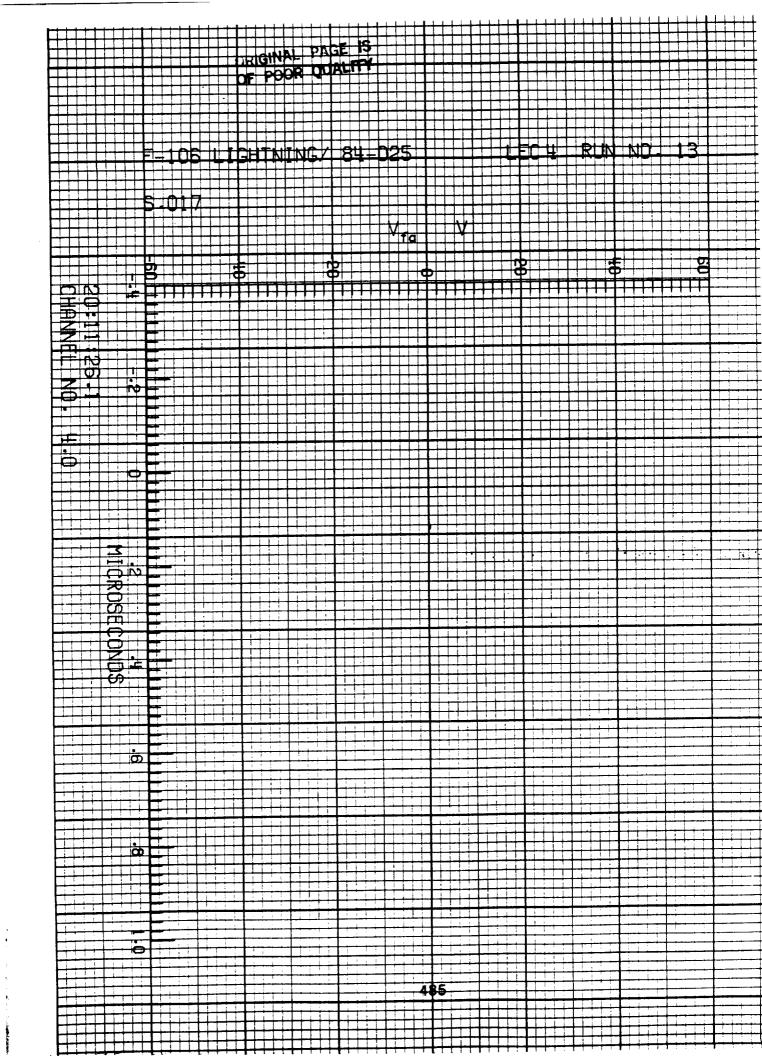


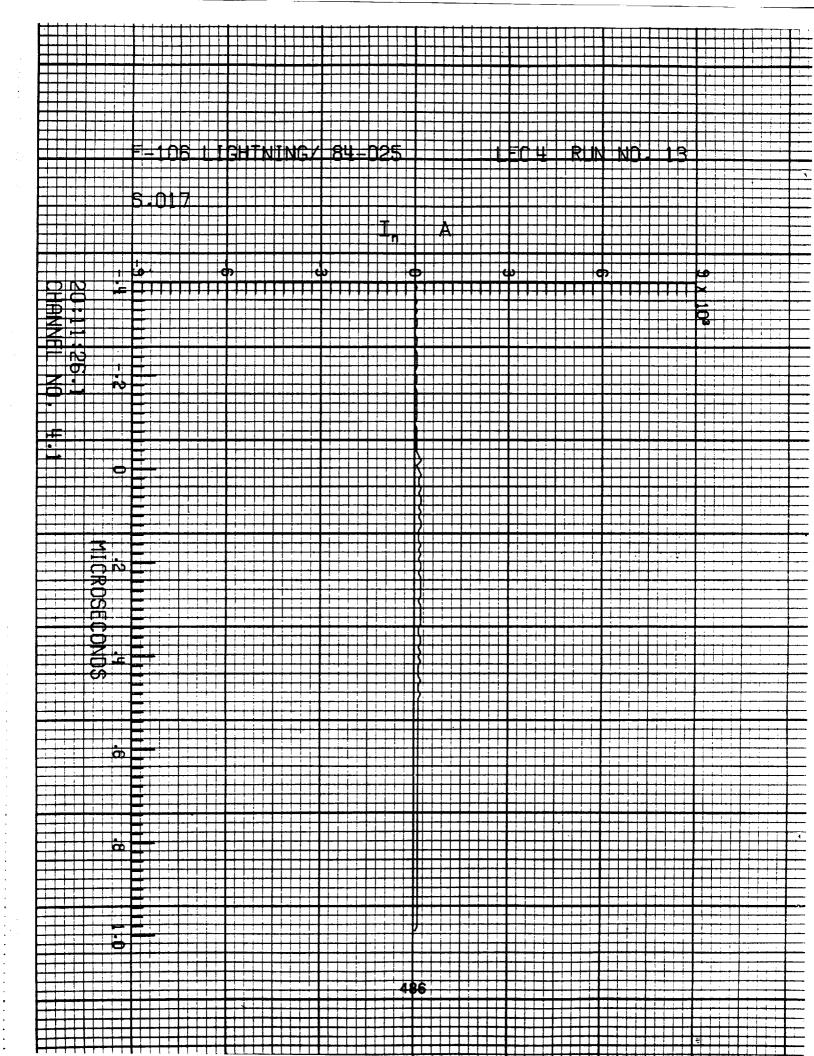


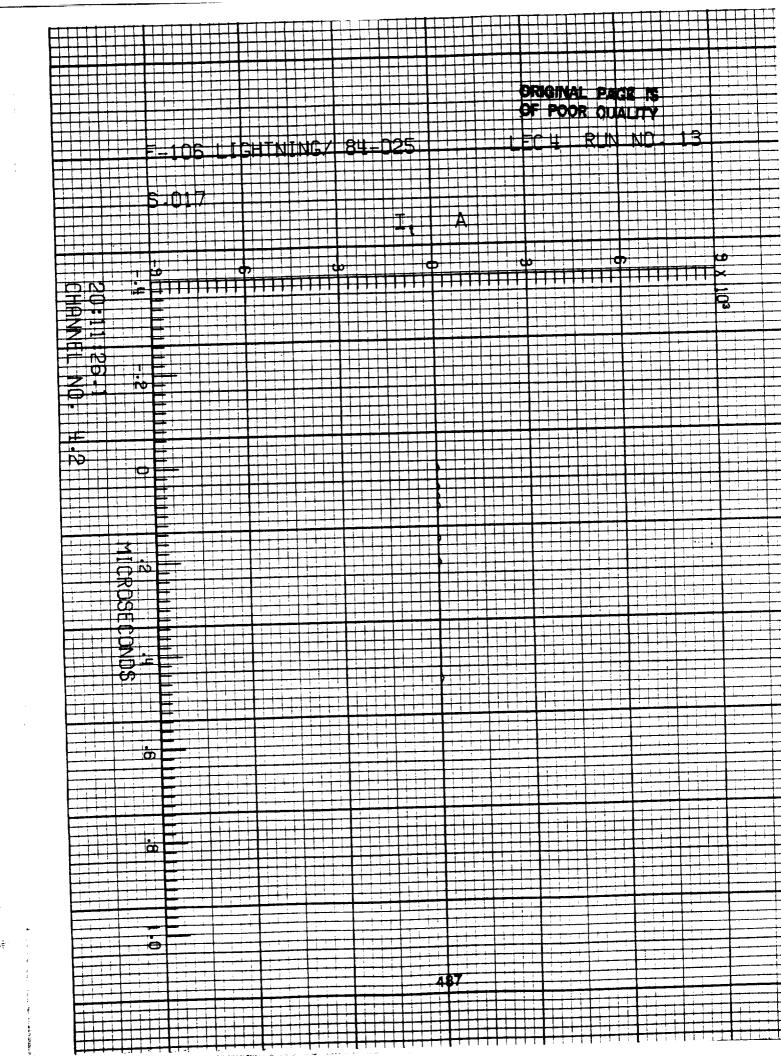


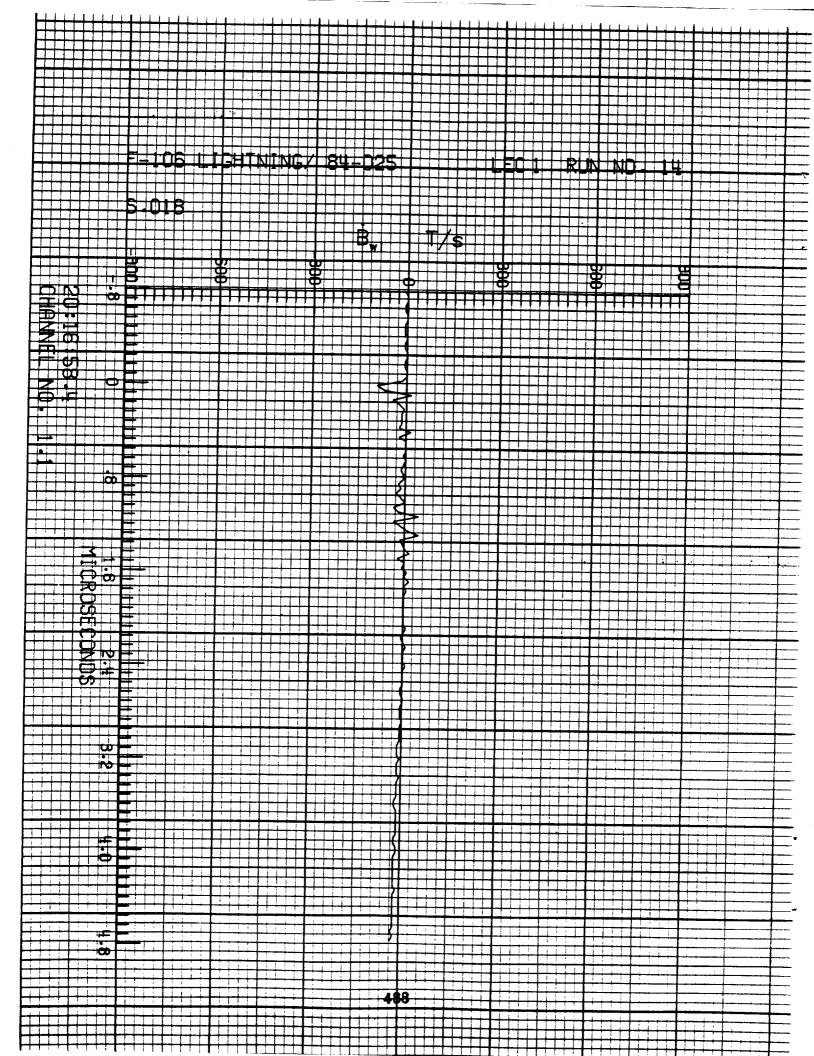


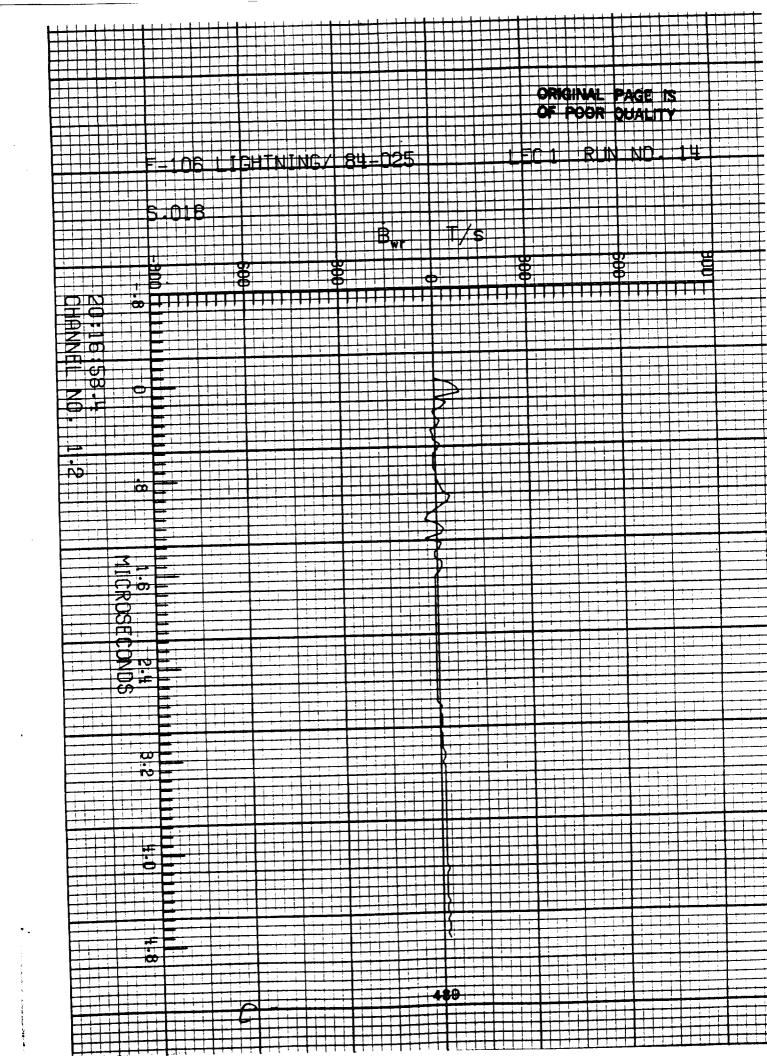




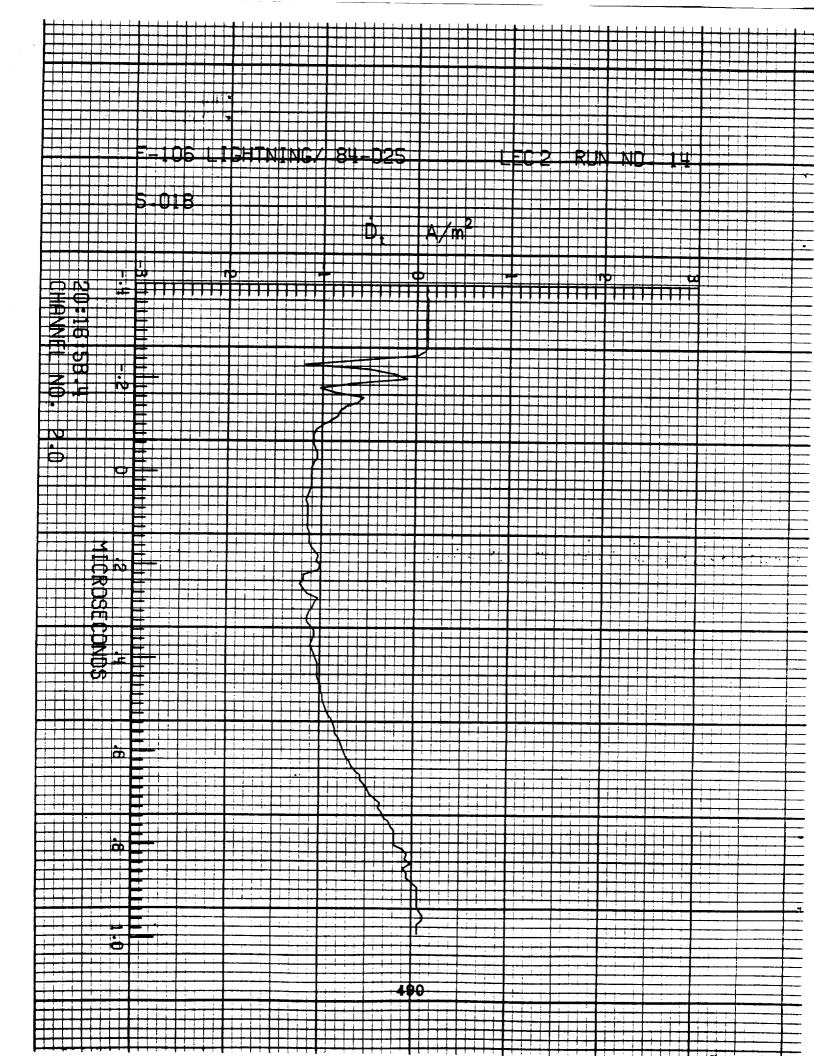


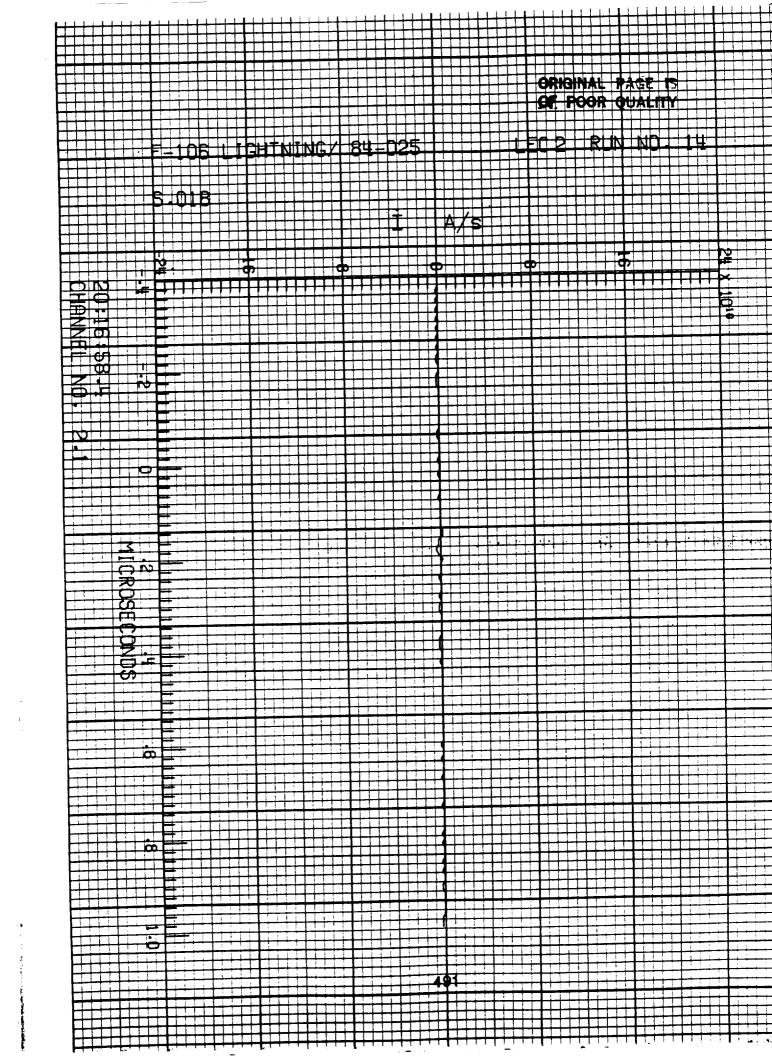


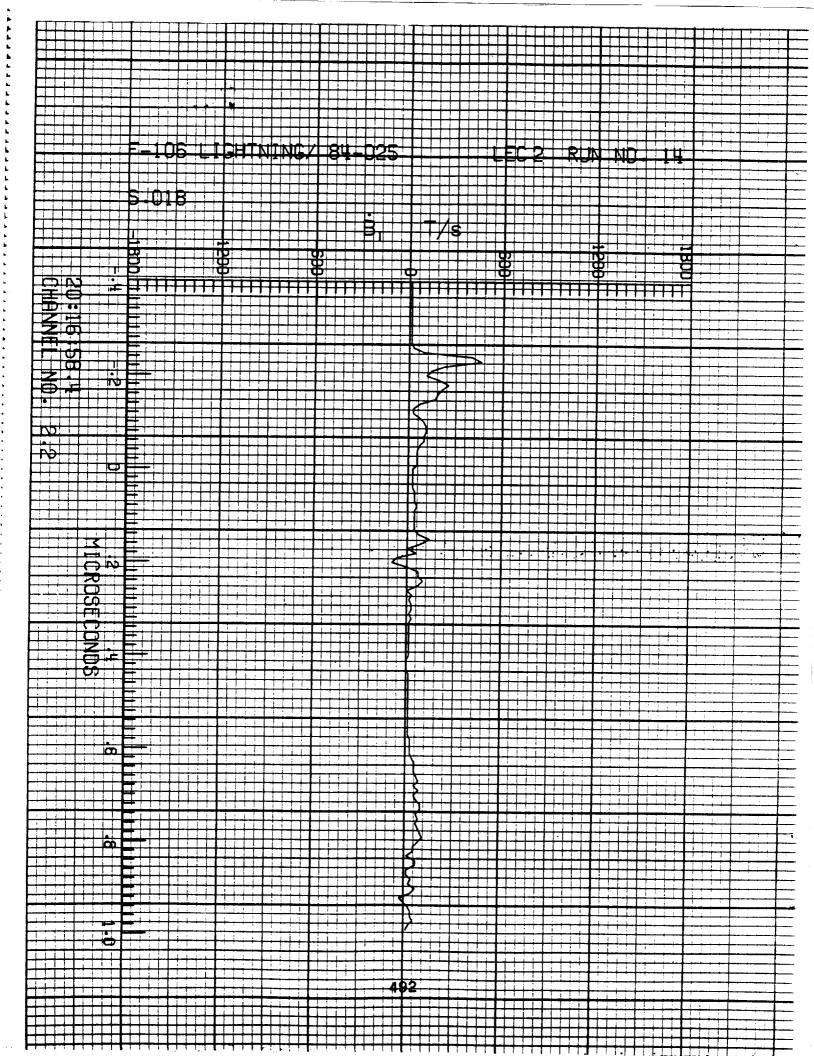


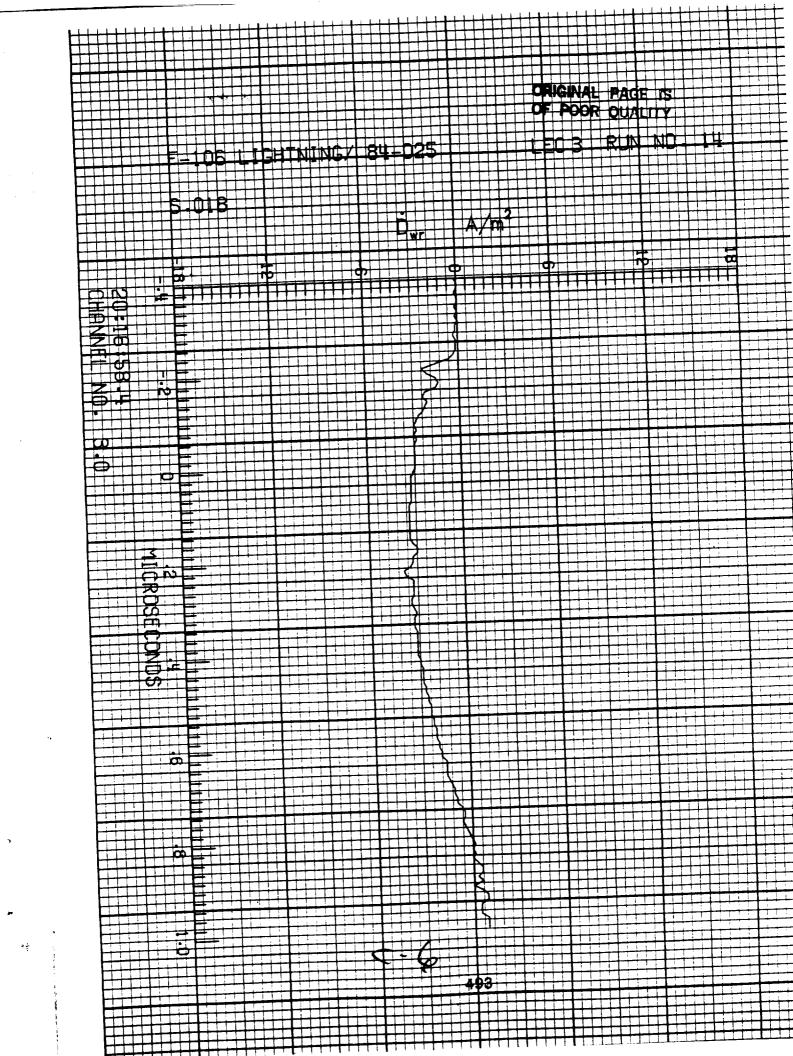


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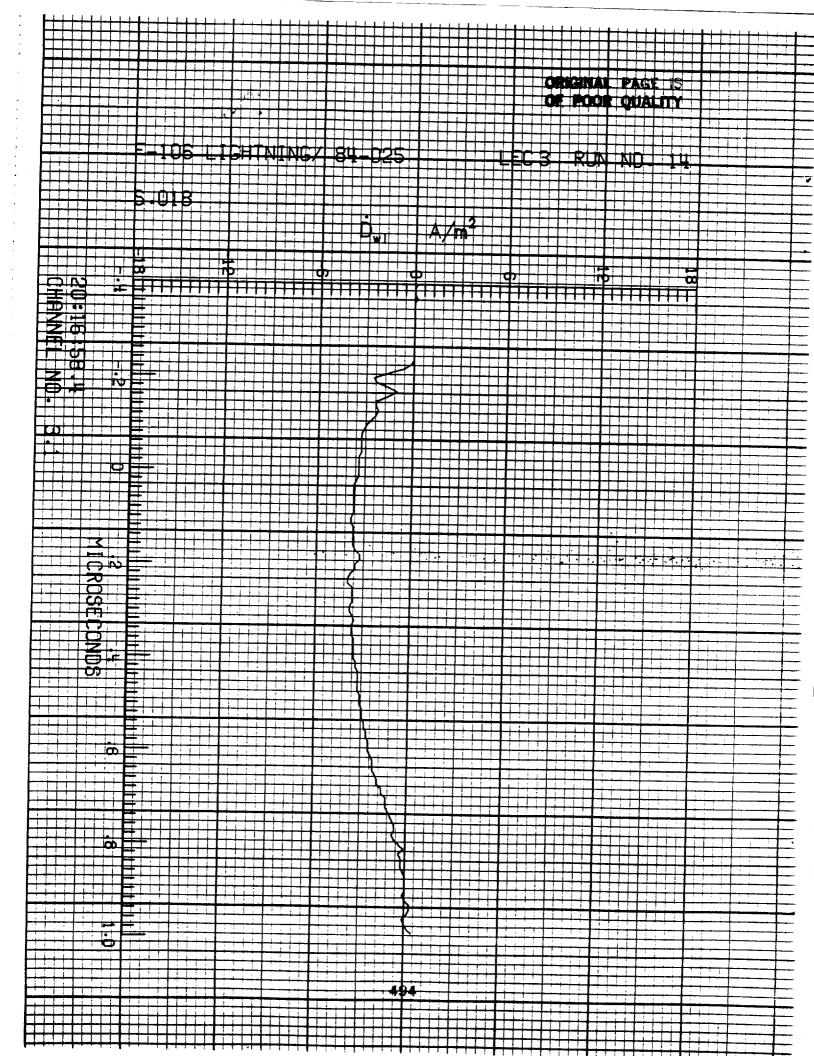


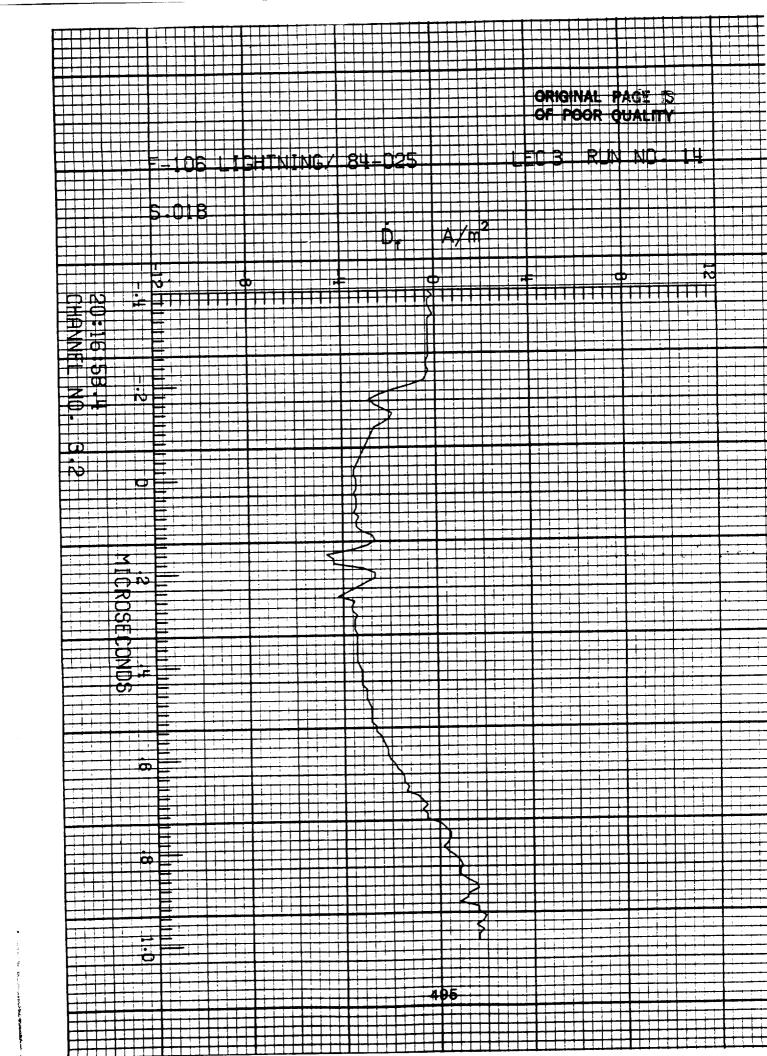


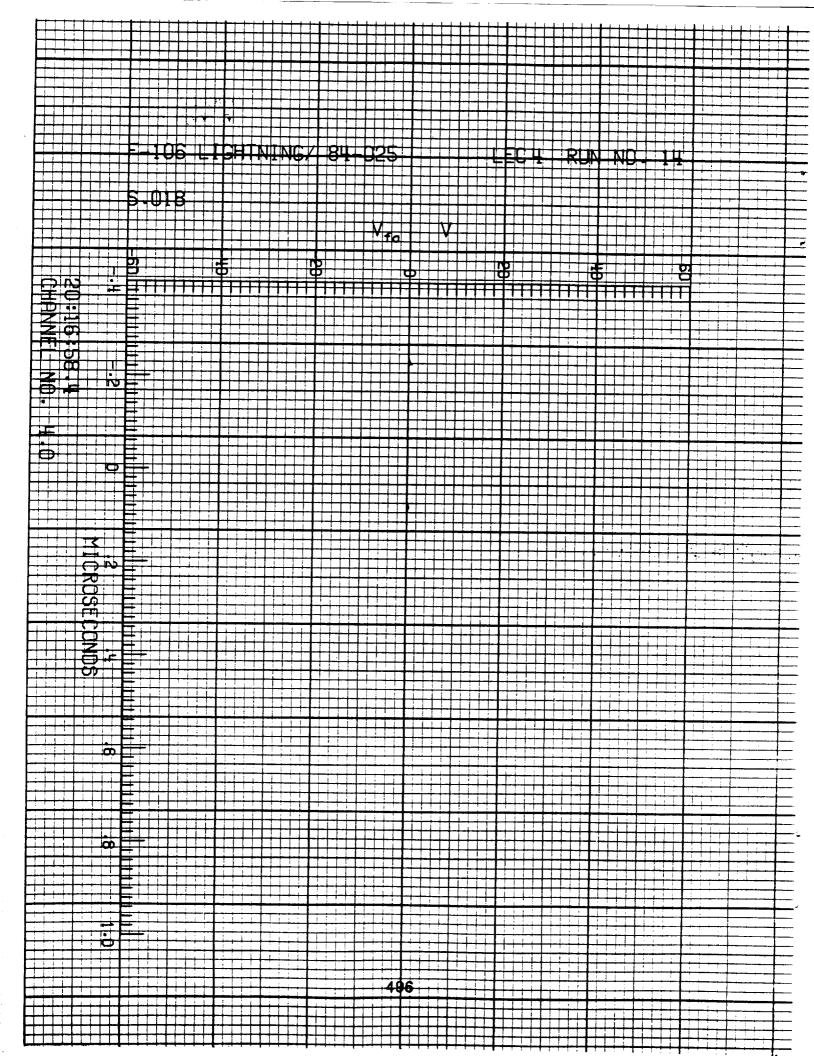


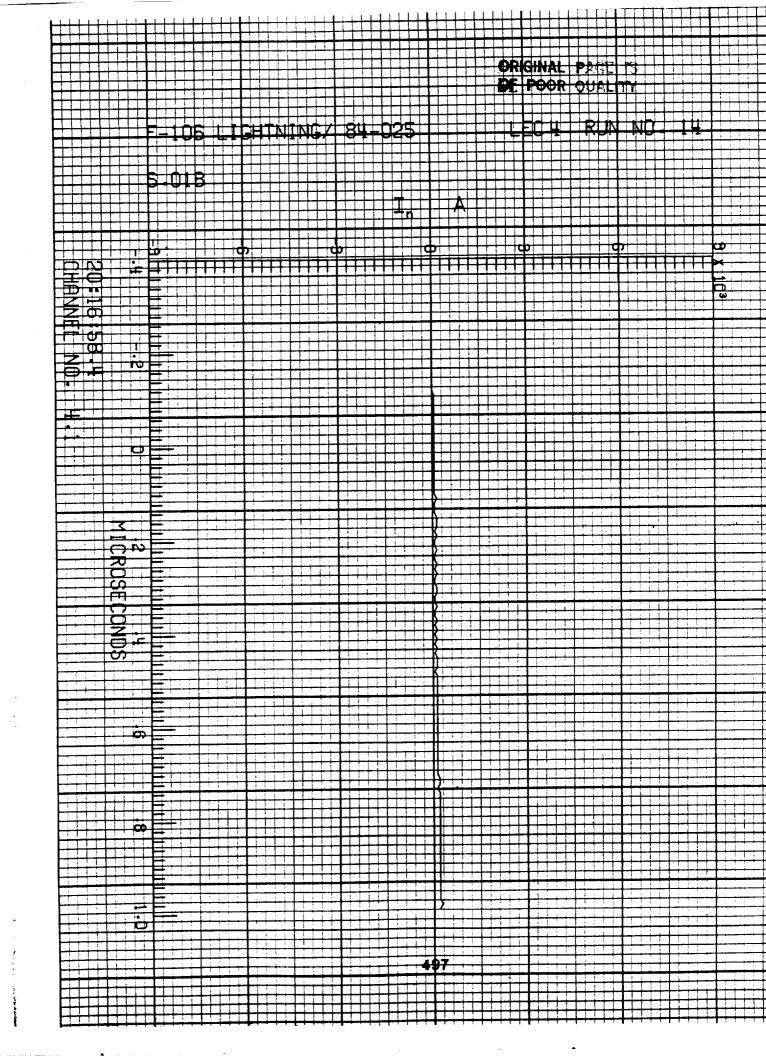


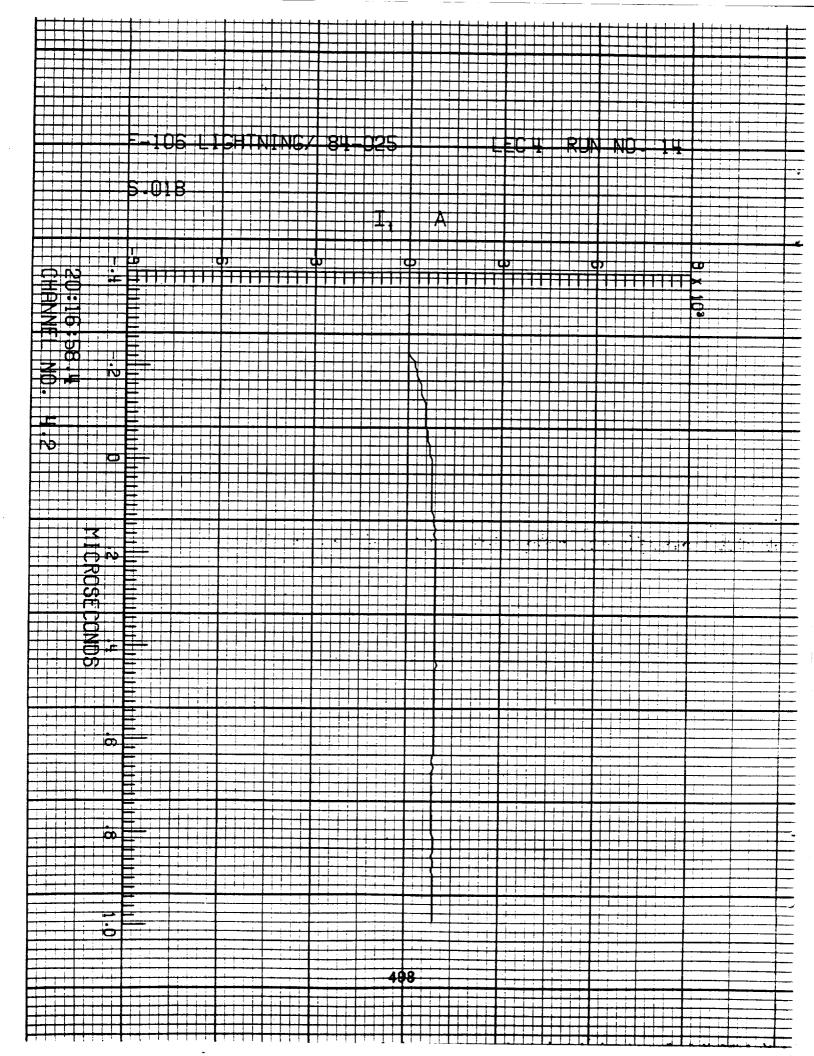
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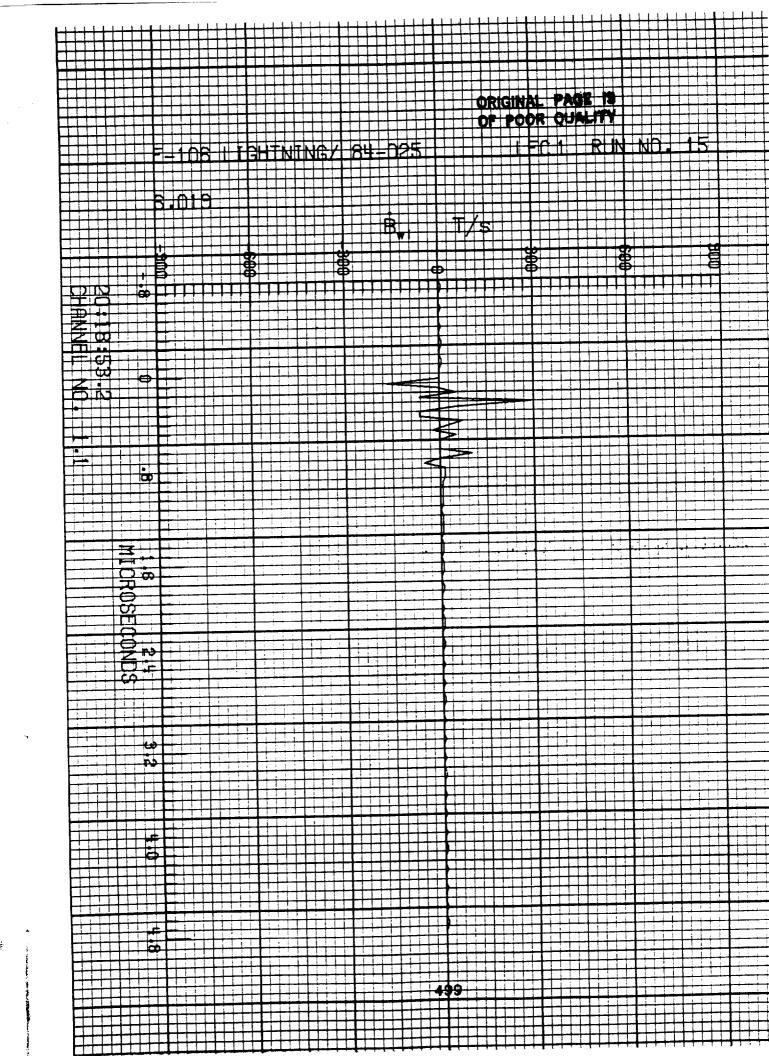
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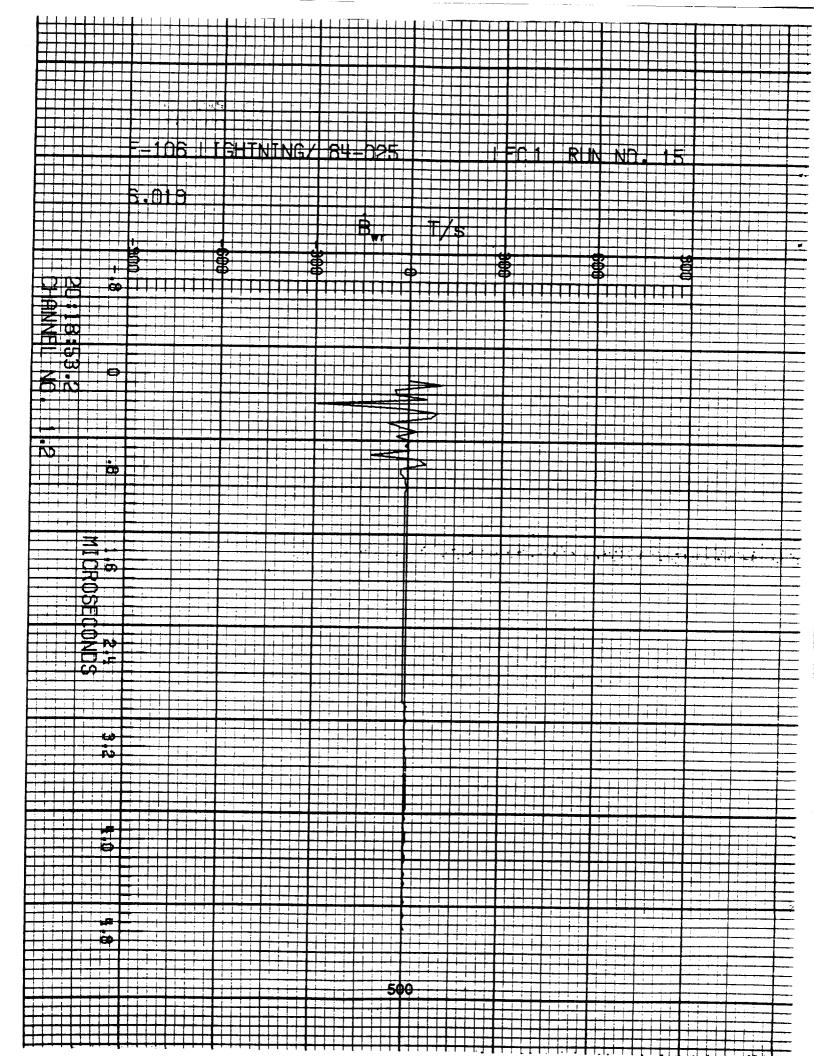


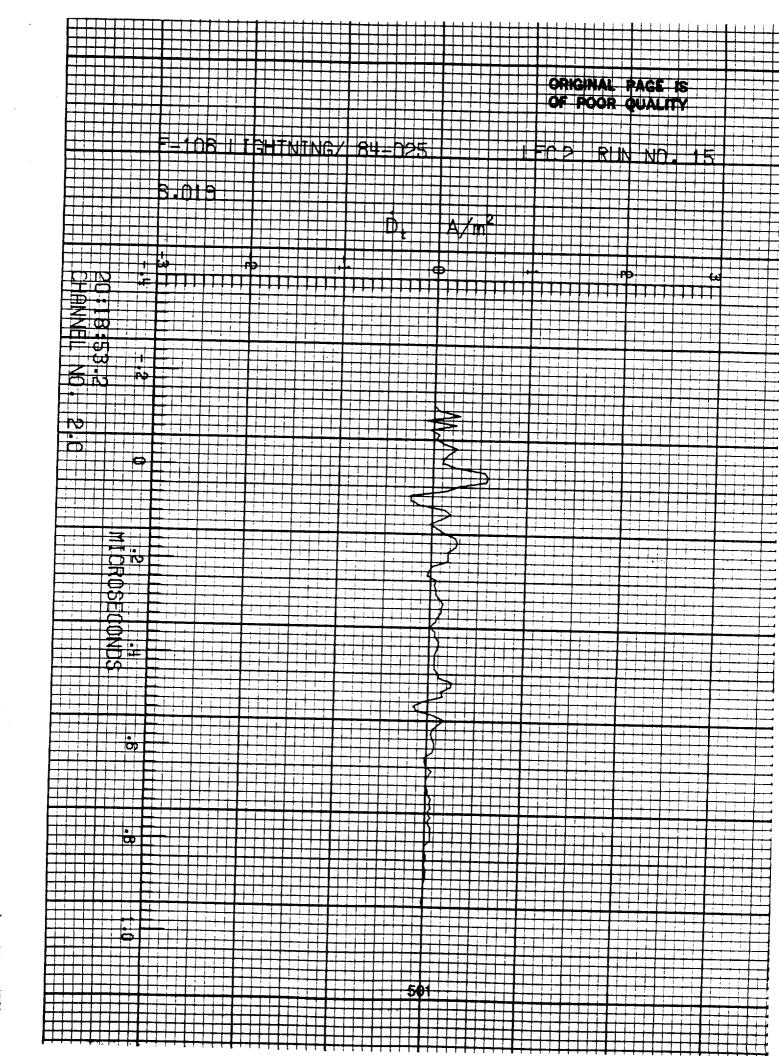


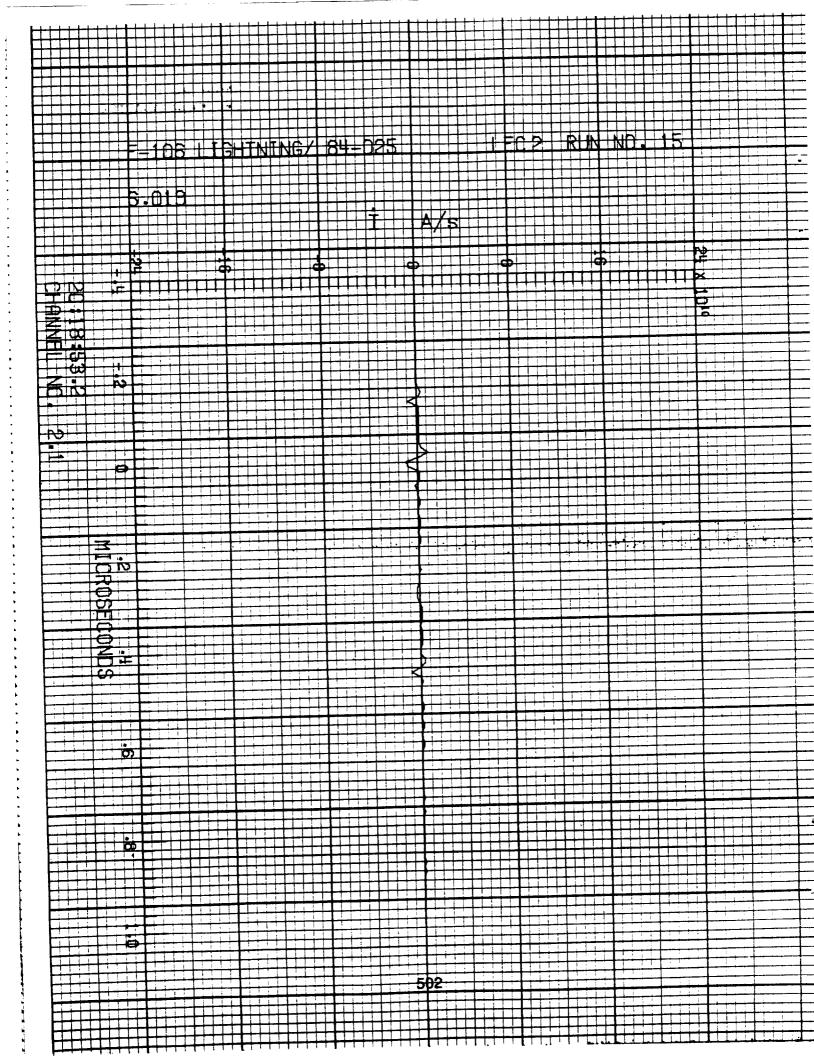


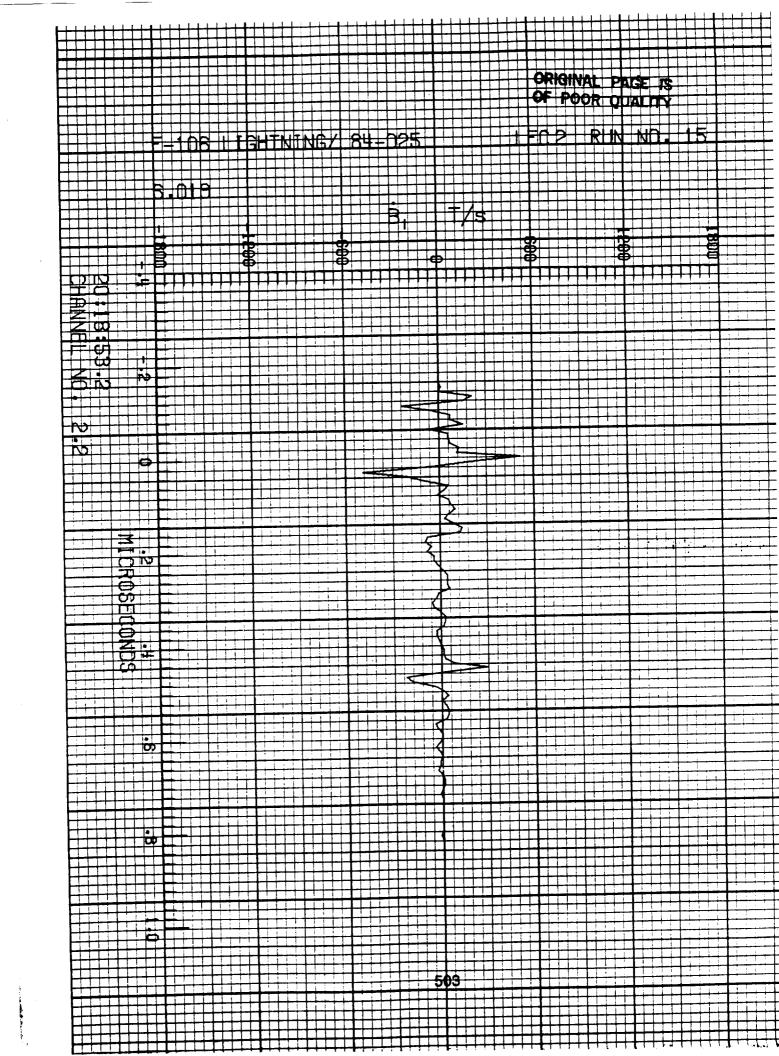


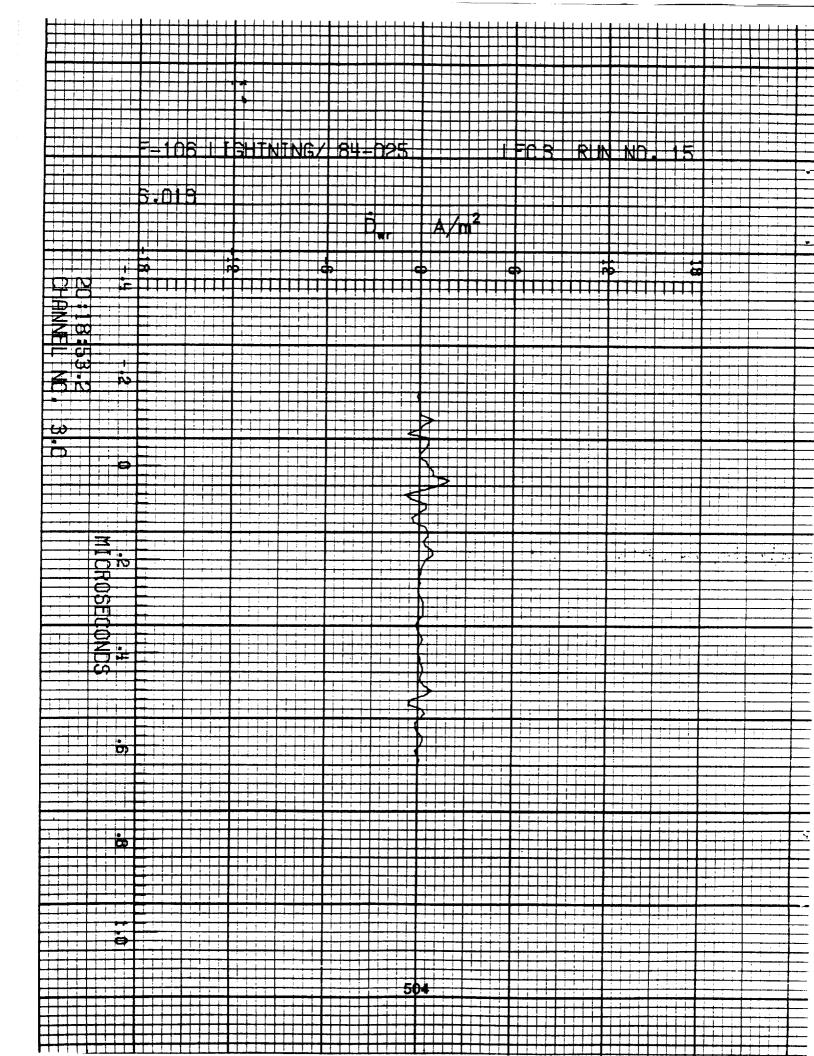


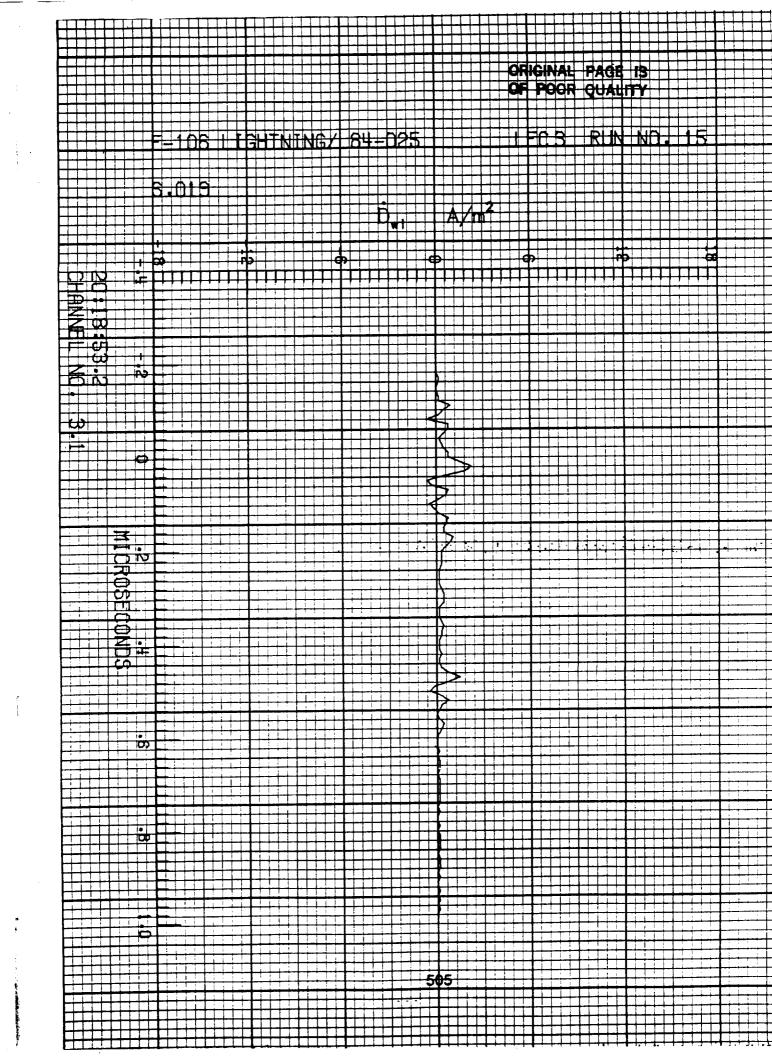


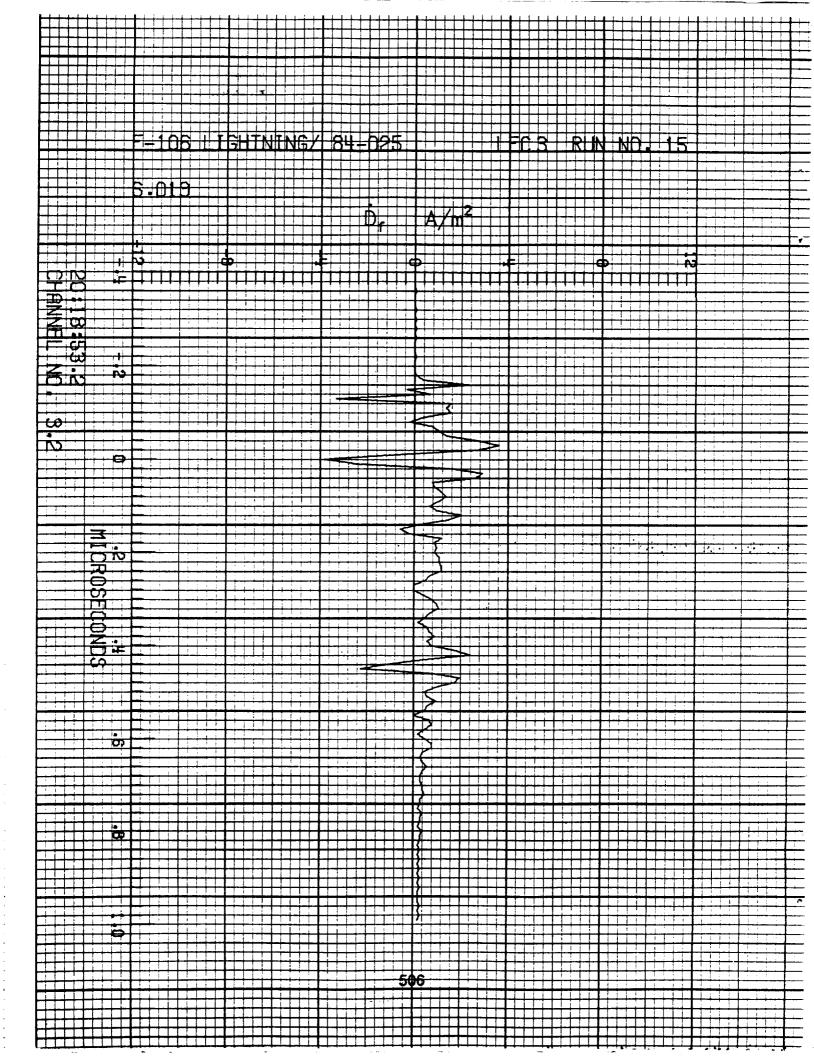


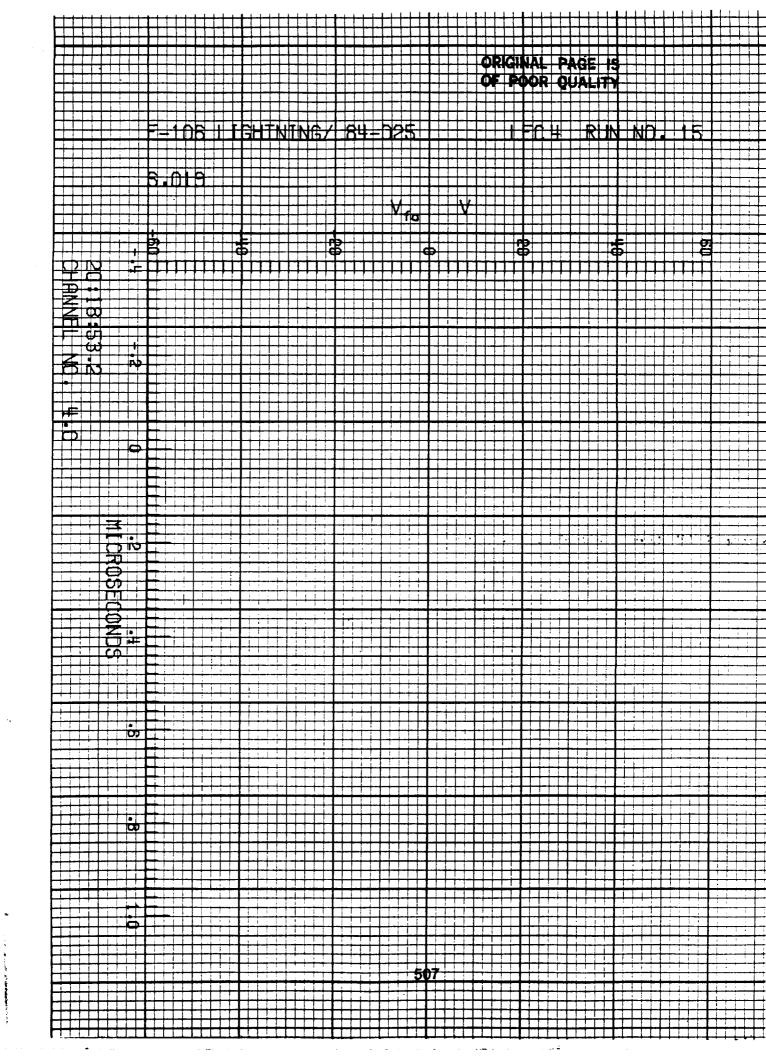




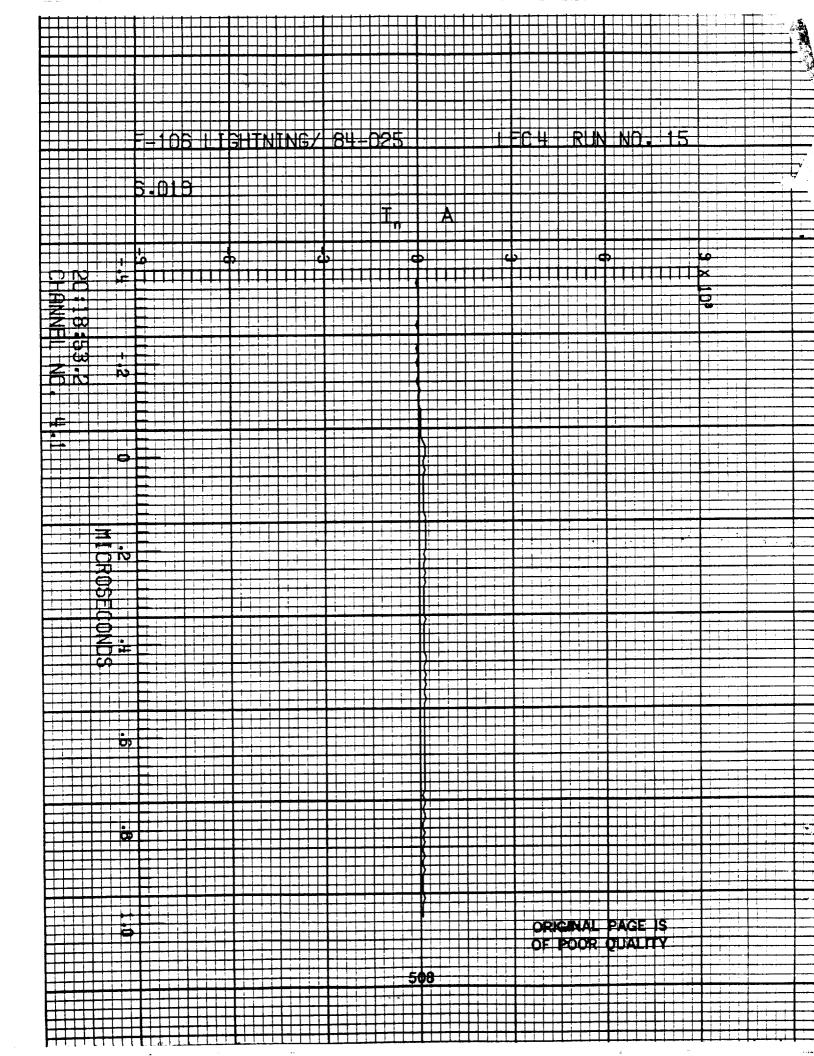








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16. Abstract			
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